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FUEL BURNER CONTROL SYSTEM

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FUEL BURNER CONTROL SYSTEM

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My invention relates to control systems for fuel burners and more particularly to such systems embodying electrical ignition means for igniting the fuel to initiate operation of the fuel burner.

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Difficulty has heretofore been encountered in the operation of fuel burners provided with such control systems since dangerous explosions are likely to occur if the operation of the ignition

10 means is inadvertently delayed until a substantial quantity of fuel has been delivered to the burner. That is, if a spark of the proper intensity is produced immediately when the burner motor is started or before any substantial quan-

15 tity of fuel has been discharged into the fire box, satisfactory ignition will take place. If, on the other hand, a spark of proper intensity is produced only after a comparatively large quantity of fuel has been supplied to the burner, there is
20 danger of an explosion.

The primary object of my invention is to provide a control system for fuel burners including an improved detector arrangement operable in response to an electrical discharge of sufficient

- 25 intensity to ignite the fuel and adapted to control the burner fuel supply mechanism in a manner such as to avoid the possibility of an explosion in case the igniter does not function properly.
- 30 More specifically, it is an object of my invention to provide an ignition detector arrangement for use in the control system described for fuel burners in which an oscillatory current is set up by the electrical discharge in the ignition means
- **35** and is utilized to condition the fuel supply of the burner for operation, the oscillatory current being of a relatively high frequency as compared to the frequency of the current supplied to the ignition means.
- 40 Further objects and advantages of my invention will become apparent as the following description proceeds and the features of novelty which characterize my invention are pointed out with particularity in the claims annexed to and 45 forming a part of this specification.

For a better understanding of my invention, reference may be had to the accompanying drawing in which the single figure is a diagrammatic representation of a fuel burner control system 50 embodying my invention and showing particu-

larly the circuit connections therefor. In the exemplary form shown in the drawing,

my invention is embodied in a control circuit adapted to control the operation of a conventional liquid fuel burner 10 in accordance with the temperature requirements of a room or other compartment supplied with heat from the burner. The burner 10 includes an electric motor 11 which serves to drive a pump 12 that supplies liquid fuel to a burner nozzle 13.

It is desirable that some arrangement be provided for automatically igniting the fuel discharged from the nozzle 13 when operation of the burner is initiated. Accordingly, a pair of electrodes 14 are arranged in spaced relation ad- 10 jacent the open end of the nozzle. An electrical discharge is produced between the electrodes by a suitable step-up ignition transformer 15 having inductively coupled primary and secondary windings. The electrodes 14 are connected across 15 the secondary winding of the ignition transformer 15 by conductors 16. The primary winding of the transformer 15 is connected to a source of electrical energy through a control circuit hereinafter described, which is adapted to ef- 20 fect cyclic operation of the fuel burner.

In accordance with my invention, I have provided an arrangement for controlling the fuel supply means of the burner 10 which is responsive to the passage of a substantially continuous 25 electric discharge between the electrodes 14 of sufficient intensity to ignite the fuel. This arrangement preferably includes an auxiliary circuit to which energy is transferred in response to changes in voltage or current at the electrodes 30 14, a capacitance and a coupling coil of low mutual inductance associated with the auxiliary circuit being utilized to render the auxiliary circuit resonant at a comparatively high frequency and thereby prevent the transfer of appreciable 35 energy to the auxiliary circuit at the frequency of the power supply to the ignition transformer 15. By comparatively high frequency is meant a frequency high as compared to the frequency of the power supply for the transformer 15. 40 Such a capacitance or inductance renders the detector arrangement insensitive to the opencircuit voltage and short-circuit current of the ignition gap while rendering it sensitive to impulses of energy transferred as a result of a dis-45 charge of predetermined intensity between the electrodes. Thus, a circuit including a capacitance and an inductance may be associated with the electrodes in such manner that an oscillatory current is set up therein upon the passage 50 of an electrical discharge of predetermined intensity between the electrodes 14. This oscillatory current may then be utilized to control the operation of the motor 11 of the burner 10.

In the construction illustrated, a condenser 55

17 is disposed within an air core inductance coll 18 and is connected in series relation therewith by conductor 19. The coil 18 is wound on a cylindrical insulating core 18ª. A second air core inductance coil 20 is arranged concentrically about the inductance coil 18 and is inductively coupled therewith. The coil 20 is wound on a cylindrical insulating core 20^a. The windings 18 and 20, and condenser 17 thus form a compact

- 10 unitary structure. The series connected winding 18 and condenser 17 are connected in shunt relation with the electrodes 14 by conductors 21. Consequently, upon the occurrence of a spark at the electrodes 14, a damped oscillatory current 15 flows in the circuit including the condenser 17
- and inductance coil 18. This current flowing through the inductance coil is induces a high frequency voltage in the secondary winding 20 which is utilized to control the operation of the 20 fuel burner 10 as is described below.
- It is desirable that fuel should be supplied to the burner 10 only in case a sustained electrical discharge of predetermined intensity is produced across the electrodes 14 as contrasted with a single 25 unrepeated discharge or weak continuous dis-
- charge which would not insure proper ignition of the fuel subsequently supplied to the nozzle 13. Consequently, I prefer to utilize the voltage induced in the secondary winding 20 to operate what
- 30 may conveniently be termed an integrating circuit control device; that is, a circuit control device which is responsive to the integrated rather than the instantaneous value of an electrical characteristic such as voltage or current.
- In the control circuit illustrated, an electro-35 thermal relay 22 serves as the integrating circuit control device. The relay 22 includes a U-shaped conductor or wire 23 having its ends secured to the opposite sides of an insulating projection 24
- 40 on the base 25 and passing over a peripherally grooved insulating disk 26 also mounted on the The conductor 23 has a comparatively base 25. high resistance as well as a high coefficient of thermal expansion. The terminals of the sec-
- 45 ondary winding 20 are connected to the ends of the conductor 23 by conductors 27. Consequently, the voltage induced in the secondary winding 20 will cause a current to flow through the conductor 22 and heat the same. When a sustained
- 50 electrical discharge of predetermined intensity sufficient to ignite the fuel passes between the electrodes 14, the integrated heating effect of the current flowing through the conductor 23 will result in a sufficient expansion of the con-
- 55 ductor 23 to cause it to operate a circuit controlling device. The electro-thermal relay is preferably so proportioned as to effect fairly rapid actuation thereof when a discharge of the required intensity or ignition value is produced.
- The circuit controlling elements of the electro-60 thermal relay 22 include a pair of normally open contacts 28. One of these contacts is mounted on the base 25 and the other is secured to a movable supporting arm including a channel-
- 65 shaped outer link 29, which is pivotally connected by a pin 30 to a second channel-shaped link 31. The link 31 is in turn rigidly secured to the outer end of a flexible spring arm 32 fixed at its other end to a projection 33 on the base
- 70 25. The conductor 23 passes through an aperture 34 formed in a projection 35, which extends laterally from link 29 through the side of link 31. The parts of the relay are so arranged that the resilient arm 32 normally tends to swing the 75 links 31 and 29 in a direction to close the con-

tacts 28. The conductor 23 passing through the aperture 34 in the projection 35 is made short enough, however, so that the contacts 28 are normally maintained open, the arm 32 being flexed toward the conductor 23. It will thus be ×. seen that when the conductor 23 is heated by the passage of a sustained current therethrough, its consequent elongation will permit the contacts 28 to be closed by the resilient arm 32.

Since accidental breakage of the conductor 23 19 would result in the same motion of the arm 32 as is caused by heating of the conductor, an arrangement has been provided to prevent sustained closure of the contacts 28 in case of such breakage. This arrangement includes a pin 36 15 rigidly secured to the base 25 and spaced a sufficient lateral distance from the link 29 that it does not engage the same during the normal operation of the relay. Upon breakage of the conductor 23, however, the arm 32 and its at- 20 tached links 31 and 29 swing in a clockwise direction farther than during their normal movement and, consequently, the link 29 is brought into contact with the pin 36. As a result, the link 29 is swung about its pivot 30, upon being 25 pressed against the pin 36, so that the contacts 28 are maintained in open position.

Contacts 28 are closed momentarily during the abnormal motion of link 29, but not long enough to initiate operation of the burner.

I have shown, for purposes of illustration, a specific preferred form of burner control in connection with the improved ignition detecting arrangement described, but it should be understood that any desired main control may be used. In 35 the specific arrangement illustrated, the control circuit is conditioned for operation by a main switch exemplified as a bimetallic thermostatic switch 37 which may be conveniently located within the chamber or room to be heated. 40

The exemplary control circuit is adapted to supply electrical energy to the ignition transformer 15 upon closure of contacts 38 of the thermostatic switch 37, when the temperature of the chamber in which the switch is located falls 45 to a predetermined value. Thus, upon closure of the contacts 38, actuating winding 39 of an ignition control relay, 40 is energized by current supplied thereto from secondary winding 41 of a 50 transformer 42.

Primary winding 43 of the transformer 42 is connected to a suitable source of alternating current 44, such as a household lighting system. through normally closed contacts 45 of a thermal safety switch 46. One terminal of the relay 55 winding 39 is connected to the transformer 42. by a circuit including a conductor 47 extending from the transformer secondary winding 41 to the thermostatic switch 37, contacts 38, conductor 48, normally closed contacts 49-50 and \$1-52 60 of a combustion responsive switch mechanism 53, conductor 54, heating coil 55 of the safety switch 46, and conductor 56. The other terminal of the relay winding 39 is connected to the second terminal of the power transformer secondary 65 winding by a conductor 57. Consequently, upon closure of the contacts 38 of the thermostatic switch 37, the energizing circuit for the relay winding 39 is completed and contacts 58 and 59 of the ignition relay 40 are closed. 70

The closure of ignition relay contacts 59 completes an energizing circuit for the primary winding of the ignition transformer 15. Thus, one terminal of the primary winding of the ignition transformer is permanently connected to one side 75

of the power supply line 44 by a conductor 60. The other terminal of the transformer primary winding is connected to the other side of the supply line 44 through a conductor 61, contacts 59,

conductor 62 and contacts 45 of safety switch 46. The contacts 58 of the ignition control relay 40 serve to shunt out the main thermostatic switch 31 from the control circuit of the ignition control relay. Thus, upon closure of the contacts 58, the

10 thermostatic switch is shunted out of the energizing circuit of the relay winding 39 by conductors 64 and 65.

Upon energization of the ignition transformer 15 described, an electric discharge is produced 15 between the electrodes 14 and a high frequency voltage is induced in the secondary winding 20 of the ignition detector. After the high fre-

- quency current has flowed through the conductor 23 of the electro-thermal relay 22 for a sufficient 20 time, the conductor 23 is elongated due to thermal
- expansion so as to permit the closure of contacts 28.

The contacts 28 are associated with the energizing circuit of the burner motor 11 in such 25 manner that the burner motor is conditioned for operation upon the closure of these contacts. Thus, the energizing circuit of actuating winding 66 of a motor control relay 67 is completed upon closure of the contacts 28. Current is supplied

30 to the winding 66 from one terminal of the secondary winding 41 of the transformer 42 through conductor 47, conductor 68, contacts 28 and conductor 69. The other terminal of the secondary winding 41 of the transformer 42 is permanently connected to the relay winding 66 through conductors 57 and 70.

Energization of the winding 66 causes the closure of contacts 71 and 72 of the motor control

- relay 67, which in turn results in the energization 40 of burner motor 11. Thus, one terminal of the motor 11 is permanently connected to one side of the supply line 44 through conductor 60, while the other terminal of the motor 11 is connected to the other side of the supply line 44 through
- 45 conductor 73, contacts 71, conductors 74 and 62 and contacts 45 of safety switch 46. The motor 11 is thus set in operation and fuel is supplied under pressure to the nozzle 13 where it is ignited by the electrical discharge between the electrodes 50 f4.

It will be seen that if a sustained electrical discharge of predetermined strength is not had at the electrodes 14, either because of short circuiting of the gap or failure of the gap voltage

- 55 due to any other cause, the conductor 23 will not be heated sufficiently to permit closure of the contacts 28. In such case, the motor control relay \$7 will not be energized and no fuel will be supplied to the nozzle \$3. Hence, with the circuit
- 60 arrangement described, the existence of a suitable ignition discharge at the electrodes 14 is a positive prerequisite to the operation of the burner fuel supply means.
- If satisfactory operation of the ignition means 65 is not had within a predetermined time, contacts 45 of the safety switch 46 are opened, disabling the entire control system as is hereinafter described. The safety switch 46 can only be reclosed by subsequent manual operation so that
- 70 the attention of the operator is drawn to the failure of the ignition apparatus to operate properly. The combustion responsive switch 53 is adapted to remove the motor control relay 67 from the control of the ignition detecting device and place

75 it under the control of the main thermostatic

switch 37 as well as subsequently to deenergize the ignition transformer 15 in the event of successful ignition of the fuel. In order to effect this operation, the mechanism **53** is of the usual thermostatic type comprising a bimetallic thermostatic member 75 located within the furnace flue or stack 76, which is heated by the products of combustion leaving the furnace. When the thermostatic element 75 becomes heated, it rotates an actuating member 77 in a counterclock- 10 wise direction, thus opening the contacts 49 and 50. Upon further rotation of the actuating member 77, contacts 78 and 79 are closed, thus completing an energizing circuit for the actuating winding 66 of the motor control relay 67 inde- 15 pendent of the electro-thermal relay contacts 28. This circuit extends from the secondary winding of the transformer 42 through conductor 47, contacts 38 of the main switch 37, conductor 48, contacts 78-79, conductor 80, protective resistance 20 81, conductor 82, contacts 72 of the motor control relay 67, and conductor 83 to one terminal of winding 66. The other terminal of the relay winding 66 is, of course, permanently connected to the transformer 42 through conductors 57 25 and 70.

Upon further rotation of the actuating member **17** of stack switch **53**, contacts **51**—**52** are opened, breaking the energizing circuit of the actuating winding **39** of the ignition control relay **40**. The **30** winding **39** is thus deenergized permitting the contacts **58** and **59** to open, which in turn breaks the energizing circuit of the ignition transformer **15**. The electrical discharge between the electrodes **14** is thus terminated when the heating of **35** the switch **53** indicates that satisfactory ignition of the fuel has been effected.

From the foregoing, it will be seen that the energizing circuit of the motor control relay 67 is in this part of the cycle, controlled by the con- 40 tacts 38 of the main thermostatic switch 37. After the fuel burner has been in operation for a sufficient length of time to raise the chamber temperature above the control point of the thermostatic switch 37, the contacts 38 are again 45opened. The energizing circuit for actuating coil 66 of the motor control relay 67 is thus broken, thereby opening contacts 11 and 12 and in turn deenergizing the burner motor 11 to shut off the burner. The cycle described above is repeated 50 at intervals in order to maintain the temperature of the chamber being heated within predetermined temperature limits.

It will be noted that the heating coil 55 of the safety switch 46 is energized immediately upon 55 the initiation of the control cycle by the main control thermostatic switch 37. This heating coil 55 is so positioned with respect to a bimetallic thermostatic latch 84 that the latter will be heated so as to permit the contacts 45 of the safety 60 switch to open after a predetermined length of time. Thus, if satisfactory ignition is not had within a predetermined interval of time, the contacts 45 of the safety switch 46 will be opened, deenergizing the actuating winding 39 of the igni- 65tion control relay 40 and rendering the apparatus inoperative until the safety switch 46 is manually reset. If satisfactory ignition of the fuel is effected, however, the energizing circuit for the heating coil 55 of the safety switch is opened by 70contacts 51 and 52 of the combustion responsive switch 53.

It will thus be seen that I have provided a compact and simple arrangement for positively controlling the fuel supply of a fuel burner in 75 such manner that no fuel will be supplied to the burner until satisfactory operation of the ignition means thereof is had. Moreover, the circuit arrangement of the improved ignition detector means is such that normal cyclic operation

of the burner under control of a main thermostatic switch is permitted.

Although I have shown a particular embodiment of my invention in connection with a liquid 10 fuel type burner, I do not intend to limit the invention to the particular construction shown and described but aim to cover all modifications falling within the spirit and scope of the inven-

tion as expressed in the appended claims.

15 I claim as my invention:

1. A control system for a fuel burner comprising, in combination, electric motor driven means for supplying fuel to the burner, a supply circuit for said means, a spark igniter circuit including 20 spark electrodes associated with said fuel supply

means and a low frequency current supply for said electrodes, a high frequency circuit associated with said ignition circuit and energized to high frequency oscillations solely by normal spark

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at said electrodes, a thermally operated time delay switch having the heating element thereof energized solely by said high frequency circuit, said time delay switch having its contacts arranged to control said first-named circuit whereby to initiate fuel supply to the burner only after a sustained normal spark has occurred at said electrodes.

2. A control system for a fuel burner comprising, in combination, means for supplying fuel 10 to the burner, a spark igniter circuit including spark electrodes associated with said fuel supply means and adapted to be connected to a low frequency current supply source, a high frequency circuit associated with said ignition circuit and energized by high frequency oscillations solely by normal sparking between said electrodes, and control means responsive only to a sustained energization of said high frequency circuit for a predetermined time interval for governing said fuel supply means whereby to initiate fuel supply to the burner only after a sustained normal spark has occurred at said electrodes.

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