

Floods of December 1966 in the Kern-Kaweah Area, Kern and Tulare Counties, California

GEOLOGICAL SURVEY WATER-SUPPLY PAPER 1870-C



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By WILLARD W. DEAN

With a section on GEOMORPHIC EFFECTS IN
THE KERN RIVER BASIN

By KEVIN M. SCOTT

FLOODS OF 1966 IN THE UNITED STATES

GEOLOGICAL SURVEY WATER-SUPPLY PAPER 1870-C



UNITED STATES DEPARTMENT OF THE INTERIOR

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FLOODS OF 1966 IN THE UNITED STATES

FLOODS OF DECEMBER 1966 IN THE KERN-KAWEAH AREA, KERN AND TULARE COUNTIES, CALIFORNIA

By WILLARD W. DEAN

ABSTRACT

Past records of peak flow and 3-day storm-runoff volume in the Kern, Tule, and Kaweah River basins in California were greatly exceeded by the floods of December 1966. Streams rose rapidly following precipitation of as much as 15 inches in a 24-hour period on December 5-6 during a strong inflow of warm moist Pacific air across central California. As heavy rain continued, extremely high peak discharges occurred at most gaging stations between 2300 hours December 5 and 1800 hours December 6.

Snowmelt was not a major cause of the floods, although some snow that had accumulated during minor November and early December storms was melted. This snowmelt was offset by snowpack accumulation at high altitudes where little runoff occurred during the storm.

This report covers the area of most intense precipitation and runoff. Areas of central California to the north and west had severe floods, but these, in general, were not nearly as great as previous record floods. The terrain of the flood area described in the report ranges from the rolling foothills at the east edge of the flat Tulare Lake basin to the steep slopes of the Sierra Nevada where considerable area is above an altitude of 9,000 feet. This report includes discussions of the antecedent hydrology and the meteorology of the storm; a description of the floods, storage regulation, flood damage, comparison to previous floods, sedimentation, channel changes, and flood frequency; a summary of flood stages and discharges; and detailed information on stage, discharge, and reservoir contents for December 1966.

INTRODUCTION

On December 4-6, 1966, an intense Pacific storm brought heavy precipitation to the Kern, Tule, Kaweah, and intervening smaller river basins for 48 hours. Storm runoff increased rapidly to peak flows greater than those previously experienced at most gaging stations

upstream from storage reservoirs. The stations include one station with continuous records since 1912. Peak flows generally were 1.5 to 2 times the magnitude of the probable 50-year flood. On the Kern River near Kernville the 1966 flood stage was somewhat lower than the historic flood of December 1867. The area covered in this report of extreme flooding in the Sierra Nevada and the foothills east of the valley floor is outlined in figure 1. Severe floods that occurred in central California to the west and north are not described in the report.

Damage was less than might be expected from a flood of this record-breaking magnitude because the mountain and foothill areas are sparsely populated. Three reservoirs operated by the U.S. Army Corps of Engineers controlled the floods and prevented catastrophic damage to Bakersfield, Porterville, Visalia, and other downstream

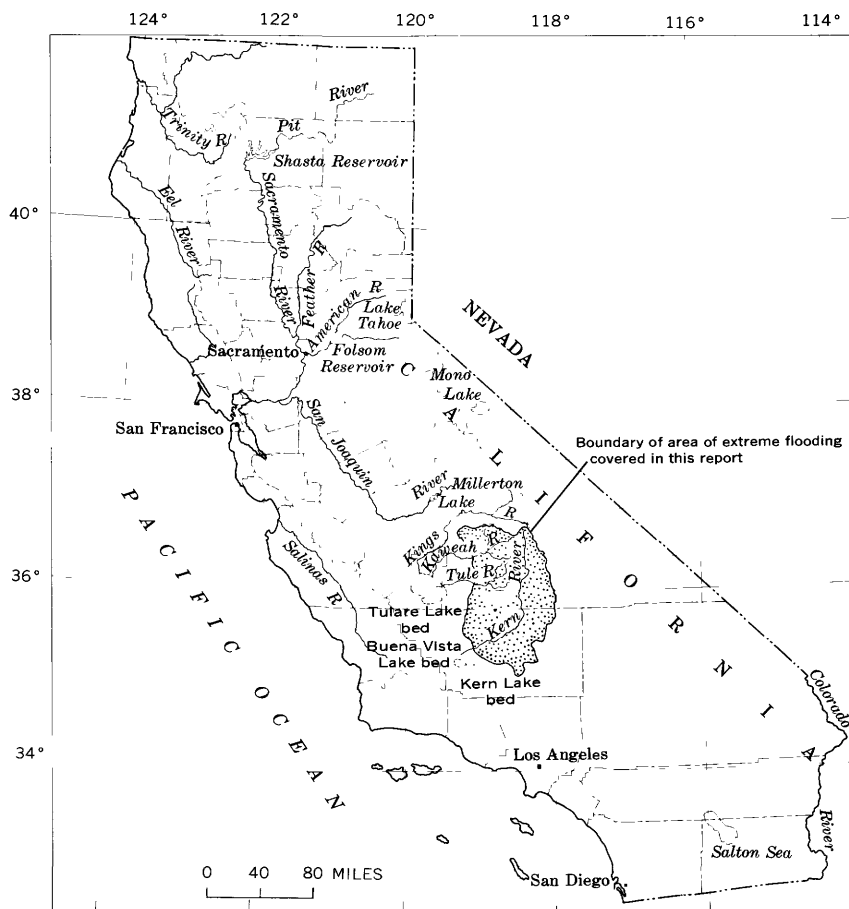


FIGURE 1.—Area of extreme flooding in December 1966.

cities. Actual damage is estimated at \$13 million in mountain and foothill areas upstream from these reservoirs. This total includes \$4,500,000 damage to U.S. Forest Service and National Park Service facilities. The three reservoirs are estimated to have prevented a total of \$81,300,000 in potential downstream damage. Three lives were lost in the flood.

This report provides detailed hydrologic data for use in flood-control planning and in other studies involving flood hydrology. Flood stage and discharge information collected by the U.S. Geological Survey is presented for the flood area. This information includes all available data on stage and discharge for each gaging station during the period of storm runoff, a summary table of flood stages and discharges, a comparison to the maximum floods previously known, and the estimated recurrence interval. Information provided by other agencies on storm precipitation, flood damage, and storage regulation is included.

Pacific standard time on a 24-hour clock basis is used in this report. Numbers in figure 2 are assigned to all gaging sites on a downstream basis following the order used in U.S. Geological Survey publications on surface-water supply and quality. National network identification numbers are also listed in the summary table and in the station-data tabulations for all sites where data are collected on a continuing basis.

Special reports have been prepared for other notable floods in the area flooded in December 1966. The publications that contain this information are U.S. Geological Survey Water-Supply Papers 843, 1137-F, 1260-D, 1650-A and B, and 1830-A.

ACKNOWLEDGMENTS

The data in this report were collected as part of the cooperative programs between the U.S. Geological Survey and the California Department of Water Resources, the U.S. Army Corps of Engineers, the Bureau of Reclamation, and the Forest Service. Records for several stations were furnished by the Southern California Edison Co. and the Pacific Gas and Electric Co. Records for the Kern River near Bakersfield were furnished by the Kern County Land Co.

The data were collected and compiled under the supervision of R. Stanley Lord, district chief of the California district of the Water Resources Division. The field surveys and office computations were supervised by Edward J. Jones, Herman A. Ray, and Verrie F. Pearce of the Sacramento office.

The cooperation of the U.S. Army Corps of Engineers in providing information on storm precipitation, storage regulation, and flood damage is gratefully acknowledged.

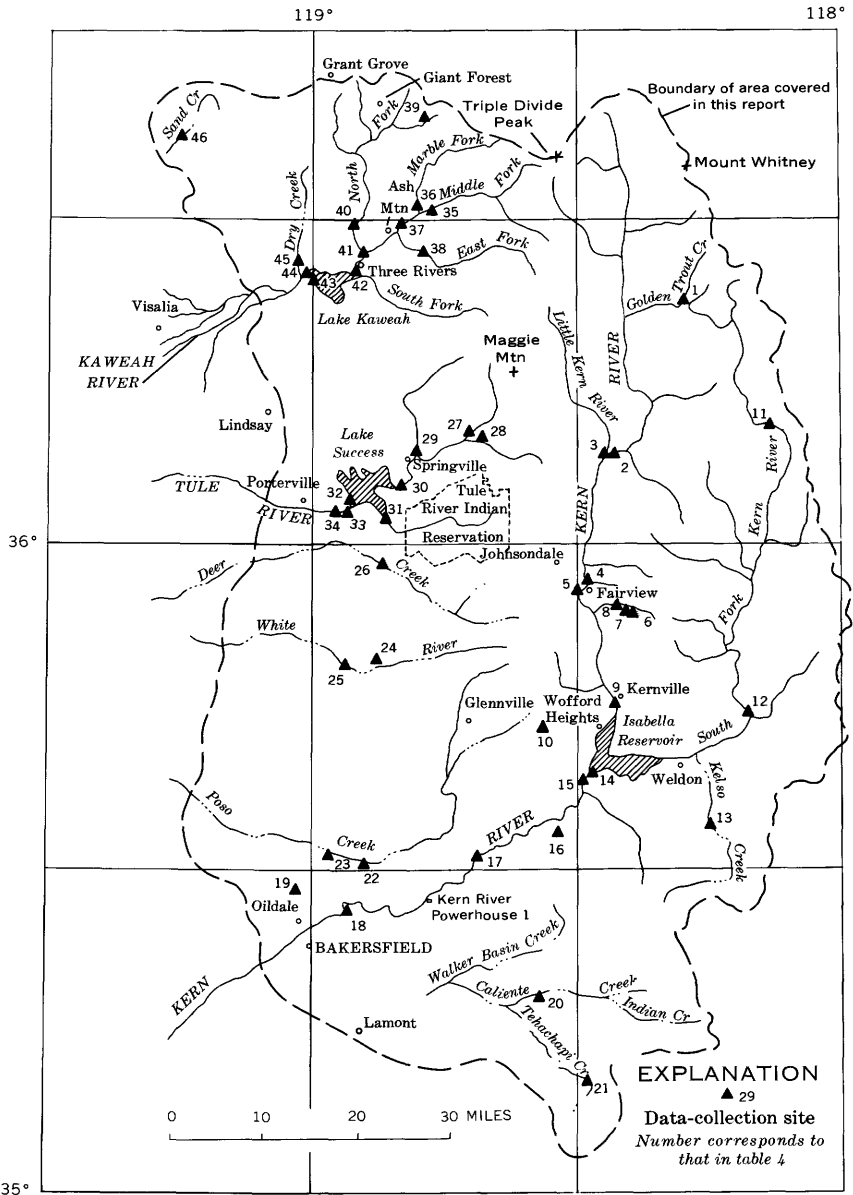


FIGURE 2.—Location of gaging stations.

PRECIPITATION

The primary cause of the floods in December 1966 was the persistent moderate to heavy rainfall that began about 1600 hours on December 4 and continued until 1800 hours on December 6. Antecedent precipitation had reduced soil-moisture deficiencies. Some melting of accumulated low-altitude snow may have augmented flood peaks slightly. The intense precipitation of up to 15 inches in 24 hours would have been sufficient to cause record floods without any antecedent precipitation or snow.

Above-normal precipitation occurred during the latter part of November from several small storms. On December 2, a moderate storm deposited 2-6 inches of precipitation at mountain stations. Late in the afternoon of December 4, an influx of warm moist Pacific air began the period of heavy precipitation and runoff that culminated in the flood peaks late on December 5 or early on December 6. Hourly precipitation at selected stations is plotted in figure 3. The precipitation intensity lessened for a few hours before noon on December 5. Very heavy precipitation resumed after noon and increased generally to its highest rates during the evening of December 5.

Daily and monthly precipitation totals are listed in table 1. More complete data for these and many additional stations are published in the December 1966 Climatological Data report of the U.S. Weather Bureau (1967). Observations of accumulated precipitation tabulated in table 1 are made at 0800 hours at many nonrecording rain gages. Thus the amounts recorded for December 7 at Johnsondale, Glennville, Giant Forest, Grant Grove, and Ash Mountain actually fell on December 6. Daily observations are made later in the day at Wofford Heights (sunset), Kern River powerhouse 1 (1700), Springville (midnight), and Three Rivers powerhouse 2 (1400). Amounts for these stations more nearly represent precipitation on the dates shown.

TABLE 1.—Precipitation, in inches, at selected stations

Station	Altitude (ft)	November		December							Total for month	Percentage of normal
		Total for month	Percentage of normal	1	2	3	4	5	6	7		
Johnsondale.....	4,680	4.58	0	0.0	3.15	Trace	6.46	14.94	5.90	30.61
Glennville.....	3,140	2.07	0	.09	.92	0	1.52	4.38	1.71	8.74
Wofford Heights.....	2,700	1.16	0	.04	1.14	1.04	2.60	6.04	.14	11.03
Kern River powerhouse 1.....	970	1.28	147	0	.02	.57	.01	.97	1.82	.07	3.54	200
Springville Ranger Station.....	1,050	2.38	0	1.66	.02	.21	5.04	3.85	0	10.93
Giant Forest.....	6,412	5.83	158	0	.15	5.80	.06	5.81	12.90	3.03	28.02	335
Grant Grove.....	6,600	5.72	0	.17	4.86	.16	4.33	10.09	3.43	23.33
Ash Mountain.....	1,708	5.83	266	0	.09	2.46	.08	2.98	7.33	2.58	15.65	316
Three Rivers powerhouse 2.....	950	3.72	220	0	.34	1.41	0	2.03	7.90	.17	11.99	310

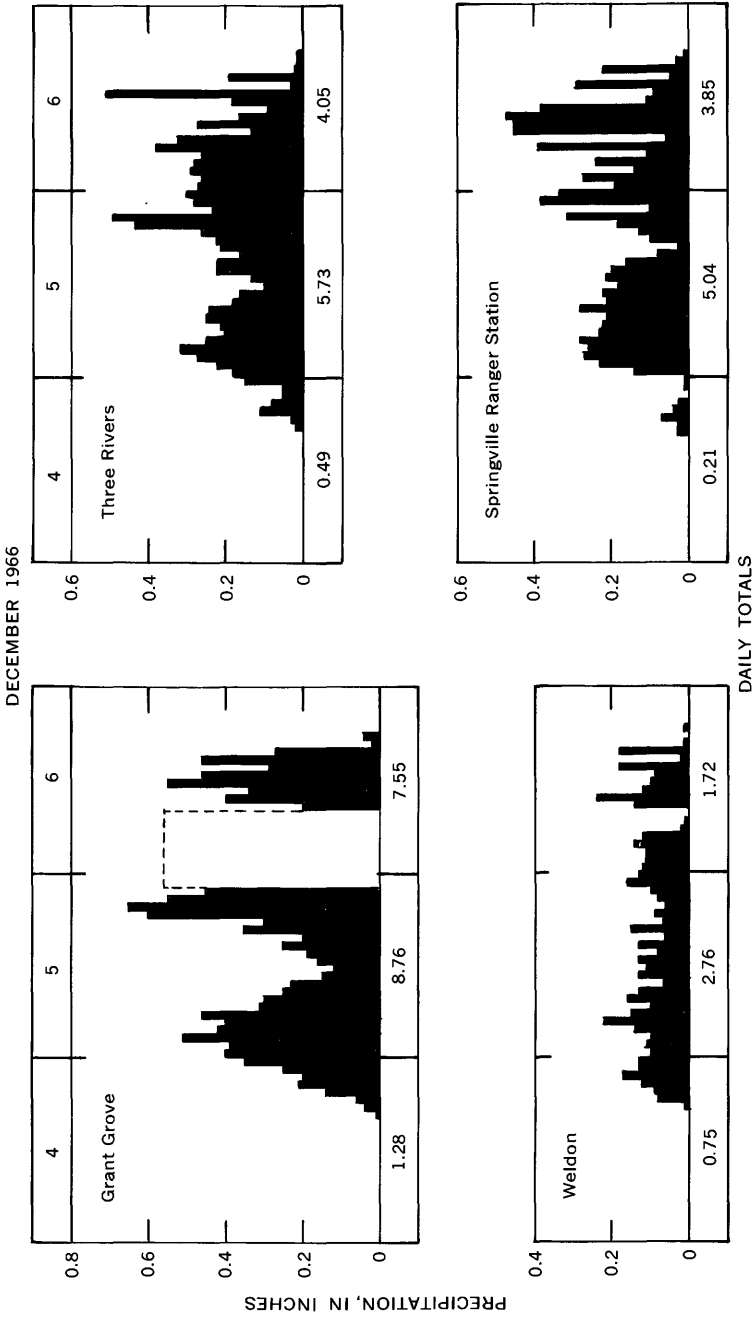
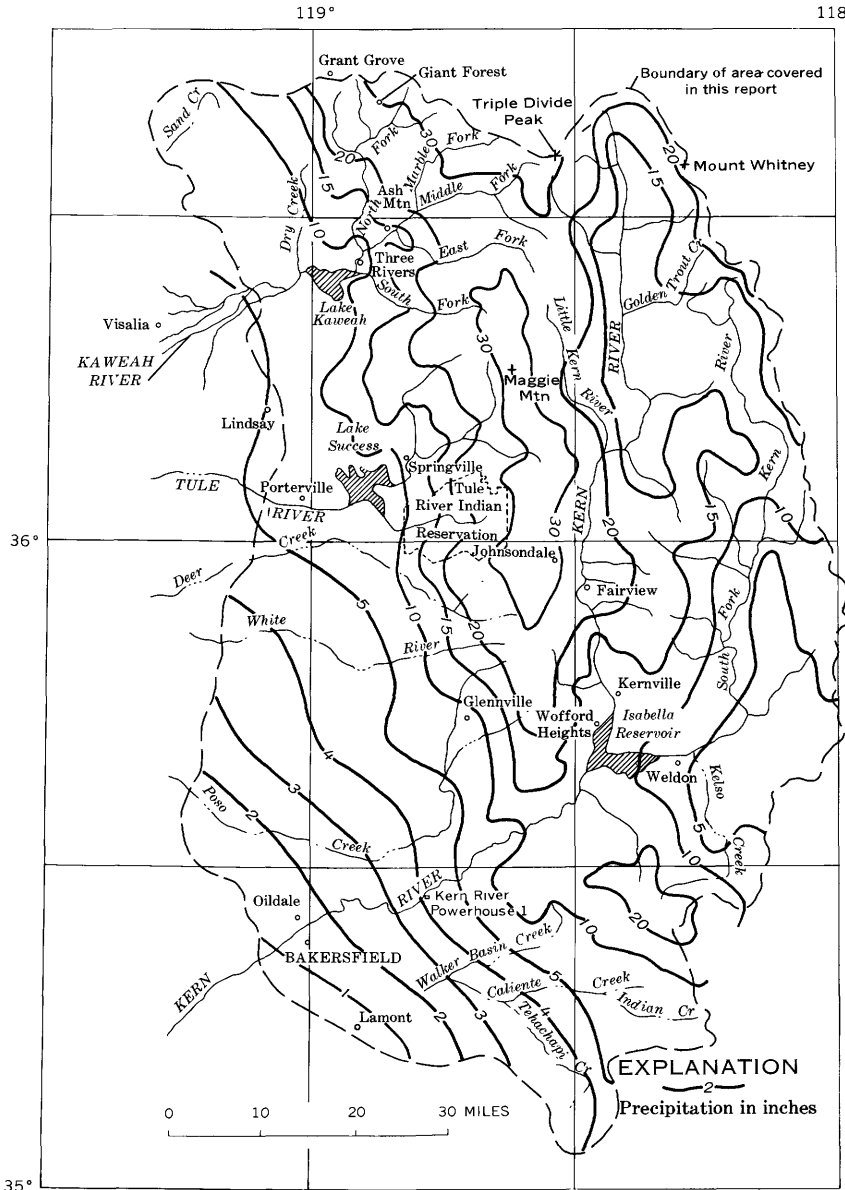


Figure 3.—Hourly precipitation at selected stations.

Measurements at the many high-altitude snow courses in the flood area are not made until January 1 or February 1 of each year. Therefore, there are few data on snowpack accumulation or loss during the storm. Snow depth on the ground is measured daily at Grant Grove (alt, 6,600 ft); however, no snow was reported on the ground there before the December storm, and the 4 inches reported at 0800 hours December 5 was gone December 6. During an inspection of Kern River basin gaging stations December 8 and 9, no snow was noted on the ground below 7,000 feet altitude, but thin patches of saturated snow and snow-ice were noted between 7,000 and 8,000 feet, and continuous snow cover was noted above 8,500 feet. At the Golden Trout Creek gaging station (site 1) the snow on the ground at 9,000 feet consisted of a 2-foot-deep dense frozen base which was covered with 1 foot of powder snow. Evidently rain had fallen at that altitude during part of the storm, but the snowpack absorbed most of the rain. Above 9,000 feet the storm precipitation caused little runoff in the Kern River basin.

The isohyetal map (fig. 4) adapted from data furnished by the U.S. Army Corps of Engineers (1967, pl. 3) shows the generalized total precipitation December 2-6 over the flood area. The map is based on all available precipitation data from recording gages, non-recording daily observation gages, and high-altitude storage gages. Precipitation accumulated since September 1966 in storage gages was measured December 13 and proportioned on the basis of lower altitude daily precipitation records to estimate total December 2-6 storm precipitation for the high altitudes.

To relate precipitation to runoff in the December 1966 flood area, it is necessary to determine the altitude above which precipitation fell as snow and did not contribute to runoff. Analysis by the U.S. Corps of Engineers (1967, chart 1) indicates that the incoming warm moist air brought rain as high as 8,000 feet altitude during the evening of December 5 and up to 10,000 feet early on December 6. This rainfall melted most of the shallow residual snowpack from December 2-4 and previous storms. Observation by the Corps of Engineers of the snowpack near high-altitude precipitation gages in the Kern, Tule, and Kaweah River basins on December 13 indicated that heavy rain had fallen during the December 5-6 storm above 8,000 feet altitude. Personal observation December 9 of snowpack and stream-channel conditions at the Golden Trout Creek gaging station disclosed that little storm runoff had occurred above 9,000 feet in the Kern River basin. To the west, runoff probably occurred from all altitudes in the Tule River basin (highest alt, 10,042 ft) because practically the entire basin was bare, with only patches of snowpack being observed at highest altitudes December 8. No direct observations were made to define



Isohyetal Lines from U.S. Army Corps of Engineers (1967, pl. 3)

FIGURE 4.—Isohyets of total precipitation. December 2-6, 1966.

the upper altitude boundary of the runoff-producing area in the Kaweah River basin. The altitude of the snowline in the Kaweah River basin probably was comparable to that in the Tule River basin, with little snow below 9,000–10,000 feet altitude.

The effect of the altitude of the snowline on runoff is demonstrated by use of area-altitude curves (fig. 5). Assuming that there was little direct runoff from areas above 9,000 feet altitude, about 80 percent of the Kern River drainage area above Isabella Reservoir contributed storm runoff to the peak of the December 1966 flood. Likewise, at least 90 percent of the Kaweah River drainage area above Lake Kaweah contributed runoff, and virtually 100 percent of the Tule River drainage area above Lake Success contributed.

In contrast, a colder storm with snow down to 6,000 feet altitude would cause rain and runoff over only 35 percent of the Kern River basin, 50 percent of the Kaweah River basin, and 80 percent of the Tule River basin. Such a storm occurs often over these areas during the period of December through March when Pacific airflow from the west or northwest has a temperature as much as 5° Celsius colder than the temperature during the storm period of December 5–6, 1966. Under these conditions the runoff-producing area of the Kern River basin would be less than half that during the December 1966 flood and that of the Kaweah River basin only a little more than half. Runoff from the Tule River basin is affected less by temperature differences because a much smaller part of the drainage area is higher than 6,000 feet altitude. In the Kern and Kaweah River basins, however, the precipitation during the relatively warm storm of December 1966 fell as rain over a much larger part of the drainage than usual and produced much greater runoff than usual during a winter storm.

The area-altitude curves (fig. 5) were approximated on the basis of 100 or more points selected on a uniform square grid system and were arrayed by altitude zones. The curves were smoothed after plotting cumulative percentages of points above indicated altitudes.

GENERAL DESCRIPTION OF THE FLOODS

The intense 48-hour storm on December 4–6, 1966, caused record-breaking floods in the Buena Vista Lake and Tulare Lake basins (fig. 1). Severe flooding extended over the Kern, Tule, and Kaweah River basins in a 60- by 100-mile area in the Sierra Nevada northeast of Bakersfield. Moderate flooding occurred in the Kings River basin and other basins to the north and in streams draining from the Coast Range to the west.

Hydrographs of daily mean discharge at key gaging stations on Kern, Tule, and Kaweah Rivers are shown in figure 6. The hydro-

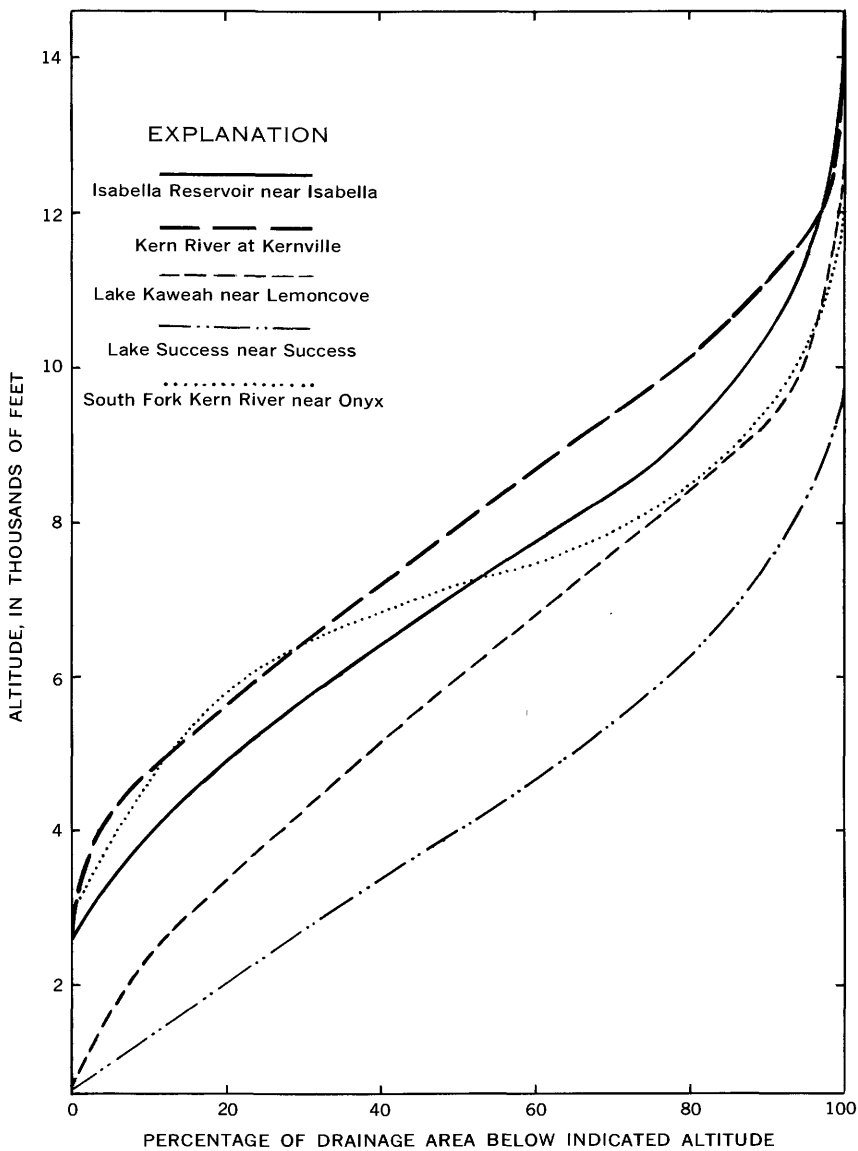


FIGURE 5.—Area-altitude relations upstream from selected gaging stations or reservoirs.

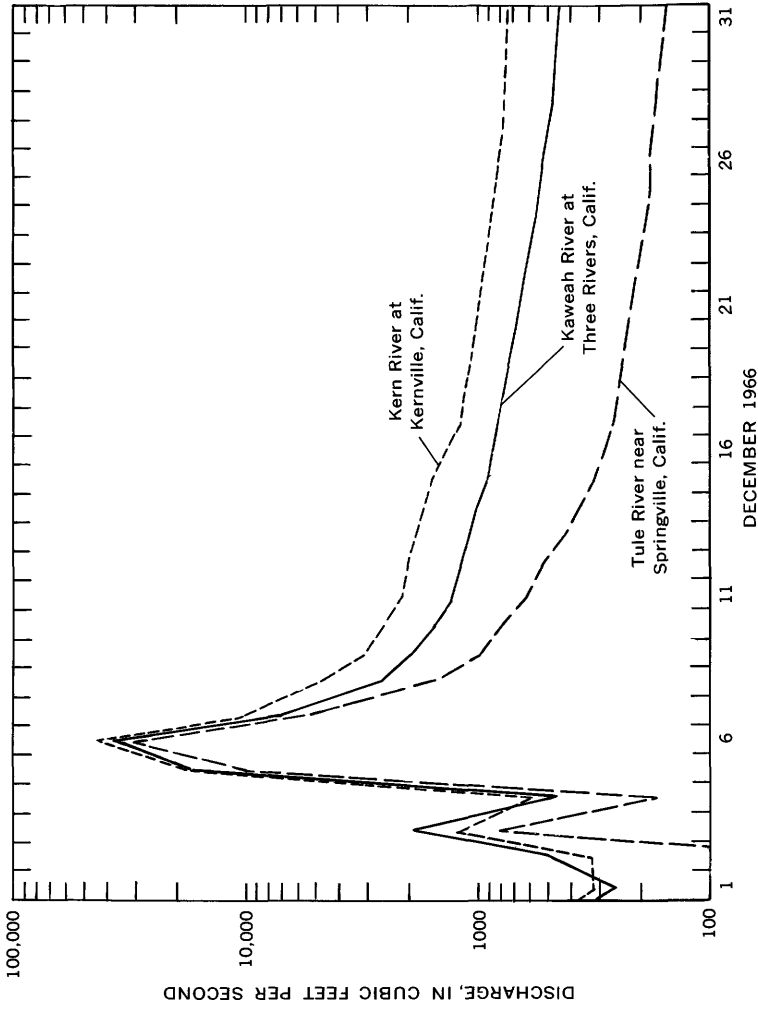


FIGURE 6.—Hydrographs showing daily mean discharge at selected gaging stations.

graph shape is remarkably similar for the three rivers. Flood peaks were the greatest of record at many gaging stations in the Kern, Tule, and Kaweah River basins. Damage was severe in all headwater areas. Most highway bridges were destroyed or severely damaged. Culverts were overflowed or plugged with debris, or usually a combination of both. Sustained discharge in excess of normal channel capacity eroded streambeds and streambanks and damaged all adjacent structures. Details regarding the flood in each basin are given in the following sections.

KERN RIVER BASIN

The Kern River basin upstream from the gaging station near Bakersfield (site 18), a drainage area of 2,407 square miles, ranges in altitude from 450 feet to 14,495 feet at the summit of Mount Whitney. Runoff from 2,074 square miles, 86 percent of the area above the Bakersfield gage, is controlled in Isabella Reservoir (site 14). Records are available from 18 gaging stations in the Kern River basin to document the flood. A good sample of different hydrologic conditions is provided because runoff is measured from drainage areas with a wide range of size, altitude, and location in the basin. Eleven of the stations were installed since the November 1950 and December 1955 floods, which were the greatest previous floods of record. Continuous records are available since 1893 for Kern River near Bakersfield and since 1912 for Kern River near Kernville.

Peak flows of the December 1966 flood exceeded previous maximums at all stations except those on Golden Trout Creek, the one at South Fork Kern River near Olancha (site 11), and those below Isabella Dam (sites 15, 17, 18). The stations on Golden Trout Creek and South Fork Kern River near Olancha are at high altitudes above which December 1966 storm precipitation fell mostly as snow. Flows during December 1966 at the three stations on Kern River downstream from Isabella Dam were less than those during several floods prior to completion of the dam in 1954. Detailed hydrographs during December 4-7, 1966, at four selected Kern River stations are shown in figure 7. The hydrograph of computed inflow to Isabella Reservoir near Isabella (site 14) shows unusual fluctuations on December 4; the trend of actual inflow probably follows that of the Kern River at Kernville.

The maximum discharge of 60,000 cfs (cubic feet per second) of the Kern River near Kernville (site 5) on December 6, 1966, was more than twice the previous maximum of 27,400 cfs in November 1950 and December 1955. The maximum discharge of 28,700 cfs on the South Fork Kern River near Onyx (site 12) was eight times as great as the previous maximum of 3,460 cfs recorded in February 1963. The computed maximum bihourly inflow of 96,900 cfs to Isabella Reservoir

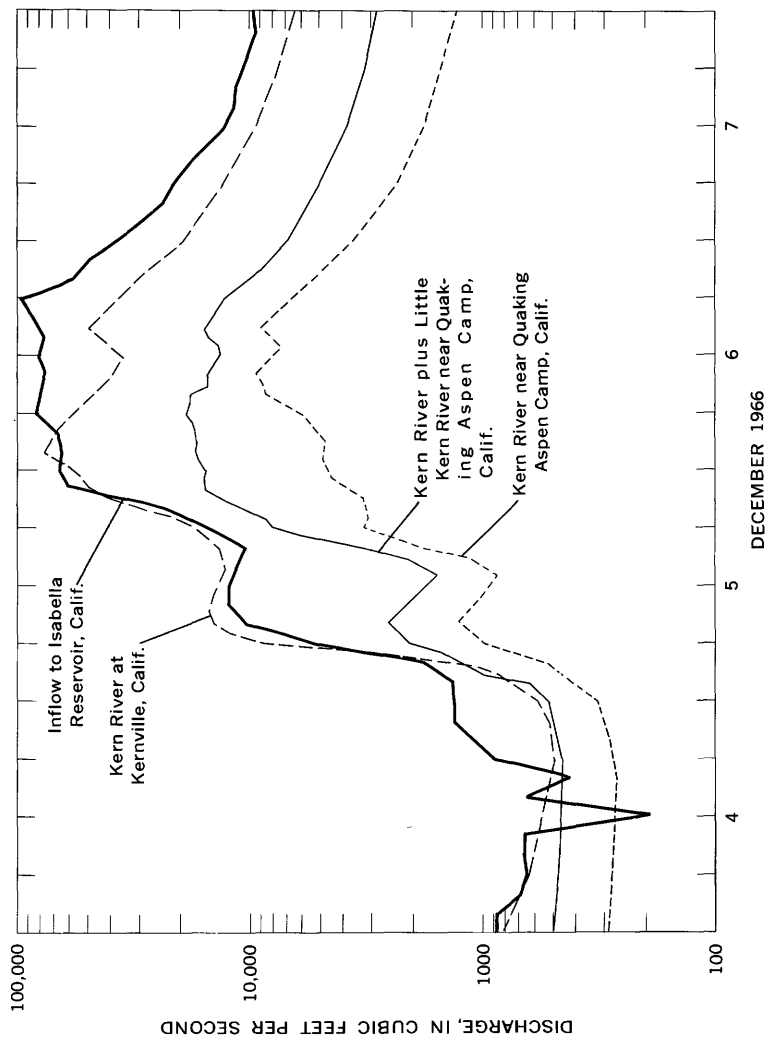


Figure 7.—Hydrographs showing discharge at selected gaging stations in Kern River basin.

near Isabella was 2.5 times the previous maximum flow of 39,000 cfs at the damsite in November 1950 prior to dam construction.

Little storm runoff occurred above 9,000 feet altitude where the precipitation fell during part of the storm as snow and during the remainder as rain, as the freezing level changed during the storm. When inspected on December 9, the channel of Golden Trout Creek was nearly full of ice and frozen saturated snow. There was no evidence of substantial high flow during the storm. Snow already on the ground apparently absorbed and held most of the rain that fell upstream from this gaging station.

The next highest Kern River basin gaging station is at 7,840 feet on the South Fork Kern River near Olancha. A moderate peak occurred on December 6, but the yield per square mile was low because of a substantial noncontributing area above about 9,000 feet. The relations between drainage area and altitude upstream from the gaging stations on the South Fork Kern River near Onyx and the Kern River at Kernville are shown in figure 5.

For the December 1966 flood the computed peak runoff per square mile at main Kern River gaging stations increases in a downstream direction because downstream tributaries drain more area at altitudes below 9,000 feet. The unit runoff of Kern River tributaries near Fairview and Kernville exceeded 100 cfs per square mile. The greatest known unit runoff was 490 cfs per square mile from a 1.21-square-mile area above a crest-stage gage (slope-area measurement) at Kern River tributary near Miracle Hot Springs (site 16). Heavy precipitation on December 6 caused this peak and the peak discharge of 9,290 cfs at Kern River near Bakersfield (site 18) on December 7 that was the result of storm runoff from the 333-square-mile drainage area downstream from Isabella Dam. The only release from Isabella Dam for the first 10 days during and after the flood was the 300-500 cfs released to Borel Canal for power production.

Damage was heavy along stream channels in the Kern River basin. The road from Kernville upstream to Johnsondale is close to the river at many locations. This road was obliterated at the outside bank of many river bends, and the pavement was scoured away in other locations. The modern steel girder and concrete deck bridge at Kernville was destroyed by floodflow. Bridge debris, including one 3-foot by 40-foot steel girder, was moved several hundred feet downstream. A trailer court and other buildings along the river at Kernville were badly damaged.

The flood destroyed the water-stage recorder structures and the measuring cableways on the Kern River at Kernville (site 9) and South Fork Kern River near Onyx (site 12). The series of four pictures in figure 8, taken by personnel of the U.S. Forest Service or



A. November 27, 1966



B. December 5, 1966



C. December 6, 1966



D. December 7, 1966

FIGURE 8.—Flow at gaging-station site, Kern River at Kernville, before, during, and after flood of December 1966. (Photographs courtesy of U.S. Forest Service.)

November 27 and December 5, 6, and 7, shows the gaging-station site on the Kern River at Kernville before and after the flood. The gaging station on the Little Kern River near Quaking Aspen Camp was tilted downstream when the riverbank of boulders and cobbles was scoured away, but the station remained in operation. The concrete recorder structure on the Kern River near Kernville survived the flood, although the recorder was submerged and the cableway destroyed. Later this station also had to be replaced because the low-flow channel had been scoured during the flood below the altitude of the intake pipes to the gage well. The gaging station on Kelso Creek near Weldon was put out of service permanently when a sand fill 8 feet deep plugged the channel during flow recession on December 6. The fill extends on a level plain 200 feet wide from cutbank to cutbank in the alluvial terrain. Most gages were destroyed and discharge-rated culverts were plugged at small-area crest-stage gage stations in the Kern River basin.

The flood caused the loss of two lives in the Kern River basin. One woman died from exposure after she and a companion were isolated by the flood in the Lamont Meadows area on the South Fork Kern River. One man cleaning a weir on the lower Kern River fell into the river and suffered a fatal heart attack.

TULE RIVER BASIN

The Tule River drains a fan-shaped 391-square-mile area above Lake Success east of Porterville. The drainage area extends from an altitude of 560 feet at the reservoir to 10,042 feet at the crest of Maggie Mountain on the Tule-Kern River basin drainage divide. The relation between drainage area and altitude in the Tule River basin above Lake Success is shown in figure 5. Only a very small part of the basin is above 9,000 feet altitude and was noncontributing during the 1966 flood. Steep slopes in the upper part of this basin cause rapid concentration of runoff during all major storms. The basin is heavily timbered above 5,000 feet altitude. Lower slopes are covered with brush and scrub timber. Valleys along the North Fork Tule and main Tule Rivers have large open cultivated fields.

Records for the December 1966 flood are available from eight gaging stations in the Tule River basin. Detailed hydrographs at three selected stations in the basin are shown for the period December 4-7 in figure 9. The December 1966 maximum flow of 49,600 cfs at the gaging station on the Tule River near Springville (site 30) was the greatest flood of record and more than double the previous record flow of 22,400 cfs in November 1950. Records at a former gage site inundated by Lake Success in 1961 show that the 1950 flood was the greatest during the period of record, from 1901 to 1960. The December 1955 peak

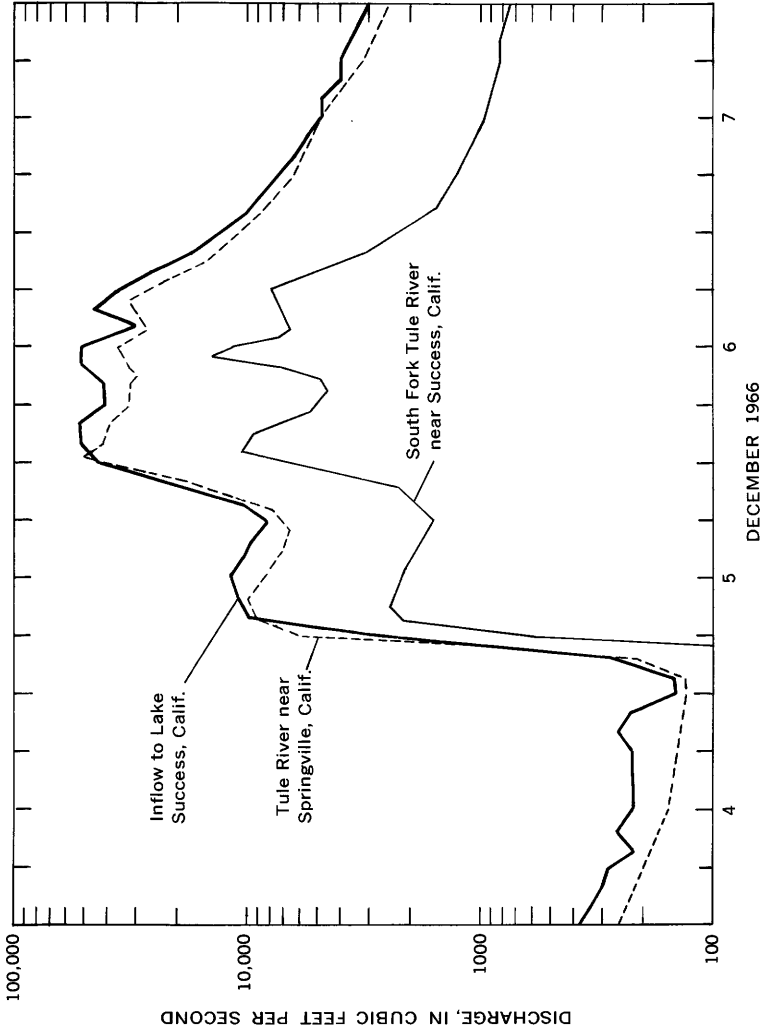


FIGURE 9.—Discharge hydrographs at selected gaging stations in the Tule River basin.

discharge was slightly less than that in 1950 and thus was the third highest recorded flood on the Tule River. The December 1966 peak discharge of 14,300 cfs on the South Fork Tule River near Success (site 31) was also more than double the previous record flow of 7,000 cfs in November 1950. The computed maximum bihourly inflow to Lake Success near Success (site 32) of 52,800 cfs on December 6 similarly was 1.7 times the peak flow of 32,000 cfs in November 1950 at a former gaging station near the damsite. The 85,400 acre-feet of nominal storage capacity in Lake Success plus 16,000 acre-feet of flood surcharge storage were utilized by the Corps of Engineers to reduce the record-high inflow of December 1966 to a peak outflow of 9,050 cfs about 18 hours later.

Peak runoff of 430 cfs per square mile from a 39.3-square-mile area on the North Fork of Middle Fork Tule River near Springville (site 27) was the highest in the Tule River basin. Unit runoff exceeded 130 cfs per square mile throughout the basin.

Damage in the Tule River basin was greatest along headwater stream channels, where all manmade structures suffered some degree of damage. The concrete bridge across North Fork Tule River at Springville and two bridges across the Tule River downstream from Springville were destroyed. Houses along the banks of the Tule River at Springville were damaged severely by flooding. Many road culverts on normally small channels were destroyed when they were plugged or overflowed by the record runoff. On the Tule River Indian Reservation a 6-year-old boy died from exposure when he was isolated after a bridge washed out. Some flooding occurred in agricultural areas downstream from Lake Success during sustained release of floodwater December 6-11.

Gaging stations were heavily damaged, including total destruction of the station on the North Fork Tule River at Springville (site 29) adjacent to the bridge that was destroyed. Downstream, the station on Tule River near Springville survived the destruction of the bridge to which it was attached, but had to be rebuilt at a different site because of channel scour. Upstream, two low-flow gaging stations belonging to the Southern California Edison Co. were badly damaged.

KAWEAH RIVER BASIN

The Kaweah River basin includes 560 square miles of forest, brush, and open areas above Lake Kaweah, the Corps of Engineers' flood-control and conservation reservoir east of Visalia. Headwater drainage extends up to an altitude of 12,634 feet at the summit of Triple Divide Peak on the Great Western Divide, which separates the Kaweah River basin from the Kern River basin to the east. Triple Divide Peak lies at the juncture with the Kings River basin to the north. The

relation between drainage area and altitude in the Kaweah River basin above Lake Kaweah is shown in figure 5.

Eleven continuous, partial-record, and crest-stage gaging stations provide flood records in the Kaweah River basin. Eight are upstream from Lake Kaweah, one is on the reservoir, and two are downstream. Detailed hydrographs for December 4-7, 1966, at four selected stations are shown in figure 10.

Adding the hydrograph of Kaweah River at Three Rivers (site 41) to that of South Fork Kaweah River at Three Rivers (site 42) gives an estimated peak discharge of 78,500 cfs on December 6, 1966, from the 505-square-mile drainage area upstream from the junction of the two streams. The December 6, 1966, peak stages at these two stations were slightly higher than the floodmarks for December 23, 1955. The maximum discharge during the period 1903-60 was 80,700 cfs December 23, 1955, at a former gaging-station site near Three Rivers. The drainage area was 520 square miles at the former site, now submerged in Lake Kaweah.

The computed maximum bihourly inflow on December 6 to Lake Kaweah near Lemoncove (site 43) was 82,700 cfs. The drainage area at Lake Kaweah is 560 square miles. The 1966 maximum flow of 23,900 cfs at North Fork Kaweah River at Kaweah (site 40) exceeded the 1955 peak discharge of 21,500 cfs. The December 1955 and December 1966 floods were of approximately equal magnitude in the vicinity of Three Rivers and Kaweah. However, upstream December 1966 peak discharges at Middle Fork Kaweah River (site 37) and Marble Fork Kaweah River near Potwisha Camp (site 36) were only about half those of 1955. The maximum discharge of 14,500 cfs on December 6, 1966, at Dry Creek near Lemoncove (site 45), tributary to the Kaweah River downstream from Lake Kaweah, was more than double the peak discharge of 6,070 cfs on December 23, 1955, at a slope-area measurement site 2 miles upstream. Thus the 1966 flood peaks in the Kaweah River basin were about half those of 1955 in upstream tributaries, equal to those of 1955 in the vicinity of Three Rivers, and twice those of 1955 on a downstream tributary.

Figure 11 is a plot of cumulative hourly precipitation at the recording gage at Grant Grove (alt, 6,000 ft) and computed cumulative hourly runoff at the gaging station on the Kaweah River at Three Rivers. Runoff is expressed in equivalent inches of depth over the 418-square-mile drainage area. The peak hourly precipitation recorded was 0.65 inches, although hourly precipitation probably was greater sometime during a 10-hour period when the only record at Grant Grove is from a nonrecording gage. A radio-reporting precipitation gage at Giant Forest indicated a total of 4.1 inches of precipitation during the period of 1600 to 2000 hours December 5.

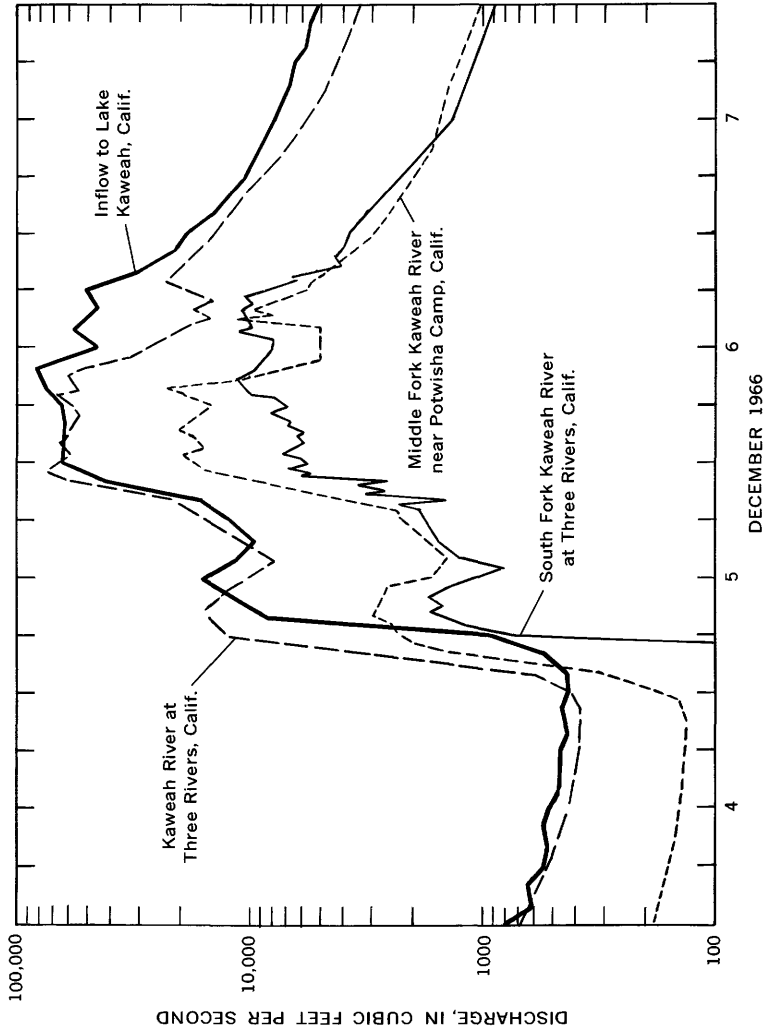


FIGURE 10.—Discharge hydrographs at selected gaging stations in the Kaweah River basin.

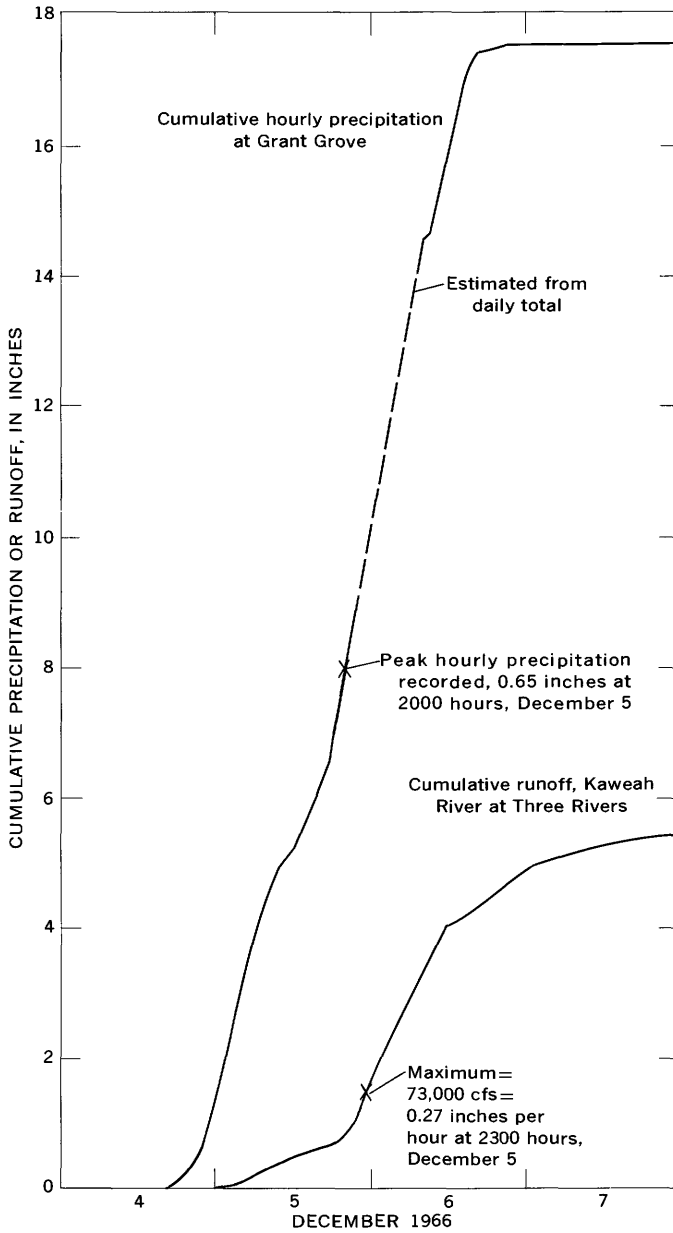


FIGURE 11.—Cumulative precipitation or runoff in the Kaweah River basin.

The maximum runoff rate of the Kaweah River at Three Rivers was equivalent to 0.27 inches per hour at 2300 hours on December 5. Total runoff past this gaging station during December 1966 was equivalent to 7.59 inches. Total precipitation during December was 23.33 inches at Grant Grove. Assuming that Grant Grove precipitation data are somewhat representative of the basin mean, then about two-thirds of the precipitation that fell in December remained in storage in the Kaweah River basin as snow, ground water, and soil moisture. Evapotranspiration losses would be small during December.

MISCELLANEOUS BASINS

Available records indicate that the December 1966 flood was the greatest flood of record on most major streams within the Kern-Kaweah area. These include Poso Creek draining the area west of the lower Kern River basin, Deer Creek draining the area west of the Kern River and south of the Tule River, and Sand Creek draining the area west of the North Fork Kaweah River. Peak runoff was less to the south on Caliente and Tehachapi Creeks, which were close to the south boundary of the intense storm precipitation. Poso Creek and White River, which is a smaller stream in the western foothills between Poso Creek and Deer Creek, had lower peak discharges in December 1966 than the estimated maximums during the flood of March 9, 1943.

The 10,000 cfs peak discharge on December 6, 1966, on Deer Creek near Terra Bella (site 26) was particularly destructive. The main road to California Hot Springs follows Deer Creek and crosses it at several locations. All bridges were destroyed or badly damaged. Downstream irrigation diversion structures were washed out and were further damaged by deposition of coarse sediment. The damage pattern on Deer Creek was very similar to that in the Kern and Tule River headwater areas.

STORAGE REGULATION

Three reservoirs were operated by the Corps of Engineers to reduce floodflows and keep flood damage to comparatively low amounts downstream from the reservoirs. All inflow from the Kern River basin was stored in Isabella Reservoir during the critical peak runoff period. No releases were made at Isabella Dam until December 17, except to Borel Canal for power generation. A peak discharge of 9,290 cfs on December 7 on the Kern River near Bakersfield resulted from tributary inflow below Isabella Dam. In contrast, the

computed peak bihourly inflow to Isabella Reservoir was 96,900 cfs on December 6.

Lake Success filled rapidly during the record-high Tule River basin inflow December 5 and 6. Flow began over the spillway crest during the afternoon of December 6 and peaked at 8,260 cfs at 0400 hours December 7. Releases through Success Dam outlet works were manipulated to obtain 6 feet of surcharge above the ungated spillway crest. This caused 16,000 acre-feet of surcharge storage and greatly reduced the rate of discharge to the lower Tule River. The combined flow through the outlet works and over the spillway reached a peak of 9,050 cfs. The computed peak bihourly inflow was 52,800 cfs (fig. 12).

Storage in Lake Kaweah was also regulated to provide maximum flow reduction downstream. At the time of the peak bihourly inflow of 82,700 cfs on December 6, floodflow from Dry Creek entering Kaweah River downstream from the reservoir filled all available channel capacity, and there was no significant release at Terminus Dam. As local flows receded, the release was stepped up to 5,740 cfs on December 8. Approximately 99 percent of the available reservoir space was utilized, but there was no spill at Terminus Dam.

FLOOD DAMAGE

The recordbreaking floodflows of December 1966 caused severe damage in mountain and foothill areas. Parts of the communities of Kernville, Lamont, Springville, and Three Rivers adjacent to streams were damaged heavily by stream overflow, streambank erosion, and deposition of sediment and debris. Roads and bridges were hard hit, and some bridges were totally destroyed. Many smaller culverts and bridges were damaged to some degree from debris and overflows. Inundation of downstream agricultural areas caused additional damage.

Storage in Isabella Reservoir, Lake Success, and Lake Kaweah reduced record inflows to near channel capacity downstream and prevented catastrophic damage to Bakersfield, Porterville, Visalia, and smaller downstream cities. Data on the amount of flow reduction are given in the preceding section. Flood-damage prevention has been estimated by the U.S. Army Corps of Engineers (1967, p. A-24, A-16, A-12) as \$51,300,000 downstream from Isabella Dam, \$10,400,000 downstream from Success Dam, and \$19,600,000 downstream from Terminus Dam. The benefit by operation of the three reservoirs thus was \$81,300,000 in a single flood.

Actual flood damage was determined by the Corps of Engineers to have totalled \$18,003,000. A detailed breakdown by type of damage is

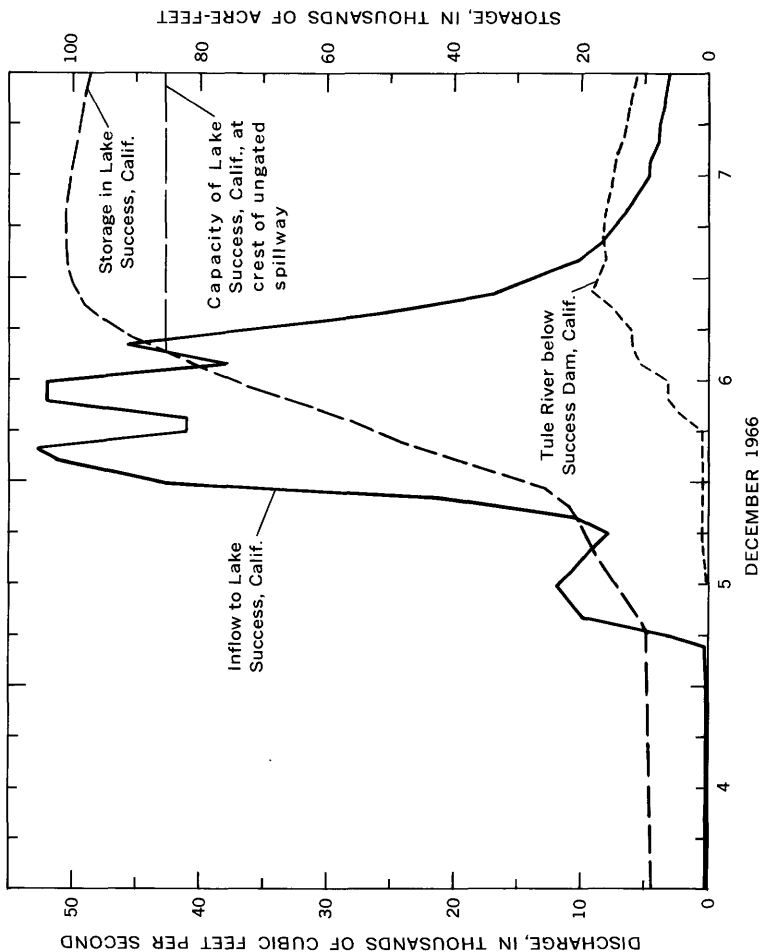


FIGURE 12.—Storage regulation and discharge in the Tule River basin.

given in a report of the U.S. Army Corps of Engineers (1967) for the Kern-Tule-Kaweah area. The damage is summarized below:

<i>Stream basin</i>	<i>Mountain and foothill area</i>	<i>Valley floor</i>	<i>Total</i>
Kern River.....	\$4,369,000	\$271,000	\$4,640,000
Caliente Creek.....	355,000	774,000	1,129,000
Poso Creek.....	83,000	1,215,000	1,298,000
Tule River.....	4,647,000	1,539,000	6,186,000
Kaweah River.....	3,468,000	1,282,000	4,750,000
Total.....	12,922,000	5,081,000	18,003,000

The figure for flood damage in mountain and foothill areas include \$4,457,000 damage to U.S. Forest Service and National Park Service facilities.

COMPARISON TO PREVIOUS FLOODS

Descriptions and streamflow data for floods of record in the Kern, Tule, and Kaweah River basins are found in Water-Supply Papers 843, 1137-F, 1260-D, 1650-A and B, and 1830-A. Historic floods of 1861-62, 1867, 1875, 1879, 1884, 1890, and 1893 are discussed in Water-Supply Papers 843, 1137-F, and 1650-A. No reliable estimates of flood discharge can be made for these earlier years. The information available indicates that the flood in December 1867 was the largest on all three streams, and the flood in January 1862 probably was the second highest, prior to 1900.

Streamflow records began in October 1893 on the Kern River, in May 1901 on the Tule River, and in May 1903 on the Kaweah River. Records are continuous since those dates. Gaging sites were moved upstream on the Tule River in November 1961 and on the Kaweah River in February 1962, when new reservoirs inundated former sites. The peak discharge of the Tule River near Springville has been estimated for the 1950 and 1955 floods on the basis of the ratio of the drainage area at the present site near Springville and that at the former site downstream near Porterville. The peak discharge of the Kaweah River during the 1963 and 1966 floods has been estimated at the former site near Three Rivers by the summation of flow at present gaging stations on the Kaweah River at Three Rivers (upstream from South Fork) and the South Fork Kaweah River at Three Rivers (near mouth). These estimates permit comparison of all major floods on the Tule and Kaweah Rivers since records began in 1901 and 1903, respectively.

Records indicate that the rain-produced floods of 1950, 1955, 1963, and 1966 were the greatest since streamflow records began in the Kern, Tule, and Kaweah River basins. The peak discharges during the four floods at principal long-term gaging stations on these rivers are listed in table 2. The December 1966 flood was by far the greatest in the Kern and Tule River basins. In the Kaweah River basin the December 1955

peak discharge near Three Rivers was about the same in magnitude as the estimated peak discharge in 1966. For the South Fork Kern, Tule, and Kaweah Rivers, peak discharge during several lesser floods prior to 1950 exceeded slightly the fourth highest discharge of the four floods listed in table 2.

TABLE 2.—Peak discharge at selected stations during the floods of 1950, 1955, 1963, and 1966

Station	Peak discharge (cfs)			
	November 1950	December 1955	February 1963	December 1966
Kern River near Kernville.....	27, 000	27, 200	24, 000	60, 000
South Fork Kern River near Onyx..	2, 180	2, 050	3, 460	28, 700
Tule River near Springville.....	22, 400	21, 500	10, 100	49, 600
Kaweah River near Three Rivers..	52, 000	80, 700	31, 900	78, 500

The 3-day flood runoff volume during the same floods and at the same stations is listed in table 3. The December 1966 3-day volume on the Kern and Tule Rivers was several times that during previous floods. The estimated 3-day volume in 1966 on the Kaweah River slightly exceeded that of 1955.

TABLE 3.—Runoff at selected gaging stations for 3-day periods during the floods of 1950, 1955, 1963, and 1966

1950		1955		1963		1966	
Period	Runoff (acre-ft)	Period	Runoff (acre-ft)	Period	Runoff (acre-ft)	Period	Runoff (acre-ft)
Kern River near Kernville							
Nov. 18.....	4, 200	Dec. 23.....	31, 900	Jan. 31.....	14, 200	Dec. 5.....	23, 800
19.....	25, 600	24.....	11, 100	Feb. 1.....	25, 000	6.....	66, 600
20.....	5, 890	25.....	6, 270	2.....	6, 960	7.....	15, 300
18-20.....	35, 690	23-25.....	49, 270	Jan. 31-Feb. 2...	46, 160	5-7.....	105, 700
South Fork Kern River near Onyx							
Nov. 18.....	83	Dec. 23.....	1, 260	Jan. 31.....	2, 280	Dec. 5.....	6, 900
19.....	2, 740	24.....	2, 960	Feb. 1.....	4, 800	6.....	27, 800
20.....	1, 020	25.....	1, 040	2.....	2, 720	7.....	4, 780
18-20.....	3, 843	23-25.....	5, 260	Jan. 31-Feb. 2...	9, 800	5-7.....	39, 480
Tule River near Springville							
Nov. 18.....	3, 020	Dec. 23.....	16, 000	Jan. 31.....	8, 150	Dec. 5.....	16, 900
19.....	17, 700	24.....	3, 940	Feb. 1.....	9, 780	6.....	59, 900
20.....	2, 450	25.....	2, 220	2.....	2, 240	7.....	10, 200
18-20.....	23, 170	23-25.....	22, 160	Jan. 31-Feb. 2...	20, 170	5-7.....	87, 000
Kaweah River near Three Rivers							
Nov. 18.....	15, 700	Dec. 23.....	84, 900	Jan. 31.....	26, 500	Dec. 5.....	36, 100
19.....	31, 700	24.....	30, 000	Feb. 1.....	37, 900	6.....	89, 000
20.....	8, 330	25.....	16, 300	2.....	8, 790	7.....	16, 800
18-20.....	55, 730	23-25.....	131, 200	Jan. 31-Feb. 2...	73, 190	5-7.....	141, 900

Comparison of the historic flood of December 1867 with that of December 1966 is possible at two locations. At the gaging station on the Kern River near Kernville drift logs were found in 1938 that are believed to have been deposited during the peak of the flood of 1867; the logs were 13 feet above the peak stage of the flood of February 1937. The peak stage for the flood of 1966 was 10.3 feet higher than that of February 1937, but whether the peak discharge in 1867 was greater than that in 1966 is open to conjecture. In fact, the Kern River channel at the gage site was scoured considerably in 1966 and thus may have carried a greater floodflow at a given stage than in 1867; nevertheless, the peak discharges of 1867 and 1966 may have been approximately the same in the Kern River in the vicinity of Kernville.

At the former gaging station on the Kaweah River near Three Rivers the maximum stage of the December 1867 flood was about 22.7 feet, referred to the datum of the December 1955 flood, whose flood peak stage was 22.24 feet. As previously explained, the peak discharge of the December 1966 flood on the Kaweah River is estimated to have been about the same as that in December 1955, but the 3-day flood runoff was greater in 1966. Thus the 1867, 1955, and 1966 peak discharges in the Kaweah River basin were about the same; however, the 1867 peak near Three Rivers probably was slightly greater than the peaks in 1955 and 1966.

FLOOD FREQUENCY

A method for determining the probable magnitude and return frequency of floods for recurrence intervals between 1.2 and 50 years for streams in the flood area is presented by Young and Cruff (1967) in Water-Supply Paper 1686. On the basis of regional equations presented in that report, the recurrence interval for the December 1966 flood has been determined (table 4) for all gaging sites with 10 years or more of record, unregulated flow, and more than 10 square miles of drainage area. The procedure for computing flood magnitude given in Water-Supply Paper 1686 is not applicable at sites where the drainage area is less than 10 square miles.

A ratio of the 1966 peak discharge to the 50-year flood is given whenever the December 1966 flood exceeded the probable 50-year flood. Extension of calculated flood-frequency curves beyond 50 years is not recommended because of limitations of available flood records. Comparison of the peak discharge for a given flood with the probable 50-year flood provides an approximate measure of the severity of the flood. In general, gaging stations with a lower percentage of high-altitude drainage area had the larger ratios. The highest ratio determined was 3.5 for North Fork of Middle Fork Tule River near Springville (site 27).

Other methods may be used to analyze flood frequency including the uniform technique (log-Pearson type III) described in a U.S. Water Resources Council report (1967). Use of other techniques could produce different recurrence intervals for peak discharges of December 1966 from those given in this report.

GEOMORPHIC EFFECTS IN THE KERN RIVER BASIN

By KEVIN M. SCOTT

Effects of the 1966 flood in the Kern River drainage basin were impressive, not only in channels, which were radically modified, but on sparsely vegetated hillslopes as well. Overland flow clearly occurred over much of the basin, in spite of the fact that lower hillslopes are mantled by grus, a fragmental accumulation formed by weathering from granite and having a high infiltration capacity. Much of the basin is underlain by vast expanses of bare granitic rock, the effect of which was to increase the rapidity of runoff. Local rillwash and gulleying occurred on depositional surfaces, but rangeland was not extensively eroded because of the high infiltration capacity of grus.

Press reports of numerous large landslides in the area referred in large part to relatively small failures of artificial slopes and roadcuts. Failures of natural slopes were rare because of the anisotropic nature of the bedrock and a thin soil cover rather than a lack of intensity of the storm. Small tributaries with steep gradients were locally the sites of mudflows which transported large volumes of forest debris and boulders to the main channels. The driver of a Corps of Engineers truck, attempting the first postflood traverse of the main Kern River canyon, reported that he got $2\frac{1}{4}$ miles into the canyon when a mudslide sent rocks "as big as houses" onto the road in front of his vehicle.

Small tributaries were radically affected by the storm runoff. Most striking were the changes in channel configuration in the normally dry desert washes of the southeastern part of the Kern River drainage basin. Here the effects were those of a widespread desert thunderstorm: overland flow, flashy runoff, widespread rill formation on depositional surfaces, and major changes in main channels. These effects are strikingly demonstrated in the Kelso Creek watershed, draining into the South Fork Kern River near Weldon. The main channel of Kelso Creek has been widened by lateral scour and now is bounded by nearly vertical cutbanks. The bed of the channel has undergone appreciable fill, apparently continuously along its entire length. Fill was locally at least 12 feet deep, inundating a stunted growth of willows along the previous thalweg.

Fill at the site of a former stream-gaging station was about 8 feet deep, leaving only the recorder shelter protruding above the surface.

The fill is almost entirely sand, as is the material exposed in the eroded cutbanks. A few coarse fragments are incorporated in the sand and were apparently transported during upper regime flow by progressive movement into a downstream scour pocket as described by Fahenstock and Haushild (1962). Local excavation of the fill reveals that the fill is constant in its grain size and that there is a lack of crossbedding with depth. Figure 13 shows the Kelso Creek channel at the gaging station after the flood. The small white recorder shelter is visible near the left bank of the filled channel.

The flood was equally devastating in larger tributaries, such as the South Fork Kern River. Where confined, the flood removed much vegetation and cut into but did not extensively overtop old terrace levels; however, the flood did not consistently fill or scour along its course. The flood occupied all the previous flood channel and left extensive sand berms up to a level 2 feet below the high-water mark. Peak flow was sufficiently competent to move the coarsest bed material present, as indicated by relationships of deposited boulders to vegetation. Where the South Fork debouches onto its fan, deposition was widespread, burying many fences and much vegetation.



FIGURE 13.—Kelso Creek near Weldon; downstream view; January 1967.

Effects in the canyon of the main Kern River were similar to those in the South Fork drainage, but were of a larger scale. Flow depth was at least 25 feet over much of the flood route, and with a relatively high gradient, flow was sufficiently competent to move all material previously in the channel, including boulders 10–15 feet in intermediate diameter. The pool-and-riffle pattern was modified. Much vegetation was lost and transported to Lake Isabella; however, little timber of economic value was lost. The pool above a diversion dam on the main Kern River near Fairview was completely filled with flood detritus.

Boulder and timber “jams” were formed in both the Kern and South Fork Kern Rivers, similar in this respect to other floods of mountain rivers (Krumbein, 1942). Such deposits consist of an abrupt front composed of boulders and timber. In an upstream direction, material becomes progressively finer. The surface of the deposit has a lower gradient than that of the reach in which it occurs, and coarse material is commonly present on the surface as a lag deposit. The snouts of the jams apparently formed at channel constrictions or in areas of reduced competency and acted as dams for the finer material. The low-water channel then formed laterally to the jam. These deposits, with apparently random spacing, do not seem to be related to riffles, which show a characteristic spacing related to channel width.

No definite idea of the flood frequency can be obtained from the erosional and depositional effects relative to previous deposits. On the main Kern River, the flood locally overtopped a terrace level at 20–25 feet with mature Coulter pines. A second pronounced terrace level occurs at a level 40–45 feet above the main Kern River thalweg. Some trees in the main channel that were older than 200 years were destroyed by the flood. The relative magnitude of the flood on the South Fork Kern River was similar—the flood locally overtopped a terrace 15–18 feet above the stream thalweg.

SEDIMENTATION AND CHANNEL CHANGES

No direct measurements of fluvial sediment are available for the flood area. Hydrographers reported visibly high suspended-sediment load and very audible moving bedload at streamflow-measuring stations. Large areas of channel scour and fresh deposits of sand were evident in all streams after recession of floodflow.

Reconnaissance surveys by the U.S. Army Corps of Engineers, Sacramento District, indicate an accumulation of 2,550 acre-feet of sediment in headwater reaches of Lake Success on the Tule River between May 1961 and November 1967. Depth of sediment was as great as 12 feet on the ranges surveyed. Surveys show that 2,500 acre-feet of sediment up to 25 feet deep was deposited between June 1962 and

November 1967 in the headwater reaches of Lake Kaweah on the Kaweah River. These estimates do not include sediment deposits below the reservoir water levels at the time the surveys were made or the suspended sediment that passed through the reservoirs.

The sediment accumulation in Lake Success corresponds to an average annual rate of 1.1 acre-feet per square mile for the 1961-67 period and in Lake Kaweah to 0.9 acre-foot per square mile for 1962-67. These rates are about double the average annual sediment yields in this area, which are estimated to be less than 0.5 acre-foot per square mile. Much of the sediment in Lakes Success and Kaweah was deposited during the December 1966 flood, although part must have accumulated during the February 1963 and lesser floods.

There is little documentation of channel changes except at gaging-station cableways where stream cross sections are surveyed often during streamflow measurements. The greatest changes measured were in the Kern River basin, where the 1966 peak flows were most in excess of previously recorded maximums. Channel cross sections before and after the flood are plotted for two gaging stations in figure 14. The cross section on the Kern River at Kernville was widened considerably when sand and other small alluvial material was scoured from the left bank for a considerable distance. The section on the South Fork Kern River near Onyx was enlarged greatly in both width and depth with a maximum scour over 5 feet deep. Part of this scour was induced by the total destruction of a concrete weir. Figure 15 shows the scoured left bank and streambed and the top of the tipped concrete recorder shelter and stilling well which stood at the left end of the concrete control section before the flood. The A-frame for the former gaging cableway upstream from the recorder installation was dropped about 4 feet vertically when the left bank was eroded.

DETERMINATION OF FLOOD DISCHARGES

The operation of a streamflow-measuring station consists principally of the measurement of stage and discharge and the definition of the stage-discharge relation from which discharge can be calculated for a given stage. The development of a stage-discharge relation is based upon current-meter discharge measurements throughout the range of stage experienced, or through a sufficient part of the range that the discharge corresponding to the maximum stage can be obtained by a reasonable extension of the stage-discharge relation, or rating curve. Short extensions of a rating curve are usually made by logarithmic plotting, by velocity-area studies, or by use of other hydraulic or hydrologic principles.

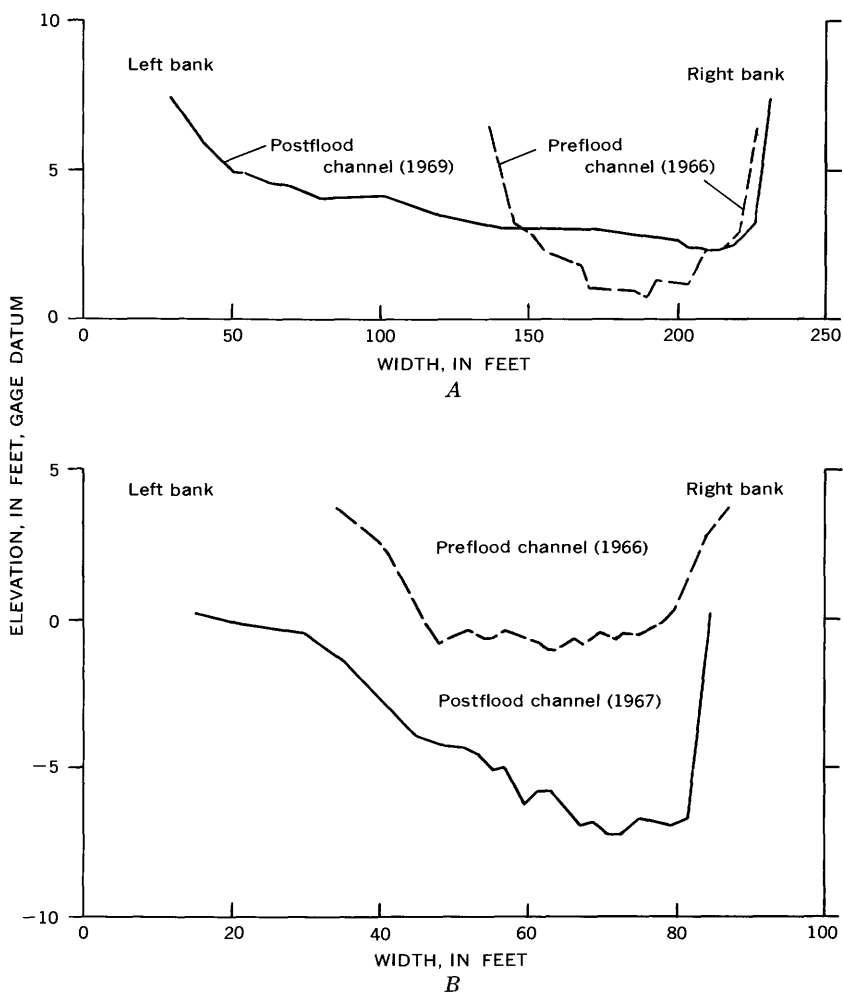


FIGURE 14.—Change in river-channel cross section of the Kern River at Kernville (A) and the South Fork Kern River near Onyx (B), 1966, 1967, and 1969.

Because of the record-breaking magnitude of the December 1966 floods, it was impossible to obtain current-meter discharge measurements at or near peak stage at most of the gaging stations. Most foothill and mountain roads were flooded, washed out, or blocked by debris during the flood crests December 6. Stream-gaging cableways at several stations were destroyed. Measurements were resumed at most Tule and Kaweah River stations December 7; Kern River stations were measured beginning December 8 by utilizing a helicopter to transport hydrographers and equipment to the stations.

For most of the gaging stations at which no extremely high-water current-meter measurements were made, peak discharges were obtained by slope-area measurements, computation of flow through culverts, contracted-opening measurements, critical-depth measurements, and other types of indirect discharge measurements. These indirect measurements are based on channel geometry and high-water profiles obtained by field survey and are computed by use of procedures and equations based on established hydraulic principles. They are indirect only in the sense that the data are collected subsequent to the passage of the peak discharge.



FIGURE 15.—South Fork Kern River near Onyx, upstream view, January 1967.

SUMMARY OF FLOOD STAGES AND DISCHARGES

Flood stages and discharges at 46 gaging stations, crest-stage stations, miscellaneous sites, and reservoir stations are summarized in table 4. The reference numbers in the table correspond to those on the location map (fig. 2) and aid in locating the sites at which peak discharges were determined.

TABLE 4.—Summary of flood stages and discharges

No. of station	Perma-nent station	Stream and place determination	Drainage area (sq mi)	Maximum previously known				Maximum December 1966				
				Period of record	Year	Gage height (ft)	Discharge (cfs)	Day	Gage height (ft)	Cfs	Recur-rence interval (yr)	
Buena Vista Lake basin												
1	1853	Golden Trout Creek near Cartago, Calif.	23.6	1956-66	1958	5.24	182	6	5.65	40	1.69	1
2	1853.5	Kern River near Quaking Aspen Camp, Calif.	530	1960-66	1963	7.98	4,060	6	10.89	9,360	17.7	10
3	1854	Little Kern River near Quaking Aspen Camp, Calif.	132	1957-66	1963	9.19	7,370	6	12.60	13,100	99.2	11.4
4	1856	Packsaddle Canyon Creek near Fairview, Calif.	4.05	1959-66	1963	3.91	12,200	6	12.0	660	163	
5	1860	Kern River near Kernville, Calif.	848	1912-66	1950, 1955	17.55	27,400	6	22.77	60,000	70.8	11.5
6	1863.4	Sanon Creek tributary B near Fairview, Calif.	.46	1962-66	1963	.87	3.1	5	1.93	22.1	48.0	
7	1863.6	Sanon Creek tributary C near Fairview, Calif.	.35	1962-66	1963	1.03	2.7	6	2.71	60	171	
8	1863.8	Sanon Creek tributary E near Fairview, Calif.	.20	1962-66	1965	.57	1.1	6	(?)	24	120	
9	1870	Kern River at Kernville, Calif.	1,000	1905-12, 1963-66	1955	16.2	29,400	6	22.2	74,000	73.3	11.6
10	1872	Shirley Creek tributary near Alta Sierra, Calif.	.27	1959-66	1962, 1963	18.4	38,700	6	13.70	60	148	
11	1882	South Fork Kern River near Olancho, Calif.	146	1956-66	1958	5.50	1,280	6	4.98	1,010	6.92	4
12	1895	South Fork Kern River near Onyx, Calif.	530	1911-14, 1919-42	1963	6.79	3,460	6	12.0	28,700	54.2	12.0
13	1897	Kelso Creek near Weldon, Calif.	101	1958-66	1965	37.2	1,340	6	11.7	5,500	57.4	11.9
14	1905	Isabella Reservoir near Isabella, Calif.	2,074	1933-66	1958	42,594.83	4,455,200	21,22	42,582.32	496,900	4.67	11.6
15	1910	Kern River below Isabella Dam, Calif.	2,074	1945-53	1950	28.6	39,000	30	10.10	72,160		
16	1918	Kern River tributary near Miracle Hot Springs, Calif.	1.21	1959-66	1958	15.14	74,870	6	13.10	593	490	
17	1925	Kern River near Democrat Springs, Calif.	2,258	1950-53	1950	30.7	40,000	6	18.55	710,100		
18	1940	Kern River near Bakersfield, Calif.	2,407	1893-1963	1950	13.68	74,370	7	4454.94	79,290		
19	1940.5	Tumbleweed Creek near Olddale, Calif.	2.40	1958-66	1963	4.65	783,040	6	2.25	1	42	
20	1964	Caliente Creek above Tehachapi Creek, Calif.	165	1961-66	1963	7.48	1,410	6	6.90	1,140	6.91	5
21	1964.2	Tehachapi Creek near Tehachapi, Calif.	53.2	1962-66	1963	8.530	1,700	6	1.06	52	.98	

Tulare Lake basin

22	1973	Poso Creek near Oildale, Calif.	230	1959-66	1964	6.38	359	6	11.57	4,300	1.87	8
23	1980.5	Mon Canyon Creek near Oildale, Calif.	2.38	1958-66	1958	8.6	2,750	6	3.90	9	3.78	
24	1963	Coho Creek near White River, Calif.	12.9	1959-66	1964	5.08	35	6	7.72	221	17.1	
25	1995	White River near Duco, Calif.	92.9	1942-53, 1958-66	1960	(2)	2,300	6	4.58	1,080	11.6	4
26	2020	Deer Creek near Terra Bella, Calif.	130	1959-66	1950	13.06	12,430	6	13.83	16,900	76.9	13.5
27	2020	North Fork of Middle Fork Tulare River near Springville, Calif.	39.3	1959-66	1955	12.47	19	6	12.71	48	160	
28	2024.5	Winding Creek near Camp Nelson, Calif.	.30	1959-66	1963	11.66	4,600	5	23	24,200	248	13.1
29	2031	North Fork Tulare River at Springville, Calif.	97.6	1957-66	1963	10.29		6	17.18	49,600	220	12.8
30	2022	Tulare River near Springville, Calif.	225	1950-66	1950	11.36	22,400	6	12.50	14,300	181	11.7
31	2045	South Fork Tulare River near Success, Calif.	109	1930-54, 1956-66	1950		7,100	6				
32	2047	Lake Success near Success, Calif.	391	1961-66	1955	4 612.74	66,100	7	4 688.63	101,300	135	12.2
33	2049	Tulare River below Success Dam, Calif.	393	1950-61	1950	3 26	32,000	6		7 9,050		
34	2049.5	Tulare River tributary near Success, Calif.	1.13	1962-53	1933	9.25	7 2,953	6				
35	2065	Middle Fork Kaweah River near Potwisha Camp, Calif.	102	1949-66	1962	11.76	8	6	14.63	219	194	12.1
36	2080	Marble Fork Kaweah River at Potwisha Camp, Calif.	51.4	1950-66	1955	13.4	46,800	6	17.7	23,300	228	
37	2085	Middle Fork Kaweah River tributary near Hammond, Calif.	1.90	1959-66	1963	18.41	152	6	30.63	879	463	
38	2087.3	East Fork Kaweah River near Three Rivers, Calif.	85.8	1952-55, 1957-66	1963	11.00	2,850	6	21	13,000	152	11.3
39	2090	Dorst Creek near Kaweah Camp, Calif.	6.11	1959-66	1963	23.85	1,540	6	30.73	2,010	329	
40	2095	North Fork Kaweah River at Kaweah, Calif.	129	1910-66	1955	14.1	21,500	6	14.7	23,900	185	12.3
41	2099	Kaweah River at Three Rivers, Calif.	418	1958-66	1963	13.68	30,900	6	16.69	73,000	175	12.0
42	2101	South Fork Kaweah River at Three Rivers, Calif.	86.7	1958-66	1963	17.9	(2) 2,440	6	9.30	11,600	134	11.4
43	2109	Lake Kaweah near Lemoncove, Calif.	560	1961-66	1965	4 688.96	139,900	8	4 692.77	147,400	148	12.1
44	2109.5	Kaweah River below Terminus Dam, Calif.	561	1961-66	1963	8.28	7 5,080	8	8.62	7 3,740		
45	2113	Dry Creek near Lemoncove, Calif.	80.4	1959-66	1963	5.08	1,600	6	7.30	14,500	175	13.0
46	2120	Sand Creek near Orange Cove, Calif.	26.8	1944-66	1965	4.80	775	6	5.60	1,350	50.4	28
				1943			1,000-1,200					

1 Ratio of peak discharge to 50-year flood.
 2 Unknown.
 3 Site and (or) datum then in use; see station description.
 4 Altitude, in feet.
 5 Contents, in acre-feet.
 6 Two-hour average peak inflow, in cubic feet per second.
 7 Affected by storage and (or) diversions; see station description.
 8 Maximum daily mean discharge, in cubic feet per second.

The derivation of the peak data is explained in the station description for each site. The peak discharges in table 4 are those actually determined; that is, no adjustments for upstream storage have been made for stations downstream from reservoirs. For reservoir stations the peak stage, contents, and computed peak bihourly inflow are given.

Explanation of data in the 13 columns of table 4 follows:

Number.—The number by which each station is referenced in this report. The numerical order follows the Geological Survey's standard downstream order for listing stations.

Permanent station number.—The number used in the Geological Survey's Water-Supply Papers of surface-water supply in the United States and the annual surface-water basic-data reports for California.

Stream and place of determination.—The permanent name adopted for the site to which the listed data apply; each name is unique.

Drainage area.—The gross drainage area, in square miles, above the station site as determined by the topography.

The last nine columns of the table give data for all known floods at the site:

Period of record.—The period of known floods prior to December 1966.

Year.—The calendar year of the maximum discharge known prior to December 1966.

Day.—The date of the peak discharge or stage during the flood of December 1966.

Gage height and discharge.—Data in each pair of columns are associated with the year or day in the preceding column. The 1966 peak discharge is also expressed in cubic feet per second per square mile of drainage area.

Recurrence interval.—The average interval of time in which the peak discharge of December 1966 can be expected to be exceeded once. When the recurrence interval is greater than 50 years, the ratio of the peak discharge to the discharge of the 50-year flood is shown.

EXPLANATION OF STATION DATA

Detailed information on stage and discharge during the floods of December 1966 are given in the following section. Many of the data are in addition to records published in annual streamflow reports of the Geological Survey. The data consist of descriptions of the stations or sites, tables of daily discharge at gaging stations for December 1966, and tables of stages and discharges at indicated times for many of the gaging stations.

The station description gives information relative to the location of the gage, size of drainage area above the gage, nature of the gage-height record obtained during the period covered by this report, datum of gage, definition of the stage-discharge relation, peak stage and discharge during the December 1966 floods and previous maximum of record, maximum data for floods outside the period of record, effect of regulation and diversion, and other pertinent general information.

The table of daily mean discharge gives data for the month of December 1966 to show discharges during antecedent and recession periods. The monthly figures of the table show the monthly mean discharge, in cubic feet per second; the volume of monthly runoff, in acre-feet; and the volume of monthly runoff, in inches, at selected stations. Monthly figures for a few stations downstream from a reservoir have been adjusted for change in contents of the reservoir.

The table of stages and discharges at indicated times gives sufficient data so that hydrographs of stage and discharge can be drawn. The period of time covered is from prior to the start of the major rise to an arbitrary cutoff point on the recession and is not the same for all stations. The stages and associated discharges given should not be used to prepare a stage-discharge relation (rating curve) for use outside the flood period. For many stations the relation used to compute the discharge was shifted from the basic rating for various reasons, such as backwater from debris blockage or other changes in control condition.

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STATION DATA

BUENA VISTA LAKE BASIN

(1) 11-1853. Golden Trout Creek near Cartago, Calif.

Location.--Lat 36°22'20", long 118°17'15", in NW $\frac{1}{4}$ SW $\frac{1}{4}$ sec.10, T.18 S., R.34 E., on right bank 0.5 mile upstream from Tunnel Ranger Station, and 15 miles west of Cartago.

Drainage area.--23.6 sq mi.

Gage-height record.--Water-stage recorder graph. Altitude of gage is 8,940 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements; affected by ice Dec. 5-11, 22-25, 27-31.

Maxima.--December 1966; Discharge, about 40 cfs 1330 hours Dec. 6 (gage height, 5.65 ft, backwater from ice).
1956 to November 1966; Discharge, 182 cfs May 31, 1958 (gage height, 4.05 ft); gage height, 5.24 ft Feb. 12, 1959 (backwater from ice).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	9.7	9.....	12	17.....	10	25.....	9.5
2.....	9.5	10.....	11	18.....	10	26.....	9.7
3.....	13	11.....	11	19.....	9.7	27.....	10
4.....	22	12.....	10	20.....	9.7	28.....	9.7
5.....	28	13.....	10	21.....	9.7	29.....	9.5
6.....	35	14.....	10	22.....	9.7	30.....	9.5
7.....	27	15.....	10	23.....	9.7	31.....	9.5
8.....	20	16.....	10	24.....	9.5		
Monthly mean discharge, in cubic feet per second.....							12.7
Runoff, in inches.....							.64
Runoff, in acre-feet.....							801

(3) 11-1854. Little Kern River near Quaking Aspen Camp, Calif.

Location.--Lat 36°08'05", long 118°26'10", in SE $\frac{1}{4}$ SE $\frac{1}{4}$ sec.31, T.20 S., R.33 E., on left bank 600 ft upstream from mouth, and 5 miles east of Quaking Aspen Camp.

Drainage area.--132 sq mi.

Gage-height record.--Water-stage recorder graph. Datum of gage is 4,682 ft above mean sea level (river-profile survey).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 1,200 cfs and by slope-area measurements at 7,370 and 13,100 cfs.

Maxima.--December 1966: Discharge, 13,100 cfs 0600 hours Dec. 6 (gage height, 12.60 ft, from recorder graph; 13.0 ft, from flood profile).
1957 to November 1966: Discharge, 7,370 cfs Feb. 1, 1963 (gage height, 9.19 ft, from recorder graph; 10.05 ft, from floodmarks).
Flood of Dec. 23, 1955, reached a stage of 12.4 ft, from floodmarks (discharge, 12,200 cfs).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1....	48	9....	826	17....	345	25....	249
2....	127	10....	692	18....	329	26....	242
3....	312	11....	580	19....	313	27....	226
4....	100	12....	516	20....	298	28....	223
5....	3,110	13....	470	21....	294	29....	223
6....	7,880	14....	412	22....	277	30....	211
7....	2,160	15....	381	23....	270	31....	205
8....	1,200	16....	361	24....	260		
Monthly mean discharge, in cubic feet per second.....							746
Runoff, in inches.....							6.52
Runoff, in acre-feet.....							45,900

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	
Dec. 3	2400	2.17	126	Dec. 5	1700	6.40	2,910	Dec. 6	1200	8.84	5,730	
					1800	7.62	4,560		1300	9.32	6,600	
	4	0800	2.03	98		2000	9.34	7,660		1400	9.74	7,370
		1400	1.99	90		2100	10.59	9,840		1630	9.58	7,060
		1800	2.00	92		2200	11.40	11,200		1800	9.12	6,240
		2100	2.02	96		2300	11.67	11,600		2100	8.02	4,350
		2400	2.08	108		2400	11.32	11,100		2400	7.32	3,270
	5	0200	2.68	254	6	0100	11.73	11,700	7	0600	6.85	2,590
		0300	3.60	610		0200	12.18	12,400		1200	6.35	1,970
		0400	3.89	755		0400	12.00	12,100		1800	6.09	1,670
		0500	3.92	772		0500	12.16	12,400		2400	5.97	1,540
		0600	4.44	1,090		0600	12.60	13,100				
		0700	4.73	1,290		0700	11.60	11,000	8	0600	5.81	1,380
		0800	4.79	1,340		0800	10.90	9,600		1200	5.58	1,170
		1100	4.25	970		0900	9.34	6,630		1800	5.40	1,020
		1330	3.98	808		1000	8.82	5,700		2400	5.27	924
		1500	4.25	970		1100	8.63	5,370				

(4) 11-1856. Packsaddle Canyon Creek near Fairview, Calif.

(Crest-stage station)

Location.--Lat 35°56'40", long 118°28'30", in sec.12, T.23 S., R.32 E., at culvert on county road, Sequoia National Forest, 1.8 miles northeast of Fairview.

Drainage area.--4.05 sq mi.

Gage-height record.--Crest stages only; gage and culvert destroyed by flood. Altitude of gage is 3,600 ft (from topographic map).

Discharge record.--Peak discharge by computation at critical-depth section.

Maxima.--December 1966: Discharge, 660 cfs Dec. 6 (gage height, 12.0 ft, from floodmarks).

1959 to November 1966: Discharge, 223 cfs Jan. 31, 1963 (gage height, 9.91 ft, in gage well; 10.6 ft, from floodmarks).

FLOODS OF 1966 IN THE UNITED STATES

(5) 11-1860. Kern River near Kernville, Calif.

Location.--Lat 35°56'00", long 118°29'10", in NE $\frac{1}{4}$ sec.14, T.23 S., R.32 E., on left bank 3 miles upstream from Salmon Creek, and 15 miles north of Kernville.

Drainage area.--848 sq mi.

Gage-height record.--Water-stage recorder graph except 2300 hours Dec. 5 to 1530 hours Dec. 14. Datum of gage is 3,542.3 ft above mean sea level (river-profile survey).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 6,000 cfs and by slope-area measurement at 60,000 cfs; relation indefinite Dec. 14-31. Discharge Dec. 6-31 estimated on basis of weather records and records for nearby stations.

Maxima (river only).--December 1966: Discharge, 60,000 cfs about 0200 hours Dec. 6 (gage height, 22.77 ft, from floodmarks).

1912 to November 1966: Discharge, 27,200 cfs Dec. 23, 1955 (gage height, 17.55 ft).

(river and canal).--December 1966: Discharge, 60,000 cfs about 0200 hours Dec. 6.

1912 to November 1966: Discharge, 27,400 cfs Nov. 19, 1950, Dec. 23, 1955.

Remarks.--Kern River No. 3 Canal diverts up to 630 cfs 1 mile upstream from station.

Figures of mean discharge and discharge at indicated times represent the combined flow of Kern River and Kern River No. 3 Canal.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	309	9.....	2,200	17.....	1,100	25.....	750
2.....	338	10.....	1,900	18.....	1,100	26.....	748
3.....	1,040	11.....	1,600	19.....	1,000	27.....	680
4.....	438	12.....	1,500	20.....	960	28.....	660
5.....	12,000	13.....	1,400	21.....	900	29.....	660
6.....	33,600	14.....	1,300	22.....	850	30.....	650
7.....	7,700	15.....	1,250	23.....	830	31.....	640
8.....	3,540	16.....	1,150	24.....	790		
Monthly mean discharge, in cubic feet per second.....							2,696
Runoff, in inches.....							3.67
Runoff, in acre-feet.....							165,800

Discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Dis-charge	Date	Hour	Dis-charge	Date	Hour	Dis-charge	Date	Hour	Dis-charge
Dec. 1	2400	309	Dec. 3	0500	1,880	Dec. 4	1000	423	Dec. 5	0700	5,910
				0700	1,580		1700	376		0800	5,850
				0800	1,540		2100	404		0900	6,180
	2000	327		1000	1,290		2300	465		1400	5,570
	2200	338		1100	1,033		2400	531		1700	8,570
	2400	564		1400	733					1900	21,100
				2000	558		5	0200		2000	29,000
				2200	545			0400		2400	43,800
				2400	544			0600			

(6) 11-1863.4. Salmon Creek tributary B near Fairview, Calif.

Location.--Lat 35°54'05", long 118°23'05", in SE $\frac{1}{4}$ NE $\frac{1}{4}$ sec.26, T.23 S., R.33 E., on left bank 0.15 mile upstream from junction with Salmon Creek, 6.3 miles east of Fairview, and 10.3 miles north of Kernville.

Drainage area.--0.46 sq mi.

Gage-height record.--Water-stage recorder graph except 2400 hours Dec. 5 to 1430 hours Dec. 9. Altitude of gage is 7,360 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by computation of flow over 120° V-notch weir and by slope-area measurement at 22.1 cfs. Discharge Dec. 5-9 based on partial record, slope-area measurement, weather records, and records for Salmon Creek tributaries C and E.

Maxima.--December 1966: Discharge, 22.1 cfs 2400 hours Dec. 5 (gage height, 1.93 ft, result of release of stored water from debris jam).
1962 to November 1966: Discharge, 3.1 cfs Feb. 1, 1963 (gage height, 0.87 ft).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	0.004	9.....	1.39	17.....	0.40	25.....	0.28
2.....	.03	10.....	1.04	18.....	.37	26.....	.26
3.....	.08	11.....	.82	19.....	.35	27.....	.24
4.....	.02	12.....	.67	20.....	.32	28.....	.22
5.....	2.66	13.....	.60	21.....	.30	29.....	.22
6.....	11.0	14.....	.54	22.....	.30	30.....	.22
7.....	4.40	15.....	.48	23.....	.28	31.....	.20
8.....	2.40	16.....	.42	24.....	.28		
Monthly mean discharge, in cubic feet per second.....							0.993
Runoff, in inches.....							2.49
Runoff, in acre-feet.....							61.0

(7) 11-1863.6. Salmon Creek tributary C near Fairview, Calif.

Location.--Lat 35°54'15", long 118°23'30", in NE $\frac{1}{4}$ NW $\frac{1}{4}$ sec.26, T.23 S., R.33 E., on left bank 0.1 mile upstream from junction with Salmon Creek, 6.0 miles east of Fairview, and 10.5 miles north of Kernville.

Drainage area.--0.35 sq mi.

Gage-height record.--Water-stage recorder graph Dec. 1 to 0600 hours Dec. 6. Altitude of gage is 7,200 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by computation of flow over 120° V-notch weir and by slope-area measurement at 60 cfs. Discharge Dec. 6-31 estimated on basis of records for Salmon Creek tributary B, and weather records.

Maxima.--December 1966: Discharge, 60 cfs Dec. 6 (gage height, 2.71 ft, from floodmarks).

1962 to November 1966: Discharge, 2.7 cfs Feb. 1, 1963 (gage height, 1.03 ft).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1....	0.02	9....	2.20	17....	0.39	25....	0.26
2....	.07	10....	1.20	18....	.37	26....	.25
3....	.09	11....	.90	19....	.35	27....	.24
4....	.05	12....	.70	20....	.32	28....	.23
5....	2.31	13....	.60	21....	.31	29....	.22
6....	18.0	14....	.52	22....	.29	30....	.21
7....	7.00	15....	.48	23....	.28	31....	.20
8....	3.70	16....	.43	24....	.27		
Monthly mean discharge, in cubic feet per second.....							1.370
Runoff, in inches							4.51
Runoff, in acre-feet.....							84.2

(8) 11-1863.8. Salmon Creek tributary E near Fairview, Calif.

Location.--Lat 35°54'15", long 118°23'45", in NW $\frac{1}{4}$ NW $\frac{1}{4}$ sec.26, T.23 S., R.33 E., on left bank 0.2 mile upstream from junction with Salmon Creek, 5.7 miles east of Fairview, and 10.5 miles north of Kernville.

Drainage area.--0.20 sq mi.

Gage-height record.--Water-stage recorder graph Dec. 1 to 1000 hours Dec. 6. Altitude of gage is 7,200 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by computation of flow over 120° V-notch weir and by slope-area measurement at 24 cfs. Discharge Dec. 6-31 estimated on basis of records for Salmon Creek tributary B, weather records, and slope-area measurement.

Maxima.--December 1966: Discharge, 24 cfs Dec. 6 (gage height, unknown).
1962 to November 1966: Discharge, 1.1 cfs Apr. 29, 1965 (gage height, 0.57 ft).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	0.008	9.....	1.40	17.....	0.24	25.....	0.16
2.....	.01	10.....	.72	18.....	.22	26.....	.15
3.....	.03	11.....	.51	19.....	.21	27.....	.15
4.....	.008	12.....	.42	20.....	.19	28.....	.14
5.....	.69	13.....	.36	21.....	.18	29.....	.13
6.....	10.0	14.....	.32	22.....	.17	30.....	.12
7.....	5.40	15.....	.29	23.....	.17	31.....	.12
8.....	2.50	16.....	.26	24.....	.16		
Monthly mean discharge, in cubic feet per second.....							0.821
Runoff, in inches.....							4.73
Runoff, in acre-feet.....							50.5

(10) 11-1872. Shirley Creek tributary near Alta Sierra, Calif.

(Crest-stage station)

Location.--Lat 35°43'15", long 118°29'55", in SW $\frac{1}{4}$ sec.25, T.25 S., R.32 E., at culvert on Evans road, Sequoia National Forest, 3 miles east of Alta Sierra.

Drainage area.--0.27 sq mi.

Gage-height record.--Crest stages only. Altitude of gage is 4,120 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by computation of flow through culvert.

Maxima.--December 1966: Discharge, 60 cfs Dec. 6 (gage height, 13.70 ft).
1959 to November 1966: Discharge, 14 cfs Feb. 8, 1962 and Feb. 1, 1963; gage height, 11.57 ft Feb. 1, 1963.

(11) 11-1882. South Fork Kern River near Olancha, Calif.

Location.--Lat 36°11'00", long 118°07'40", in NW $\frac{1}{4}$ SW $\frac{1}{4}$ sec.18, T.20 S., R.36 E., on left bank 50 ft upstream from small unnamed left bank tributary, 2.0 miles downstream from Snake Creek, and 9.7 miles southwest of Olancha.

Drainage area.--146 sq mi.

Gage-height record.--Water-stage recorder graph. Altitude of gage is 7,840 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements.

Maxima.--December 1966: Discharge, 1,010 cfs 2000 hours Dec. 6 (gage height, 4.98 ft).
1956 to November 1966: Discharge, 1,280 cfs May 10, 1958 (gage height, 5.50 ft).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	25	9.....	311	17.....	88	25.....	43
2.....	24	10.....	258	18.....	78	26.....	42
3.....	24	11.....	199	19.....	69	27.....	36
4.....	17	12.....	157	20.....	64	28.....	35
5.....	42	13.....	128	21.....	64	29.....	34
6.....	613	14.....	111	22.....	56	30.....	33
7.....	664	15.....	102	23.....	47	31.....	32
8.....	440	16.....	94	24.....	46		
Monthly mean discharge, in cubic feet per second.....							128
Runoff, in inches.....							1.01
Runoff, in acre-feet.....							7,890

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge
Dec. 4	2400	1.07	4.6	Dec. 6	0600	3.44	317	Dec. 7	1200	4.15	570
					0900	4.10	550		1800	4.37	675
					1200	4.40	690		2400	4.14	566
					1500	4.59	785				
					1900	4.90	960	8	0600	3.95	490
					2000	4.98	1,010		1000	3.87	460
					2400	4.79	894		1200	3.61	368
6	0200	2.55	123						1600	3.69	396
	0400	2.90	186	7	0600	4.38	680		2400	3.66	386

(12) 11-1895. South Fork Kern River near Onyx, Calif.

Location (revised).--Lat 35°44'22", long 118°10'33", T.25 S., R.35 E., (unsurveyed), on left bank 0.8 mile north of State Highway 178, 1.6 miles upstream from Canebrake Creek, and 5 miles northeast of Onyx.

Drainage area.--530 sq mi.

Gage-height record.--Water-stage recorder graph Dec. 1 to 2000 hours Dec. 5; station destroyed by flood. Altitude of gage is 2,900 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 3,000 cfs and by slope-area measurement at 28,700 cfs. Discharge Dec. 6-31 estimated on basis of records for Kern River at Kernville, Little Kern River near Quaking Aspen Camp, and inflow into Isabella Reservoir.

Maxima.--December 1966: Discharge, 28,700 cfs Dec. 6 (gage height, 12.0 ft, from floodmarks).

1911-14, 1919-42, 1947 to November 1966: Discharge, 3,460 cfs Feb. 1, 1963 (gage height, 6.79 ft) but may have been exceeded by flood of Jan. 25, 1914 (observed maximum gage height, 7.2 ft and rising, at site then in use).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	55	9.....	900	17.....	325	25.....	205
2.....	55	10.....	700	18.....	310	26.....	195
3.....	176	11.....	600	19.....	280	27.....	186
4.....	79	12.....	530	20.....	265	28.....	180
5.....	3,480	13.....	465	21.....	250	29.....	172
6.....	14,000	14.....	420	22.....	235	30.....	168
7.....	2,410	15.....	385	23.....	225	31.....	162
8.....	1,200	16.....	360	24.....	215		
Monthly mean discharge, in cubic feet per second.....							942
Runoff, in inches.....							2.05
Runoff, in acre-feet.....							57,890

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge
Dec. 1	2400	2.07	52	Dec. 3	1800	2.62	139	Dec. 5	0800	5.00	1,390
					2400	2.44	104		0900	5.15	1,520
2	0300	2.08	53	4	1200	2.22	70	1000	5.12	1,490	
					1500	2.03	47	1200	5.26	1,610	
					2100	2.16	62	1300	5.35	1,700	
					2300	2.30	81	1400	5.60	1,920	
					2400	2.50	115	1600	6.78	3,450	
3	0200	2.85	192	5	2400	2.32	84	1800	7.95	5,880	
					0500	3.15	282	2000	8.52	7,460	
					1000	2.81	182				
					1200	2.80	180	0200	2.56	127	
								0400	3.52	424	
			0600	4.45	955						

(13) 11-1897. Kelso Creek near Weldon, Calif.

Location.--Lat 35°34'10", long 118°15'05", in NW $\frac{1}{4}$ sec.20, T.27 S., R.35 E., on left bank 0.5 mile upstream from Woolstaff Creek, and 7 miles southeast of Weldon.

Drainage area.--101 sq mi.

Gage-height record.--Water-stage recorder graph Dec. 1-5; flood-deposited detritus destroyed station effectiveness. Altitude of gage is 3,180 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements and weir discharge computations below 7 cfs and by one slope-area measurement at 1,180 cfs. Maximum discharge Dec. 6 estimated on basis of field survey of site.

Maxima.--December 1966: Discharge, about 5,800 cfs Dec. 6 (gage height, 11.7 ft, from floodmarks).
1958 to November 1966: Discharge, 1,340 cfs Aug. 15, 1965 (gage height, 6.20 ft, from floodmarks).

(14) 11-1905. Isabella Reservoir near Isabella, Calif.

Location.--Lat 35°38'50", long 118°28'50", in SW $\frac{1}{4}$ sec.19, T.26 S., R.33 E., in main control tower near left abutment of main dam on Kern River, 1.5 miles north of Isabella, and 2.8 miles upstream from Erskine Creek.

Drainage area.--2,074 sq mi.

Gage-height record.--Water-stage recorder graph. Datum of gage is at mean sea level (levels by Corps of Engineers).

Contents record.--Contents computed from capacity table dated June 1966.

Maxima.--December 1966: Computed bihourly inflow, 96,900 cfs 1700 to 1900 hours Dec. 6; contents, 337,400 acre-ft 2300 hours Dec. 21 to 0930 hours Dec. 22 (elevation, 2,582.32 ft).

1953 to November 1966: Contents, 455,200 acre-ft June 28, 1958 (elevation, 2,594.83 ft).

Remarks.--Reservoir is formed by earthfill dam, with sidehill spillway and auxiliary earthfill dam, completed in 1954; regulation of discharge from reservoir began Apr. 15, 1954. Usable capacity, 569,700 acre-ft between elevations 2,470.0 ft (invert of main outlet) and 2,605.5 ft (spillway crest) above mean sea level. Dead storage, 326 acre-ft. Surcharge flood control storage, 271,800 acre-ft between ungated spillway crest and elevation 2,627.0 ft (maximum spillway design flood pool). Figures given herein represent total contents. Records furnished by Corps of Engineers.

Contents, in acre-feet at 2400 hours, December 1966

Day	Contents	Day	Contents	Day	Contents	Day	Contents
1.....	82,710	9.....	311,900	17.....	336,300	25.....	331,100
2.....	83,010	10.....	317,500	18.....	336,800	26.....	328,900
3.....	84,620	11.....	322,000	19.....	336,900	27.....	326,200
4.....	85,300	12.....	325,400	20.....	337,200	28.....	322,900
5.....	116,700	13.....	328,500	21.....	337,400	29.....	319,800
6.....	260,400	14.....	330,900	22.....	336,800	30.....	316,600
7.....	292,700	15.....	333,000	23.....	335,400	31.....	313,300
8.....	304,500	16.....	334,800	24.....	333,300		
Change in contents, in acre-feet.....							+230,500

Average inflow, in cubic feet per second, for bihourly periods ending at indicated time, 1966

Date	Hour	Inflow	Date	Hour	Inflow	Date	Hour	Inflow	Date	Hour	Inflow	
Dec. 4	0100	877	Dec. 5	0700	5,260	Dec. 6	1300	81,400	Dec. 7	1900	10,700	
	0300	876		0900	10,900		1500	76,700		2100	10,100	
	0500	664		1100	12,700		1700	86,000		2300	9,130	
	0700	634		1300	12,500		1900	96,900				
	0900	651		1500	11,200		2100	57,300		8	0100	9,160
	1100	651		1700	10,400		2300	49,400		0300	8,200	
	1300	191		1900	15,200					0500	7,230	
	1500	650		2100	23,600		7	0100		37,300	0700	7,250
	1700	420		2300	59,900		0300	29,400		0900	7,260	
	1900	874					0500	24,100		1100	6,290	
	2100	1,100		6	0100		65,600	0700		22,100	1300	6,300
	2300	1,340		0300	64,300		0900	18,200		1500	4,820	
		0500	67,400	1100	15,600	1700	6,320					
5	0100	1,340	0700	83,000	1300	12,800	1900	5,830				
	0300	1,340	0900	79,400	1500	11,900	2100	5,340				
	0500	1,800	1100	75,400	1700	11,500	2300	5,340				
							9	0100	5,850			

(15) 11-1910. Kern River below Isabella Dam, Calif.

Location.--Lat 35°38'30", long 118°28'55", in S¹/₄NW¹/₄ sec.30, T.26 S., R.33 E., on right bank 200 ft downstream from highway bridge, 0.6 mile downstream from Isabella Dam, and 1.6 miles southwest of Isabella.

Drainage area.--2,074 sq mi.

Gage-height record.--Digital-recorder tape punched at 15-minute intervals and auxiliary graphic water-stage recorder graph. Datum of gage is 2,435.07 ft above mean sea level (levels by Corps of Engineers).

Discharge record.--Stage-discharge relation defined by current-meter measurements.

Maxima.--December 1966: Discharge, 2,160 cfs 1730 hours Dec. 30 (gage height, 10.10 ft).

1945-53 (prior to regulation by Isabella Reservoir): Discharge, 39,000 cfs Nov. 19, 1950 (gage height, 28.6 ft from floodmark, present site and datum), from rating curve extended above 1,100 cfs on basis of slope-area measurement of peak flow.

1954 to November 1966: Discharge, 4,870 cfs June 28, 1958 (gage height, 15.14 ft).

Remarks.--Flow regulated by Isabella Reservoir (see station 11-1905) beginning Apr. 15, 1954. Total monthly runoff includes 29,300 acre-ft diverted from Isabella Reservoir through Borel Canal and returned to the river downstream from this station and 230,500 acre-ft stored in Isabella Reservoir.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	35	9.....	8.0	17.....	167	25.....	1,440
2.....	25	10.....	5.8	18.....	651	26.....	1,560
3.....	8.0	11.....	5.0	19.....	651	27.....	1,800
4.....	5.0	12.....	5.0	20.....	651	28.....	1,960
5.....	12	13.....	5.0	21.....	711	29.....	1,900
6.....	31	14.....	6.0	22.....	944	30.....	1,870
7.....	7.9	15.....	7.0	23.....	1,260	31.....	2,130
8.....	8.6	16.....	7.0	24.....	1,440		
Monthly mean discharge, in cubic feet per second.....							623
Runoff, in inches, adjusted.....							2.70
Runoff, in acre-feet, adjusted.....							298,100

(16) 11-1918. Kern River tributary near Miracle Hot Springs, Calif.

(Crest-stage station)

Location.--Lat 35°33'15", long 118°34'45", in SE¹/₄NW¹/₄ sec.30, T.27 S., R.32 E., at culvert on State Highway 178, Sequoia National Forest, 3.5 miles southwest of Miracle Hot Springs.

Drainage area.--1.21 sq mi.

Gage-height record.--Crest stages only; gage destroyed by flood. Datum of gage is 2,453.4 ft.

Discharge record.--Peak discharge by slope-area measurement.

Maxima.--December 1966: Discharge, 593 cfs Dec. 6 (gage height, 13.10 ft, from floodmarks).

1959 to November 1966: Discharge, 5.0 cfs Feb. 8, 1962 (gage height, 6.80 ft).

(17) 11-1925. Kern River near Democrat Springs, Calif.

Location.--Lat 35°31'20", long 118°40'40", in NE¼SE¼ sec.6, T.28 S., R.31 E., on left bank 1.0 mile southwest of Democrat Springs, and 2.1 miles upstream from Cow Creek.

Drainage area.--2,258 sq mi.

Gage-height record.--Water-stage recorder graph except Dec. 1 to 0200 hours Dec. 6 and Dec. 7-23. Altitude of gage is 1,850 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements. Discharge Dec. 1-5 and Dec. 7-23 estimated on basis of records for Kern River below Isabella Dam, Kern River near Bakersfield, and weather records.

Maxima (river only).--December 1966: Discharge, 10,100 cfs 1800 hours Dec. 6 (gage height, 18.55 ft).

1950-53 (prior to regulation by Isabella Reservoir): Discharge, 40,000 cfs Nov. 19, 1950 (gage height, 30.7 ft), from rating curve extended above 8,700 cfs on basis of computation of maximum flow over dam (basic data for computation furnished by Southern California Edison Co.).

1954 to November 1966: Discharge, 3,960 cfs June 12, 1958 (gage height, 13.68 ft).

(river and conduit).--December 1966: Discharge, 10,100 cfs 1800 hours Dec. 6.

1950-53 (prior to regulation by Isabella Reservoir): Discharge, 40,000 cfs Nov. 19, 1950.

1954 to November 1966: Discharge, 4,370 cfs June 12, 1958.

Remarks.--Flow regulated by Isabella Reservoir (see station 11-1905). Kern River No. 1 conduit diverts up to 420 cfs upstream from station. Figures of mean discharge and discharge at indicated times represent the combined flow of Kern River and Kern River No. 1 conduit.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge	
1.....	418	9.....	478	17.....	650	25.....	2,020	
2.....	359	10.....	463	18.....	1,220	26.....	2,040	
3.....	430	11.....	459	19.....	1,220	27.....	2,340	
4.....	452	12.....	468	20.....	1,230	28.....	2,450	
5.....	903	13.....	475	21.....	1,270	29.....	2,500	
6.....	4,600	14.....	538	22.....	1,500	30.....	2,510	
7.....	1,090	15.....	556	23.....	1,810	31.....	2,680	
8.....	601	16.....	556	24.....	2,010			
Monthly mean discharge, in cubic feet per second.....								1,301
Runoff, in acre-feet.....								79,930

Discharge, in cubic feet per second, at indicated time, 1966.

Date	Hour	Dis-charge	Date	Hour	Dis-charge	Date	Hour	Dis-charge	Date	Hour	Dis-charge
Dec. 5	2400	631	Dec. 6	0200	1,270	Dec. 6	0700	4,420	Dec. 6	1800	10,100
				0300	2,640		1100	2,470		2400	3,200
	6	0100		0500	4,240		1300	2,810			

(18) 11-1940. Kern River near Bakersfield, Calif.

Location.--Lat 35°25'54", long 118°56'43", in NW¼SW¼ sec.2, T.29 S., R.28 E., on left bank 1.9 miles upstream from Sacramento Gulch, 0.8 mile northeast of Oil City, and 5.8 miles northeast of Bakersfield Post Office.

Drainage area.--2,407 sq mi.

Gage-height record.--Water-stage recorder graph. Datum of gage is at mean sea level.

Discharge record.--Stage-discharge relation defined by current-meter measurements below 8,000 cfs.

Maxima.--December 1966: Discharge, 9,290 cfs 0100 hours Dec. 7 (elevation, 454.94 ft); daily discharge, 4,790 cfs Dec. 6.
 1893-1953 (prior to regulation by Isabella Reservoir): Discharge, 36,000 cfs Nov. 19, 1950 (elevation, 461.37 ft).
 1954 to November 1966: Daily discharge, 3,940 cfs June 18, 1958.

Remarks.--Flow regulated by Isabella Reservoir beginning in 1954 (see station 11-1905). Mean discharge is computed for 24-hour period from noon on date listed to noon on following day. Records furnished by Kern County Land Company.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	440	9.....	503	17.....	600	25.....	2,080
2.....	408	10.....	487	18.....	1,280	26.....	2,150
3.....	427	11.....	494	19.....	1,290	27.....	2,360
4.....	476	12.....	493	20.....	1,280	28.....	2,540
5.....	951	13.....	501	21.....	1,340	29.....	2,490
6.....	4,790	14.....	566	22.....	1,560	30.....	2,450
7.....	1,150	15.....	585	23.....	1,820	31.....	2,710
8.....	668	16.....	585	24.....	2,080		
Monthly mean discharge, in cubic feet per second.....							1,341
Runoff, in acre-feet.....							82,460

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge
Dec. 3	2400	49.42	424	Dec. 6	0200	49.75	782	Dec. 7	1100	50.30	1,620
					0800	49.65	671		1200	50.15	1,510
4	0800	49.42	426		1100	51.67	3,330		2200	49.67	1,160
	1000	49.47	472		1200	52.25	4,320		2400	49.67	1,160
	1200	49.47	473		1300	52.42	4,540				
	2400	49.47	476		1800	51.00	2,460	8	1200	49.44	840
					2300	54.55	8,140		1700	49.35	713
5	1000	49.47	478		2400	54.80	8,850		2100	49.38	729
	1200	49.48	488						2400	49.34	707
	1230	49.49	498	7	0100	54.94	9,290				
	1800	49.49	500		0300	54.30	7,620				
	2400	49.70	725		0800	50.80	2,170				

(19) 11-1940.5. Tumbleweed Creek near Oildale, Calif.

(Crest-stage station)

Location.--Lat 35°27'55", long 119°01'30", in NW¼ sec.25, T.28 S., R.27 E., at culvert on county road 3.2 miles north of Oildale.

Drainage area.--2.40 sq mi.

Gage-height record.--Crest stages only. Altitude of gage is 765 ft (from topographic map).

Discharge record.--Peak discharge by computation of flow through culvert.

Maxima.--December 1966: Discharge, 1 cfs Dec. 6 (gage height, 2.25 ft).
1958 to November 1966: Discharge, 104 cfs Feb. 13, 1963 (gage height, 4.65 ft).

(20) 11-1964. Caliente Creek above Tehachapi Creek, near Caliente, Calif.

Location.--Lat 35°18'40", long 118°34'10", in SE¼SW¼ sec.17, T.30 S., R.32 E., on right bank 0.5 mile upstream from Harper Canyon, 1.0 mile upstream from Oiler Canyon, and 3.6 miles northeast of Caliente.

Drainage area.--165 sq mi.

Gage-height record.--Water-stage recorder graph except 1830 to 2030 hours Dec. 6. Altitude of gage is 1,575 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 61 cfs and by slope-area measurement at 1,410 cfs. Discharge 1830 to 2030 hours Dec. 6 estimated on basis of floodmarks at the station.

Maxima.--December 1966: Discharge, 1,140 cfs 2000 hours Dec. 6 (gage height, 6.90 ft, from floodmarks).
1961 to November 1966: Discharge, 1,410 cfs Aug. 8, 1963 (gage height, 7.48 ft, from floodmarks).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	0	9.....	14	17.....	1.5	25.....	1.3
2.....	0	10.....	14	18.....	1.5	26.....	1.3
3.....	0	11.....	9.9	19.....	1.5	27.....	1.2
4.....	0	12.....	7.6	20.....	1.6	28.....	1.5
5.....	.90	13.....	4.9	21.....	1.6	29.....	1.5
6.....	196	14.....	2.6	22.....	1.2	30.....	1.4
7.....	84	15.....	1.5	23.....	1.3	31.....	1.2
8.....	22	16.....	1.5	24.....	1.5		
Monthly mean discharge, in cubic feet per second.....							12.3
Runoff, in inches.....							.086
Runoff, in acre-feet.....							754

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Discharge	Date	Hour	Gage height	Discharge	Date	Hour	Gage height	Discharge	
Dec. 5	0000	-	0	Dec. 6	0700	1.83	14	Dec. 6	1700	3.70	196	
	0830	-	0		0730	2.35	42		1800	4.78	415	
	0830	1.22	.7		0800	2.22	33		2000	6.90	1,140	
	1100	1.33	1.7		0830	2.65	66		2200	4.52	374	
	1500	1.22	.7		0900	2.75	75		2400	3.85	244	
	1800	1.20	.6		0930	2.50	53					
	2000	1.25	.9		1000	2.66	66		7	0200	3.70	219
	2200	1.35	1.9		1200	2.38	44		0400	2.90	109	
	2400	1.57	5.8		1400	2.30	38		0700	2.56	75	
					1530	2.37	43		0900	2.40	61	
6	0200	1.64	7.6	1630	3.85	221	2400	2.33	49			
	0400	1.82	13									

(21) 11-1964.2. Tehachapi Creek near Tehachapi, Calif.

Location.--Lat 35°10'25", long 118°28'45", in NE $\frac{1}{4}$ SW $\frac{1}{4}$ sec.6, T.32 S., R.33 E., on right bank 1.3 miles downstream from Brite Creek, and 3.2 miles northwest of Tehachapi.

Drainage area.--53.2 sq mi.

Gage-height record.--Water-stage recorder graph except Dec. 17-21. Datum of gage is 3,534.48 ft above mean sea level.

Discharge record.--Stage-discharge relation defined by computation of flow over weir. Discharge Dec. 17-21 estimated as no flow based on recorded range in stage.

Maxima.--December 1966: Discharge, 52 cfs 1830 hours Dec. 6 (gage height, 1.06 ft).
1962 to November 1966: Discharge, 1,700 cfs Aug. 8, 1963 (gage height, 5.30 ft, in gage well; 6.40 ft, from floodmarks, site and datum then in use), from slope-area measurement of maximum flow.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	0	9.....	0	17.....	0	25.....	0
2.....	0	10.....	0	18.....	0	26.....	0
3.....	0	11.....	0	19.....	0	27.....	0
4.....	0	12.....	0	20.....	0	28.....	0
5.....	.10	13.....	0	21.....	0	29.....	0
6.....	8.2	14.....	0	22.....	0	30.....	0
7.....	.50	15.....	0	23.....	0	31.....	0
8.....	0	16.....	0	24.....	0		

Monthly mean discharge, in cubic feet per second.....	0.28
Runoff, in inches.....	.006
Runoff, in acre-feet.....	17

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	
Dec. 4	2400	0.32	0	Dec. 5	2300	0.38	0.20	Dec. 6	1830	1.06	52	
					2400	.40	.50		1900	1.00	43	
	5	0300	.32						2100	.76	16	
		0400	.36		6	0500	.44		2200	.70	11	
		1700	.33			1000	.38		2400	.57	4.2	
		1800	.38			1400	.44					
		1900	.35			1600	.52		7	0300	.45	1.3
		2000	.35			1700	.84			0600	.38	.20
		2200	.40			1800	1.04			0900	.36	.10
						1800	.99			2400	.33	0

TULARE LAKE BASIN

(22) 11-1978. Poso Creek near Oildale, Calif.

Location.--Lat 35°30'50", long 118°54'15", in SW $\frac{1}{4}$ SW $\frac{1}{4}$ sec.6, T.28 S., R.29 E., on downstream side of highway bridge opposite mouth of Hillvale Canyon, 10 miles northeast of Oildale, and 12 miles northeast of Bakersfield.

Drainage area.--230 sq mi.

Gage-height record.--Digital-recorder tape punched at 15-minute intervals except Dec. 1 to 1400 hours Dec. 10. Altitude of gage is 700 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 300 cfs and by contracted opening measurement at 4,300 cfs. Discharge Dec. 1-10 estimated on basis of weather records and records for South Fork Tule River near Success.

Maxima.--December 1966: Discharge, 4,300 cfs Dec. 6 (gage height, 11.57 ft).
1959 to November 1966: Discharge, 359 cfs Dec. 28, 1964 (gage height, 6.38 ft).

Flood of Apr. 4, 1958, reached a stage of 8.6 ft, from floodmarks (discharge, 2,750 cfs, furnished by Kern County Land Company).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	4.0	9.....	120	17.....	30	25.....	28
2.....	4.0	10.....	76	18.....	29	26.....	29
3.....	43	11.....	56	19.....	29	27.....	29
4.....	12	12.....	42	20.....	29	28.....	28
5.....	547	13.....	37	21.....	29	29.....	28
6.....	2,130	14.....	33	22.....	28	30.....	29
7.....	750	15.....	33	23.....	28	31.....	28
8.....	200	16.....	31	24.....	28		
Monthly mean discharge, in cubic feet per second.....							147
Runoff, in inches.....							.74
Runoff, in acre-feet.....							9,020

(23) 11-1980.5. Mon Canyon Creek near Oildale, Calif.

(Crest-stage station)

Location.--Lat 35°31'45", long 118°58'25", in NW $\frac{1}{4}$ NW $\frac{1}{4}$ sec.4, T.28 S., R.28 E., at culvert on county road, 8 miles northeast of Oildale.

Drainage area.--2.38 sq mi.

Gage-height record.--Crest stages only. Altitude of gage is 640 ft (from topographic map).

Discharge record.--Peak discharge estimated on basis of water surface profiles in culvert.

Maxima.--December 1966: Discharge, 9 cfs Dec. 6 (gage height, 3.90 ft).
1958 to November 1966: Discharge, 35 cfs Apr. 1, 1964 (gage height, 5.08 ft).

(24) 11-1993. Coho Creek near White River, Calif.

(Crest-stage station)

Location.--Lat 35°49'50", long 118°51'35", in NE $\frac{1}{4}$ NE $\frac{1}{4}$ sec.20, T.24 S., R.29 E., at culvert on county road, 1.6 miles northwest of White River.

Drainage area.--12.9 sq mi.

Gage-height record.--Crest stages only. Altitude of gage is 1,090 ft (from topographic map).

Discharge record.--Peak discharge by computation of flow through culvert.

Maxima.--December 1966: Discharge, 221 cfs Dec. 6 (gage height, 7.72 ft).
1959 to November 1966: Discharge, 1 cfs Nov. 11, 1960 (gage height not determined).

(25) 11-1995. White River near Ducor, Calif.

Location.--Lat 35°48'54", long 118°55'47", in SE $\frac{1}{4}$ NE $\frac{1}{4}$ sec.27, T.24 S., R.28 E., on right bank 0.2 mile downstream from Tyler Gulch, and 8.3 miles southeast of Ducor.

Drainage area.--92.9 sq mi.

Gage-height record.--Water-stage recorder graph. Altitude of gage is 685 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 660 cfs.

Maxima.--December 1966: Discharge, 1,080 cfs 1340 hours Dec. 6 (gage height, 4.58 ft).
1942-53, 1958 to November 1966: Discharge, about 2,300 cfs Mar. 9, 1943 (estimated by U.S. Bureau of Reclamation).

Remarks.--Records furnished by U.S. Bureau of Reclamation.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	-	9.....	20.0	17.....	3.5	25.....	3.3
2.....	-	10.....	12.0	18.....	3.5	26.....	3.3
3.....	-	11.....	10.0	19.....	4.2	27.....	3.3
4.....	-	12.....	8.5	20.....	4.2	28.....	3.3
5.....	16.0	13.....	7.9	21.....	3.8	29.....	3.3
6.....	622.0	14.....	6.5	22.....	3.8	30.....	3.5
7.....	119.0	15.....	5.2	23.....	3.5	31.....	3.1
8.....	36.0	16.....	4.5	24.....	3.3		
Monthly mean discharge, in cubic feet per second.....							29.7
Runoff, in inches.....							.37
Runoff, in acre-feet.....							1,830

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	
Dec. 4	2400	-	0	Dec. 6	0830	3.89	496	Dec. 7	0300	3.33	233	
					1000	4.08	632		0600	3.07	154	
	5	1800	-		1130	3.83	457		0900	2.87	110	
		1830	2.51		1230	4.16	700		1200	2.74	87	
		1930	2.66		1340	4.58	1,080		1800	2.54	60	
		2400	2.56						2400	2.42	48	
	6	0300	2.53		1500	4.37	880		8	0600	2.34	41
		0330	4.33		1600	4.20	732		1200	2.28	33	
		0400	3.98		1800	4.22	748		1800	2.24	26	
		0500	4.23		1930	4.50	990		2400	2.21	22	
		0600	4.33		2100	4.25	772					
					2400	3.75	410					

(26) Deer Creek near Terra Bella, Calif.

(Miscellaneous site)

Location.--Lat 35°58'42", long 118°52'26", in NE $\frac{1}{4}$ NE $\frac{1}{4}$ sec.31, T.22 S., R.29 E., 0.3 mile upstream from county road bridge, 4 miles upstream from U.S. Bureau of Reclamation gaging station, and 9.6 miles east of Terra Bella.

Drainage area.--130 sq mi, approximately.

Discharge record.--Maximum discharge by slope-area measurement.

Maximum.--December 1966: Discharge, 10,000 cfs Dec. 6.

(27) 11-2020. North Fork of Middle Fork Tule River near Springville, Calif.

Location.--Lat 36°10'29", long 118°41'41", T.20 S., R.30 E. (unsurveyed), on right bank 1.2 miles upstream from mouth, 2.2 miles downstream from Hossack Creek, and 7.4 miles northeast of Springville.

Drainage area.--39.3 sq mi.

Gage-height record.--Digital-recorder tape punched at 15-minute intervals except 2045 hours Dec. 5 to 1900 hours Dec. 6. Altitude of gage is 2,920 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 270 cfs and by critical-depth determinations at 5,460 and 12,400 cfs. Discharge 2045 hours Dec. 5 to 1900 hours Dec. 6 estimated on basis of floodmarks, weather records, and records for nearby stations.

Maxima.--December 1966: Discharge, 16,900 cfs 0600 hours Dec. 6 (gage height, 13.83 ft, from floodmarks).

1939 to November 1966: Discharge, 12,400 cfs Dec. 23, 1955 (gage height, 12.47 ft, from floodmarks), from rating curve extended above 300 cfs on basis of critical-depth determination; gage height, 13.06 ft Nov. 19, 1950, from floodmarks.

Remarks.--Pacific Gas and Electric Co. conduit diverts part of flow 2.5 miles upstream from station. Figures given herein represent combined flow of North Fork of Middle Fork Tule River and Pacific Gas and Electric Co. conduit; diversion is minor during floods.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	23	9.....	443	17.....	120	25.....	64
2.....	72	10.....	320	18.....	109	26.....	61
3.....	183	11.....	254	19.....	101	27.....	56
4.....	54	12.....	213	20.....	94	28.....	53
5.....	3,780	13.....	185	21.....	88	29.....	50
6.....	13,300	14.....	161	22.....	80	30.....	48
7.....	3,460	15.....	144	23.....	73	31.....	47
8.....	790	16.....	129	24.....	69		
Monthly mean discharge, in cubic feet per second.....							794
Runoff, in inches.....							23.30
Runoff, in acre-feet.....							48,840

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge
Dec. 5	0100	-	42	Dec. 5	1500	-	1,270	Dec. 7	0300	-	6,280
	0200	-	54		1700	-	2,160		0600	-	4,780
	0300	-	1,080		1800	-	4,050		0900	-	3,550
	0500	-	1,670		2000	-	11,000		1200	-	2,510
	0600	-	2,020	2100	-	11,200	1500		-	2,220	
	0700	-	1,960	2400	-	13,600	1800		-	1,800	
	0800	-	2,100				2100		-	1,470	
	0900	-	1,860	6	0600	13.83	16,900		2400	-	1,220
1200	-	1,300		1900	11.92	11,100					
				2400	10.61	7,940					

(28) 11-2024.5. Winding Creek near Camp Nelson, Calif.

(Crest-stage station)

Location.--Lat 36°09'35", long 118°40'30", in sec.25, T.20 S., R.30 E., (unsurveyed), at culvert on State Highway 190, 4 miles northwest of Camp Nelson.

Drainage area.--0.30 sq mi.

Gage-height record.--Crest stages only. Altitude of gage is 3,500 ft (from topographic map).

Discharge record.--Peak discharge by computation of flow through culvert.

Maxima.--December 1966: Discharge, 48 cfs Dec. 6 (gage height, 12.71 ft).
1959 to November 1966: Discharge, 19 cfs Feb. 1, 1963 (gage height, 11.66 ft).

(29) 11-2031. North Fork Tule River at Springville, Calif.

Location.--Lat 36°08'22", long 118°48'15", in SE $\frac{1}{4}$ sec.35, T.20 S., R.29 E., on left bank 0.1 mile upstream from Middle Fork Tule River, 0.8 mile northeast of Springville, and 12.9 miles northeast of Porterville.

Drainage area.--97.6 sq mi.

Gage-height record.--Digital-recorder tape punched at 15-minute intervals Dec. 1; station destroyed by flood. Altitude of gage is 1,040 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 3,900 cfs and by slope-area measurement at 24,200 cfs.

Maxima.--December 1966: Discharge, 24,200 cfs about midnight Dec. 5 (gage height, about 23 ft).
1957 to November 1966: Discharge, 4,600 cfs Jan. 31, 1963 (gage height, 10.29 ft).

Cooperation.--Records furnished by California Department of Water Resources and reviewed by Geological Survey. December 1966 record estimated by Geological Survey.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	7.3	9.....	405	17.....	107	25.....	56
2.....	5.8	10.....	310	18.....	97	26.....	53
3.....	294	11.....	230	19.....	88	27.....	50
4.....	60	12.....	185	20.....	81	28.....	48
5.....	4,230	13.....	165	21.....	75	29.....	47
6.....	14,200	14.....	145	22.....	70	30.....	45
7.....	2,090	15.....	130	23.....	65	31.....	44
8.....	734	16.....	118	24.....	60		
Monthly mean discharge, in cubic feet per second.....							784
Runoff, in inches.....							9.26
Runoff, in acre-feet.....							48,190

(30) 11-2032. Tule River near Springville, Calif.

Location.--Lat 36°05'41", long 118°50'09", in SE $\frac{1}{4}$ SW $\frac{1}{4}$ sec.15, T.21 S., R.29 E., on left bank 15 ft upstream from highway bridge, 2 miles southwest of Springville, and 4 miles downstream from North Fork.

Drainage area.--225 sq mi.

Gage-height record.--Water-stage recorder graph. Altitude of gage is 800 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 3,500 cfs and by slope-area measurement at 49,600 cfs.

Maxima.--December 1966: Discharge, 49,600 cfs 0030 hours Dec. 6 (gage height, 17.18 ft, from recorder graph; 19.7 ft, from flood profile).
1950 to November 1966: Discharge, 22,400 cfs (revised) Nov. 19, 1950 (gage height, unknown).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	47	9.....	990	17.....	266	25.....	185
2.....	44	10.....	770	18.....	254	26.....	185
3.....	812	11.....	620	19.....	243	27.....	174
4.....	171	12.....	532	20.....	235	28.....	170
5.....	8,510	13.....	427	21.....	225	29.....	168
6.....	30,200	14.....	360	22.....	212	30.....	164
7.....	5,150	15.....	314	23.....	200	31.....	156
8.....	1,590	16.....	285	24.....	191		
Monthly mean discharge, in cubic feet per second.....							1,737
Runoff, in inches.....							8.90
Runoff, in acre-feet.....							106,800

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge		
Dec. 4	0600	3.97	194	Dec. 5	1900	9.70	7,600	Dec. 6	1000	14.02	33,100		
	1200	3.86	158		2000	10.45	9,260		1200	14.59	36,000		
	1800	3.80	140		2100	12.29	14,500		1300	13.57	30,900		
	2400	3.75	126		2200	13.02	17,600		1400	12.37	26,100		
5	0200	3.76	129	6	2300	15.00	29,000	7	1700	13.79	32,000		
	0400	4.03	215		2400	16.57	42,700		1900	11.42	22,300		
	0500	5.73	1,390		0030	17.18	49,600		2100	9.82	15,900		
	0600	8.81	5,820			0230	15.79		42,000	2400	8.27	10,800	
	0800	10.32	8,960			0400	15.14		38,700	0200	7.67	9,010	
	1000	10.74	9,920			0600	14.05		33,200		0600	6.75	6,270
	1500	9.44	7,050			0800	13.82		32,100		1200	6.16	4,740
	1700	9.16	6,490			0900	13.07		26,900		1800	5.54	3,120
									2400	5.28	2,450		

(31) 11-2045. South Fork Tule River near Success, Calif.

Location.--Lat 36°02'30", long 118°51'25", in NW $\frac{1}{4}$ SW $\frac{1}{4}$ sec.4, T.22 S., R.29 E., on left bank 0.5 mile upstream from Crew Creek, 4 miles southeast of Success, and 5 miles upstream from mouth.

Drainage area.--109 sq mi.

Gage-height record.--Water-stage recorder graph. Altitude of gage is 770 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 3,100 cfs and by slope-area measurements at 7,100 and 14,300 cfs.

Maxima.--December 1966: Discharge, 14,300 cfs 1100 hours Dec. 6 (gage height, 12.50 ft, from recorder graph; 13.3 ft, from floodmarks).
1930-54, 1956 to November 1966: Discharge, 7,100 cfs Nov. 19, 1950 (gage height, 11.36 ft).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	9.9	9.....	377	17.....	66	25.....	58
2.....	9.4	10.....	247	18.....	51	26.....	57
3.....	137	11.....	171	19.....	43	27.....	52
4.....	36	12.....	133	20.....	51	28.....	48
5.....	1,710	13.....	114	21.....	59	29.....	48
6.....	6,660	14.....	109	22.....	60	30.....	46
7.....	1,110	15.....	95	23.....	60	31.....	45
8.....	575	16.....	77	24.....	62		
Monthly mean discharge, in cubic feet per second.....							399
Runoff, in inches.....							4.22
Runoff, in acre-feet.....							24,550

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	
Dec. 1	2400	3.56	9.5	Dec. 5	0400	3.88	30	Dec. 6	1000	10.70	6,750	
	2	1200	3.55		8.7	0500	4.00		42	1100	12.50	14,300
		1800	3.55		8.7	0600	6.00		575	1200	11.65	11,600
		2200	3.60		11	0800	8.15		2,140	1300	10.20	7,360
2400		3.67	15		0930	8.46	2,450		1400	9.85	6,510	
3	0100	3.77	21		1300	8.06	2,050		1800	10.43	7,930	
	0200	4.40	95		1800	7.51	1,560		2000	9.10	4,950	
	0500	5.43	340		2100	8.15	2,140		2200	7.85	3,020	
	0900	4.92	201		2200	8.80	2,820		2400	7.20	2,300	
	1300	4.50	112		2300	9.90	4,680		7	0300	6.40	1,550
	1800	4.25	74		2400	10.70	6,750			0600	6.03	1,240
4	2400	4.10	54		6	0130	11.61		10,200	1200	5.56	944
	0900	3.97	39	0300		11.40	9,310	1630	5.40	860		
		1530	3.90	32		0500	10.20	5,380	1800	5.33	824	
		1600	3.84	26		0600	10.11	5,130	2000	5.32	818	
		2400	3.83	25		0800	9.30	3,530	2400	5.15	740	
						0900	9.50	3,900				

(32) 11-2047. Lake Success near Success, Calif.

Location.--Lat 36°03'40", long 118°55'18", in SE $\frac{1}{4}$ NW $\frac{1}{4}$ sec.35, T.21 S., R.28 E., in control tower near right abutment of Success Dam on Tule River, 5 miles east of Porterville.

Drainage area.--391 sq mi.

Gage-height record.--Water-stage recorder graph. Datum of gage is at mean sea level, datum of 1929 (levels by Corps of Engineers).

Contents record.--Contents computed from capacity table dated June 1966.

Maxima.--December 1966: Computed bihourly inflow, 52,800 cfs 0300 to 0500 hours Dec. 6; contents, 101,300 acre-ft 0425 hours Dec. 7 (elevation, 658.63 ft). 1961 to November 1966: Contents, 66,100 acre-ft June 22-26, 1965 (elevation, 642.74 ft).

Remarks.--Lake is formed by earthfill dam and dike. Storage began November 1961. Usable capacity, 85,400 acre-ft between elevations 559.0 ft (invert of outlet structure) and 652.5 ft (spillway crest). Surcharge flood-control storage, 117,400 acre-ft between ungated spillway crest and elevation 686.8 ft (maximum spillway design flood pool). Dead storage, 720 acre-ft. Figures given herein represent usable contents. Records furnished by Corps of Engineers.

Contents, in acre-feet at 2400 hours, December 1966

Day	Contents	Day	Contents	Day	Contents	Day	Contents	
1.....	7,360	9.....	88,500	17.....	70,000	25.....	61,000	
2.....	7,480	10.....	83,000	18.....	67,900	26.....	60,100	
3.....	9,150	11.....	76,800	19.....	66,200	27.....	59,100	
4.....	9,650	12.....	73,400	20.....	65,100	28.....	58,000	
5.....	28,400	13.....	74,300	21.....	64,300	29.....	56,900	
6.....	100,500	15.....	74,400	22.....	63,500	30.....	55,700	
7.....	97,600	15.....	73,300	23.....	62,700	31.....	54,600	
8.....	93,200	16.....	71,800	24.....	61,900			
<u>Change in contents in acre-feet.....</u>								+47,370

Average inflow, in cubic feet per second, for bihourly periods ending at indicated time, 1966

Date	Hour	Inflow	Date	Hour	Inflow	Date	Hour	Inflow	Date	Hour	Inflow			
Dec. 4	0100	370	Dec. 5	0700	2,930	Dec. 6	1300	52,000	Dec. 7	1900	3,910			
	0300	334		0900	9,830		1500	37,900		2100	3,600			
	0500	296		1100	11,000		1700	45,500		2300	3,290			
	0700	290		1300	11,900		1900	36,300						
	0900	224		1500	10,400		2100	25,300		8	0100	2,980		
	1100	260		1700	9,420		2300	16,900			0300	3,010		
	1300	224		1900	8,010						0500	2,410		
	1500	224		2100	10,400		7	0100		13,500		0700	2,460	
	1700	224		2300	21,400			0300		10,300		0900	2,380	
	1900	224						0500		8,580		1100	2,150	
	2100	260		6	0100		43,100			0700	7,380		1300	1,860
	2300	230			0300		51,100			0900	6,390		1500	2,010
					0500		52,800			1100	5,660		1700	2,030
5	0100	146		0700	41,100		1300	4,700		1900	1,620			
	0300	152		0900	41,200		1500	4,720		2100	1,810			
	0500	266		1100	52,000		1700	3,910		2300	1,520			
									9	0100	1,620			

(34) 11-2049.5. Tule River tributary near Success, Calif.

(Crest-stage station)

Location.--Lat 36°03'27", long 118°54'48", in NE $\frac{1}{4}$ SE $\frac{1}{4}$ sec.35, T.21 S., R.28 E., at culvert on State Highway 190, 1.8 miles south of Success.

Drainage area.--1.13 sq mi.

Gage-height record.--Crest stages only. Altitude of gage is 630 ft (from topographic map).

Discharge record.--Peak discharge by computation of flow through culvert.

Maxima.--December 1966: Discharge, 219 cfs Dec. 6 (gage height, 14.63 ft).
1959 to November 1966: Discharge, 8 cfs Mar. 6, 1962 (gage height, 11.76 ft).

(35) 11-2065. Middle Fork Kaweah River near Potwisha Camp, Calif.

Location.--Lat 36°30'45", long 118°47'25", in NW $\frac{1}{4}$ sec.25, T.16 S., R.29 E., on right bank 0.7 mile southeast of Potwisha Camp, and 0.9 mile upstream from confluence with Marble Fork Kaweah River.

Drainage area.--102 sq mi.

Gage-height record.--Water-stage recorder graph. Altitude of gage is 2,100 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 1,000 cfs and by slope-area measurement at 46,800 cfs.

Maxima.--December 1966: Discharge, 23,300 cfs 0800 hours Dec. 6 (gage height, 17.7 ft).

1949 to November 1966: Discharge, 46,800 cfs Dec. 23, 1955 (gage height, 29.0 ft, from floodmarks, at datum 0.70 ft higher), by slope-area measurement of maximum flow.

Remarks.--Middle Fork Kaweah River No. 3 conduit diverts 0.5 mile upstream from station. Figures given herein represent combined flow of Middle Fork Kaweah River and Middle Fork Kaweah River No. 3 conduit; diversion is minor during floods.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	117	9.....	596	17.....	237	25.....	161
2.....	229	10.....	476	18.....	227	26.....	156
3.....	455	11.....	392	19.....	217	27.....	146
4.....	138	12.....	338	20.....	207	28.....	146
5.....	3,360	13.....	301	21.....	193	29.....	144
6.....	10,500	14.....	277	22.....	182	30.....	140
7.....	1,720	15.....	261	23.....	173	31.....	134
8.....	846	16.....	247	24.....	167		
Monthly mean discharge, in cubic feet per second.....							738
Runoff, in inches.....							8.34
Runoff, in acre-feet.....							45,390

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	
Dec. 3	2400	-	183	Dec. 5	1800	8.88	2,220	Dec. 6	1600	12.99	9,570	
	4	0700	-		155	1900	9.00		2,340	1700	12.25	7,580
		1100	-		145	2200	13.00		9,600	1800	11.42	5,760
		2100	-		138	2300	15.00		15,200	1900	11.28	5,500
		2300	-		149	2400	15.70		17,300	2300	9.88	3,330
2400	-	168	6	0100	16.45	19,600	2400	9.60	2,980			
5	0200	-		320	0200	15.30	16,100	7	0200	9.30	2,640	
	0400	-		1,340	0300	15.85	17,800		0400	9.10	2,440	
	0500	-		1,640	0400	16.65	20,200		0700	8.50	1,870	
	0600	9.00		2,340	0600	14.85	14,800		0900	8.28	1,690	
	0700	9.15		2,490	0800	17.70	23,300		1400	8.00	1,470	
0800	9.60	2,980		0900	13.60	11,300	2400	7.32	1,070			
1100	9.25	2,590		1100	11.00	5,000	8	0800	6.90	875		
1200	8.28	1,690		1400	11.02	5,040		1100	6.80	830		
1400	8.28	1,690		1500	13.60	11,300		1500	6.74	805		
	8.01	1,480	1530	12.30	7,700	2400		6.45	684			

(36) 11-2080. Marble Fork Kaweah River at Potwisha Camp, Calif.

Location.--Lat 36°31'10", long 118°48'10", in SE $\frac{1}{4}$ sec.23, T.16 S., R.29 E., on left bank 0.1 mile north of Potwisha Camp, and 0.3 mile upstream from confluence with Middle Fork Kaweah River.

Drainage area.--51.4 sq mi.

Gage-height record.--Water-stage recorder graph. Altitude of gage is 2,150 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 560 cfs, computed flow over dam at 4,000 cfs, and slope-area measurement at 12,500 cfs.

Maxima.--December 1966: Discharge, 6,400 cfs 0900 hours Dec. 6 (gage height, 11.50 ft).
1950 to November 1966: Discharge, 12,500 cfs Dec. 23, 1955 (gage height, 13.4 ft), from rating curve extended above 1,100 cfs on basis of slope-area measurement of maximum flow.

Remarks.--Marble Fork Kaweah River No. 3 conduit diverts 0.3 mile upstream from station. Figures given herein represent combined flow of Marble Fork Kaweah River and Marble Fork Kaweah River No. 3 conduit; diversion is minor during floods.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	51	9.....	322	17.....	139	25.....	98
2.....	116	10.....	255	18.....	133	26.....	97
3.....	265	11.....	223	19.....	128	27.....	89
4.....	76	12.....	199	20.....	125	28.....	90
5.....	1,700	13.....	181	21.....	120	29.....	90
6.....	4,540	14.....	163	22.....	112	30.....	88
7.....	1,100	15.....	152	23.....	109	31.....	83
8.....	522	16.....	145	24.....	104		
Monthly mean discharge, in cubic feet per second.....							375
Runoff, in inches.....							8.40
Runoff, in acre-feet.....							23,040

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge
Dec. 3	2400	-	94	Dec. 5	1000	6.84	1,170	Dec. 6	0700	11.30	6,000
					1100	6.32	928		0900	11.50	6,400
4	0900	-	72	1300	5.81	724	1400	9.88	3,760		
	1300	-	70	1400	5.88	752	1700	10.40	4,460		
	1400	-	67	1500	6.20	880	1800	10.26	4,260		
	2000	-	66	1600	6.60	1,050	2000	9.36	3,150		
	2300	-	82	1700	7.00	1,250	2300	8.35	2,130		
	2400	-	93	2000	9.52	3,320	2400	8.17	1,990		
5	0200	-	160	2100	9.87	3,740	7	0200	7.84	1,740	
	0400	-	954	2200	10.56	4,700		0700	7.00	1,250	
	0500	-	1,260	2300	10.86	5,180		1000	6.62	1,050	
	0700	7.56	1,560	2400	10.98	5,370		1200	6.45	968	
	0800	7.57	1,560	6	0300	10.91		5,260	1900	6.00	780
					0500	10.74		4,980	2400	5.73	664

(37) 11-2085. Middle Fork Kaweah River tributary near Hammond, Calif.

(Crest-stage station)

Location.--Lat 36°29'35", long 118°49'30", in NW $\frac{1}{4}$ SW $\frac{1}{4}$ sec.34, T.16 S., R.29 E., at culvert on State Highway 198, Sequoia National Park, 2.7 miles northeast of Hammond.

Drainage area.--1.90 sq mi.

Gage-height record.--Crest stages only; gage destroyed by flood. Altitude of gage is 1,740 ft (from topographic map).

Discharge record.--Peak discharge by computation of flow through culvert and flow over road.

Maxima.--December 1966: Discharge, 879 cfs Dec. 6 (gage height, 30.63 ft, from floodmarks).
1959 to November 1966: Discharge, 152 cfs Feb. 1, 1963 (gage height, 18.41 ft).

(38) 11-2087.3. East Fork Kaweah River near Three Rivers, Calif.

Location.--Lat 36°27'05", long 118°47'15", in NW $\frac{1}{4}$ sec.14, T.17 S., R.29 E., on left bank just downstream from diversion dam, and 6.6 miles east of Three Rivers.

Drainage area.--85.8 sq mi.

Gage-height record.--Water-stage recorder graph Dec. 1-4. Altitude of gage is 2,500 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 850 cfs and by critical-depth computation at diversion dam at 13,000 cfs. Discharge Dec. 5-31 estimated on basis of weather records, records for nearby stations, and critical-depth computation.

Maxima (river only).--December 1966: Discharge, 13,000 cfs Dec. 6 (gage height, 21 ft, from flood profile).

1952-55, 1957 to November 1966: Discharge, 2,850 cfs Feb. 1, 1963 (gage height, 11.00 ft).

(river and conduit).--December 1966: Discharge, 13,000 cfs Dec. 6.
1952-55, 1957 to November 1966: Discharge, 2,850 cfs Feb. 1, 1963.

Remarks.--East Fork Kaweah River No. 1 conduit diverts up to 30 cfs upstream.

Mean discharge figures are the combined flow of East Fork Kaweah River and East Fork Kaweah River No. 1 conduit. Diversion is minor during floods.

Records furnished by Southern California Edison Co. and reviewed by Geological Survey. Maximum discharge computed by Geological Survey.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	37	9.....	400	17.....	225	25.....	143
2.....	218	10.....	360	18.....	201	26.....	143
3.....	199	11.....	320	19.....	201	27.....	132
4.....	91	12.....	300	20.....	176	28.....	125
5.....	3,200	13.....	291	21.....	168	29.....	122
6.....	8,000	14.....	254	22.....	157	30.....	119
7.....	1,500	15.....	249	23.....	157	31.....	85
8.....	550	16.....	225	24.....	153		
Monthly mean discharge, in cubic feet per second.....							597
Runoff, in inches.....							8.02
Runoff, in acre-feet.....							36,700

(39) 11-2090. Dorst Creek near Kaweah Camp, Calif.

(Crest-stage station)

Location.--Lat 36°38'45", long 118°48'15", in SE $\frac{1}{4}$ SW $\frac{1}{4}$ sec.2, T.15 S., R.29 E., at culvert on Generals Highway, Sequoia National Park, 6 miles northwest of Kaweah Camp.

Drainage area.--6.11 sq mi.

Gage-height record.--Crest stages only. Altitude of gage is 6,700 ft (from topographic map).

Discharge record.--Peak discharge by computation of flow through culvert.

Maxima.--December 1966: Discharge, 2,010 cfs Dec. 6 (gage height, 30.73 ft, from flood profile).
1959 to November 1966: Discharge, 1,540 cfs Feb. 1, 1963 (gage height, 28.85 ft).

(40) 11-2095. North Fork Kaweah River at Kaweah, Calif.

(Crest-stage partial-record station)

Location.--Lat 36°29', long 118°55', in SE $\frac{1}{4}$ sec.34, T.16 S., R.28 E., on left bank 1.2 miles upstream from Mannikin Creek, 1.5 miles north of Kaweah, and 3 miles upstream from mouth.

Drainage area.--129 sq mi.

Gage-height record.--Floodmarks only. Datum of gage is 1,027.7 ft above mean sea level (river-profile survey).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 3,200 cfs and by slope-area measurement at 21,500 cfs.

Maxima.--December 1966: Discharge, 23,900 cfs Dec. 6 (gage height, 14.7 ft, from flood profile).
1910 to November 1966: Discharge, 21,500 cfs Dec. 23, 1955 (gage height, 14.1 ft, from flood profile).

(41) 11-2099. Kaweah River at Three Rivers, Calif.

Location.--Lat 36°26'38", long 118°54'09", in SW $\frac{1}{4}$ SW $\frac{1}{4}$ sec.13, T.17 S., R.28 E., on right bank opposite schoolhouse in Three Rivers, 0.25 mile downstream from North Fork Kaweah River.

Drainage area.--418 sq mi.

Gage-height record.--Water-stage recorder graph. Datum of gage is 809.62 ft above mean sea level, datum of 1929.

Discharge record.--Stage-discharge relation defined by current-meter measurements below 13,000 cfs and by slope-area measurements at 30,900 and 73,000 cfs.

Maxima.--December 1966: Discharge, 73,000 cfs 2300 hours Dec. 5 (gage height, 16.69 ft, from recorder graph; 19.0 ft, from flood profile).
1958 to November 1966: Discharge, 30,900 cfs Feb. 1, 1963 (gage height, 13.68 ft, from recorder graph; 14.80 ft, from flood profile).
Flood of Dec. 23, 1955, reached a stage of 17.9 ft, from floodmarks.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	268	9.....	1,900	17.....	815	25.....	549
2.....	494	10.....	1,560	18.....	766	26.....	531
3.....	1,910	11.....	1,360	19.....	730	27.....	505
4.....	472	12.....	1,200	20.....	695	28.....	481
5.....	16,600	13.....	1,090	21.....	665	29.....	474
6.....	37,100	14.....	1,000	22.....	624	30.....	467
7.....	7,010	15.....	920	23.....	599	31.....	458
8.....	2,650	16.....	863	24.....	571		
Monthly mean discharge, in cubic feet per second.....							2,752
Runoff, in inches.....							7.99
Runoff, in acre-feet.....							169,200

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge
Dec. 1	2400	3.42	227	Dec. 4	2200	4.22	383	Dec. 6	0700	16.38	66,800
					2400	4.32	411		0730	15.68	54,400
2	0800	3.37	218						0900	16.06	60,400
	0900	3.21	190	5	0200	4.87	603		1000	15.40	50,200
	1100	3.40	223		0400	7.60	3,800		1100	14.00	33,200
	1300	3.35	214		0600	10.00	12,000		1200	13.10	27,600
	1800	3.50	250		0830	10.80	15,600		1400	11.50	19,100
	2000	4.94	700		1100	10.00	12,000		1500	10.68	15,100
	2200	6.17	1,550		1200	9.45	9,700		1600	11.15	17,400
	2400	7.25	3,110		1400	9.00	7,900		1700	10.60	14,700
					1800	10.00	12,000		1900	12.19	22,600
3	0200	8.13	5,120		2000	12.32	23,300		2100	11.55	19,400
	0400	7.62	3,850		2100	13.50	29,800		2400	10.75	15,400
	0700	6.67	2,180		2200	15.90	57,700				
	1200	5.87	1,250		2300	16.69	73,000	7	0400	9.67	10,600
	1800	5.42	888		2400	16.30	65,200		0800	8.97	7,800
	2400	5.05	685						1200	8.37	5,810
4	0600	4.70	538	6	0100	16.02	59,600		1500	8.02	4,850
	1200	4.38	430		0200	16.23	63,800		1800	7.76	4,200
	1800	4.22	383		0500	15.63	53,600		2200	7.50	3,600
					0600	15.95	58,400		2400	7.42	3,440

(43) 11-2109. Lake Kaweah near Lemoncove, Calif.

Location.--Lat 36°24'53", long 119°00'07", in SE $\frac{1}{4}$ SW $\frac{1}{4}$ sec.25, T.17 S., R.27 E., in control tower near left abutment of Terminus Dam on Kaweah River, 2.1 miles northeast of Lemoncove.

Drainage area.--560 sq mi.

Gage-height record.--Water-stage recorder graph. Datum of gage is at mean sea level, datum of 1929 (levels by Corps of Engineers).

Contents record.--Contents computed from capacity table dated June 1966.

Maxima.--December 1966: Computed bihourly inflow, 82,700 cfs 0900 to 1100 hours Dec. 6; contents, 147,200 acre-ft 0100 hours Dec. 8 (elevation, 692.77 ft).
October 1961 to November 1966: Contents, 139,900 acre-ft June 14, 1965 (elevation, 688.96 ft).

Remarks.--Reservoir is formed by earthfill dam and earthfill auxiliary dam; completed and storage began in February 1962. Usable capacity, 149,400 acre-ft between elevations 520.0 ft (invert of outlet structure) and 694.0 ft (spillway crest). Dead storage, 166 acre-ft. Figures given herein represent total contents. Surcharge flood-control storage, 117,400 acre-ft between ungated spillway crest and elevation 745.1 ft (maximum spillway design flood pool). Records furnished by Corps of Engineers.

Contents, in acre-feet at 2400 hours, December 1966

Day	Contents	Day	Contents	Day	Contents	Day	Contents
1.....	7,850	9.....	142,500	17.....	102,500	25.....	71,400
2.....	8,100	10.....	140,100	18.....	96,000	26.....	69,800
3.....	10,500	11.....	136,800	19.....	89,500	27.....	67,900
4.....	8,800	12.....	131,800	20.....	82,800	28.....	66,200
5.....	35,800	13.....	126,400	21.....	78,600	29.....	64,500
6.....	139,100	14.....	120,800	22.....	76,600	30.....	62,800
7.....	147,200	15.....	114,900	23.....	74,600	31.....	60,800
8.....	144,700	16.....	108,900	24.....	73,000		
Change in contents in acre-feet.....							+52,100

Average inflow, in cubic feet per second, for bihourly periods ending at indicated time, 1966

Date	Hour	Inflow	Date	Hour	Inflow	Date	Hour	Inflow	Date	Hour	Inflow		
Dec. 4	0100	797	Dec. 5	0700	879	Dec. 6	1300	45,600	Dec. 7	2100	5,810		
	0300	614		0900	8,320		1500	57,800		2300	5,580		
	0500	638		1100	11,500		1700	45,600					
	0700	543		1300	16,800		1900	50,900		8	0100	5,220	
	0900	528		1500	11,400		2100	30,400			0300	4,990	
	1100	558		1700	9,590		2300	22,000			0500	4,760	
	1300	516		1900	12,100						0700	4,410	
	1500	477		2100	16,300		7	0100		19,000		0900	4,180
	1700	481		2300	42,700			0300		14,500		1100	3,940
	1900	478						0500		12,300		1300	3,940
	2100	432						0700		10,900		1500	3,520
	2300	461		6	0100		63,800	0900		9,630		1700	3,890
			0300	63,800	1100	8,720		1900	3,530				
5	0100	415		0500	62,400	1300	8,130		2100	3,650			
	0300	430		0700	64,500	1500	7,200		2300	3,540			
	0500	535		0900	76,900	1700	6,260						
				1100	82,700	1900	6,510	9	0100	3,410			

(44) 11-2109.5. Kaweah River below Terminus Dam, Calif.

Location.--Lat 36°24'51", long 119°00'42", in SE $\frac{1}{4}$ SE $\frac{1}{4}$ sec.26, T.17 S., R.27 E., on left bank 0.6 mile downstream from Terminus Dam, and 2.2 miles northeast of Lemoncove.

Drainage area.--561 sq mi.

Gage-height record.--Digital-recorder tape punched at 15-minute intervals. Datum of gage is 495.90 ft above mean sea level (levels by Corps of Engineers).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 4,100 cfs.

Maxima.--December 1966: Discharge, 5,740 cfs 1445 hours Dec. 8 (gage height, 8.62 ft).
1961 to November 1966: Discharge, 5,080 cfs Jan. 31, 1963 (gage height, 8.28 ft).

Remarks.--Flow regulated by Lake Kaweah (see station 11-2109). Monthly runoff figures include 52,100 acre-ft stored in Lake Kaweah.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	651	9.....	3,590	17.....	4,180	25.....	1,430
2.....	198	10.....	3,120	18.....	4,200	26.....	1,400
3.....	877	11.....	3,200	19.....	4,200	27.....	1,460
4.....	1,300	12.....	3,870	20.....	4,210	28.....	1,430
5.....	1,310	13.....	4,010	21.....	2,950	29.....	1,370
6.....	1,150	14.....	4,000	22.....	1,650	30.....	1,400
7.....	4,920	15.....	4,010	23.....	1,700	31.....	1,420
8.....	5,320	16.....	4,020	24.....	1,420		
Monthly mean discharge, in cubic feet per second.....							2,578
Runoff, in inches, adjusted.....							7.04
Runoff, in acre-feet, adjusted.....							210,600

Gage height, in feet, and discharge, in cubic feet per second, at indicated times, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	
Dec. 3	2400	5.32	1,360	Dec. 6	0200	2.70	263	Dec. 7	2000	8.31	5,140	
					0400	1.68	110		2400	8.31	5,140	
4	0400	5.31	1,360	0600	1.29	73	8	0400	8.31	5,140		
	0800	5.29	1,340	1000	1.19	65		0800	8.32	5,160		
	1200	5.30	1,350	1200	1.15	62		1200	8.31	5,140		
	1600	5.28	1,340	1400	1.08	57		1200	8.31	5,140		
	2000	5.27	1,330	1600	3.05	339		1400	8.59	5,680		
	2400	5.25	1,320	1800	6.39	2,310		1445	8.62	5,740		
				2000	7.35	3,490		1600	8.57	5,640		
5	0400	5.24	1,310	2200	7.68	4,010	2000	8.56	5,620			
	0800	5.32	1,360	2400	7.69	4,020	2400	8.56	5,620			
	1000	5.62	1,600	7	0200	7.70	4,040	9	0400	8.55	5,600	
	1200	5.75	1,700		0400	8.06	4,690		0600	7.04	3,070	
	1400	5.80	1,750		0600	8.26	5,050		1000	7.11	3,150	
	1600	4.92	1,100		1000	8.30	5,120		2400	7.11	3,150	
	1800	4.88	1,080		1200	8.31	5,140		10	1200	7.10	3,120
	2000	4.92	1,100		1600	8.32	5,160			2400	7.10	3,120
	2200	5.00	1,150									
	2400	5.11	1,220									

(45) 11-2113. Dry Creek near Lemoncove, Calif.

Location.--Lat 36°25'30", long 119°01'20", in NW $\frac{1}{4}$ NW $\frac{1}{4}$ sec.26, T.17 S., R.27 E., on left bank 400 ft downstream from Pogue Canyon, 1.3 miles upstream from mouth, and 2.8 miles north of Lemoncove.

Drainage area.--80.4 sq mi.

Gage-height record.--Water-stage recorder graph except Dec. 8-15. Altitude of gage is 515 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 9,400 cfs. Discharge Dec. 8-15 estimated on basis of discharge measurements, records for nearby stations, and weather records.

Maxima.--December 1966: Discharge, 14,500 cfs 0900 hours Dec. 6 (gage height, 7.30 ft, from recorder graph, 8.94 ft, from floodmarks).
1959 to November 1966: Discharge, 1,600 cfs Feb. 1, 1963 (gage height, 5.08 ft).

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	0	9.....	70	17.....	16	25.....	11
2.....	0	10.....	48	18.....	14	26.....	11
3.....	.70	11.....	37	19.....	14	27.....	11
4.....	1.2	12.....	31	20.....	14	28.....	9.6
5.....	670	13.....	27	21.....	13	29.....	9.6
6.....	6,370	14.....	22	22.....	12	30.....	9.6
7.....	537	15.....	19	23.....	12	31.....	8.5
8.....	115	16.....	17	24.....	11		
Monthly mean discharge, in cubic feet per second.....							263
Runoff, in inches.....							3.77
Runoff, in acre-feet.....							16,150

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	
Dec. 3	2400	2.38	4.7	Dec. 5	2000	4.09	574	Dec. 6	1200	5.81	8,530	
					2100	4.21	658		1230	5.21	6,640	
	4	0600	2.34	2.3		2200	4.55	980		1230	5.53	7,620
		1200	2.26	.3		2400	6.28	6,050		1300	5.01	6,050
		1500	-	0						1300	5.33	7,080
		2400	-	0	6	0100	6.53	7,620		1400	4.92	5,720
						0200	6.53	7,620		1500	4.60	4,840
	5	0900	-	0		0500	6.39	6,700		1700	4.72	5,160
		1000	2.85	.72		0600	6.90	10,300		1700	4.62	4,880
		1030	4.10	580		0800	6.96	10,800		1900	3.70	2,800
		1100	4.40	820		0900	7.30	14,500		2200	2.94	1,610
		1130	4.63	1,080		1000	6.51	9,750		2400	2.58	1,220
		1230	4.41	830		1030	6.69	9,830				
		1300	4.53	956		1100	5.29	6,960	7	0600	1.92	706
		1400	4.50	920		1130	5.81	8,530		0900	1.57	532
		1830	4.10	580		1200	5.04	6,100		1200	1.27	420
										2400	.70	218

(46) 11-2120. Sand Creek near Orange Cove, Calif.

Location.--Lat 36°37'35", long 119°14'45", in NW¹/₄ sec.15, T.15 S., R.25 E., on right bank 3.8 miles east of Orange Cove.

Drainage area.--26.8 sq mi.

Gage-height record.--Water-stage recorder graph. Altitude of gage is 710 ft (from topographic map).

Discharge record.--Stage-discharge relation defined by current-meter measurements below 200 cfs.

Maxima.--December 1966: Discharge, 1,350 cfs 0840 hours Dec. 6 (gage height, 5.60 ft, from recorder graph; 6.78 ft, from floodmarks).
1944 to November 1966: Discharge, 775 cfs (revised) Dec. 23, 1955 (gage height, 4.80 ft).

Remarks.--Records furnished by U.S. Bureau of Reclamation. Discharges above 200 cfs computed by Geological Survey.

Mean discharge, in cubic feet per second, December 1966

Day	Discharge	Day	Discharge	Day	Discharge	Day	Discharge
1.....	-	9.....	3.9	17.....	0.6	25.....	0.6
2.....	-	10.....	2.1	18.....	.6	26.....	.6
3.....	-	11.....	1.5	19.....	.6	27.....	.6
4.....	-	12.....	1.1	20.....	.6	28.....	.6
5.....	-	13.....	.9	21.....	.6	29.....	.6
6.....	345	14.....	.8	22.....	.6	30.....	.6
7.....	46	15.....	.7	23.....	.6	31.....	.6
8.....	10	16.....	.6	24.....	.6		
Monthly mean discharge, in cubic feet per second.....							13.6
Runoff, in inches.....							.58
Runoff, in acre-feet.....							836

Gage height, in feet, and discharge, in cubic feet per second, at indicated time, 1966

Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge	Date	Hour	Gage height	Dis-charge		
Dec. 5	2400	1.45	11	Dec. 6	0900	5.60	1,350	Dec. 7	0400	2.45	83		
	6	0100	2.97		159	0930	4.90		835	0800	2.22	56	
		0200	3.00		164	1000	4.38		561	1200	2.04	42	
		0400	2.85		139	1100	4.22		493	1600	1.88	31	
		0600	3.00		164	1400	4.35		548	2000	1.73	23	
		0700	3.48		264	1600	4.01		414	2400	1.62	18	
		0730	3.75		335	1800	3.72		326	8	0600	1.48	13
		0800	4.20		485	2100	3.15		192		1200	1.37	10
		0830	5.00		895	2400	2.82		134		1800	1.27	7.5
						2400	1.18		5.7				

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