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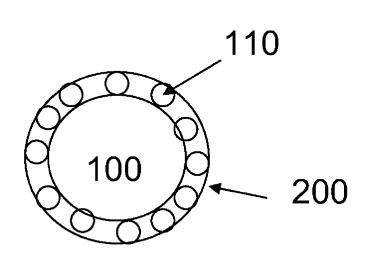


FIG. 2

(57) Abstract: The present disclosure relates to anode materials having high surface areas and improved cycle performance made by surface treatments of spheroidized graphite powders. The surface treatments provide a high surface area protective coating over the spheroidized graphite powder. The anodes made according to the disclosed embodiments have improved cycle life and long term high temperature storage performance. In the disclosed embodiments, a spheroidized graphite powder is coated with a high surface area protective coating. The high surface area protective coating improves the performance and durability of an anode made from disclosed material. The high surface area protective coating can include polymers, metal compounds and/or hard carbon. Further, in some embodiments, a protective coating, that may or may not have a high surface area but does have increased durability, can be formed by heat treating the spheroidized graphite in oxidizing or inert atmospheres.



ANODE MATERIAL

Cross Reference to Related Applications

[0001] This application claims the benefit of United States Provisional Application 61/288,595, filed on December 21, 2010, the entire contents of which are hereby incorporated by reference.

Background

[0002]Battery manufacturers are continuing to increase energy density, power characteristics, cycle life and safety characteristics, while decreasing the cost, of anode materials. Flaky natural graphite can be used as an anode material by transforming it into spherical particles through a process called spheroidization. Crystalline flake graphite (or flake graphite for short) occurs as isolated, flat, plate-like particles with hexagonal edges if unbroken and when broken the edges can be irregular or angular. Spheroidization of flake graphite can be accomplished by repeated pulverization of the flake graphite with a relatively small impact mill such as an air classifier mill (ACM) or pin mill. When pulverization is conducted, it is necessary to repeat the operation at least 10 times to produce a spherical shape with a high powder density. In order to obtain the targeted particle size (e.g., about 8-20 μm average), the average diameter of raw and flaky natural graphite should be about 1 μm to 50 µm. This finalized spheroidized powder can be used as an anode active material in a battery, for example, a lithium ion battery. Spheriodized graphite powder is typically a high surface area material that is useful to make anodes for high power, i.e., low impedance or low direct current resistance, battery applications. However, the efficiency of first charge and discharge of an anode made from this material is usually too low to achieve promising cell capacity. In addition, high temperature storage performance, i.e., good calendar life, is also poor for such anodes. The high surface area graphite powder does not perform well as at higher temperatures because of the loss of cyclable lithium generated from the solid electrolyte interphase (SEI) film reformation with electrolyte during cycling, i.e., during operation, and high temperature storage.

[0003] Instead, in order to increase the durability, i.e., cycle performance, of the natural graphite powders, the graphite is coated with pitch, which reduces the surface area of the graphite powder, but also increases the durability of the anode. Pitch is the name for any of a number of viscoelastic, solid polymers. Pitch can be made from petroleum products or

plants. Pitch coated natural graphite is widely used for consumer battery applications such as laptops and cell phones. Pitch coated natural graphite is used because of its durability and low cost. Pitch coated graphite powder is good for cycling at low rate and calendar life (long term high temperature storage) because the pitch coating can minimize the side reactions with the electrolyte during cycling and high temperature storage. However, the pitch coating reduces the surface area of the active sites on the anode particles.

[0004] Because of the reduced surface area of the pitch coated graphite, cycle performance of the pitch coated anode materials is not well suited to a high power automotive application. With pitch coated anode materials, the interface between the pitch coated layer and the core graphite deteriorates during high power cycling operations. Accordingly, slightly higher surface area graphite powder has been used for high power applications.

[0005] The surface area of the anode powder is an important part of a lithium ion battery cell which affects cycling, storage, and safety performances of the battery. Appropriate surface area of anode powder will allow rapid reaction with lithium ions in the electrolyte. A high surface area anode, such as spheroidized graphite also can be good for regeneration power and high discharge cycling. A low surface area pitch coated graphite anode material performs well in terms on durability, but is not ideal for a high power application. Thus, an anode powder that creates a durable anode for high power applications is needed.

Summary

[0006] In one aspect, the present disclosure relates to an anode powder. The anode powder includes a spheroidized graphite powder and a high surface area protective coating surrounding the graphite powder, wherein, the coated powder has a higher surface area than the untreated graphite powder. In some embodiments, the anode powder has a particle size between about 5 um and about 20 um. In some embodiments, the anode powder has a surface area between about 5m²/g and about 20m²/g. In some embodiments, the anode powder has a Raman spectroscopy peak intensity ratio of D band/G band less than 0.3. In some embodiments, the anode powder has a Raman spectroscopy peak intensity ratio of D band/G band above about 0.3. In some embodiments, the high surface area protective coating can be a metal compound powder. In some embodiments, the metal compound powder includes a metal oxide powder. In some embodiments, the metal oxide powder is selected from Al₂O₃, Y₂O₃, TiO₂, Cs₂O₃, ZrO₂, and ZnO. In some embodiments, the metal compound powder can

- 2 -

be a metal fluoride powder. In some embodiments, the metal fluoride powder can be AlF₃, ZrF₄, TiF₄, CsF₃, YF₃, or ZnF₂. In some embodiments, the high surface area protective coating can be a mixture of metal compound powder and polymer. In some embodiments, the high surface area protective coating can be a hard carbon coating. In some embodiments, the coating has an oxygen content of between about 1% and about 6%. In some embodiments, the coating has a carbon, oxygen double bond percentage of above about 3%.

[0007] Another aspect of the disclosure relates to a method of making an anode powder. The method includes providing a spheroidized graphite powder, coating the graphite powder with a high surface area protective coating, and heat treating the coated graphite power to form an anode material that has a higher surface area than the untreated graphite powder. In some embodiments, the anode powder has a surface area between about 5m²/g and about 20m²/g. In some embodiments, the anode powder has a Raman spectroscopy peak intensity ratio of D band/G band less than 0.3. In some embodiments, the anode powder has a Raman spectroscopy peak intensity ratio of D band/G band above about 0.3. In some embodiments, the method includes heat treating the coated graphite powder in an oxidizing atmosphere. In some embodiments, the method includes heat treating the coated graphite powder in an inert atmosphere. In some embodiments, coating can be coating the spheroidized graphite powder with a metal compound powder. In some embodiments, coating can be coating the spheroidized graphite powder with a metal oxide powder. In some embodiments, the metal oxide powder is selected from the group consisting of Al₂O₃, Y₂O₃, TiO₂, Cs₂O₃, and ZnO. In some embodiments, the coating comprises coating the spheroidized graphite powder with a metal fluoride powder. In some embodiments, the metal fluoride powder is selected from the group consisting of AlF₃, ZrF₄, TiF₄, CsF₃, YF₃, and ZnF₂. In some embodiments, coating can be coating the spheroidized graphite powder with a hard carbon precursor.

[0008] Another aspect of the present disclosure relates to an anode. The anode includes an anode layer disposed on a conductive sheet, the anode layer including an electroactive powder, the electroactive powder including: a spheroidized graphite powder; and a high surface area protective coating surrounding the graphite powder; wherein, the coated powder has a higher surface area than the untreated graphite powder.

[0009] Another aspect relates to a battery. The battery includes a cathode, an anode, wherein the anode includes an anode powder, the anode powder including a spheroidized graphite powder and a high surface area protective coating surrounding the graphite powder,

- 3 -

wherein, the coated powder has a higher surface area than the untreated graphite powder; and an electrolyte in ionic communication with both the cathode and the anode.

Brief Description of the Drawings

[0010] For a more complete understanding of various embodiments of the present disclosure, reference is now made to the following descriptions taken in connection with the accompanying drawings in which:

- FIG. 1 illustrates a metal compound coated anode powder particle according embodiments of the present disclosure;
- FIG. 2 illustrates a metal compound/polymer coated anode powder particle according embodiments of the present disclosure;
- FIG. 3 illustrates a hard carbon coated anode powder particle according embodiments of the present disclosure.

Description

[0011] The present disclosure relates to anode materials having high surface areas and improved cycle performance made by surface treatments of spheroidized graphite powders. The surface treatments provide a high surface area protective coating over the spheroidized graphite powder. The anodes made according to the disclosed embodiments have improved cycle life and long term high temperature storage performance. In the embodiments discussed below, a spheroidized graphite powder is coated with a high surface area protective coating. The high surface area protective coating improves the performance and durability of an anode made from disclosed material. The high surface area protective coating can include polymers, metal compound and/or hard carbon. Further, in some embodiments, a protective coating, that may or may not have a high surface area but does have increased durability, can be formed by heat treating the spheroidized graphite in oxidizing or inert atmospheres.

Lithium Ion Batteries

[0012] A lithium-ion battery (sometimes called Li-ion battery or LIB) is a family of rechargeable battery types in which lithium ions move from the negative electrode to the positive electrode during discharge, and back when charging. Chemistry, performance, cost, and safety characteristics vary across LIB types. Unlike lithium primary batteries (which are

- 4 -

disposable), lithium-ion cells use an intercalated lithium compound as the electrode material instead of metallic lithium.

[0013] The three primary functional components of a lithium-ion battery are the anode, cathode, and electrolyte. The anode of a conventional lithium-ion cell is made from carbon, the cathode is a metal oxide, and the electrolyte is a lithium salt in an organic solvent. The most commercially popular anode material is graphite. Typically, the anode material is disposed on a conductive sheet and contains an electroactive powder. The cathode is generally one of three materials: a layered oxide (such as lithium cobalt oxide); a polyanion (such as lithium iron phosphate); or a spinel (such as lithium manganese oxide). The electrolyte is typically a mixture of organic carbonates such as ethylene carbonate or diethyl carbonate containing complexes of lithium ions. These non-aqueous electrolytes generally use non-coordinating anion salts such as lithium hexafluorophosphate (LiPF₆); lithium hexafluoroarsenate monohydrate (LiAsF₆); lithium perchlorate (LiClO₄); lithium tetrafluoroborate (LiBF₄); and lithium triflate (LiCF₃SO₃) and are in ionic communication with both the anode and the cathode.

[0014] Depending on materials choices, the voltage, capacity, life, and safety of a lithium-ion battery can change dramatically.

[0015] Pure lithium is highly reactive. It reacts vigorously with water to form lithium hydroxide and hydrogen gas is liberated. Thus, a non-aqueous electrolyte is typically used, and a sealed container rigidly excludes water from the battery pack.

[0016] The present disclosure relates to improvements to the anode of the lithium ion battery. In particular, the described embodiments relate to an improved anode powder that can increase the performance and durability of the anode and the battery itself. By maximizing the surface area of the anode powder and providing a protective coating to the anode powder, an anode material that has high performance and good durability can be made.

Metal Compound Powder Coating

[0017] In one aspect, the disclosure relates to a high power, durable anode material having a metal compound powder coating. In one embodiment, as shown in FIG. 1, the anode material includes a spheriodized graphite powder 100 coated with a plurality of metal compound powder particles 110 to form a metal compound powder coated anode powder.

- 5 -

The graphite powder has a diameter of about 8 to 20 microns. The metal compound powder coating can be a layer of a metal oxide or metal fluoride. The metal compound powder layer can have a thickness of about a few nanometers to about 50 nanometers. Further, the metal compound powder layer is not necessarily a continuous layer of metal compound powder particles.

[0018]In another embodiment, as shown in FIG. 2, the metal compound powder particles 110 can be added to a polymer coating layer 200 on the spheriodized graphite powder 100 to form a metal compound polymer coating composite. The metal compound polymer composite layer can have a thickness of about a few nanometers to about 50 nanometers. The polymer coating layer 200 can be, for example, amorphous carbon, hard carbon precursors or soft carbon precursors. Hard carbon is formed by thermally decomposing a polymer resin. Exemplary hard carbon precursors include polyimide resin, furan resin, phenol resin, polyvinyl alcohol resin, cellulose resin, epoxy resin, and polystyrene resin. The hard carbon polymers can be used with or without curing agent. Soft carbon can be pitch materials. Exemplary soft carbon precursors include petroleum pitch, coat tar pitch, and chemically processed pitches. Preferred compounds include those with high carbon content after thermal decomposition, for example, the carbon content being in the range of about 1% to about 10%... Additionally, other active additives can be used in addition to the metal compound powder and polymer, for example, conducting carbon or carbon black. In the metal compound polymer composite coating the polymer coating layer can support the metal compound powder on the graphite surface. The particle size of metal compound powder in both examples is typically in the range of about 10 nm to about 500 nm. The metal compound powder also has a high surface area, e.g., 50- 100 m²/gram. Accordingly, the nano metal compound powder particles have a higher surface area than the natural graphite materials (having a surface area of about $0.5 \text{m}^2/\text{g}$ to $6 \text{m}^2/\text{g}$). When these metal compound powder particles are added to the graphite, they increase the surface area of the composite coated particle. As discussed above, for a high power application, a higher surface area is needed to obtain the high power performance. Therefore, by introducing metal compound powder into the graphite powder, anodes for high power or high energy density lithium ion cells can be manufactured.

[0019] Further, the metal compound powder also increases the long term storage performance of the anode. The additional metal compound powder material can help obtain

- 6 -

better electrolyte wetting, which improves electrolyte graphite surface contact during cycling. Further, the addition of the metal compound powder can produce anode materials with good calendar life, including both a long cycle life, e.g., the anode will not deteriorate during use, and good storage performance, e.g., the anode will not deteriorate during storage.

[0020] The metal compound powder coated graphite powder can be a hydrogen fluoride (HF) scavenger to improve long term cycle life and high temperature storage performance. If the cell has retained moisture, the moisture can react with LiPF₆ salt (a common electrolyte salt used in lithium ion batteries) forming a strong acid (HF) which may deteriorate the cathode material. Prior systems have added metal compound powder into the formed electrode to react with the HF once it is formed, i.e., the metal compound powder was mixed with the polymer binder of the electrode. However, it is difficult to uniformly distribute the metal compound powder into the electrode during the mixing and coating processes and a large amount of metal compound powder was needed to achieve a desirable improvement in performance. Here, however, a method for preparing uniformly coated metal compound powder on the graphite active material prior to formation of the electrode is described. The mechano-chemical process discussed below permits a uniform application of the metal compound powder to the graphite powder. The metal compound powder is inert and nonreactive with polymer material during a carbonization process. Therefore, it is possible to achieve molecular level uniform mixing on the graphite powder while simultaneously reducing the amount of metal compound powder used and maximizing the capacity on the anode.

[0021] The metal compound powder can be a metal oxide can be selected from Al₂O₃, Y₂O₃, TiO₂, Cs₂O₃, ZnO, ZrO₂ and other similar metal oxides or fluorides, for example, those from an amphoteric element compound, i.e., a compound that can react as either an acid or a base. For example, alumina can react with HF and reduce the formation of LiF, which can deteriorate the cell performance by consuming HF through a side reaction. The metal compound powder also can be a metal fluoride, for example, one of AlF₃, ZrF₄, TiF₄, CsF₃, YF₃, and ZnF₂.

[0022] In another embodiment, nano scale silicon or tin metal powder can be added, in addition to the metal compounds discussed above, during the process of spheroidization and pitch coating. In this embodiment, the graphite material retains the conducting pathway and high capacity during cycling, even if the metal compound breaks down.

- 7 -

[0023] In another embodiment, to improve performance capacity of the graphite material, a secondary metal powder and/or metal oxide powder can be added, e.g., Si, Ag, Fe, Pd, Pb, Al, Si, or In. Preferably, one or more SiO or SnO or SnO₂ powder is added to the graphite powder and polymer. The added SiO or SnO or SnO₂ powder in the final anode product can react with the lithium of the lithium battery to improve the capacity of the anode material. This process can improve uniform distribution of the metal powder between the primary graphite particles boundaries. Therefore, the final product would contain composite particles of graphite, the primary metal compound powders and polymers mentioned above, and the secondary metal powders and/or oxides described in this paragraph. This graphite interlocked structure with the secondary metal oxide powder can facilitate high capacity and better cycle performance because the conducting path can be preserved throughout the active material powder. The described material can produce electrodes with a long cycle and improved storage performance. Further, the described material contributes to improved processing, especially electrolyte wetting.

[0024] Once the spheroidized graphite powder is coated with the metal compound powder or the metal compound powder/polymer composite, the coated graphite can be heat treated. The heat treatment increases cycling and storage performance. The heat treatment can occur in an oxidizing atmosphere or in an inert atmosphere. The above anode powders keep the surface area high by adding a high surface area metal oxide such as alumina or a hard carbon precursor and heat treatment in order to produce an anode that will have required cycle and long term storage performance.

Hard Carbon Coating

[0025] In another embodiment, as shown in FIG. 3, a hard carbon coating 300 can be employed to improve the cycle performance of the anode material. The hard carbon coating 300 has a higher surface area than the graphite powder 100; therefore, the coating of the graphite powder 100 with the hard carbon coating 300 increases the surface area of the finalized anode powder. The hard carbon coating 300 is formed by thermally decomposing a hard carbon precursor, for example, a polymer resin, for example, phenol-novolac resin is decomposed into a high surface area high carbon content hard carbon coating that achieves the higher surface area and better cycle performance when coated on the spheriodized graphite particles 100. The same materials can be used as for the hard carbon precursor in the second metal compound embodiment discussed above. For the hard carbon coating, it is

- 8 -

possible to use a synthetic polymer. That is, polyimide resin, furan resin, phenol resin, polyvinyl alcohol resin, cellulose resin, epoxy resin, polystyrene resin, and carbonhydrate materials such as sugars and polyacrylonitrlies, etc. can be used as the hard carbon coating. Preferred compounds include those compounds with high carbon content after thermal decomposition, for example, between about 1% to about 10% carbon. To improve coating yield and properties of surface area, the powder type hard carbon precursor is used with the curing agent of hexamethylenediamine and is treated to make the precursor thermoplastic. Further, the localized heating caused by high shear and compressive forces of the processing creates fused composite particles without using a solvent. This process is suitable for making the coating process inexpensive. Wet methods also can be applicable to achieve hard carbon layer by using the solvent soluble polymer resin and by using an additional heat treatment in inert atmosphere.

[0026] Anode powders made with a hard carbon precursor coating can have a surface area between about $5\text{m}^2/\text{g}$ to about $20\text{m}^2/\text{g}$ and a Raman spectroscopy peak intensity ratio of D band/G band above about 0.3. The surface area of a hard carbon coating can be $10\text{ m}^2/\text{g}$ to about 1,000 m²/g. The highest surface areas can be obtained if using 100% hard carbon and heat treatment at 100 degrees Celsius. The oxygen percentage in the hard carbon coating can be about 1% to about 6%. The carbon oxygen double bond percentage can be higher than 3%.

Methods

[0027] Five different methods were applied to spheroidized graphite powder to create an anode powder having a long cycle life and improved storage performance while keeping a high surface area, compared to the prior art pitch coated and non-treated powders anode materials. The five methods include:

- 1. Metal compound powder and polymer coating of graphite powder, followed by heat treatment of coated graphite powder in oxidizing atmosphere;
- 2. Metal compound powder coating of graphite powder, followed by heat treatment of coated graphite powder in inert atmosphere;
- 3. Heat treatment of graphite powder in oxidizing atmosphere;

4. Heat treatment of graphite powder in inert atmosphere; and

5. Hard carbon precursor coating of graphite powder.

Metal compound Powder Anode Method

[0028] In the first embodiment, a metal compound powder and polymer coating are combined for a composite coating of the graphite powder. In the second embodiment, the metal compound powder can be coated directly on the spheroidized powder without a polymer coating. After metal compound powder coating, a heat treatment is conducted on the polymer/metal compound powder coated graphite powder in inert atmosphere. The metal compound powder is retained or implemented on the graphite powder surface by shear stresses between particles during mechano-chemical process. In both embodiments, the coating of metal compound powder nanoparticles is conducted by high shear and compressive forces which creates composite particles without using a solvent. In other words, a mechano-chemical coating process was used for this metal compound powder coating. In this mechanical process, the graphite powder can be damaged (as discussed below) and may need to be recovered by the additional heat treatment in oxidizing and inert atmosphere. Other wet methods can be applicable to this metal compound coating by using a water or solvent soluble metal compound and by using an additional heat treatment in oxidizing or inert atmosphere.

Heat Treatment

[0029] In other embodiments, the protective coating for the graphite powder is formed by heat treatment of the spheroidized graphite powder. The heat treatment can occur in an oxidizing atmosphere or an inert atmosphere. The heat treatment can be used to lower irreversible capacity loss by reducing the damaged portions of the graphite powder resulting from the spheroidization and/or coating process. For example, during the spheroidization process, the crystalline graphite can become disordered. The disordered sections can be more active than the crystalline sections of the graphite. The disordered sections are more fragile than the crystalline sections. Therefore, the disordered sections can become damaged or can break down during cycling, thereby decreasing the durability of the anode. In the coating processing the high shear and compressive forces also can damage the crystalline structure of the graphite. Heat treatment can remove these damaged sections of the graphite and improve the graphite crystalline structure of the particle. Therefore, the heat treatment process can improve the durability of the finalized anode product. The electrochemical characteristics of

- 10 -

oxidized graphite have been reported by several groups, for example, Peled et al. (E. Peled, et al. J. Electrochem. Soc., 143 (1996)) and Wu et al. (Y. P. Wu. et al, Solid State Ionics, 156 (2003)). In these studies, the anode's efficiency was increased, the irreversible capacity loss was decreased, and cycle performance was improved by eliminating structural disordered surfaces during the previous spheroidization.

[0030] Further, the heat treatment process can deposit functional groups, for example, C=O on the surface of the graphite. With the addition of these functional groups, the SEI film becomes more stable. The increased stability increases the durability and cycling performance of the anode because there is no side reaction with the electrolyte during cycling and long term storage. Therefore, the heat treatment can improve the cycle performance of the anode.

[0031] Typically, the temperature range of the heat treatment is from 500° C to 1000° C in oxidizing atmosphere. If the temperature is too low, no oxidation reaction occurs. If the temperature is too high, product yield will be too low because of the excess reaction of oxygen with carbon, resulting in more production of CO_2 and a greater loss of carbon active material.

[0032] The temperature range of the heat treatment is from 900°C to 2200°C in inert atmosphere. If the temperature is too low, disordered parts, i.e., graphite edge particles having a high surface area as a result of the spheroidization process, are not recovered. If the temperature is too high, the cost is high, the efficiency can be lower and the cycle performance can be worse due to a highly ordered graphitic surface and low efficiency of the effective material.

[0033] The anode powders made according to the above methods can have a surface area between about $5\text{m}^2/\text{g}$ and about $20\text{m}^2/\text{g}$ and a Raman spectroscopy peak intensity ratio of D band/G band less than about 0.4. The oxygen percentage in the heat treated coatings can be about 1% to about 6%. The carbon oxygen double bond percentage can be between higher than 3%.

Hard Carbon Coating

[0034] In another embodiment, the graphite powder can be coated with a hard carbon coating. The hard carbon coating is formed by thermally decomposing a hard carbon

precursor, for example, a polymer resin, for example, phenol-novolac resin is decomposed into a high surface area high carbon content hard carbon coating that achieves the higher surface area and better cycle performance when coated on the spheriodized graphite particle. To improve coating yield and properties of surface area, the powder type hard carbon precursor is used with the curing agent of hexamethylenediamine and is treated to make the precursor thermoplastic. The localized heating caused by high shear and compressive forces creates fused composite particles without using a solvent. This process is suitable for making the coating process inexpensive. In addition, other wet methods can be applicable to achieve hard carbon layer by using the solvent soluble polymer resin and by using the additional heat treatment in inert atmosphere. The solvent can be an organic or in organic solvent. The exemplary thereof includes toluene, benzene, tetrahydrofuran, xylene, methanol, ethanol, hexane, cyclohexane, or water or a mixture thereof.

Safety Concerns

[0035] The high surface area anode material made from all the above methods can deteriorate the safety characteristics of the anode because of high reaction site with electrolyte on anode side. Thus, a water based styrene-butadiene rubber (SBR)/ carboxymethyl cellulose (CMC) binder can be used in the anode composition to manage the safety performance of the disclosed high surface area anode material. The SBR/CMC can be added when the electrode is made. But, it is not limited to the binder selection such as polyimide, PAA (Poly(acrylic acid)), and PVDF (Polyvinylidene fluoride), etc.

Examples:

[0036] The following describes manufacture and testing of anodes according to embodiments of the present disclosure and the prior art.

Example 1 - Al₂O₃ /pitch coating/ heat treatment in inert atmosphere

[0037] Al₂O₃ nanoparticles and pitch powder was added to an already spheroidized graphite powder in the following ratios: 2% Al₂O₃ and 3% pitch powder, relative to the spheroidized graphite, i.e., 2:3:95 Al₂O₃ pitch: graphite. This mixture was mechanically mixed using high shear and compressive forces to create fused, uniform composite particles. The pitch coating was carbonized in a tube furnace in an inert atmosphere (either nitrogen or argon) by first heating to 600°C at a rate of 4°C/min and then continuing to heat at a rate of

- 12 -

10°C/min up to 1000°C. The temperature was held at 1000°C for 2 hours before the furnace was allowed to cool to ambient temperature with no forced cooling. The gas flow rate was 2.75 SLPM.

[0038] The electrode was made by coating copper foil with a water-based slurry that contained (by weight) 41.4% Al₂O₃/pitch coated graphite, 0.724% SBR, 0.426% CMC, and 57.4% water. After drying at 100°C for 10 minutes, the electrode coating weight was approximately 5 mg/cm². The electrodes are then pressed to a thickness of 35 μm (one sided, not including foil thickness).

[0039] First charge capacity, reversible capacity, and efficiency were determined by CR2025 coin cells, using excess lithium as the counter electrode.

[0040] Cylindrical 18650 cells were built using a standard nanophosphate cathode. The cycle life was tested under +1C/-2C charge/discharge rates. High temperature storage was tested at 60°C, to determine resistance growth, recovered capacity, and retained capacity. Discharge rate was tested at 1A, 5A, 10A, 20A, and 30A at room temperature. Safety was tested using a nail penetration test that was conducted at 100% state of charge (SOC) and 60°C.

[0041] Example 2 - Al₂O₃ coating/heat treatment in oxidizing atmosphere

[0042] 2% Al₂O₃ nanoparticles were added to an already spheroidized graphite powder. This mixture was mechanically mixed using high shear and compressive forces to create fused, uniform composite particles. This powder was heat treated in air or another oxidizing environment. Compressed air was used at a flow rate of 1.14-4.25 SLPM. The furnace was heated to 550°C at a rate of 10°C/min, and held at 550°C for 8 hours. The furnace was then allowed to cool to ambient temperature with no forced cooling.

[0043] The electrode build method and testing by coin cell and 18650 cells was identical to the method used in Example 1.

[0044] Example 3 - Heat treatment in oxidizing atmosphere

[0045] Spheroidized graphite powder with a particle size ranging from 8-20µm (average 15 um) was heat treated in air or another oxidizing environment. Compressed air was used at a flow rate of 1.14-4.25 SLPM. The furnace was heated to 550°C at a rate of 10°C/min, and

- 13 -

held at 550°C for 8 hours. The furnace was then allowed to cool to ambient temperature with no forced cooling.

[0046] The electrode build method and testing by coin cell and 18650 cells was identical to the method used in Example 1.

[0047] Example 4 - Heat treatment in inert atmosphere

[0048] Spheroidized graphite powder with a particle size ranging from 8-20µm was heat treated in nitrogen by first heating to 600°C at a rate of 5°C/min and then continuing to heat at a rate of 10°C/min up to 1200°C. The temperature was held at 1200°C for 2 hours before the furnace was allowed to cool to ambient temperature with no forced cooling. The gas flow rate was 2.75 SLPM.

[0049] The electrode build method and testing by coin cell and 18650 cells was identical to the method used in Example 1.

[0050] Example 5 - Hard carbon precursor coating

[0051] 4% phenol-novolac resin powder (hard carbon precursor) was added to an already spheroidized graphite powder. This mixture was mechanically mixed using high shear and compressive forces which created fused, uniform composite particles. The hard carbon precursor coating was carbonized in a tube furnace in an inert atmosphere (either nitrogen or argon) by first heating to 150°C at a rate of 10°C/min. After holding at 150°C for 10 minutes, the rate was reduced to 4°C/min until 600°C was reached. Simultaneously, the heating rate was increased again to a rate of 10°C/min, up to 1000°C. The temperature was held at 1000°C for 2 hours before the furnace was allowed to cool to ambient temperature with no forced cooling. The gas flow rate was 2.75 SLPM.

[0052] The electrode build method and testing by coin cell and 18650 cells was identical to the method used in Example 1.

[0053] Comparative example 1 - Pitch coating

[0054] 5% Pitch powder was added to an already spheroidized graphite powder. This mixture was mechanically mixed using high compressive forces to create fused, uniform composite particles. The pitch coating was carbonized in a tube furnace in an inert

- 14 -

atmosphere (either nitrogen or argon) by first heating to 600°C at a rate of 4°C/min and then continuing to heat at a rate of 10°C/min up to 1000°C. The temperature was held at 1000°C for 2 hours before the furnace is allowed to cool to ambient temperature with no forced cooling. The gas flow rate is 2.75 SLPM.

[0055] The electrode build method and testing by coin cell and 18650 cells was identical to the method used in Example 1. Other performances were okay though. The cycle performance was terrible.

[0056] Comparative example 2 - Non-treatment: as received and spheroidized powder

[0057] The spheroidized graphite powder remained untreated and the electrode was built using a method identical Example 1. This powder had reasonable cycle performance but, poor storage performance.

[0058] The results of the above five examples and two comparative examples are depicted in tables 1-6, below. For each example, tables 1-6 lists the particle size (median particle diameter, in micrometers). Table 1 lists the 18650 initial performances (including initial capacity in ampere-hours, n-ICL (irreversible capacity loss after formation and storage at 45C for three days: Ampere-hours), and DCR (direct current resistance in milliohms). Table 2 lists the 18650 performance cycles (remaining % cell capacity after 300 cycles). Table 3 lists the storage performance (including % capacity retention and recovery after four weeks and % DCR growth after four weeks). Table 4 lists the coin cycle performance (remaining % cell capacity after 200 cycles). Table 5 lists the powder surface area (m²/g). Table 6 shows the XPS date including carbon, oxygen, and C=O bond percentages and the Raman spectroscopy data, including D/G peak ratios for the exemplary anode powders.

[0059] In order to determine the surface area of the powder, it was first degassed under nitrogen for a minimum of 3 hours at 190°C. It was then measured using the multi-point Brunauer-Emmett-Teller (BET) method. The equipment used was a Micromeritics Gemini 2360 with 10 relative pressure (P/P_o) targets between 0.03 and 0.29. The adsorption gas was nitrogen.

[0060] Particle size was determined using a Malvern Instruments Mastersizer 2000. The dispersant was water, with 4 drops Triton X-100 surfactant that had been diluted in water to a ration of 1:100.

- 15 -

[0061] Raman spectroscopy was conducted to check the surface properties of graphite powder by using Argon laser beam. That is, it has a peak G-band around 1580cm-1. G-band is a peak which is observed corresponding to a crystalline or ordered structure grown and formed by aromatic rings. In addition to G-band peak, it has another peak D-band around 1360cm-1. D-band is a peak which is observed corresponding to an irregular or disordered non-crystalline structure. The ratio of peak intensities D-band and G-band become larger as the ratio of disordered structure portion at the surface layer of graphite particles.

[0062] X-ray photoelectron spectroscopy (XPS) is an analytical technique for the study of thin material layers that uses x-rays to stimulate desorption of electrons in the near surface region of a specimen. The kinetic energy of these emitted electrons (called photoelectrons) is measured using a hemispherical electron spectrometer. The XPS spectra are generally plotted with binding energy on the horizontal axis and electron intensity on the vertical axis. For XPS analysis, samples were pressed into indium foil for support and attached to stainless steel holders using stainless steel screws and then installed in the vacuum chamber of a VersaProbe XPS Microprobe instrument manufactured by Physical Electronics USA of Chanhassen, MN. The chamber was evacuated to a base pressure of ≈1x10-8 torr. A hemispherical energy analyzer was used for electron detection. XPS survey spectra were collected to identify the elements present on the sample surfaces and multiplex spectra were collected to calculate elemental compositions. High-resolution spectral data were also collected for the C1s photoelectron line. Data were collected at the surface level using a monochromated aluminum K-alpha x-ray source. XPS spectral data are shown in table 1.

Table 1

		18650 initial performance		e
	Particle size, um (D50)	Initial capacity, Ah	n-ICL, %	DCR (mohm)
Example 1	15.5	1.02	13.23	29.3
Example 2	15.4	1.01	8.01	28.1
Example 3	15.3	1.05	13.95	29.9
Example 4	15.1	1.06	13.21	28.65
Example 5	15.9			
Comparative 1	15.5	1.00	14.17	29.4
Comparative 2	15.3	1.03	19.4	28.9

Table 2

		18650 cycle
	Particle size, um (D50)	Capacity retention %, 18650 at 300 cyles
Example 1	15.5	98
Example 2	15.4	88
Example 3	15.3	97
Example 4	15.1	96
Example 5	15.9	Х
Comparative 1	15.5	68
Comparative 2	15.3	96

Table 3

		Storage		
	Particle size, um (D50)	% Retention - 4 weeks	% Recovery - 4 weeks	%DCR Growth - 4 weeks
Example 1	15.5	84.6	89	10.9
Example 2	15.4	89.4	90.9	15.4
Example 3	15.3	88.3	90.3	12.3
Example 4	15.1	88.6	89.9	2.8
Example 5	15.9	х	Х	х
Comparative 1	15.5	88.8	90.2	16.8
Comparative 2	15.3	86.4	87.9	16.2

Table 4

	Particle size, um (D50)	Coin cycle Capacity retention %, at 300 cycles
Example 1	15.5	87
Example 2	15.4	X
Example 3	15.3	90
Example 4	15.1	X
Example 5	15.9	92
Comparative 1	15.5	х
Comparative 2	15.3	х

Table 5

	Particle size, um (D50)	Powder Surface Area cm₂/g
Example 1	15.5	5.67
Example 2	15.4	8.72
Example 3	15.3	6.43
Example 4	15.1	6.47
Example 5	15.9	16.3
Comparative 1	15.5	4.01
Comparative 2	15.3	6.75

Table 6

	XP	r'S	Raman Spectroscopy
	O, %	C=O, %	D/G Peak ratio
Example 2			0.18
Example 3	4.69	4.66	0.09
Example 4	2.27	4.25	0.18
Example 5	1.44	3.93	0.46
Comparative 1			0.53
Comparative 2	6.33	2.9	0.41

[0063] While examples of the present invention have been shown and described, it will be readily apparent to those skilled in the art that various changes and modifications may be made therein without departing from the scope of the invention.

- 19 -

What is claimed is:

- 1. An anode powder comprising:
 - a spheroidized graphite powder; and
 - a high surface area protective coating surrounding the graphite powder;

wherein, the coated powder has a higher surface area than the untreated graphite powder.

- 2. The anode powder of claim 1, wherein the anode powder has a particle size between about 5 um and about 20 um.
- 3. The anode powder of any of the preceding claims, wherein the anode powder has a surface area between about $5m^2/g$ and about $20m^2/g$.
- 4. The anode powder of any of the preceding claims, wherein the anode powder has a Raman spectroscopy peak intensity ratio of D band/G band less than 0.3.
- 5. The anode powder of any of the preceding claims, wherein the anode powder has a Raman spectroscopy peak intensity ratio of D band/G band above about 0.3.
- 6. The anode powder of any of the preceding claims, wherein the high surface area protective coating comprises a metal compound powder.
- 7. The anode powder of any of the preceding claims, wherein the metal compound powder comprises a metal oxide powder.
- 8. The anode powder of any of the preceding claims, wherein the metal oxide powder is selected from the group consisting of Al₂O₃, Y₂O₃, TiO₂, Cs₂O₃, ZrO₂, and ZnO.
- 9. The anode powder of any of the preceding claims, wherein the metal compound powder comprises a metal fluoride powder.
- 10. The anode powder of any of the preceding claims, wherein the metal fluoride powder is selected from the group consisting of AlF₃, ZrF₄, TiF₄, CsF₃, YF₃, and ZnF₂.
- 11. The anode powder of any of the preceding claims, wherein the high surface area protective coating comprises a mixture of metal compound powder and polymer.

12. The anode powder of any of the preceding claims, wherein the high surface area protective coating comprises a hard carbon coating.

- 13. The anode powder of any of the preceding claims, wherein the coating has an oxygen content of between about 1% and about 6%.
- 14. The anode powder of any of the preceding claims, wherein the coating has a carbon, oxygen double bond percentage of above about 3%.
- 15. A method of making an anode powder comprising:

 providing a spheroidized graphite powder;

 coating the graphite powder with a high surface area protective coating; and

 heat treating the coated graphite power to form a coated anode powder that has a
 higher surface area than the untreated graphite powder.
 - 16. The method of any of the preceding claims, wherein the anode powder has a surface area between about $5m^2/g$ and about $20m^2/g$.
 - 17. The method of any of the preceding claims, wherein the anode powder has a Raman spectroscopy peak intensity ratio of D band/G band less than 0.3.
 - 18. The method of any of the preceding claims, wherein the anode powder has a Raman spectroscopy peak intensity ratio of D band/G band above about 0.3.
 - 19. The method of any of the preceding claims, further comprising heat treating the coated graphite powder in an oxidizing atmosphere.
 - 20. The method of any of the preceding claims further comprising heat treating the coated graphite powder in an inert atmosphere.
 - 21. The method of any of the preceding claims, wherein coating comprises coating the spheroidized graphite powder with a metal compound powder.
 - 22. The method of any of the preceding claims, wherein coating comprises coating the spheroidized graphite powder with a metal oxide powder.
 - 23. The method of any of the preceding claims, wherein the metal oxide powder is selected from the group consisting of Al₂O₃, Y₂O₃, TiO₂, Cs₂O₃, and ZnO.
 - 24. The method of any of the preceding claims, wherein the coating comprises coating the spheroidized graphite powder with a metal fluoride powder.

25. The method of any of the preceding claims, wherein the metal fluoride powder is selected from the group consisting of AlF₃, ZrF₄, TiF₄, CsF₃, YF₃, and ZnF₂.

26. The method of any of the preceding claims, wherein coating comprises coating the spheroidized graphite powder with a hard carbon coating.

27. An anode comprising:

an anode layer disposed on a conductive sheet, said anode layer comprising an electroactive powder,

the electroactive powder comprising:

a spheroidized graphite powder; and

a high surface area protective coating surrounding the graphite powder;

wherein, the coated powder has a higher surface area than the untreated graphite powder.

28. A battery comprising:

a cathode;

an anode, the anode comprising an anode powder, the anode powder comprising:

a spheroidized graphite powder; and

a high surface area protective coating surrounding the graphite powder;

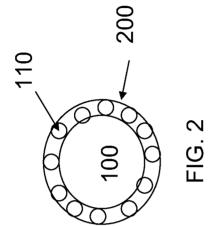
wherein, the coated powder has a higher surface area than the untreated graphite powder; and

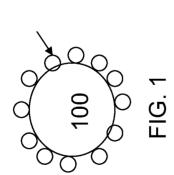
an electrolyte in ionic communication with both the cathode and the anode.

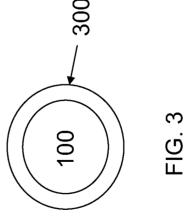
WO 2011/084817

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PCT/US2010/061631







INTERNATIONAL SEARCH REPORT

International application No. PCT/US2010/061631

IPC(8) - USPC -	A. CLASSIFICATION OF SUBJECT MATTER IPC(8) - H01M 4/70 (2011.01) USPC - 429/212 According to International Patent Classification (IPC) or to both national classification and IPC		
	DS SEARCHED Cumentation searched (classification system followed by company)	classification symbols)	
IPC(8) - H01	M 4/02, 4/583, 4/60, 4/70 (2011.01) 209, 212; 977/829, 847, 857	classification symbols)	
Documentati	on searched other than minimum documentation to the ext	tent that such documents are included in the	fields searched
Electronic da	ta base consulted during the international search (name of	data base and, where practicable, search ter	ms used)
Patbase, Go	ogle Patents		
C. DOCUI	MENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where ap	propriate, of the relevant passages	Relevant to claim No.
x	US 2009/0202917 A1 (SOTOWA et ai) 13 August 2009	(13.09.2009) entire document	1-3, 15, 27-28
Α	US 2005/0158550 A1 (OHTA et al) 21 July 2005 (21.07	7.2005) entire document	1-3, 15, 27-28
Α	US 6,770,399 B2 (UMENO) 03 August 2004 (03.08.20	04) entire document	1-3, 15, 27-28
Α	US 2002/0018934 A1 (MAJIMA et al) 14 February 2002 (14.02.2002) entire document 1-3, 15, 27-28		1-3, 15, 27-28
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Furthe	er documents are listed in the continuation of Box C.		
	Special categories of cited documents: "T" later document published after the international filing date or priority		
to be of	ament defining the general state of the art which is not considered e of particular relevance date and not in conflict with the application but cited to understand the principle or theory underlying the invention		
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cited to	ument which may throw doubts on priority claim(s) or which is do establish the publication date of another citation or other citation or other considered to involve an inventive step when the document is taken atone document is taken atone. "Y"		
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	cument published prior to the international filing date but later than "&" document member of the same patent family priority date claimed		
Date of the	actual completion of the international search	Date of mailing of the international sear	ch report
10 February	2011	02 MAR 2011	
Name and n	nailing address of the ISA/US	Authorized officer:	
Mail Stop PC	T, Attn: ISA/US, Commissioner for Patents	Blaine R. Copenhe	aver
	O. Box 1450, Alexandria, Virginia 22313-1450 acsimile No. 571-273-3201 PCT 169P-671-272-7774		

INTERNATIONAL SEARCH REPORT

International application No. PCT/US2010/061631

Box No. 11 Observations where certain claims were found unsearchable (Continuation of item 2 of first sheet)
This international search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:
1. Claims Nos.: because they relate to subject matter not required to be searched by this Authority, namely:
Claims Nos.: because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
3. Claims Nos.: 4-14, 16-26 because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).
Box No. III Observations where unity of invention is lacking (Continuation of item 3 of first sheet)
This International Searching Authority found multiple inventions in this international application, as follows:
1. As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2. As all searchable claims could be searched without effort justifying additional fees, this Authority did not invite payment of additional fees.
3. As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
4. No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:
Remark on Protest The additional search fees were accompanied by the applicant's protest and, where applicable, the payment of a protest fee. The additional search fees were accompanied by the applicant's protest but the applicable protest fee was not paid within the time limit specified in the invitation. No protest accompanied the payment of additional search fees.