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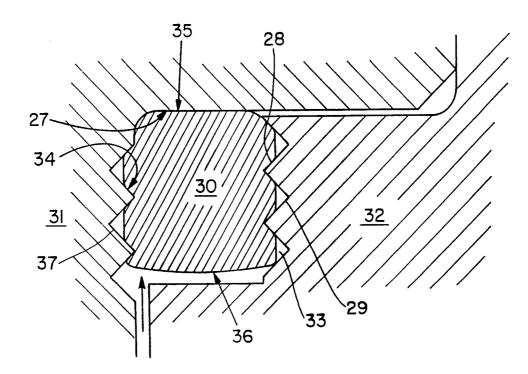
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(54) Title: HELIUM PRESSURE SEAL FOR A CRYOGENIC REFRIGERATOR



(57) Abstract

A pressure seal used for containing helium within a cryogenic refrigerator, which utilizes a linear drive assembly (5). A deformable gasket (30) is used to seal the enclosing elements of the linear drive assembly to reduce helium leakage. Concentrically serrated members (31, 32) compress onto opposite sides of the soft metal gasket (30) to form labyrinthine sealing grooves therein.

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#### HELIUM PRESSURE SEAL FOR A CRYOGENIC REFRIGERATOR

#### Background of the Invention

The present invention relates to pressure seals and more particularly to deformable gasket seals for pressurized helium containment within the linear drive system of a cryogenic refrigerator.

Helium cryogenic refrigerators utilize a linear drive assembly in which gaseous helium undergoes substantial variations in pressure. Due to the small size of the helium atom, there are substantial problems in obtaining simple inexpensive methods of sealing pressurized helium within such a refrigerator.

The most common seals used in pressurized

devices are O-rings and gaskets composed of elastomeric compounds. These seals are generally positioned within mating grooves in adjacent parts. When exposed to temperature and pressure excursions that frequently occur in cryogenic refrigerators such elastomeric seals degrade causing leakage and thus loss of efficiency or failure.

Existing helium cryogenic refrigerators have used indium or other soft metals as O-rings within mating grooves to contain pressurized helium. U.S. Patent No. 4,418,918, for example, discloses the use of a deformable metal ring, preferably made of indium, that is plastically deformed by a triangular shaped anti-rotation ring. The anti-rotation ring is compressed into the indium ring forming a

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V-shaped groove, thereby sealing the junction between rotatably secured members of a cryogenic refrigerator. Indium absorbs and retains radiation making it unsuitable for applications with possible exposure to radiation sources.

#### Summary of the Invention

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The present invention utilizes a deformable gasket; preferably a soft metal, such as copper, sandwiched between two members which partially 10 enclose the linear drive of a helium cryogenic refrigerator. These members have concentric serrations contacting opposite sides of the gasket. As the two members are comprised of metals much harder than the gasket, the application of pressure which forces the members together will cause the ser-15 rations of both members to be driven into the gasket material. The gasket is thereby deformed with concentric grooves on both sides, which match the serrations of the two "jaws" or members. resulting labyrinth of circular grooves forms an effective seal against helium that is less sensitive to surface finish than traditional helium sealing methods.

The compressive force of the jaws on the gasket
causes the bulging or expansion of its outer and
inner diameters. One of the members forms an axial
wall opposite the outer diameter or rim of the
gasket. This wall contacts and supports the deformed gasket, thereby opposing radial forces caused

by the positive pressure of helium within the refrigerator.

The copper gasket of a preferred embodiment of the invention is easily machined for throw away cost and has thermal stability over a range of ambient temperatures by approximately matching the thermal expansion coefficients of the seal assembly with the gasket.

The above, and other features of the invention,
including various novel details of construction and
combination of parts, will now be more particularly
described with reference to the accompanying drawings
and pointed out in the claims. It will be understood
that the particular helium pressure seal embodying
the invention is shown by way of illustration only
and not as a limitation of the invention. The
principle features of this invention may be employed
in various embodiments without departing from the
scope of the invention.

#### 20 Brief Description of the Drawings

Figure 1 is a cross-sectional view of a linear drive assembly of a helium cryogenic refrigerator with the deformable gasket of the present invention;

Figure 2 illustrates a magnified view of a 25 cross-section of the gasket deformed by serrated members;

Figure 3 illustrates a plan view of a gasket;
Figure 4 illustrates a magnified view of a
portion of a deformed gasket with concentric grooves
therein;

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Figure 5 illustrates a magnified view of a flange with concentric serrations used to form a seal with the gasket; and

Figure 6 illustrates a magnified plan view of a 05 plate covering one end of the drive assembly with concentric serrations to form a seal.

### Detailed Description of the Invention

A linear drive assembly of a helium cryogenic refrigerator utilizing a seal of the present invention is illustrated in Figure 1. A linear motor is used to control the movement of an armature 10 in the compressor 5 and the movement of a displacer (not shown). The linear motor utilizes an involute laminated stator 20 first disclosed in U.S. Patent application Serial No. 885,218, of G. Higham et al. filed July 14, 1986 entitled "Cryogenic Refrigeration System Having an Involute Laminated Stator for its Linear Drive Motor."

As shown in Figure 1, this compressor 5 com20 prises a reciprocating armature 10 which compresses
helium gas in a compressor head space 24. From the
head space 24 the gas passes through a port 14 in
the stationary piston 11 to pre-formed bores through
the piston 11 and plate 31 to form conduit 13.

25 Conduit 13 runs along the core of stationary piston 11, then curves at a right angle in insert 98 to a gas fitting assembly 15. From the gas fitting assembly 15, gas is delivered to a cold finger of a cryogenic refrigerator such as a split Stirling

30 refrigerator in which a displacer is housed as

disclosed in U. S. Patent 4,545,209. The stationary piston 11, mounted at one end onto plate 31, is the sole support for armature 10.

Plate 31 provides for a lead ball 53 and

retainer screw 52 for sealing the port 17. The
compressor is charged with helium gas through the
port 17. The gas is allowed to communicate with an
armature volume 12 of the piston cylinder through
port 16 which is in communication with a second

pre-formed conduit 18. During the compressor
operation, however, the ball 53 is fixed against the
plate 31 by the retainer screw 52 to close the port
17. A protective dust cover screw 19 is provided to
prevent dirt and debris from entering the ball 53

and screw 52 seal.

The armature 10 comprises an iron mass 38 fixed to a liner core 82. Iron is used because of its high magnetic permeability and high magnetic induction; however, other materials having the same characteristics may be used. A tungsten alloy ring 25, or other high density non-magnetic material, may be incorporated at one end of the armature to give more mass to adjust the resonant frequency of operation and to help keep the armature's center of gravity within the confines of the clearance seal of the piston.

In order to detect the position of the armature a sensor 80 is used to detect a target magnet 81 fitted at one end of the armature 10. The magnet 81 is mounted on an extended cylinder 85 that oscillates within an extension 86 of the armature housing 26 during motor operation. By isolating the magnet 81

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and sensor 80 away from the stator 20, the magnetic field of magnet 80 is decoupled from the magnetic field of the stator magnet 22. Preferably, the piston 11 is closely fitted within a ceramic cylinder 83 attached to armature 10 to provide a clearance seal therebetween. It is preferred that a sleeve 82, made of a non-magnetic, high resistivity, stainless steel line the cylinder 83. A cermet liner 84 is mounted on the piston 11 to form part of the clearance seal.

Surrounding the armature 10 just described is a pressure housing 26. The size of the pressure housing is constructed to allow helium gas in the working volume 12 to flow freely between the pressure housing 26 and the iron mass 38 as the armature 10 shuttles back and forth.

A stator 20 is located around the perimeter of the pressure housing 26. The stator 20 comprises two coils 21 positioned between involute laminations 23 and separated by a magnet 22. This static assembly is further described in U.S. Serial No. 885,218, by G. Higham et al. recited above, which is incorporated herein. Two shields 90 have been concentrically disposed about the involuted laminations 23 to convey the magnetic flux lines along the inside wall 51 of the housing 50.

As a consequence of the armature 10 reciprocating back and forth, mechanical vibrations are
produced by the compressor 5. To eliminate the

30 vibrations, a passive vibration absorber or dynamic
absorber 39 is attached to one end of the compressor
and is tuned to resonate at the same frequency as

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the compressor's operating frequency. Preferably,
the dynamic absorber 39 comprises a counterbalance
mass 40 mounted with flange 45 between two springs
41 and 42 having small damping characteristics. As
05 a result, the axial motion of the compressor is
countered by the axial vibration from the counterbalance mass 40 of the absorber 39. A further
description of dynamic absorber operation is found
in U.S. Serial No. 894,777, of G. Higham et al.,
10 filed August 8, 1986, entitled "A Vibration Isolation
System for a Linear Reciprocating Machine."

The present invention utilizes isolators
mounted on opposite ends of the compressor. The two
isolators have flat spiral springs 61 and 71 which

are soft in the axial direction while being very
stiff in the radial direction. The outer diameter
of the two springs 61 and 71 are attached to the
housing end plates 60 and 70 respectively. The
inner diameters are mounted onto flanges 62 and 72

using bolts 64 and 74. The springs are mounted on
elastomeric material 95 and 96 located at both ends
of compressor 5 providing a substantial level of
damping to the isolator system. Grease is applied
to the outside surface of wall 51 to help remove
heat from the stator 20 while providing damping of
internal vibration of the compressor.

A soft metallic gasket 30 is configured between the plate 31 and flange 32 that is deformed to seal the armature volume 12 of the linear drive unit from 30 the external atmosphere. Figure 2 illustrates a magnified view of the deformed gasket 30 of the

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present invention. A plate 31 with serrations 37 is forced against gasket 30 to form the grooves 34 on one side thereof. The serrations 29 of flange 32 are disposed on the opposite side of gasket 30 to 05 create grooves 28. The serrations 37 of plate 31 mate with the serrations 29 of flange 32 so that the grooves 34 corresponding to plate 31 are offset from the grooves 28 of the flange 32. The cavity adjacent each serration of the plate 31 and flange 32 is at least 20% filled by volume with the gasket material to insure a sufficiently long leakage path across the sealed gasket surface.

The gasket material is capable of withstanding a large temperature range between -62°C and 71°C 15 that such a refrigerator may typically encounter. The coefficient of thermal expansion of the gasket material can be closely matched with the thermal coefficients of both the plate 31 and the flange 32 to insure the integrity of the seal during thermal 20 transitions. Low yield stress characteristics of the selected gasket material allow it to conform with the serrations on mating plate 31 and flange 32 to compensate for mismatches in the coefficient of thermal expansion. The gasket material is also 25 relatively impermeable with respect to helium whose small atomic size renders container permeability a significant problem. A preferred embodiment utilizes annealed copper for the gasket material. Figure 3 illustrates a copper gasket annealed at 30 1000°F for 30 minutes before being deformed by plate 31 and flange 32. Annealing renders the gasket oxygen free with a hardness of about 40 on the

Rockwell F scale. The gasket can maintain helium pressures of over 1000 psi with leak rates of less than  $2 \times 10^{-8}$  scc He/sec.

The axial wall 35 of plate 31 is concentrically disposed about the gasket 30. The outer diameter or rim surface 27 of the gasket has been deformed by the compression of plate 31 against the gasket 30 and flange 32. Surface 35 of plate 31 provides support for surface 27 of gasket 30 with pressure loads applied on surface 36. As the piston is driven back and forth within the linear drive, there are large variations in pressure at seal 30 during each cycle. The axial support wall 35 is used to counter the radial forces at peak pressures tending to displace the seal radially outward.

The surface of the inner diameter 36 also bulges slightly. However, there is no requirement in the present embodiment that there be any support for the inner diameter of the gasket, as there is a positive pressure within the drive unit during normal operation. The tight annular clearances between the plate 31 and flange 32 are for alignment purposes and do not contribute to the sealing ability of the joint. The seals 30 and the lead ball 53 and screw 52 seal are the only replaceable seals used within the compressor assembly to retain helium. The remaining joints defining the armature volume between the flange 32 and pressure housing 26 as well as between the housing 26 and the extended cylinder 86 are both welded.

Figures 4, 5, and 6 illustrate magnified views of a portion of the deformed gasket, and plan views

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of the flange 32 and plate 31 showing the concentric serrations 29 and 37 of each member, respectively. Holes 120 are for bolts 121, which are used to compress the plate 31 and flange 32 together are arrayed about the serrations of each member to provide a uniform distribution of pressure. There are preferably at least two concentric serrations on both the flange 32 and plate 31 so that both leakage paths form a long labyrinth.

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#### CLAIMS

- 1. A sealed cryogenic refrigerator having a compressor comprising a piston element which alternatively compresses and expands gaseous helium in a working volume, a linear drive motor for driving the piston element, and a seal for containing the gaseous helium within the working volume, the seal comprising:
  - a deformable gasket;
- first and second members partially enclosing said working volume with each having a
  plurality of concentric serrations such that
  said gasket is configured between the serrations of each member; and
- compressive means for compressing said serrated first and second members together about the gasket such that said serrations deform the gasket forming sealing concentric grooves therein.
- 20 2. The sealed cryogenic refrigerator recited in Claim 1 further comprising an axial wall concentrically disposed about the deformed gasket such that the wall supports the gasket.

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- 3. The sealed cryogenic refrigerator recited in Claim 1 wherein the concentric serrations of said first member are aligned opposite a cavity adjacent to each serration of the second member, on opposite sides of the gasket.
- 4. The sealed cryogenic refrigerator recited in Claim 1 wherein said gasket is softer than said first and second members.
- 5. The sealed cryogenic refrigerator recited in

  Claim 1 wherein said compressive means is

  comprised of a plurality of bolts such that the
  tightening of said bolts reduces the distance
  between said serrated members.
- 6. The sealed cryogenic refrigerator recited in
  15 Claim 1 wherein said gasket contains pressurized helium within the working volume of the
  linear drive motor.
- The sealed cryogenic refrigerator recited in Claim 1 wherein the deformed gasket fills at least 20% of a serration cavity adjacent each serration.
  - 8. The sealed cryogenic refrigerator recited in Claim 1 wherein said gasket is comprised of annealed copper.

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- 9. The sealed cryogenic refrigerator recited in Claim 8 wherein said copper has a hardness of about 40 (Rockwell F scale).
- 10. The sealed cryogenic refrigerator recited in
  Claim 1 wherein each of said first and second
  members has two concentric serrations.
  - 11. The sealed cryogenic refrigerator recited in Claim 1 wherein said first and second members have coefficients of thermal expansion substantially similar to that of the gasket.
  - 12. A seal for pressurized gaseous helium containment comprising:

a deformable gasket;

first and second members enclosing pressurized helium and having a plurality of concentric serrations such that said gasket is positioned between the serrations of said members;

pressure means for applying pressure to said first and second members such that said serrations deform the gasket forming concentric grooves therein to form a seal; and

an axial wall concentric about the gasket such that the wall supports the gasket.

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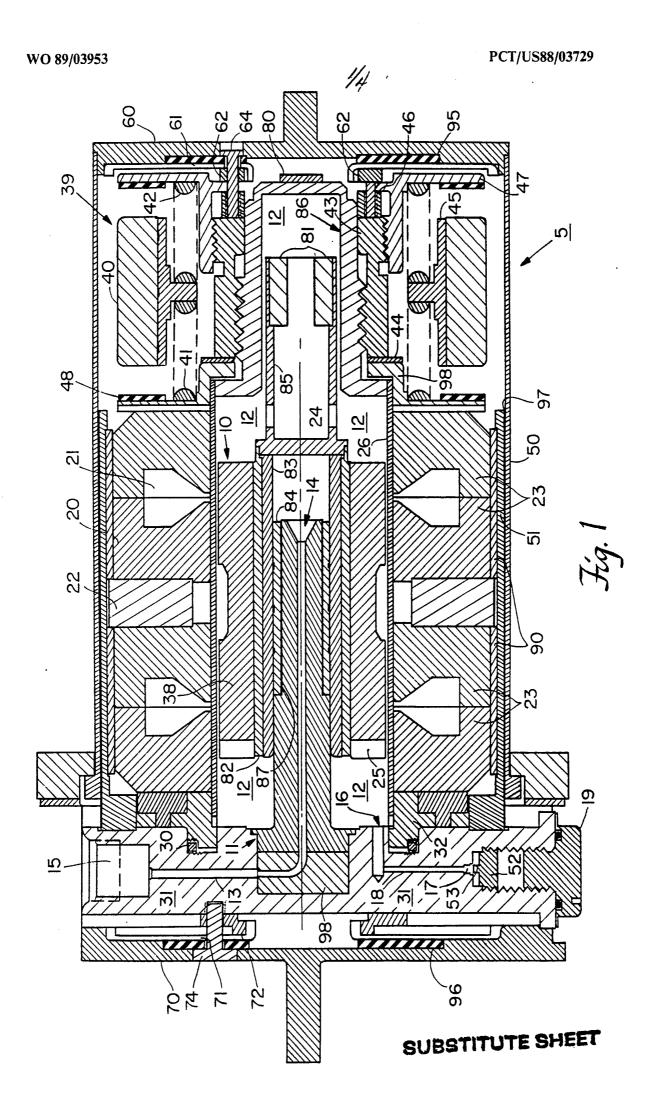
- 13. A seal as recited in Claim 12 wherein said applied pressure deforms a grooveless outer rim of the gasket such that the outer rim expands to contact the wall.
- 05 14. A seal as recited in Claim 13 wherein said pressurized helium exerts radial forces on the gasket which are opposed by the axial support wall.
- 15. A seal for pressurized helium containment
  10 comprising:

a deformable gasket with inner and outer rims such that the inner rim confines pressurized helium and the outer rim is exposed to a fluid at a pressure lower than the helium;

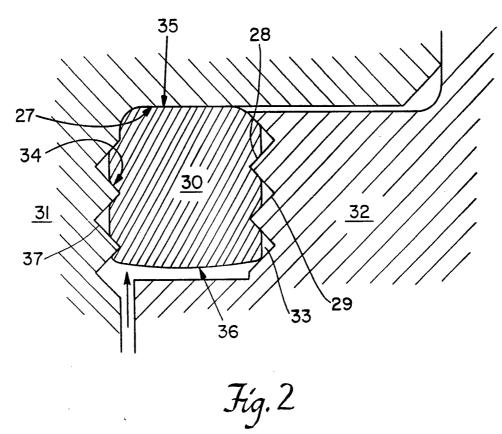
first and second members enclosing pressurized helium and having a plurality of concentric serrations such that said gasket is positioned between the serrations of said members;

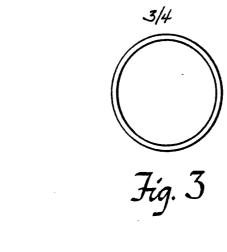
pressure means for applying pressure to said first and second members such that said serrations deform the gasket forming concentric grooves therein to form a seal; and

an axial wall concentric about the outer 25 rim of the gasket such that the wall supports the outer rim.



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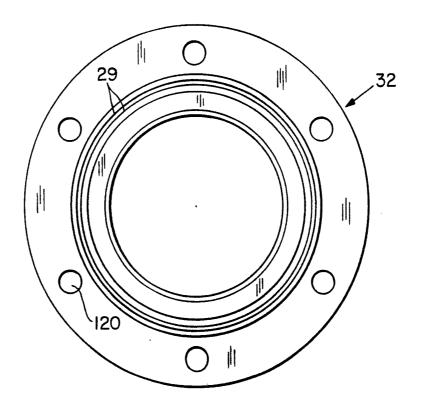


Fig. 5

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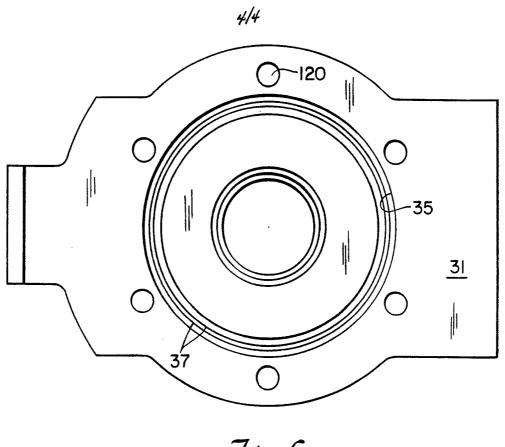


Fig. 6

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#### INTERNATIONAL SEARCH REPORT

International Application No PCT/US 88/03729

I. CLASS	IFICATION OF SUBJECT MATTER (if several class	ification symbols apply, indicate all) <sup>6</sup>	
According	to international Patent Classification (IPC) or to both Na	tional Classification and IPC	
IPC <sup>4</sup> :	F 16 J 15/08; F 16 L 23	3/00	
II. FIELDS	SEARCHED	entation Searched 7	
		Classification Symbols	
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IPC <sup>4</sup>	F 16 J; F 16 L		
	Documentation Searched other to the Extent that such Document	than Minimum Documentation is are Included in the Fields Searched <sup>9</sup>	•
III. DOCL	MENTS CONSIDERED TO BE RELEVANT		Relevant to Claim No. 13
Category *	the state of the section where an	propriate, of the relevant passages 12	Relevant to Claim No
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A	US, A, 4545209 (YOUNG) 8 October 1985 see figures and abs cited in the applicatio	tract n	1,12,15
"A" do	ial categories of cited documents: 10 incument defining the general state of the art which is not insidered to be of particular relevance ritier document but published on or after the international and date of the comment which may throw doubts on priority claim(s) or thick is cited to establish the publication date of another lation or other special reason (as specified) occument referring to an oral disclosure, use, exhibition or the means	"X" document of particular releva cannot be considered novel of involve an inventive step. "Y" document of particular releva cannot be considered to involve document is combined with on ments, such combination being in the art.	nce: the claimed invention r cannot be considered to nce: the claimed invention an inventive step when the e or more other such docu-
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# ANNEX TO THE INTERNATIONAL SEARCH REPORT ON INTERNATIONAL PATENT APPLICATION NO.

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This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 29/03/89

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Patent document cited in search report	Publication date	Patent family member(s)	Publication date	
US-A- 3301578		None		
FR-E- 6800		None		
FR-A- 626122		None		
US-A- 4545209	08-10-85	EP-A,B 0114069 JP-A- 59194657 US-A- 4578956 DE-A- 3471364 CA-A- 1247872	25-07-84 05-11-84 01-04-86 23-06-88 03-01-89	