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6.4 Single-Chip RF CMOS UMTS/EGSM Transceiver with Integrated Receive Diversity and GPS

A. Hadjichristos¹, M. Cassia¹, H. Kim², C.H. Park², K. Wang¹, W. Zhuo¹, B. Ahrari², R. Brockenbrough², J. Chen², C. Donovan², R. Jonnalagedda², J. Kim², J. Ko², H. Lee², S. Lee², E. Lei², T. Nguyen², T.Pan², S. Sridhara¹, W. Su¹, H. Yan¹, J. Yang², C. Conroy², C. Persico¹, K. Sahota¹, B. Kim²

¹Qualcomm, San Diego, CA, ²Qualcomm, Santa Clara, CA

The large commercial success of multiband multimode 3rd-generation cellular products has driven single-chip integration, SAW-filter reduction and low power consumption. State-of-the-art solutions require quad-band EGSM combined with multiband WCDMA/HSPA receiver diversity and integrated GPS. Compact form factors make single-chip SAW-less solutions highly desirable. A Quad-Band GSM/EDGE-only transceiver was published in [1], and Triple-Band WCDMA-only transceiver solutions were published in [2-4]. This work describes the first multiband WCDMA/HSPA/EGPRS single-chip transceiver with GPS and receiver diversity. This device supports UMTS Bands 1,2,3,4,5,6,8,9,10 and GSM/EDGE 800, 900, 1800, 1900MHz Bands. It is implemented in cost-effective 0.18µm RF CMOS technology and uses a reduced number of TX and RX SAW filters.

A detailed block diagram is shown in Fig. 6.4.1. This transceiver consists of a GSM TX/RX and UMTS TX $\Delta\Sigma$ PLL, an EGSM/UMTS linear-I/Q direct-conversion transmitter chain with single-ended outputs, a quad-band direct-conversion EGSM receiver, a WCDMA RX $\Delta\Sigma$ PLL, a WCDMA 4-LNA Primary Receiver having two Saw-less paths, a WCDMA 3-LNA Saw-less diversity receiver and a GPS receiver. Figures 6.4.3 and 6.4.4 show system-level performance data measured at the antenna port of a reference phone that utilizes the described transceiver and supports QB GSM/EDGE, QB WCDMA with receiver diversity and GPS.

The transmitter [5] is divided into two distinct signal paths, one for low frequency bands (824 to 915MHz) and one for high frequency bands (1710 to 1980MHz). The two paths share a common Baseband Filter and Baseband Amplifier while separate mixers are used for GSM and WCDMA/CDMA in order to optimize current consumption and noise performance. The transmitter uses on-chip baluns, integrates part of the output matching network and has 5 single-ended outputs. A simplified circuit diagram is shown in Fig. 6.4.2. An RF filter is placed between the upconverter and VGA to suppress high-order harmonics in GSM operation.

Three single-bit 3^{rd} -order $\Delta\Sigma$ fractional PLLs are used in this transceiver [1]. The first PLL provides GSM RX, and GSM/WCDMA TX LO signals. Two different VCOs and dividers in the first synthesizer optimize performance and power consumption for GSM/EDGE and WCDMA TX. PFD, CP and loop filter in the first synthesizer are shared between GSM and WCDMA TX. The reference spurs in GSM mode are less than -105 dBc, which fulfills the GSM RX bandnoise specification without any external filters as shown in Fig. 6.4.3. The RX band noise is clearly less than the -79dBm specification and uses none of the five spurious response exceptions allowed by the GSM standard. The second PLL generates the WCDMA primary and diversity RX LO signals. The third PLL creates the GPS LO signals. On-chip regulators are used in the three PLLs to meet spur and phase-noise performance. Each regulator is designed to meet both high- and low-frequency PSRR and achieves good noise filtering and spur rejection. Each PLL uses only one external component for its loop filter. It is very important that spurs from one system do not affect the other system in this multimode transceiver. Careful synthesizer programming avoids or minimizes any fractional spurs.

The GSM RX path consists of an RX front-end (RXFE) and a programmablegain low-pass filter (PG LPF). The LNA has four inputs (850, 900, 1800, and 1900MHz). In each band, the two input stages share one output LC load and mixer. An RC filter placed between the mixers and PG LPF attenuates noise and jammers. The PG LPF is a 5th-order custom filter with a programmable bandwidth (125 to 155 KHz) and gain of max 80dB. An on-chip RC tuner uses the reference clock to tune the filter response with an accuracy of ±3%. To prevent each stage of the PG LPF from saturation by DC offset (DCO), current DACs and a digital state-machine calibrate the DCO stage-by-stage [1]. An AC coupling block between stages of the PG LPF blocks DCO generated by the RXFE and earlier gain stages. Typical NF is <3 dB, IIP3 >-15 dBm and IIP2 >+48 dBm at maximum gain. A GSM 850MHz Band RX sensitivity plot is shown in Fig. 6.4.3.

Quad-band UMTS RX operation is achieved with a 4-input zero-IF receiver. Two of the 4 front-ends are single-ended LNAs requiring SAW filters between the LNA and mixer to reduce TX leakage. This allows the use of duplexers with reduced TX/RX isolation. A wideband mixer is shared between those two paths. The two UMTS differential receiver inputs use no SAW filters between the LNA and mixer. Stringent FE linearity and challenging LO phase noise are required in the SAW-less paths to cope with the -25 dBm TX leakage from the duplexer. An on-chip IM2 calibration circuitry is implemented for those two paths to minimize the IM2 products generated by the TX leakage. A 5th- order lowpass filter (LPF) is shared among all UMTS RX paths. It has a 3dB bandwidth of 2.1MHz with an accuracy of ±3% over PVT achieved through automatic on-chip RC calibration. The measured receive gain is 58dB and the noise figure is 2.6dB. Typical (calibrated) IIP2 of the two receivers without SAW filter is +60dBm referred to the LNA input. Figure 6.4.4 shows the WCDMA RX sensitivity for BC 1 (IMT), BC4 (AWS) and BC5 (Cell). It can be seen that this receiver exceeds the sensitivity requirements by several dB even without the use of TX interstage SAW filters between this transceiver and the power amplifier.

The low-IF GPS receiver [6] operates simultaneously with the WCDMA/GSM/EDGE tranceivers. The measured receive gain is 82dB, noise figure is 2.0dB, with 35dB image rejection and maximum out-of-band IIP3 is +6dBm. A secondary WCDMA diversity zero-IF receiver (DRX) achieves total receive gain of 57 to 58dB, IIP3 from -17 to -20dBm, and IIP2 better than +49dBm. Since the GPS and DRX receivers do not need to operate at the same time by design, they share a reconfigurable 3rd-order Chebychev baseband filter. The filter has a 3dB bandwidth of 1MHz in GPS mode, and 2.1MHz in WCDMA mode, with an accuracy of \pm 3% over PVT achieved through automatic on-chip RC calibration.

Figure 6.4.5 shows a summary of typical parametric performance and Fig. 6.4.6 shows the battery current (at 3.7V) vs output power in Full-Duplex WCDMA Cell (850MHz) and PCS (1900MHz) band operation. This device uses 2.1V and 2.7V supplies and consumes 63.4mA (at the battery) in Cell Band and 69mA (at the battery) in PCS Band for a chip P_o = -8dBm. In a typical 3G phone this corresponds to 0dBm at the phone antenna (a phone spends approximately >90% time at power levels lower than 0dBm). Note that these current consumption figures are very competitive when compared with the data in [2-4] considering the significant amount of integration and the SAW-less receivers in these bands. The transceivers in [2-4] are WCDMA only and use interstage SAW filters in all bands and modes. Figure 6.4.7 shows the micrograph of the presented chip which has a die size of 5.6×5.6mm².

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