

Deformation Capture and Modeling of Soft Objects

Bin Wang^{* †} Longhua Wu^{*} KangKang Yin[†] Uri Asher[‡] Libin Liu[‡] Hui Huang^{*}

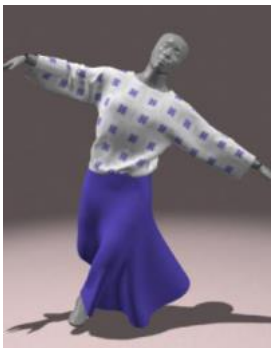
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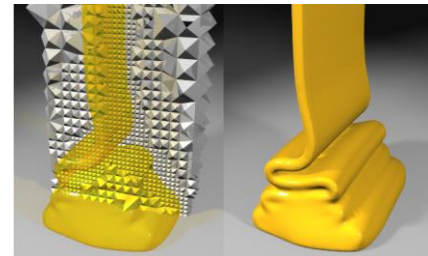
Deformation Models



Mass Spring [Baraff et. al 98]



Thin Shell [Pfaff et. al 14]



Finite Element [Batty et. al 11]

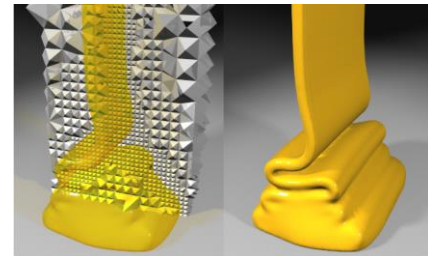
Manually Tuning



Mass Spring [Baraff et. al 98]



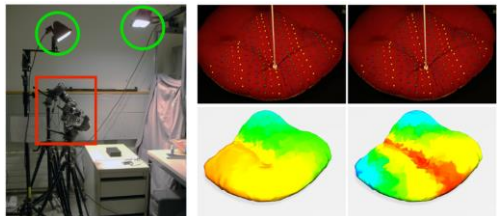
Thin Shell [Pfaff et. al 14]



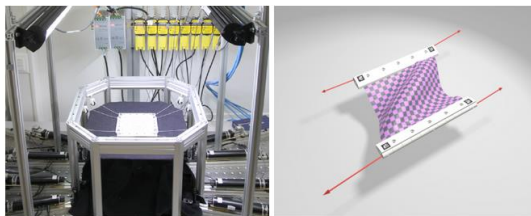
Finite Element [Batty et. al 11]

Manually tuning model's parameters
is tedious and time consuming.

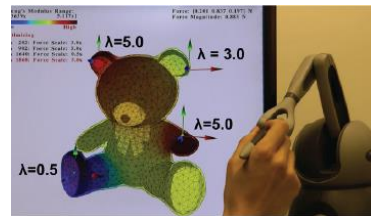
Data-Driven Modeling



[Bickel et. al 09]

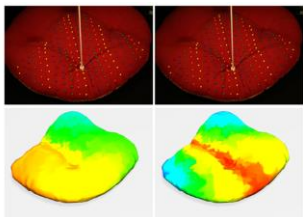


[Miguel et al. 2012]



[Xu et al. 2014]

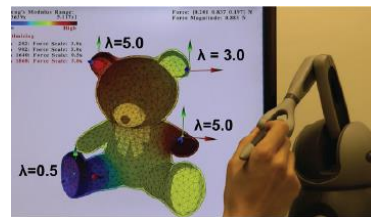
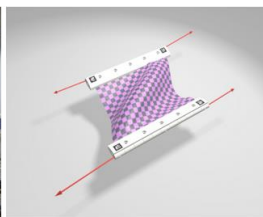
Limitations



[Bickel et. al 09]



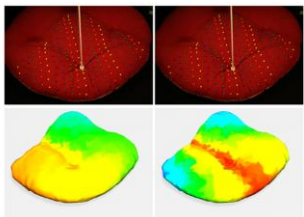
[Miguel et al. 2012]



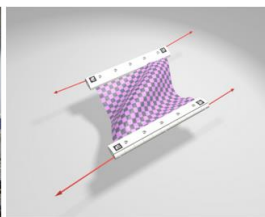
[Xu et al. 2014]

- Customized hardware system

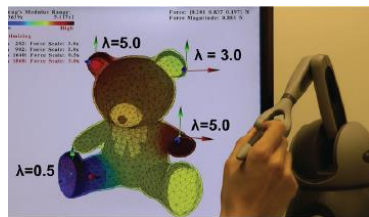
Limitations



[Bickel et. al 09]



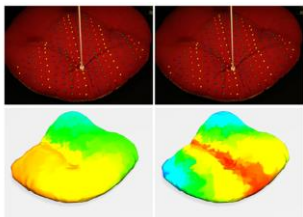
[Miguel et al. 2012]



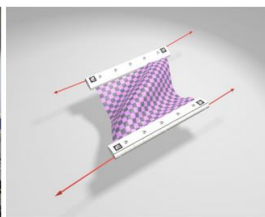
[Xu et al. 2014]

- Customized hardware system
- Oversimplified reference shape

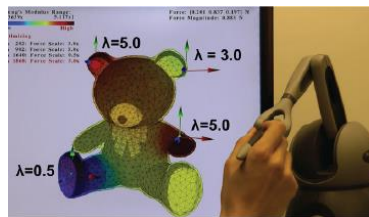
Limitations



[Bickel et. al 09]



[Miguel et al. 2012]



[Xu et al. 2014]

- Customized hardware system
- Oversimplified reference shape
- Dynamic properties are ignored

Our Goal

- Target for generic soft objects
- To estimate from pure kinematic data without force-displacement measurements
- To estimate the reference shape as well as material properties and damping coefficients

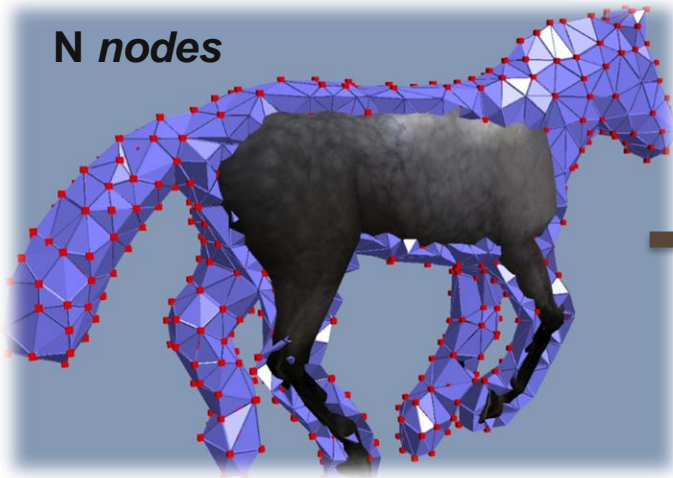
FEM-Based Deformation Simulation

$$\underline{M\ddot{x}} + \underline{D\dot{x}} + \underline{f_{\text{els}}} = \underline{f_{\text{ext}}}$$

Acceleration Damping Force Elastic Force External Force

FEM-Based Deformation Simulation

$$\underline{M}\ddot{\mathbf{x}} + \underline{D}\dot{\mathbf{x}} + \underline{f}_{\text{els}} = \underline{f}_{\text{ext}}$$



$$\ddot{\mathbf{x}}, \dot{\mathbf{x}}, \mathbf{f}_{\text{els}}, \mathbf{f}_{\text{ext}} \in \mathbf{R}^{3N \times 1}$$

$$\mathbf{M}, \mathbf{D} \in \mathbf{R}^{3N \times 3N}$$

FEM-Based Deformation Simulation

$$M\ddot{x} + D\dot{x} + f_{\text{els}} = f_{\text{ext}}$$

- Co-rotated linear model [Müller et al. 2012]

$$f_{\text{els}} = RK(R^T x - X), \text{ where } K = f(E, \nu)$$

FEM-Based Deformation Simulation

$$M\ddot{x} + D\dot{x} + f_{\text{els}} = f_{\text{ext}}$$

- Co-rotated linear model [Müller et al. 2012]

$$f_{\text{els}} = RK(R^T x - X), \text{ where } K = f(E, \nu)$$

E (Young's modulus): force \longleftrightarrow expansion/compression

ν (Poisson ratio): expansion \longleftrightarrow compression

FEM-Based Deformation Simulation

$$M\ddot{x} + D\dot{x} + f_{\text{els}} = f_{\text{ext}}$$

- Co-rotated linear model [Müller et al. 2012]

$$f_{\text{els}} = RK(R^T x - X), \text{ where } K = f(E, \nu)$$

- Rayleigh damping: $D = \alpha M + \beta K$

FEM-Based Deformation Simulation IGGRAPH2015 loads of Discovery

$$M\ddot{x} + D\dot{x} + f_{\text{els}} = f_{\text{ext}}$$

- Co-rotated linear model [Müller et al. 2012]

$$f_{\text{els}} = RK(R^T x - \mathbf{X}), \quad \text{where } K = f(E, \nu)$$

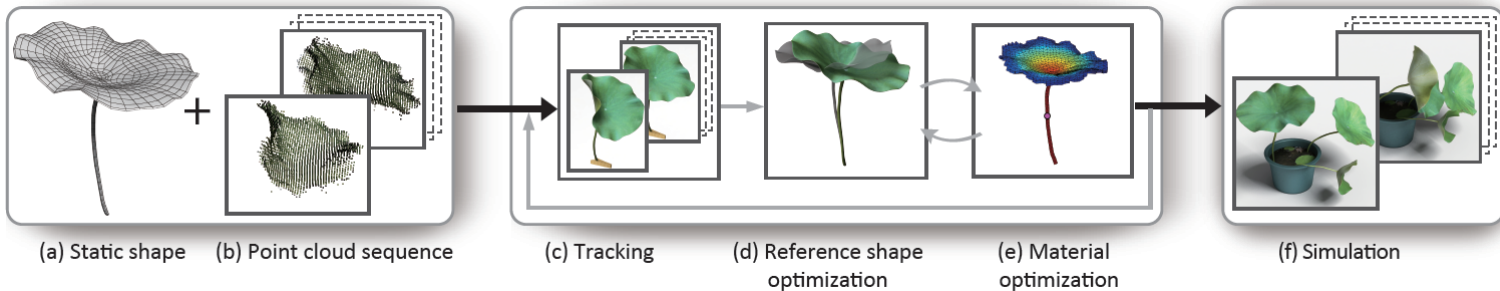
Reference shape

Young's modulus & Poisson ratio

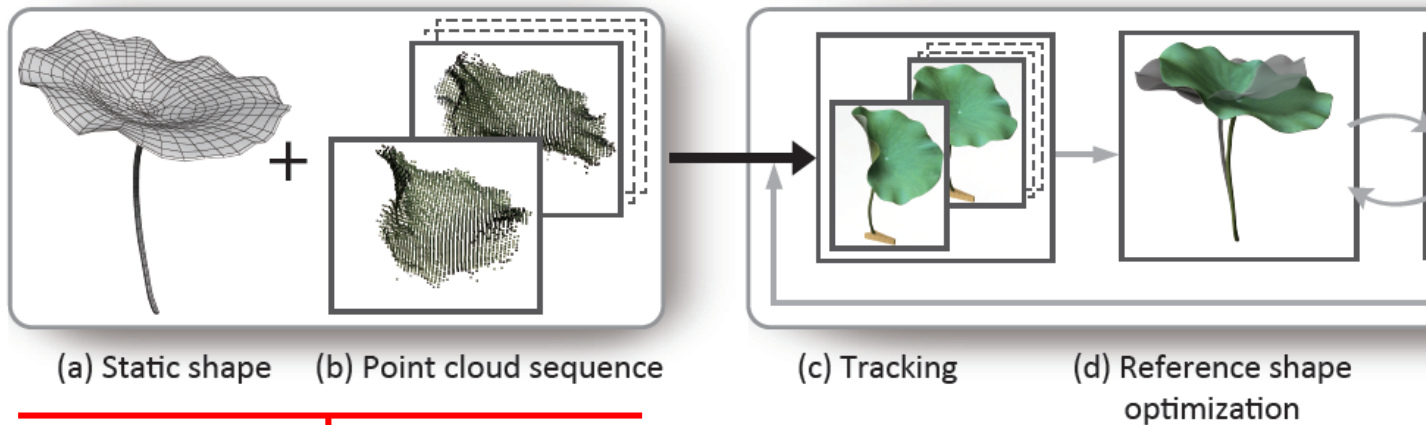
- Rayleigh damping: $D = \alpha M + \beta K$

Rayleigh damping coefficients

Overview



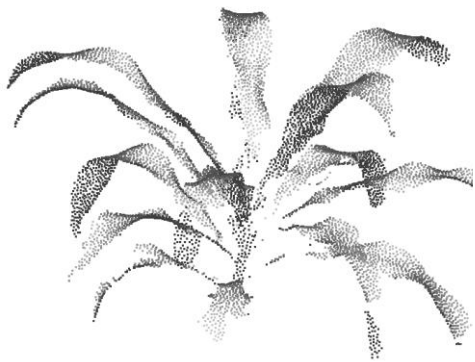
Capture



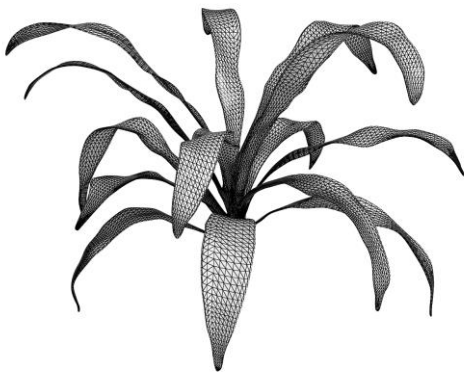
Acquisition of static shape and deformable motion.

Capture

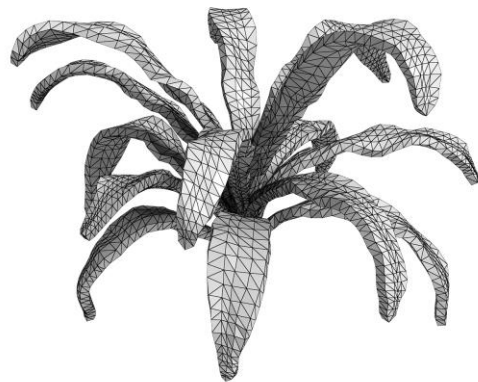
- Static shape



Point cloud



Surface mesh



Volumetric mesh

Capture

- Dynamic motion



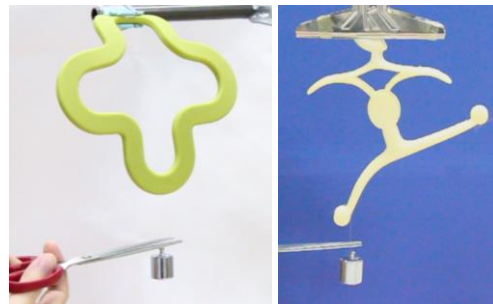
Three Kinect sensors

Capture

- Dynamic motion



Three Kinect sensors



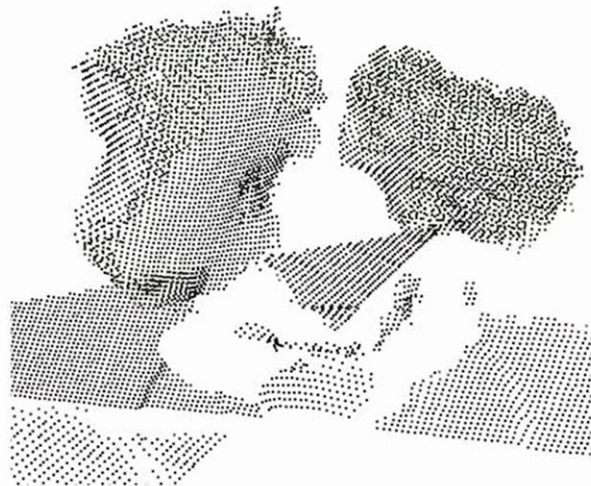
Deformation by interaction

Capture

Real objects

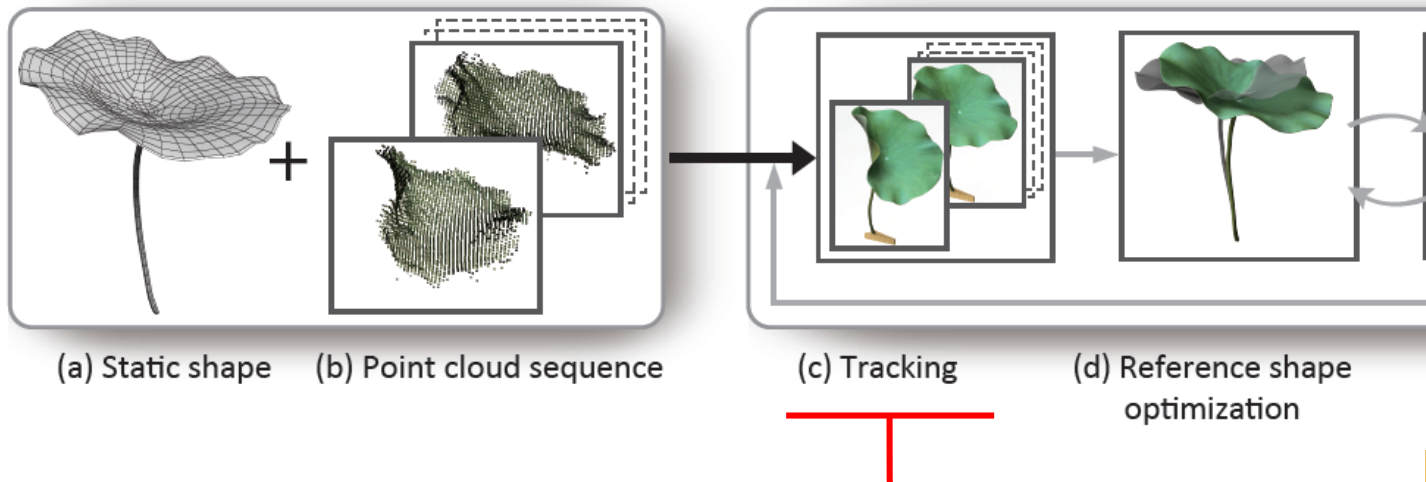


Captured point clouds



REPLAY X 1/2

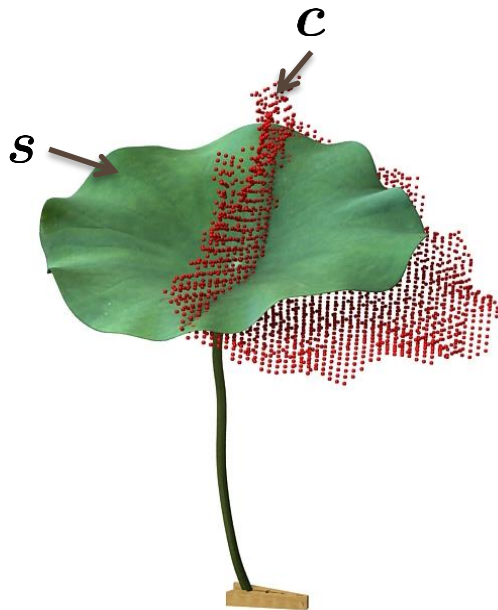
Tracking



Reconstruct mesh deformation from point clouds

Tracking

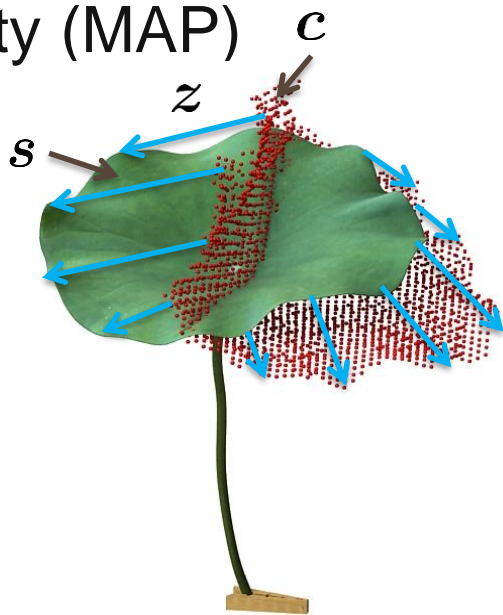
- Challenges
 - Noisy and incomplete
 - Large deformation
 - No correspondence



Tracking

- Maximum a posteriori probability (MAP)

$$\mathbf{s} = \arg \max_{\mathbf{s}} p(\mathbf{s}|\mathbf{c})$$



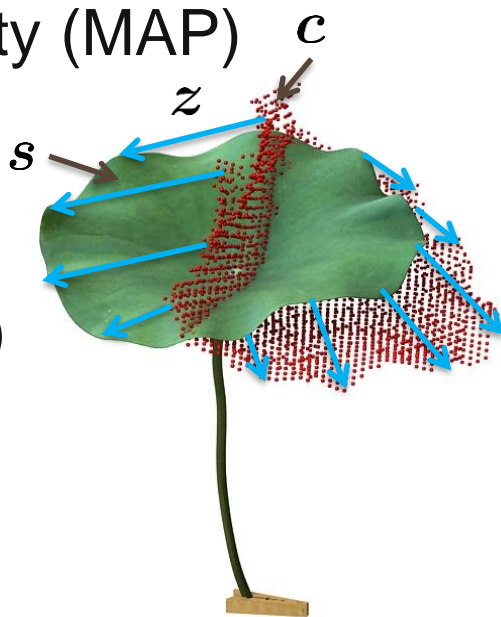
Tracking

- Maximum a posteriori probability (MAP)

$$\mathbf{s} = \arg \max_{\mathbf{s}} p(\mathbf{s}|\mathbf{c})$$

- Expectation-Maximization (EM)

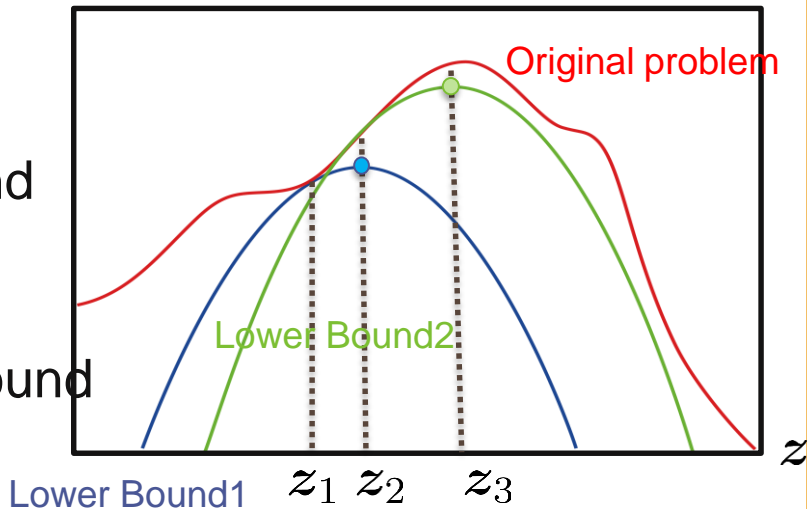
- z : latent variable
- Normally distributed



Tracking

PRML [Bishop 07]

- E step:
 - expectation
 - generate a lower bound
- M step:
 - maximize the lower bound



Tracking

- E step:
 - expectation
 - generate a lower bound
- M step:
 - maximize the lower bound
 - explain observation + minimize potential energy
 - virtual force + physics simulation

Tracking



Fitting the static shape to the first frame

Tracking

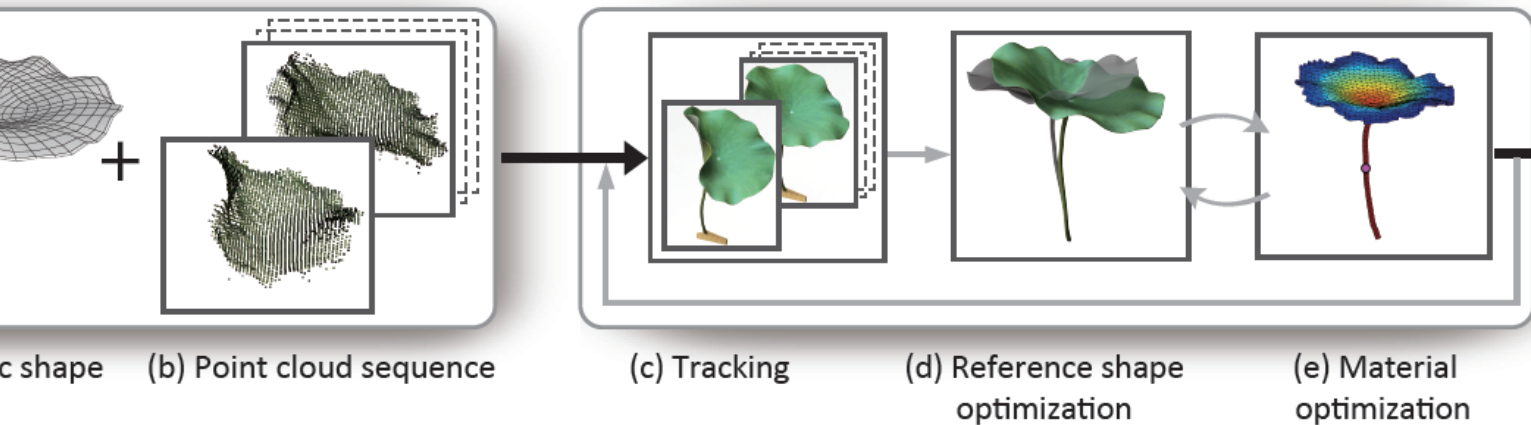
Capture



Tracking result



Optimization



Learning deformation model from motion trajectories

Optimization

- Space-time optimization

$$\min_{E, \alpha, \beta, \mathbf{X}} \mathcal{F}(E, \alpha, \beta, \mathbf{X}) = \sum_t \|\mathbf{x}_t - \hat{\mathbf{x}}_t\|^2$$

Young's modulus Rayleigh damping coefficients Reference shape

- Challenges

- High dimension, nonlinear
- Parameters coupling

Optimization

- Constrained space-time optimization

$$\min_{E, \alpha, \beta, \mathbf{X}} \mathcal{F}(E, \alpha, \beta, \mathbf{X}) = \sum_t \|\mathbf{x}_t - \hat{\mathbf{x}}_t\|^2$$

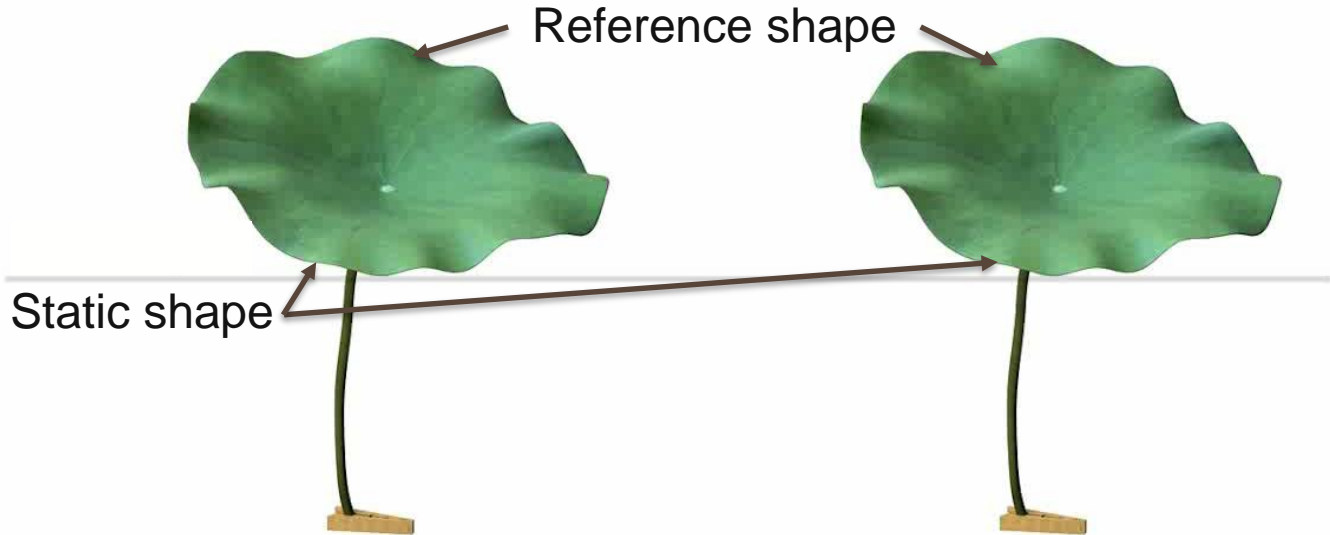
$$\text{s.t. } \mathbf{f}_{\text{els}}(\mathbf{X}) = \mathbf{f}_{\text{gravity}}$$

Splitting Scheme



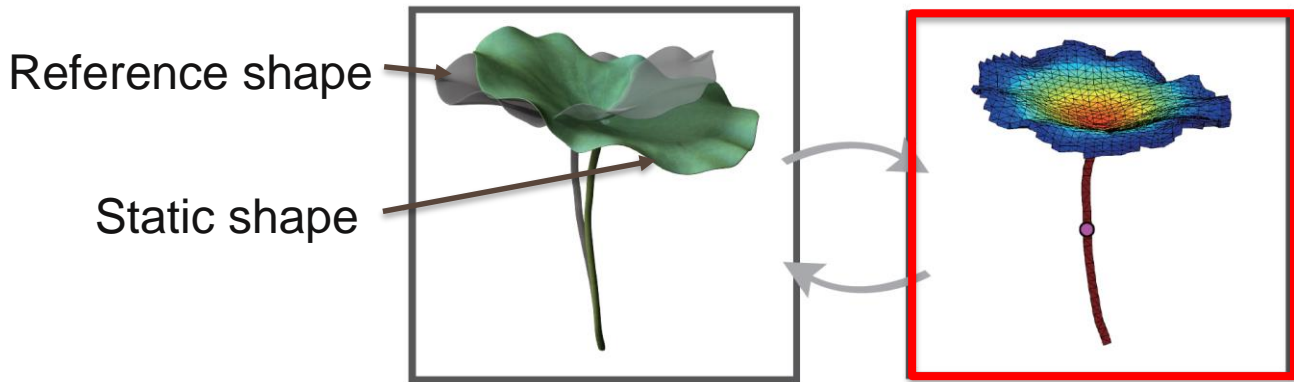
- Maintain static equilibrium
- Force residual as virtual force
- Physics simulation $\frac{\partial f}{\partial \mathbf{X}}$

Splitting Scheme



Reference shape optimization

Splitting Scheme



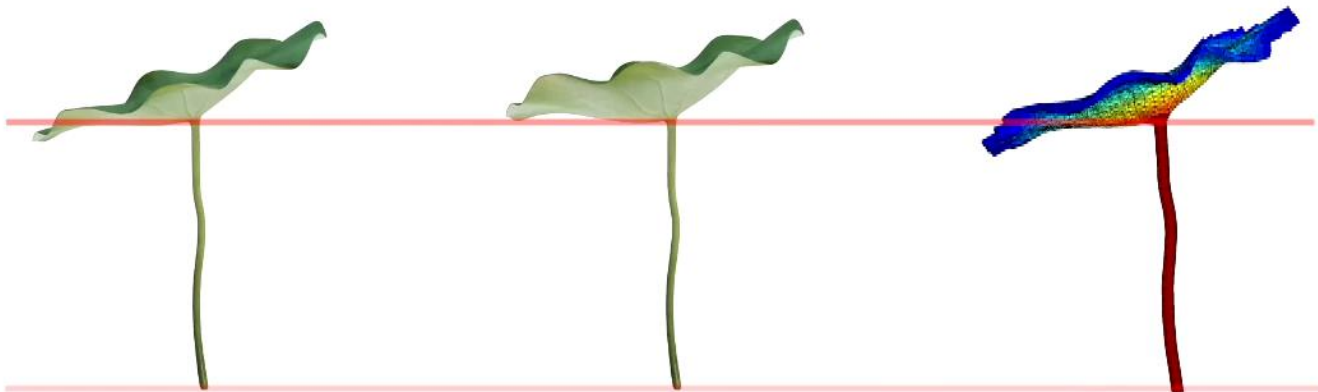
- Match full trajectory
- Gradient free downhill

Splitting Scheme

Static shape

Reference shape

Material distribution



Splitting Scheme

Tracking result

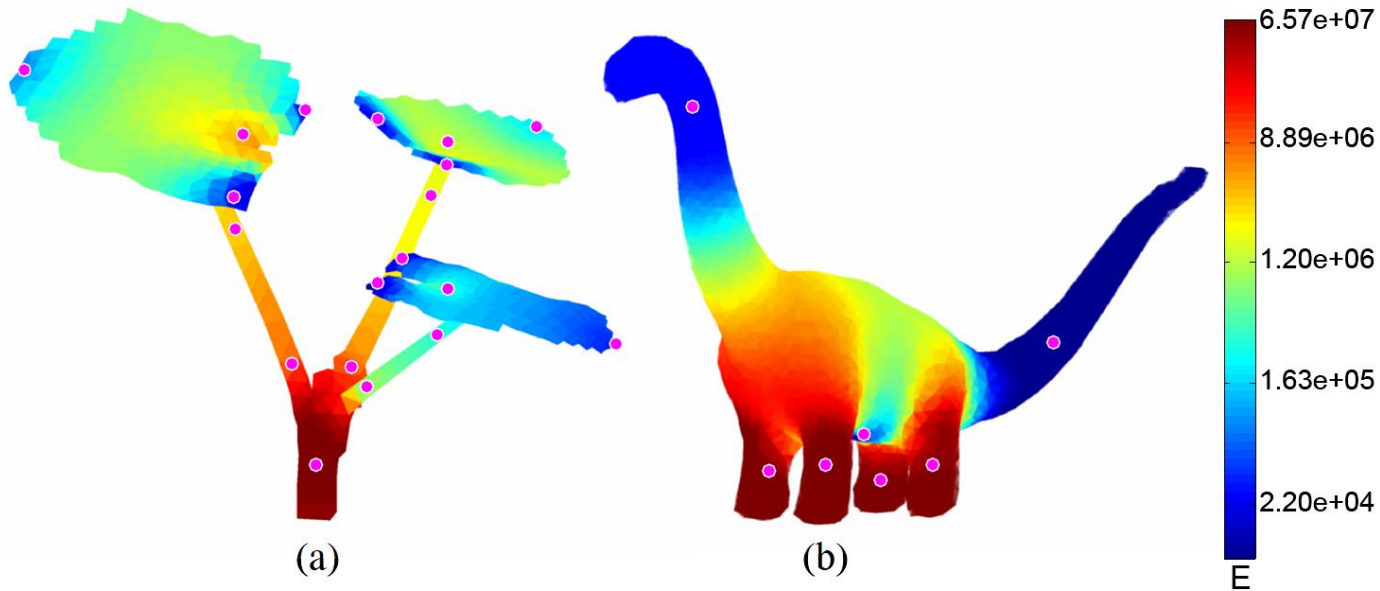


Simulation



REPLAY X 1/2

Heterogeneous Distribution



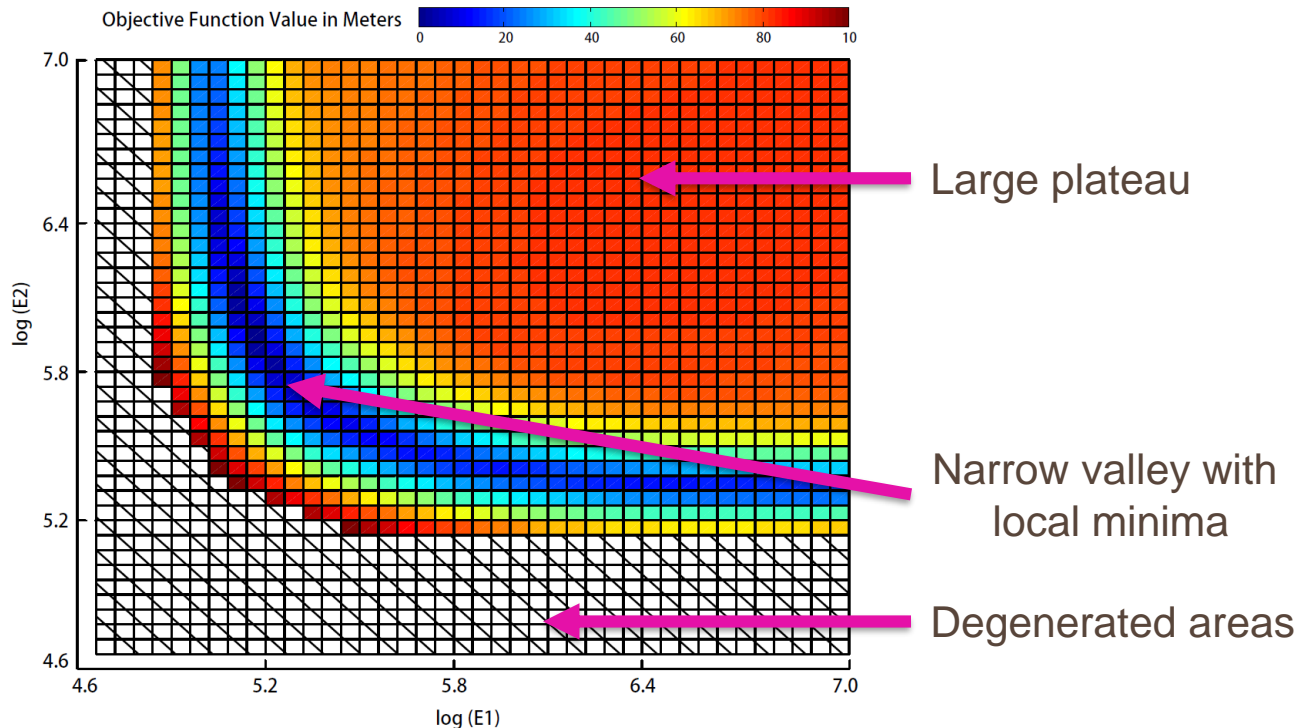
(a)

(b)

E

Multiple control points

Warm Start

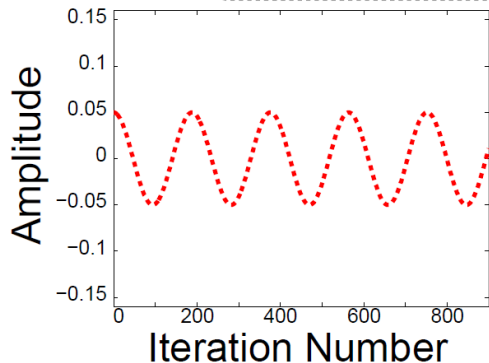


Warm Start

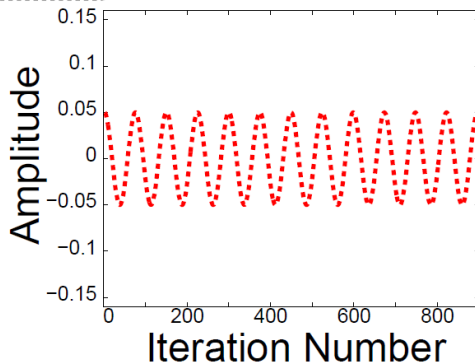
- Modal analysis

$$K\phi_i = \lambda_i M\phi_i$$

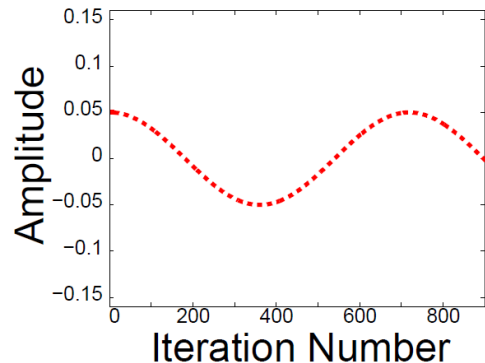
..... Natural Frequency



$E = 6.8e+05$



$E = 4.0e+06$



$E = 5.0e+04$

Warm Start

- Frequency matching
 - Captured trajectory
 - Project on to the Eigen mode



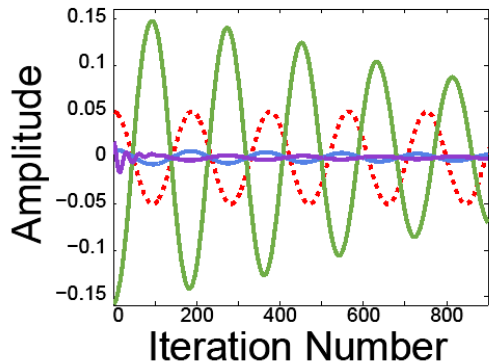
Twist

Bend

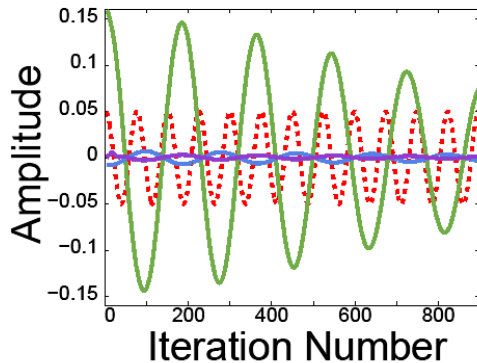
Stretch 40

Warm Start

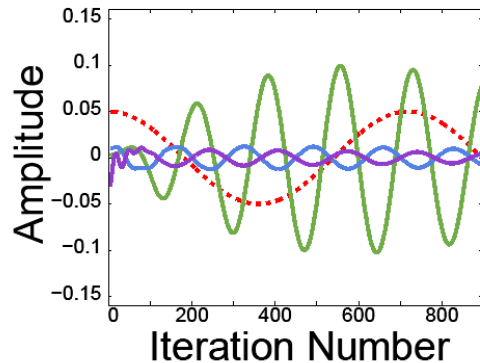
- Frequency matching



$E = 6.8e+05$

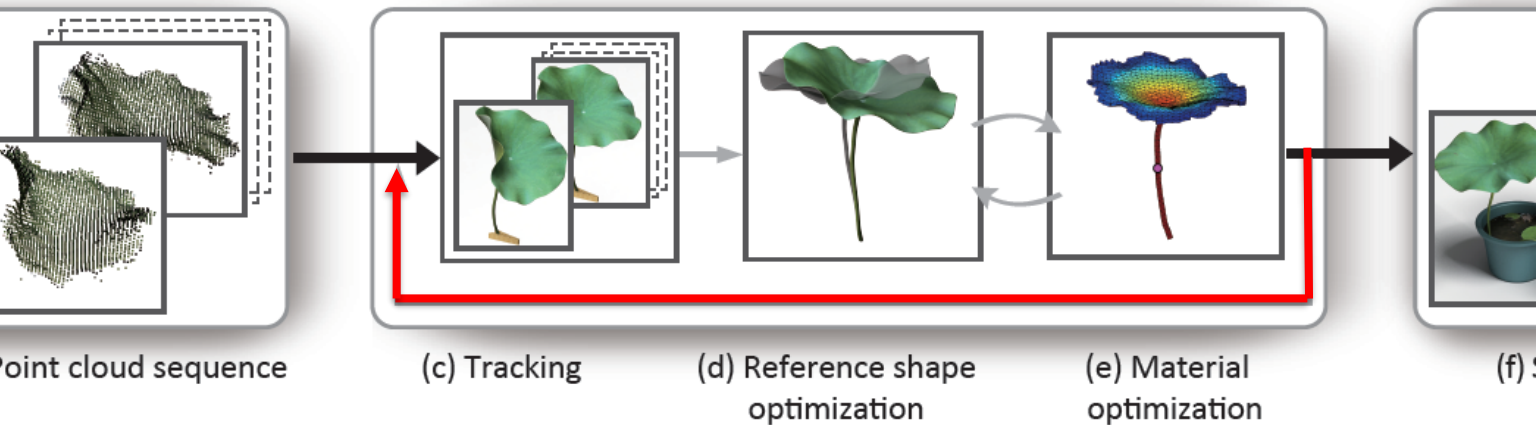


$E = 4.0e+06$



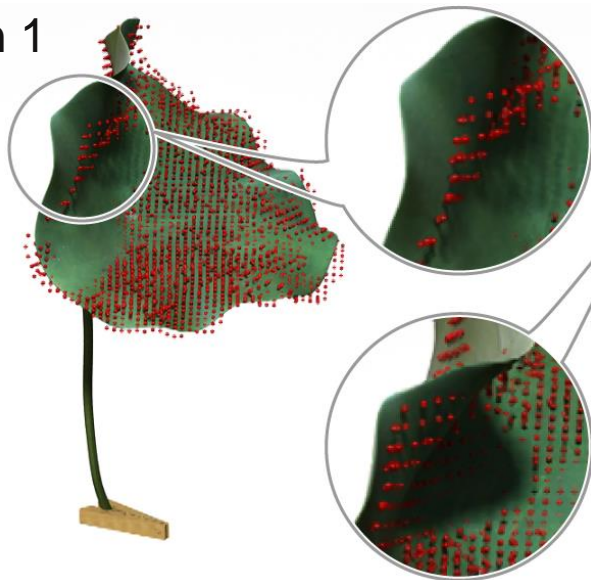
$E = 5.0e+04$

Iterative Refinement

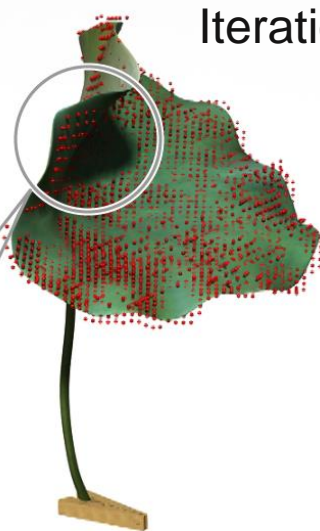


Iterative Refinement

Iteration 1

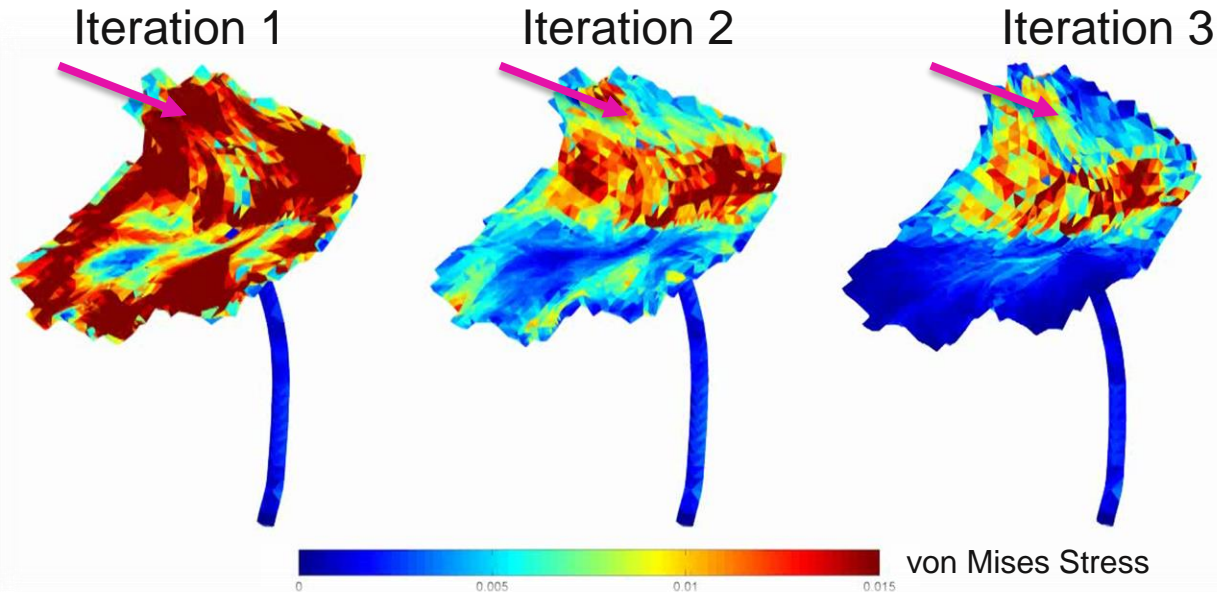


Iteration 2



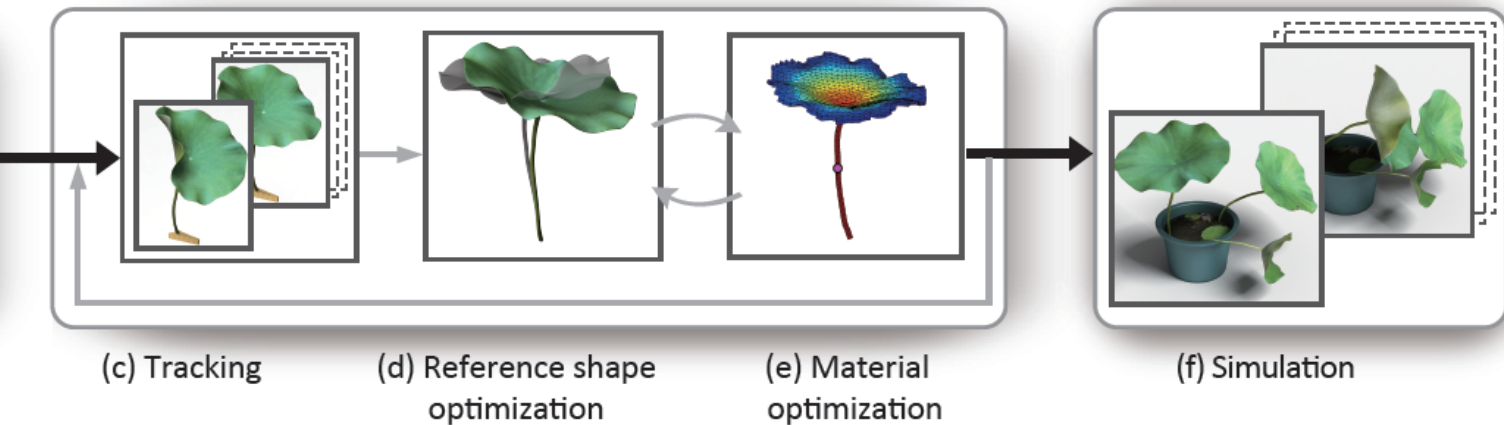
Large deformations can be reconstructed faithfully

Iterative Refinement



The stress field becomes more reasonable

Simulation



Synthesis new motion

Simulation



Simulation with water drops

Simulation

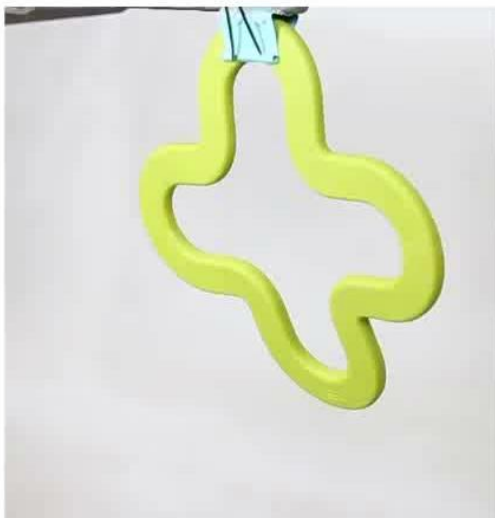


Simulation of wind effects

Validation

Validation

Ground truth

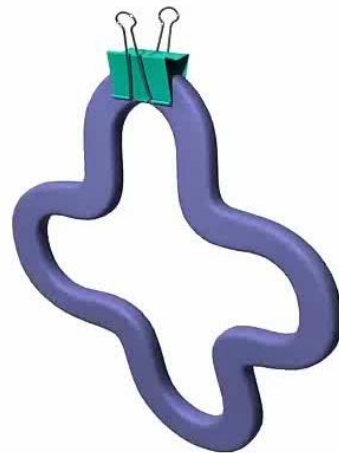


Tracking result



Mode 2 X 1/4

Simulation



Validation

Simulation



20 g

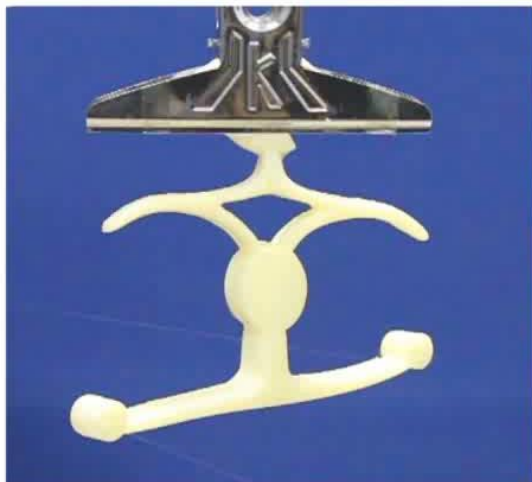
X 1/4

Ground truth



Validation

Ground truth



Tracking result



Mode 2 X 1/2

Simulation



Validation

Simulation



X 1/2

Ground truth



More Results





Simulation under user interaction

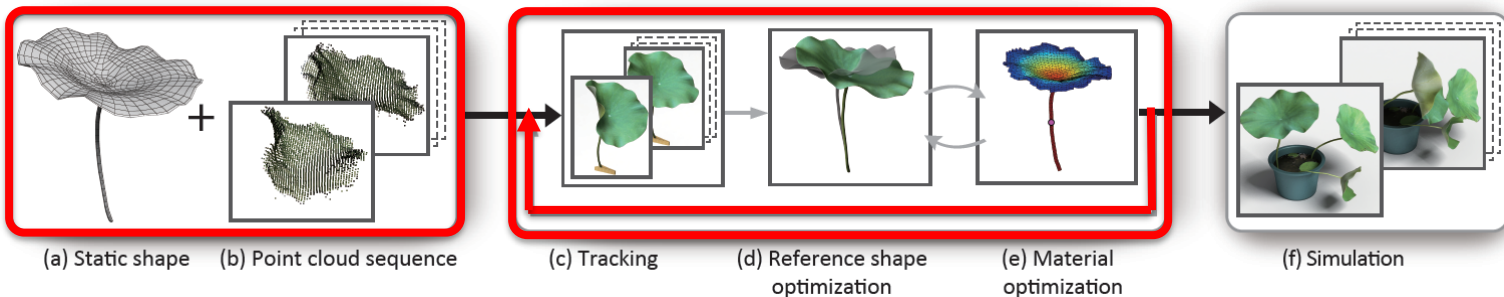


Simulation under user interaction



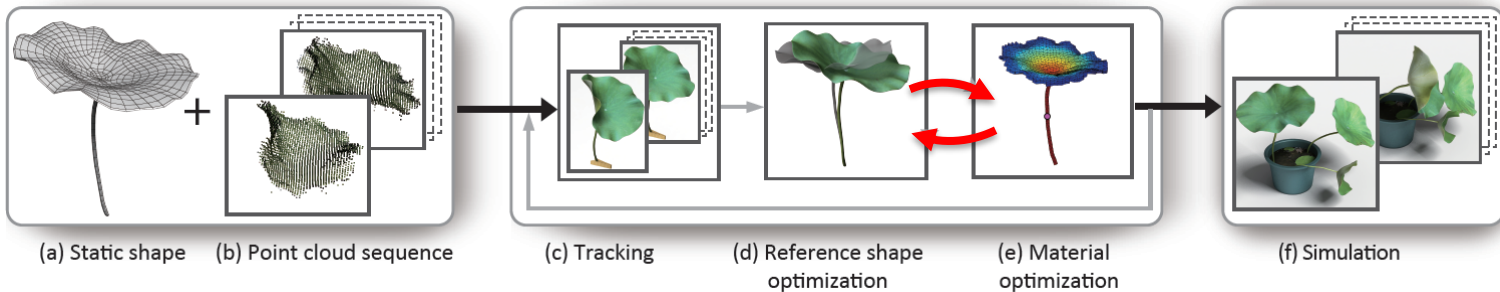
Simulation under user interaction

Conclusion



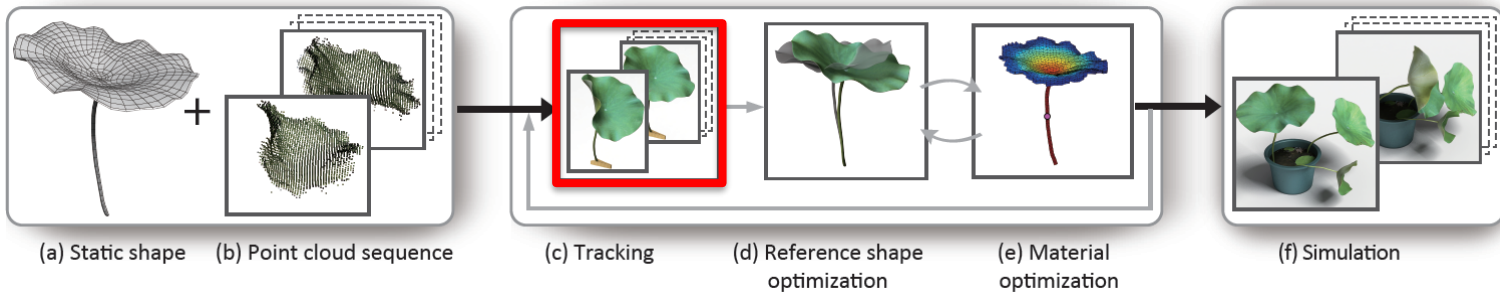
- Iterative tracking and optimization framework

Conclusion



- Iterative tracking and optimization framework
- Splitting scheme for spacetime optimization

Conclusion



- Iterative tracking and optimization framework
- Splitting scheme for spacetime optimization
- Physics-based deformation tracking

Limitations

- Missing high frequency vibration
- Poisson ratio estimation



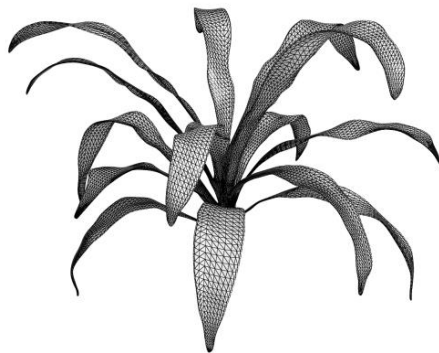
x 1/2



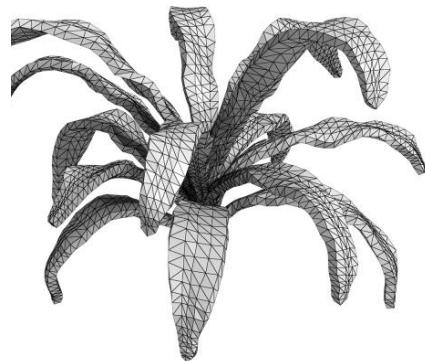
100g

Limitations

- Missing high frequency vibration
- Poisson ratio estimation
- Artificial stiffness



Surface mesh



Volumetric mesh

Limitations

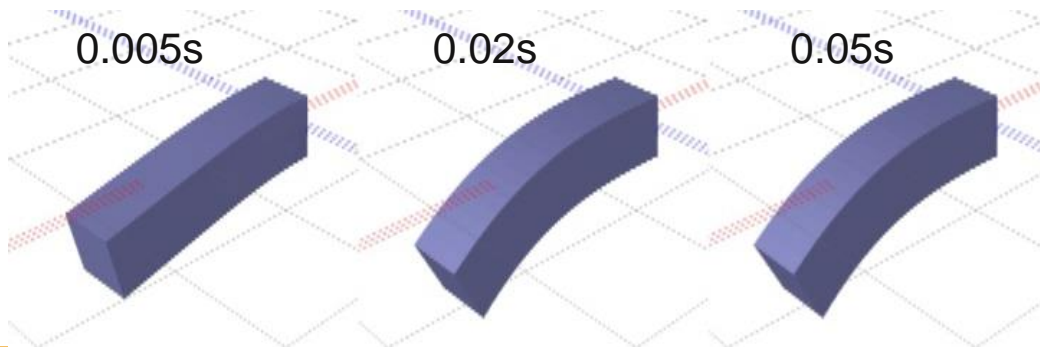
- Missing high frequency vibration
- Poisson ratio estimation
- Artificial stiffness
- Numerical damping

Time Step:

0.005s

0.02s

0.05s



Future Work

- More advanced elastic models
- Gradient-based deformation parameter optimization
- Contact-rich trajectories

Thank You!

Performance

Model	#verts.	#tets.	#nodes	#frames	track (m)	#ctrls	#iter	optimization (h)
Bar	452	3000	756	250 / 250 / 250	-	1 / 2 / 8	-	0.2 / 0.5 / 1.5
Dinosaur	19537	16270	4867	523	-	7	-	3
Pot holder	12212	7488	2316	81	13	1	2	0.7
Hanger	12837	3445	1314	44	9	1	2	0.5
Lotus	10802	6174	2197	234	25	2	3	1.0
Dracaena fragrans	1876	3244	1203	269	7	3	3	0.2
Taro plant	5832	6218	2397	239	38	13	3	2.0

Table 4: Performance statistics measured on an 8-core 3.50GHz Intel Xeon E5-2637 desktop. From left to right, the number of mesh vertices (#verts), the number of tetrahedral elements (#tets), the number of volumetric mesh nodes (#nodes), the number of frames of the captured point cloud data (#frames), tracking time in minutes (track), the number of material control points (#ctrls), the number of iterations of tracking and parameter estimation (#iter), and parameter optimization timing in hours (optimization). For Lotus and Dracaena fragrans, we only modeled a single leaf; while for Taro we modeled the whole plant with three leaves.

Accuracy

		E								α	β
Bar (1 ctrl pts)	ground truth	6.8e+5	-	-	-	-	-	-	-	2.0e-2	1.0e-3
	estimated(1 ctrl pts)	6.7e+5	-	-	-	-	-	-	-	1.9e-2	1.6e-3
	estimated(8 ctrl pts)	7.2e+5	7.2e+5	6.3e+5	6.7e+5	6.5e+5	6.6e+5	7.0e+5	6.8e+5	2.0e-2	1.3e-3
Bar (8 ctrl pts)	ground truth	1.0e+5	1.0e+6	1.0e+4	6.8e+5	2.0e+6	7.0e+4	1.0e+7	3.0e+4	2.0e-2	1.0e-3
	estimated(8 ctrl pts)	1.0e+5	1.0e+6	1.2e+4	6.6e+5	2.1e+6	6.6e+4	1.0e+7	1.9e+4	1.9e-2	6.0e-4
Dinosaur	ground truth	2.0e+5	1.0e+4	1.0e+5	1.0e+6	1.0e+6	1.0e+6	1.0e+6	-	2.0e-2	1.0e-3
	estimated(7 ctrl pts)	2.0e+5	9.9e+3	9.5e+4	1.0e+6	1.0e+6	1.0e+6	1.0e+6	-	1.9e-2	0.4e-3

Table 1: Material optimization and damping coefficients estimation for three synthetic examples: the bar in Figure 9 with one and eight material control points, and the dinosaur in Figure 5(b) with seven control points.

Convergence

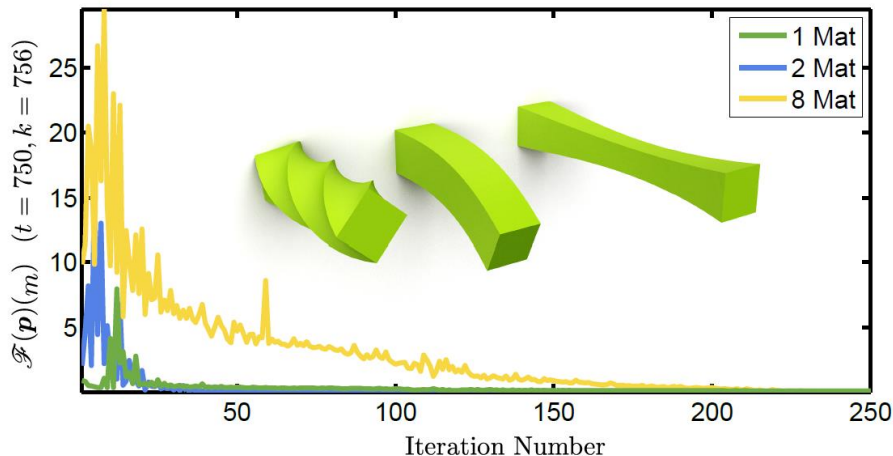


Figure 9: Convergence characteristics of our deformation parameter estimation algorithm for a synthetic bar example with three material configurations (one, two and eight material control points). The trajectories contain 750 frames and the volumetric mesh has 756 nodes.

Reference Shape Estimation




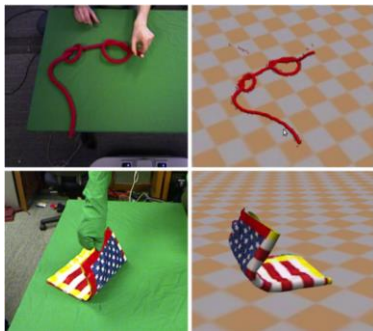
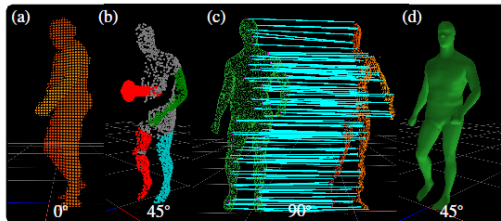
Model		 Plant	 Beam	 Phone holder
ΔX	Mean(m)	8.88e-5	2.59e-4	1.70e-3
Δx^s	Mean(m)	6.35e-5	2.22e-5	2.25e-9
ANM	Time(s)	9.27	3.25	17.99
Ours	Time(s)	12.51	6.03	21.94

Table 2: Comparison of our reference shape optimization with the ANM solver of Chen et al. [2014], in terms of both accuracy and performance. The 3D models were normalized first before we compute the average differences between the shapes. Courtesy of [Chen et al. 2014] for the images and data.

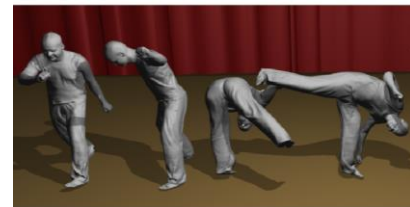
Related Work: Animation Capture



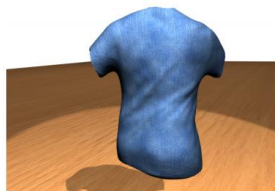
[Schulman et. al 13]



[Helten et. al 13]



[de Aguiar et. al 08]

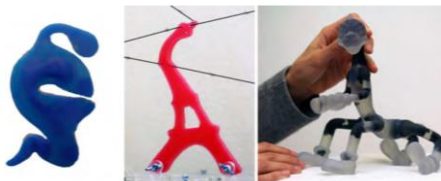


[Bradley et. al 08]



[Li et. al 09]

Related Work: Fabrication-oriented Deformation Design



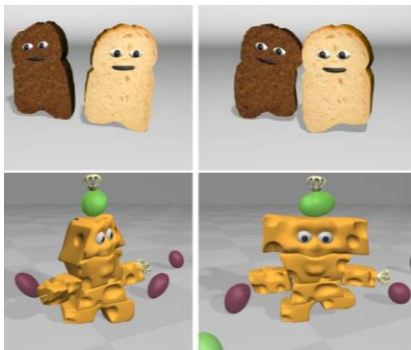
[Skouras et. al 13]



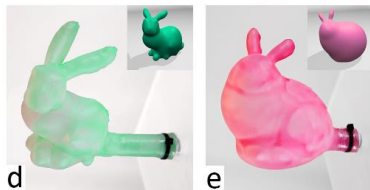
[Derouet-Jourdan et. al 13]



[Bickel et. al 10]



[Coros et. al 12]



[Skouras et. al 12]



(a)

(b)

[Chen et. al 14]

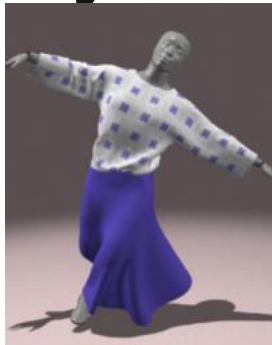
FEM-Based Deformation Simulation

$$\mathbf{M}\ddot{\mathbf{x}} + \mathbf{D}\dot{\mathbf{x}} + \mathbf{R}\mathbf{K}(\mathbf{R}^T \mathbf{x} - \mathbf{X}) = \mathbf{f}_{\text{ext}}$$

- Co-rotated Elastic Model
- Rayleigh Damping

$$\mathbf{D} = \alpha\mathbf{M} + \beta\mathbf{K}$$

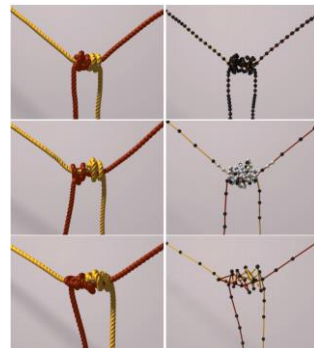
Physically-based Simulation



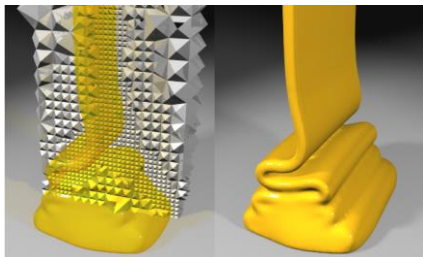
Mass Spring [Baraff et. al 98]



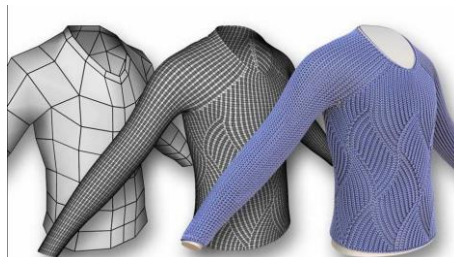
Thin Shell [Pfaff et. al 14]



Rod Element [Spillmann et. al 07]



Finite Element [Batty et. al 11]

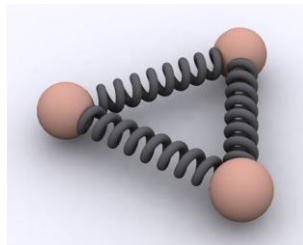


Yarn [Yuksel et. al 12]

Physically-based Deformation Models

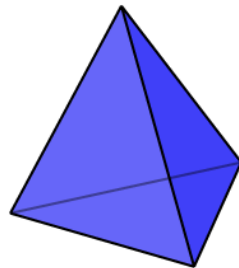
- Spring model

$$f = \underline{k}(x - \underline{x_0})$$



- FEM (Finite Element Method)

k → Young's modulus, Poisson ratio
 x_0 → Reference shape



Manual tuning these parameters for heterogeneous objects is tedious and error prone