UK Patent Application (19) GB (11) 2 145 160 A

(43) Application published 20 Mar 1985

(21) Application No 8419275

(22) Date of filing 27 Jul 1984

(30) Priority data

(31) 523056 (32) 15 Aug 1983 (33) US

(71) Applicant
Rolls-Royce Limited, (United Kingdom),
65 Buckingham Gate, London, SW1E 6AT

(72) Inventors

Douglas John Nightingale,
Benjamin Dixon Ward

(74) Agent and/or address for service K. Leaman, Rolls-Royce Limited, Patents Department, P.O. Box 31, Derby, DE2 8BJ (51) INT CL⁴ F02C 9/18 7/057 F02K 3/00

(52) Domestic classification F1J 2A1A 2A1E 3 B7G JVX F1G 5A 5C3A

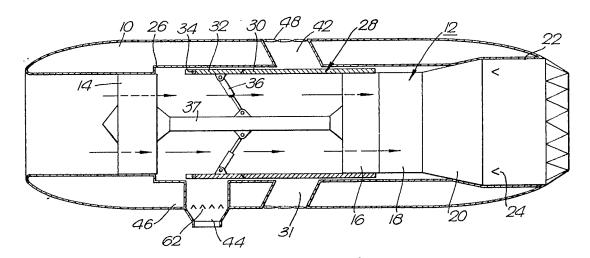
(56) Documents cited None

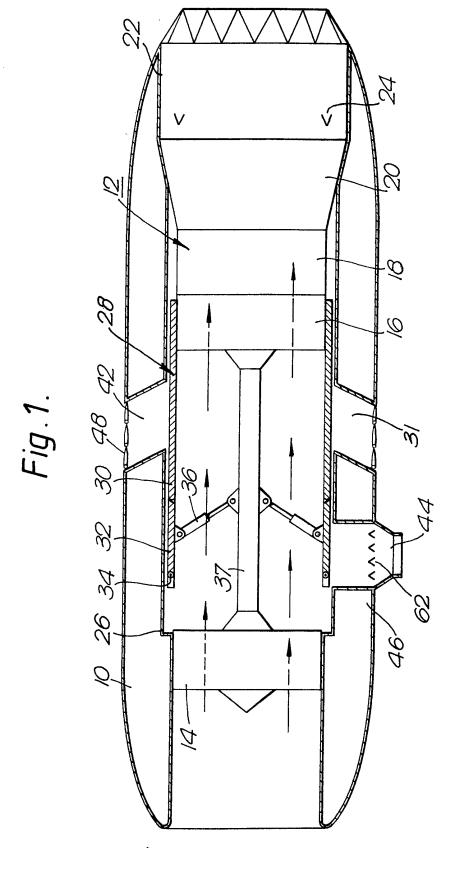
(58) Field of search F1G F1J

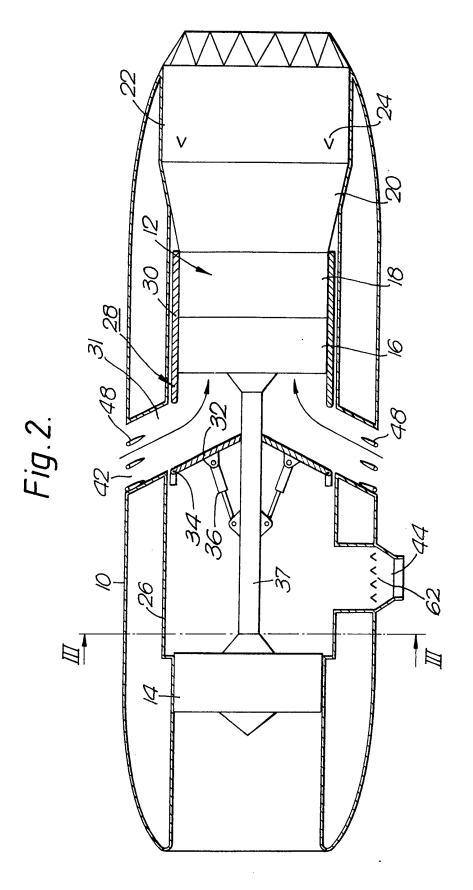
(54) Diverter valve for variable cycle gas turbine engine

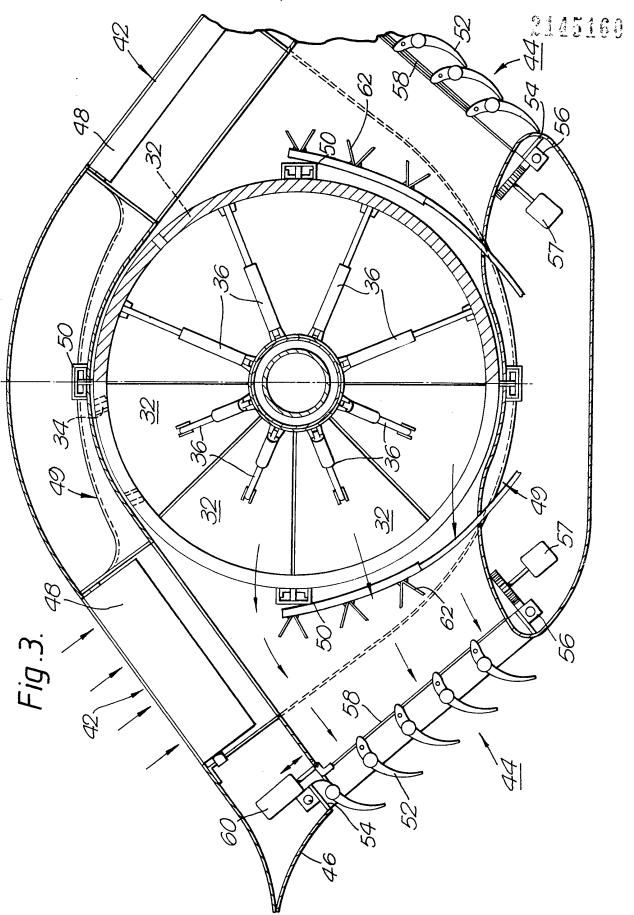
(57) The valve selectively changes the direction of flow of working fluid through a variable cycle engine which comprises first and second compressors 14, 16 spaced along a flow duct 26 having air intakes 42 leading to the second compressor 16 and outlets leading to thrust nozzles 44. The valve comprises a sleeve 30 axially movable along the duct 26 and having openings containing doors 32. Links 36 are connected to each of the doors 32 so that as the sleeve 30 is moved axially rearwardly from the position shown the doors 32 are pulled open to open the air inlets 42 and the nozzles 44 and simultaneously obturate the duct 26. In the position shown of the sleeve 30 the doors 32 and the sleeve 30 close off the air inlets 42 and nozzles 44 and open duct 26 to allow the first compressor 14 to supercharge the second compressor 16. In another arrangement the valve may divert the flow leaving first compressor 14 into a bypass duct.

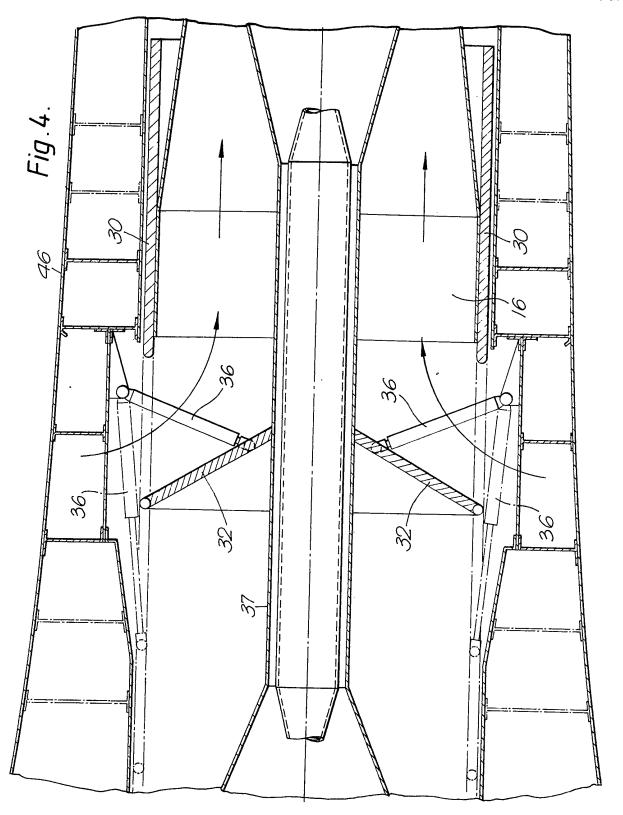
Fig.1.











GB 2 145 160 A 1

SPECIFICATION Valve for Diverting Fluid Flows in Turbomachines

This invention relates to variable cycle gas turbine engines, and in particular to valves for selectively changing the direction of flow of the working fluid through the engine.

The present invention is particularly concerned with variable cycle engines of the type generally disclosed in U.S. Patents 3913321 or 4038818 (assigned to Rolls-Royce Limited). In general, these engines comprise a first axial flow compressor and a core engine comprising, in flow series, a second compressor combustion equipment, and turbines to drive the first and second compressors, and the engine is capable of operating in two distinct modes. These modes are namely a "series flow" mode and a "parallel flow" mode. In the series flow mode the first and second compressors are connected in flow series

and the whole output flow of the first compressor supercharges the second compressor. In the "parallel flow" mode the output flow of the first compressor is prevented from supercharging the second compressor and is discharged to ambient air through either a by-pass duct or through fixed or vectorable discharge nozzles, and simultaneously an auxilliary air intake is opened up to allow air to enter the second compressor.

Variable cycle engines of the type described above offer many advantages, particularly for aircraft requiring vertical take-off and landing and also supersonic forward flight capabilities. The engine performance can be optimised for vertical take-off and landing and subsonic flight during the parallel flow mode and optimised for forward supersonic flight during the series flow mode. In this way, for vertical flight, the well proven advantages of engines such as the Rolls-Royce
 Limited Pegasus engine (used to power the British

Aerospace AV8A Harrier or the British
Aerospace/McDonnell Douglas AV8B) can be
exploited whilst enabling efficient use of the
engine in the series flow mode for supersonic
45 flight.

To enable the output flow from the first compressor to be redirected selectively for series or parallel modes of operation, it is usual to provide a diverter valve downstream of the first 50 compressor but upstream of the second compressor. Examples of such diverter valves are described in the above mentioned patents. The problems associated with prior known diverter valves reside in their complexity, weight, cost and 55 disruptive effect on the thermodynamic cycle of the engine during transition from the series flow mode to the parallel flow mode. It is very difficult to achieve transition from the series flow mode to the parallel flow mode without inducing variations 60 in flow conditions at the inlet to the second compressor. These variations may be localised and vary circumferentially around the fluid flow

annulus of the second compressor and have a

deleterious effect on the performance of the

65 engine. In general some of these problems are due to the speed of the operation of the diverter valve means and the fact that many movable parts such as doors and flaps are positioned in the airflow path and have to be operated in unison.

An object of the present invention is to provide a variable cycle engine of the type described above with a diverter valve means which is simple to operate, is lightweight, relatively inexpensive and provides a relatively uncluttered flow path during both modes of operation.

The invention will now be described, by way of example only, with reference to the accompanying drawings, in which:

Figure 1 and Figure 2 show schematically a variable cycle engine of the type described above incorporating the present invention; Figure 1 shows the engine in a "series flow" mode of operation and Figure 2 shows the engine in a "parallel flow" mode of operation.

Figure 3 is a cross-sectional view of part of the engine shown in Figures 1 and 2 illustrating in greater detail part of the valve for redirecting air flow through the engine.

Figure 4 is a cross-sectional view of a second 90 engine constructed in accordance with the present invention and shows the engine in a "parallel flow" mode of operation.

Referring to Figures 1 and 2, there is shown a generally round nacelle 10 which houses a gas 95 turbine engine 12 comprising, in flow series, a first axial flow compressor 14 and a core engine. The core engine comprises a second axial flow compressor 16, combustion means 18, turbine means 20 connected to the compressor means 14 and 16 to drive the compressor means, a jet pipe 22 and afterburning equipment 24.

The first and second axial flow compressors are spaced axially from each other by a duct 26 which houses a diverter valve 28. The diverter valve 28 consists of a hollow tubular sleeve 30 which is free to move axially along the duct 26. A plurality of doors 32 are circumferentially spaced around the engine axis inside the duct 26. One of the ends of each door is pivotally mounted on the 110 sleeve 30 at hinge 34. A plurality of telescopic

links 36 are connected at one of their ends to a tube which covers the shaft that connects the front compressor 14 to the turbine means 20. The other end of each link 36 is connected to one of

115 the doors at a point which is adjacent to the centre of pressure of the gases acting on each door, when the doors are in the position shown in Figure 2. The doors 32 are shaped and positioned such that in a first position of the sleeve 30 they

120 lie along the length of the duct 26 and obturate the openings 31 in the sleeve 30. In this position the sleeve 30, together with the doors 32, provide a flow path from the first axial flow compressor 14 to the second axial flow compressor 16, as

125 shown in Figure 1. This position of the sleeve 30 enables the engine to operate in a "series flow" mode of operation.

Figure 2 shows the engine in the "parallel flow" mode. In this mode the sleeve 30 is

GB 2 145 160 A

translated axially along the duct from the position shown in Figure 1. The telescopic links 36 are caused to pivot about their pivotal attachment to the tube 37 and cause the blocker doors to be swung inwards until each door co-operates with its adjacent door and with the tube 37 to obturate the duct 36. The doors 32 thereby uncover the openings 31 in the sleeve 30 and thereby open auxiliary air intakes 42. Translation of the sleeve 10 30 also uncovers the outlet to the front nozzles 44. This provides a flow path from the first axial flow compressor 14 to the front nozzles 44 and also provides a flow path whereby ambient air may flow into the auxilliary air intake 42 and into 15 the inlet of the second compressor 16.

Referring to Figure 3 there is shown a vertical cross-sectional view of an engine similar to that of Figure 2 taken along line III-III. The left hand side of Figure 3 shows the doors 32 in the 20 "parallel flow" position of Figure 2; the right hand side of Figure 3 shows the engine in the "series flow" mode of Figure 1. The aircraft fuselage 46 is effectively a double skin construction. The air intakes 42 are provided with shutters 48 which 25 blow inwards when the sleeve 30 is moved to unblock them. The air intakes 42 open into a plenum chamber defined by a wall 49 which conducts the air from the intakes 42 into the second compressor 16 downstream of the 30 blocker doors 32. The wall 49 houses tangential rollers 50 which are arranged along the length of the duct 26 to support the sleeve 30 as it is

translated axially. The front nozzles 44, which in Figures 1 and 2 35 are shown schamatically as projecting into the free air stream, are in fact housed within the double skinned fuselage 46 as shown in Figure 3 so as to reduce drag and provide a streamlined air frame for fast forward flight. In a preferred 40 embodiment, the nozzles 44 take the form of a plurality of vanes 52 pivotally mounted in a ring 54 supported in a bearing 56. The nozzles are capable of rotation in the bearing by means of an actuator 57, and all the vanes 52 of each nozzle 45 are linked together by a rod 58 which is moved by an actuator 60 (shown schematically). All the vanes of each nozzle are moved in unison for the purpose of varying the outlet area of the nozzles and by rotating the nozzles in their bearings 56 50 the thrust produced by the nozzles can be vectored thereby selectively to produce upward thrust (for VTOL) or forward thrust for forward flight. During the series mode of operation the vanes 52 close off the nozzles 44 to provide a 55 streamlined fuselage.

Upstream of the nozzles 44 there is provided a thrust augmentor in the form of a plurality of reheat gutters. In this way additional fuel can be burnt upstream of the nozzles to increase the 60 thrust produced by the nozzles and the nozzle outlet area increased by opening the vanes 52 to cope with the increased flow.

Referring to Figure 4 the engine is almost identical to that shown in Figures 1 and 2 except 65 that the links 36 for actuating the doors 32 are provided outside of the sleeve 30. Furthermore the links are not carried by the tube that covers the shaft 30. Instead the doors 32 are opened and closed by means of telescopic links 36 housed in 70 a recess which allows the links to be extended in the series mode to pull the door outwards, and compressed in the parallel mode to push the doors inwards. In other respects the construction of the engine is identical to that of Figures 1 to 3.

75 CLAIMS

1. A fluid flow diverter valve for a gas turbine engine of the type that comprises a fluid flow duct, first and second axial flow compressors spaced along the duct, a combustion means downstream of the compressors, turbine means downstream of the combustion means connected to the compressors to drive the compressors, one or more air outlet openings in the duct wall at a region between the first and second compressors, 85 and an auxilliary air intake in the duct wall spaced along the duct from the one or more outlet openings and located at a region between the one or more outlet openings and the second compressor, the valve comprising: a hollow 90 tubular sleeve extending co-axially along the duct, the sleeve being movable in directions along the duct, and being provided with one or more openings which in a first position of the sleeve uncover the auxilliary air intake in the duct wall; a 95 plurality of doors each of which is pivotally mounted at one of its ends on the sleeve, the doors being spaced around the axis of the duct and being shaped and positioned so that in a first position of the doors they lie along the length of the duct and at least one of the doors obturates 100 the one or more openings in the sleeve and in a second position of the doors the free end of each door is moved radially inwards and each door cooperates with the other doors and thereby 105 obturate the duct; a plurality of links each of which is pivotally mounted at one end to a member which is fixed and is pivotally connected at its other end to one of the doors; an actuator for translating the sleeve from the first position of 110 the sleeve where the sleeve and the doors obturate the one or more openings on the duct wall and the auxiliary air intake and provides a flow path from the first compressor to the second compressor, to a second position of the sleeve 115 where the links pull open the doors and move them to a position where they obturate the flow path from the first compressor to the second compressor and the sleeve uncovers the one or more outlet openings in the duct wall and 120 uncovers the auxilliary air intake.

2. A valve according to Claim 1 wherein the fixed member on which the links are pivotted is located inside the sleeve.

A valve according to Claim 1 wherein the 125 fixed member on which the links are pivotted is located outside the sleeve.

- 4. A valve according to Claim 1 wherein the one or more outlet openings lead to one or more vectorable nozzles.
- 5. A valve according to Claim 4 wherein a fuel5 burning means is provided upstream of the nozzles.

Printed in the United Kingdom for Her Majesty's Stationery Office, Demand No. 8818935, 3/1985. Contractor's Code No. 6378. Published by the Patent Office, 25 Southampton Buildings, London, WC2A 1AY, from which copies may be obtained.