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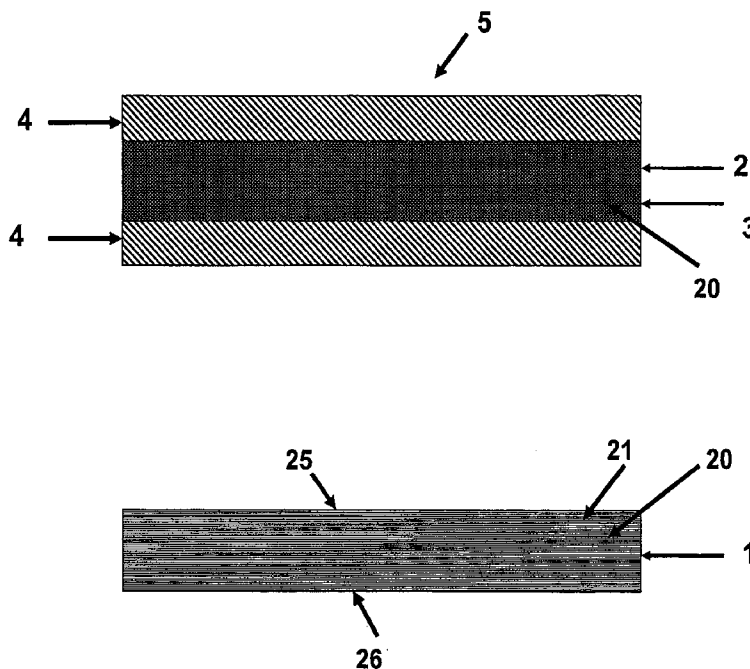
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(54) Title: INFLATABLE IMBIBED POLYMER DEVICES



(57) Abstract: The present invention provides a stretchable material suitable for use in an inflatable medical device. The stretchable material has at least one reinforcing polymer layer with a top and bottom side forming a porous matrix which is imbided with a sealing material to infiltrate and substantially seal spaces of the porous matrix and extend beyond the reinforcing polymer layer to form a surface coating.

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TITLE OF THE INVENTION

INFLATABLE IMBIBED POLYMER DEVICES

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BACKGROUND OF THE INVENTION

The present invention relates to a unique material suited for use in balloon catheters and, more particularly, to a low profile non-shortening wrapped balloon configured to expand to a predetermined diameter upon application of a predetermined pressure thereto. The unique properties of the material of the present invention enable wrapped balloons to be made without the use of internal bladders.

Balloon catheters are well known in the art. Such catheters are employed in a variety of medical procedures, including dilation of narrowed blood vessels, placement of stents and other implants, temporary occlusion of blood vessels, and other vascular uses.

In a typical application, the balloon is advanced to the desired location in the vascular system. The balloon is then pressure-expanded in accordance with a medical procedure. Thereafter, the pressure is removed from the balloon, allowing the balloon to contract and permit removal of the catheter. It is to be appreciated that prior art balloons are typically formed of an elastomeric material which is readily pressure-expanded, and also readily contracts upon removal of the inflation pressure.

Some catheter balloons constructed of both elastomeric and non-elastomeric materials have been described previously. US Patent No. 4,706,670 describes a balloon dilatation catheter constructed of a shaft made of an elastomeric tube and reinforced with longitudinal inelastic filaments. This device incorporates a movable portion of the shaft to enable the offset of the reduction in length of the balloon portion as the balloon is inflated. A major drawback to balloons of this type is the need for a bladder which increases the profile of the balloon.

Traditionally, a fluoropolymer matrix which is filled with a coating that does not extend outside the matrix permits the coating to pull away from the matrix causing holes that eventually demonstrate themselves in a "weeping" manner on the balloon. This is believed to be due to the inadequate adhesion strength between the matrix and the coating as well as the stress concentrations at those interfaces.

There is a need in the art for a low profile wrapped balloon which does not lengthen or shorten upon inflation and has the ability to withstand inflation pressure strain without disruption, while still remaining watertight without the use of a separate bladder that adds to the balloon profile. The present
5 invention fulfills this need by providing a unique material which allows for the elimination of a bladder. It also allows the balloon to readily expand under pressure without leaking.

SUMMARY OF THE INVENTION

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The present invention provides a stretchable material comprising a reinforcing polymer having a porous matrix with void spaces and a sealing material imbibed into the reinforcing polymer substantially sealing the porous matrix void spaces and extending beyond the reinforcing polymer matrix to
15 form a surface coating that can be stretched without the occurrence of holes through the thickness of the material. In a preferred embodiment, a low angle wrapped catheter balloon is comprised of a material which stretches primarily in one direction and less than 54.7 degrees is formed with said material. As the balloon is inflated to its working diameter, the wrapped material rotates towards
20 the balanced force angle of 54.7 degrees. When rotating, the wrapped material also strains perpendicular to the length of the wrap according to the following geometric relationship ($Width_F = Width_I \times (\cos \theta_F / \cos \theta_I)^2 \times (\tan \theta_F / \tan \theta_I)$) where F is Final and I is initial. This strain can exceed 500 percent in some balloons depending on the deflated to inflated diameter ratio. The present
25 invention allows for this strain to occur without inducing holes or compromising the sealing coating. The material is suitable for liquid or gas impermeable applications.

The present invention further provides a balloon catheter comprising a tubular catheter shaft having a longitudinal axis and an inflatable bladderless
30 wrapped balloon affixed to the catheter shaft wherein the balloon comprises at least one reinforcing polymer layer with a top and bottom side forming a porous matrix, said porous matrix is imbibed with a sealing material that infiltrates and substantially seals void spaces of the porous matrix and extends beyond the reinforcing polymer layer to form a surface coating. The surface coating is
35 formed on at least one side of the reinforcing polymer layer.

The present invention yet further provides a balloon catheter with a surface coating thickness which is modulated to allow for controlled porosity when strained due to inflation.

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DESCRIPTION OF THE DRAWINGS

Figures 1A and 1B show cross sections of a reinforcing polymer. Figure 1A is the reinforcing polymer prior to imbibing. Figure 1B shows the imbibed reinforcing polymer with two surface coatings.

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Figure 2 shows a cross section of a reinforcing polymer with a single surface coating.

Figure 3 shows a composite film wrapped at a low angle on a release coated core wire.

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Figure 4 shows a cross section of a balloon material layer wrapped on a wire.

Figure 5 shows a bladderless balloon with a heat treated inflation region.

Figure 6 shows a schematic diagram depicting attachment via two sealing means of a bladderless balloon to a hypotube.

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Figure 7 shows a cross section of a single coated anisotropic material

Figure 8 shows a cross section of a bladderless balloon for fluid delivery at higher pressures.

Figure 9 shows non-distensible seal wrapped onto a balloon material layer.

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Figure 10 shows a cross section of a non-distensible seal wrapped onto a balloon material layer.

DETAILED DESCRIPTION OF THE INVENTION

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It has been found that a reduction in the profile of prior art balloons using elastomeric bladders and outer reinforcing materials can be achieved using the materials of the present invention. The material of the present invention combines a reinforced matrix with elastomeric properties. This unique combination allows balloons to be formed without the need for a separate elastomeric bladder, thus providing reduced profiles. The present invention provides a reinforcing polymer suitable to withstand strain in one or more directions without leaking, and is well suited for medical devices and

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inflatable devices. The material is particularly well suited for catheter balloon applications requiring a small initial profile for entry into a vessel. The material is preferably stronger in a longitudinal direction as opposed to its transverse direction.

5 There are numerous porous membranes which would be suited to use for an imbibed polymer. As shown in the following examples, ePTFE has been used to demonstrate the present invention based upon preferred properties of thinness and drapability. While reinforcing polymers with anisotropic properties are preferred for embodiments such as catheter balloons, an isotropic
10 reinforcing polymer may be desired for other imbibed material embodiments.

 As shown in Figures 1A and 1B, the reinforcing polymer 1 comprises at least one matrix 20 with void spaces 21. The matrix should have a top side 25 and a bottom side 26. A sealing material 3 is imbibed into the reinforcing polymer 1 to form an imbibed reinforcing polymer 2. The sealing material 3
15 substantially seals the porous matrix void spaces 21 and extends beyond the reinforcing polymer matrix 20 to form a surface coating 4 on one side of the reinforcing polymer 1, as shown in Figure 2; or both sides of the imbibed reinforcing polymer 2, as shown in Figure 1A. The sealing material 3 must be of a sufficient quantity not only to seal void spaces in the reinforcing polymer,
20 but to extend beyond the matrix of the reinforcing polymer and form a continuous layer as a surface coating 4. The surface coating forms a continuous layer that is free from holes and extends beyond the matrix of the reinforcing polymer. The reinforcing polymer may be comprised of any porous polymer, including but not limited to fluoropolymers, polyamides, polyesters,
25 polycarbonates, microporous polyolefins, or UHMW polyurethanes. The matrix can be that of a form typical of any oriented matrix, including ePTFE.

 The composite film of the present invention comprises a porous reinforcing layer and a continuous polymer layer. The porous reinforcing polymer layer is preferably a thin, strong porous membrane that can be made
30 in sheet form. The porous reinforcing polymer can be selected from a group of polymers including, but not limited to, olefin, PEEK, polyamide, polyurethane, polyester, polyethylene, and polytetrafluoroethylene. In a preferred embodiment, the porous reinforcing polymer is anisotropic such that it is highly oriented in the one direction. An ePTFE membrane with a matrix tensile value
35 in one direction of greater than 690 megapascals is preferred, and greater than 960 megapascals is even more preferred, and greater than 1,200 megapascals is most preferred. The exceptionally high matrix tensile value of ePTFE

membrane allows the composite material to withstand very high hoop stress in the inflated balloon configuration. In addition, the high matrix tensile value of the ePTFE membrane makes it possible for very thin layers to be used which reduces the deflated balloon profile. A small profile is necessary for the balloon
5 to be able to be positioned in small arteries or veins or orifices. In order for balloons to be positioned in some areas of the body, the balloon catheter must be able to move through a small bend radius, and a thinner walled tube is typically much more supple and capable of bending in this manner without creasing or causing damage to the wall of the vessel.

10 In another preferred embodiment, the ePTFE membrane is relatively mechanically homogeneous. The mechanically balanced ePTFE membrane can increase the maximum hoop stress that the composite film made therefrom can withstand.

The continuous polymer layer of the present invention is coated onto at
15 least one side of the porous reinforcing polymer. The continuous polymer layer is preferably an elastomer, such as, but not limited to, aromatic and aliphatic polyurethanes including copolymers, styrene block copolymers, silicones, preferably thermoplastic silicones, fluoro-silicones, fluoroelastomers, THV and latex. In one embodiment of the present invention, the continuous polymer
20 layer is coated onto only one side of the porous reinforcing polymer. The continuous polymer layer is coated onto both sides of the porous reinforcing polymer. In a preferred embodiment, the continuous polymer layer is imbibed into the porous reinforcing polymer and the imbibed polymer fills the pores of the porous reinforcing polymer.

25 The continuous polymer layer can be applied to the porous reinforcing polymer through any number of conventional methods including, but not limited to, lamination, transfer roll coating, wire-wound bar coating, reverse roll coating, and solution coating or solution imbibing. In a preferred embodiment, the continuous polymer layer is solution imbibed into the porous reinforcing
30 polymer. In this embodiment, the continuous polymer layer is dissolved in a suitable solvent and coated onto and throughout the porous reinforcing polymer using a wire-wound rod process. The coated porous reinforcing polymer is then passed through a solvent oven and the solvent is removed leaving a continuous polymer layer coated onto and throughout the porous reinforcing
35 polymer. In some cases, such as when silicone is used as the continuous polymer layer, the coated porous reinforcing polymer may not require the removal of solvent. In another embodiment, the continuous polymer layer is

coated onto at least one side of the porous reinforcing polymer and maintained in a "green" state where it can be subsequently cured. For example, an ultraviolet light (UV) curable urethane may be used as the continuous polymer layer and coated onto the porous reinforcing polymer. The composite film
5 comprising the porous reinforcing polymer and the UV curable urethane continuous polymer layer can then be wrapped to form at least one layer of the balloon and subsequently exposed to UV light and cured. A pass is a number of layers applied in a wrapping event. A layer may comprise a single layer of composite film wrapped around the balloon.

10 Some typical examples of the reinforcing polymer can generally be found at US Patent No. 5,476,589 and US Patent Application No. 11,334,243. The surface coating is of a sufficient thickness to maintain a watertight matrix when the sealing material is stressed, inflated, or strained. The sealing material 3 is typically an elastomeric polymer or viscous flow material, such as
15 an elastomer, urethane, fluoropolymer, nylon, polyether block amide, PEBA, or other suitable material.

In one embodiment, a catheter balloon may be constructed which changes in diameter by up to 700 percent. During the diameter growth, the balloon wraps rotate towards the balanced force angle of about 54.7 degrees,
20 while the elastomer imbibed reinforcing polymer will strain perpendicular to the wrap length up to 400 – 500 percent. This aspect is unique, the perpendicular strain caused by the rotation to the balanced force angle allows higher radial elongation of the balloon at less strain on the elastomer, as compared to a balloon created from the elastomer alone. This attribute of the present
25 invention provides improved balloons with better recovery and which are of a higher strength and higher burst pressure than traditional balloons. Further, the diameter of the elastomer balloon may be formed to limit the diameter growth once the balanced forces angle is reached. This also allows for symmetrical inflation of the balloon.

30 The wrap layers when configured in accordance with the present invention form a balanced force angle which prevents the layers from incurring transverse strain as the balloon inflates. Transverse strain is the tendency for individual material layers to stretch or strain perpendicular to the wrap angle. For this reason, anisotropic materials are used which are highly oriented in the
35 direction of the wrap angle to allow for the strain in the perpendicular direction. Additionally, the balloon exhibits essentially radial symmetry upon inflation. The balloon is wrapped by winding layers at opposing directions to one another

until a desired thickness is obtained. The balloon material passes may be comprised of the same materials or different materials. While the thickness of the materials may vary, for vascular use it is advantageous to use balloon material that is less than 2 micrometers thick.

5 The following equation is useful for predicting the amount of transverse strain upon the elastomer imbibed reinforcing polymer during inflation of a balloon catheter of the present invention:

10 initial width / final inflated width = $1/(\cos \alpha_f / \cos \alpha_i)^2 \times (\tan \alpha_f / \tan \alpha_i)$

 wherein α is defined as the angle between the longitudinal axis of the balloon and the angle of the wrapped elastomer imbibed reinforcing polymer.

15 In certain applications, it may be desirable that the surface coating is formed at a thickness which allows for controlled porosity when strained due to inflation. Such controlled porosity allows delivery of a liquid in therapeutic quantities. The combination of the surface coating 4 and the imbibed

20 reinforcing polymer 2 provides a composite film 5. The composite film 5 has a surface coating possessing a greater strain capability than either the sealing material 3 or the reinforcing polymer 1 alone. In certain preferred embodiments it is desirable to use ePTFE as the reinforcing polymer 1. To produce a thin

25 strong reinforcing polymer with a desired mass and thickness, the polymer is expanded longitudinally and transversely prior to imbibing with a sealing material 3. The longitudinal expansion ratio is greater than the transverse expansion ratio. As shown in Figure 3, the composite film 5 of the present invention is suited for use as a balloon material layer 8. The composite film 5

30 can be cut or formed in longitudinal strips or narrower pieces suitable for wrapping the composite film around a core wire 6 or mandrel with or without a release coating 7. The angle of the wrap can vary depending upon the desired attributes of the finished balloon. Several different areas of differing wrap angles may exist on one balloon. In one desired embodiment the wrap angle of the composite film is between 2 and 54 degrees with respect to the longitudinal

35 axis of the balloon, and more preferably less than ten degrees with respect to the longitudinal axis of the balloon. The composite film can be wrapped at an angle with respect to the longitudinal axis which promotes inflation to a defined

diameter, then wrapped in a reverse direction at an opposing angle to the first pass for a plurality of passes forming directional layers. Upon inflation, the layers of opposing directions form a balanced force angle approaching 54 degrees relative to each other. As shown by the cross section in Figure 4, the balloon material layer 8 can be wrapped in layers around the core wire 6 (or around a release coating 7 on the wire) to form a tubular structure suitable for use as an inflatable balloon when sealed at the ends. The tubular structure may be subjected to heat and inflation pressure to form a bladderless balloon with or without the use of a mold. The balloon of the present invention does not require a bladder, but may be constructed with a bladder if desired. In one embodiment the balloon is comprised of at least two helically oriented wrap layers which form an angle of approximately 54 degrees with respect to each other upon inflation. This angle allows the forces within the filament wound pressure vessel to be at equilibrium. The inflatable balloon of the present invention further exhibits radial symmetry upon inflation and non-foreshortening. By non-foreshortening it is meant that the length of the balloon does not change by more than ten percent (more preferably 5 percent and even more preferably 2 percent) upon inflation to a rated burst pressure. As shown in Figure 5, the composite film 5 can be used as a balloon material layer 8 and formed into a bladderless balloon 9 suitable for use as a catheter. Upon inflation, the inflated region 10 expands into a predetermined shape.

Figure 6 shows a balloon catheter device 9 with a bladderless balloon attached to a hypotube. The bladderless balloon is attached to the hypotube or catheter shaft via a seal or other sealing means 13. The material of the present invention may be used as the sealing means. For example in the present invention the sealing means holds the balloon material layer 8 in contact with the hypotube 11 so that the balloon may be inflated without pressure loss. The hypotube 11 has a longitudinal axis around which the inflatable balloon is affixed. The hypotube may further comprise a hypotube wrap layer 12 surrounding the hypotube. When the hypotube wrap layer is present, the balloon material is affixed to the hypotube wrap layer via a sealing means to form a seal.

Figure 7 shows a reinforcing polymer 1 imbued with a sealing material 3 to form an imbued reinforcing polymer 2 having a double surface coating 4 layer, and forming a stretchable anisotropic material. A single surface coating may be used when only one side of the material wrap is desired to be coated.

The surface coating may be present on the inside surface or the outside surface of the balloon.

In another embodiment, Figure 8 shows a cross section of a bladderless balloon having a surface coating of a thickness allowing for controlled porosity when strained due to inflation. Controlled porosity allows delivery of a liquid from one side of the imbibed reinforcing polymer to the other side. The controlled porosity is a tortuous path, thereby allowing the therapeutic liquid to weep, (form droplets on the surface of the balloon). In another embodiment, the bladderless balloon having a surface coating of a thickness allowing for controlled porosity, weeps only at high pressure. As shown in Figure 8, the imbibed reinforcing polymer 2 has at least one surface coating 4 formed by the sealing material 3. The imbibed reinforcing polymer is formed into a bladderless balloon 9 having stretchable anisotropic material 14 properties. When the bladderless balloon is inflated by a fluid, small openings occur in the surface coating which allow movement of the fluid from the interior side of the balloon through the imbibed reinforcing polymer 2 to the outside of the balloon. Delivery of therapeutic liquid agents may be facilitated using a bladderless balloon comprised of an imbibed reinforcing polymer with a controlled porosity. This controlled porosity is able to withstand pressures greater than 10 p.s.i., before allowing fluid movement from the interior to the exterior side of the balloon.

Figure 9 shows that the bladderless balloon may be constructed to include at least one non-distending layer 7 to provide a desired shape to the bladderless balloon or to provide a continuous integrated seal on an inflatable balloon. The continuous integrated seal may be formed by using or providing a first balloon material layer 8 which is configured to form a desired balloon shape. The sealing material may be a balloon material layer 8, as such, an ePTFE reinforcing polymer imbibed with sealing material 3. The balloon shape is then wrapped with a wrap layer around said first balloon material layer so that the angle of the wrap changes to wrap at least one wrap layer at an angle sufficient to create seal over the first balloon material layer upon inflation. A second balloon material layer may then be wrapped around the seal to increase the bonding surface area of the seal if desired. In this manner the seal is located between two balloon materials to provide a gentle failure mode on a bladderless balloon. The material composite may be used to comprise the non-distensible regions. As shown in Figure 9, the core wire 6 may be provided with a release coating 25. The release coating may be of a desired thickness

to provide a desired inner diameter on the finished balloon. The release coating has a balloon material layer wrapped and set around the core wire 6 to provide a bladderless balloon.

Figure 10 provides a cross section of a non-distensible seal on a bladderless balloon. The non-distensible seal is integrated as a wrap layer on top of the balloon itself. It may be wrapped at the same time as the bladderless balloon by adjusting the wrap angle of the composite film wrap. The balloon material layer 8 is then wrapped with a non-distending layer 7 in desired areas to provide the bladderless balloon with non-distending regions, as shown in Figure 9. The non-distending regions should be comprised of balanced multiple wrap layers oriented so that the number of passes of wrap lying in one direction is equal to the number of passes of wrap in an opposite overlying direction.

The following examples are offered for illustrative purposes only and are not intended to limit the teaching of the present invention.

EXAMPLES

Example 1 – Composite Film

The ePTFE reinforcing polymer 1 used to make the composite film was made in accordance with the teachings found in US Patent No. 5,476,589 to Bacino, incorporated by reference herewith. Specifically, the ePTFE reinforcing polymer was longitudinally expanded to a ratio of 55 to 1 and transversely expanded approximately 2.25 to 1, to produce a thin strong reinforcing polymer with a mass of approximately 3.5 g/m² and a thickness of approximately 6.5 micrometers.

The composite film 3 was made by using a wire-wound rod coating process whereby a solution of Tecothane TT-1085A polyurethane (Thermedics, Inc., Woburn, MA) and tetrahydrofuran (THF) was coated onto an ePTFE reinforcing polymer. A 3 – 8 percent by weight solution of Tecothane TT-1085A polyurethane in THF was coated onto the ePTFE reinforcing polymer to produce a composite film with approximately equal amounts of Tecothane TT-1085A polyurethane as depicted in FIG. 1B on either side and throughout the ePTFE reinforcing polymer and a total polymer weight application of approximately 40 – 60 percent of the total final composite film weight.

Example 2 – Bladderless Balloon

The bladderless balloon of the present invention was made by wrapping a composite film of Tecothane TT-1085A polyurethane (Thermedics, Inc., Woburn, MA), and ePTFE reinforcing polymer over a FEP coated silver-plated copper core wire (Putnam Plastics LLC, Dayville, CT). The wrapped core wire
5 was heat treated and the center wire and FEP coating were subsequently removed to provide a hollow composite balloon tube.

The core wire was a 0.2 mm diameter silver-plated copper wire with a fluoroethylene-propylene (FEP) 5100 coating that resulted in a final wire diameter of 0.394 mm. The ePTFE reinforcing polymer used to make the
10 composite film is described in Example 1. Specifically, the ePTFE reinforcing polymer was longitudinally expanded to a ratio of 55 to 1 and transversely expanded approximately 2.25 to 1, to produce a thin strong reinforcing polymer with a mass of approximately 3.5 g/m² and a thickness of approximately 6.5 micrometers.

The composite film was made by using a wire-wound rod coating process whereby a solution of Tecothane TT-1085A polyurethane and tetrahydrofuran (THF) was coated onto an ePTFE reinforcing polymer. A 3 – 8 percent by weight solution of Tecothane TT-1085A polyurethane in THF was coated onto the ePTFE reinforcing polymer to produce a composite film with
15 approximately equal amounts of Tecothane TT-1085A polyurethane on either side and throughout the ePTFE reinforcing polymer and a total polymer weight application of approximately 40 – 60 percent of the total final composite film weight.

The composite film was slit to 5 mm wide and helically wrapped around
25 the 30.5 cm long core wire at a 4 to 5 degree angle from the longitudinal axis of the wire. The wrapped core wire was heated for approximately 5 to 30 seconds at 180°C after wrapping. The core wire was then wrapped with the composite film in the opposite direction at a 4 to 5 degree angle from the longitudinal axis of the wire and subsequently heated for approximately 5 to 30 seconds at
30 180°C. The process of wrapping the core wire in opposite directions and heating after each pass was repeated until a total of four passes of wrapping was complete. The wrapped core wire was wrapped around a pin frame with approximately 30 cm spaces between pins and approximately 180 degrees of wrap around each pin and tied at the ends before being placed into an oven
35 and heated for approximately 30 minutes at 150°C.

The core wire and the FEP coating over the core wire were removed from the composite balloon over wire construction. An approximately 2.54 cm

long section of the composite hollow balloon tube was removed from either end of a 30.5 cm long section of the balloon over wire construction. The exposed ends of the wire were clamped with hemostats and pulled by hand until the wire had been stretched approximately 5 cm, at which point it was removed from the center of the tube. The plastic FEP coating was removed in a similar fashion, but was stretched approximately 50 cm before it was removed from the balloon. A composite hollow balloon tube was produced with a first layer wrapping material at a low (4 to 5 degree) angle of wrap.

The 2.85 mm inflated diameter by 27 mm long balloon was mounted to a 0.36 mm diameter stainless steel hypotube (Creganna Medical Devices, Parkmore West Galway, Ireland) that had been helically wrapped with approximately three layers of expanded PTFE reinforcing polymer and EFEP fluoroplastic composite with the EFEP layer facing the stainless steel tube. The balloon was attached and sealed to the catheter shaft by wrapping an approximately 5 mm wide ePTFE/eFEP film circumferentially around the balloon approximately five times. One band was wrapped on each end of the balloon and was centered over the end of the balloon and the catheter such that it made a seal by contacting both the hypotube shaft and the balloon as depicted in Figure 6.

Example 3 – Bladderless Balloon with Heat Inflation Technique

The bladderless balloon of the present invention was made by wrapping a composite film of Tecothane TT-1085A polyurethane (Thermedics, Inc., Woburn, MA), and ePTFE reinforcing polymer over a FEP coated silver-plated copper core wire (Putnam Plastics LLC, Dayville, CT). The wrapped core wire was heat treated and the center wire and FEP coating were subsequently removed to provide a hollow composite balloon tube.

The core wire was a 0.2 mm diameter silver-plated copper wire with a fluoroethylene-propylene (FEP) 5100, coating that resulted in a final wire diameter of 0.394 mm. The ePTFE reinforcing polymer was longitudinally expanded to a ratio of 55 to 1 and transversely expanded approximately 2.25 to 1, to produce a thin strong reinforcing polymer with a mass of approximately 3.5 g/m² and a thickness of approximately 6.5 micrometers.

The composite film was made by using a wire-wound rod coating process whereby a solution of Tecothane TT-1085A polyurethane and tetrahydrofuran (THF) was coated onto an ePTFE reinforcing polymer. A 3 – 8 percent by weight solution of Tecothane TT-1085A polyurethane in THF was

coated onto the ePTFE reinforcing polymer to produce a composite film with approximately equal amounts of Tecothane TT-1085A polyurethane on either side and throughout the ePTFE reinforcing polymer and a total polymer weight application of approximately 40 – 60 percent of the total final composite film weight.

5 The composite film was slit to 5 mm wide and helically wrapped around the 30.5 cm long core wire at a 4 to 5 degree angle from the longitudinal axis of the wire. The wrapped core wire was heated for approximately 5 to 30 seconds at 180°C after wrapping. The core wire was then wrapped with the composite
10 film in the opposite direction at a 4 to 5 degree angle from the longitudinal axis of the wire and subsequently heated for approximately 5 to 30 seconds at 180°C. The process of wrapping the core wire in opposite directions and heating after each pass was repeated until a total of four passes of wrapping was complete. The wrapped core wire was wrapped around a pin frame with
15 approximately 30 cm spaces between pins and approximately 180 degrees of wrap around each pin and tied at the ends before being placed into an oven and heated for approximately 30 minutes at 150°C.

The core wire and the FEP coating over the core wire were removed from the composite balloon over wire construction. An approximately 2.54 cm
20 long section of the composite hollow balloon tube was removed from either end of a 30.5 cm long section of the balloon over wire construction. The exposed ends of the wire were clamped with hemostats and pulled by hand until the wire had been stretched approximately 5 cm, at which point it was removed from the center of the tube. The plastic FEP coating was removed in a similar fashion,
25 but was stretched approximately 50 cm before it was removed from the balloon. A composite hollow balloon tube was produced with a first layer wrapping material at a low (4 to 5 degree) angle of wrap.

A 15.25 cm long section of the composite hollow balloon tube was tied into a knot and clamped with a hemostat on one end. The opposite end was
30 slipped through a Qosina male touhy borst with spin lock fitting (#80343, Qosina Corporation, Edgewood, NY), and a Monoject blunt needle with Aluminum luer lock hub (model # 8881-202389, Sherwood Medical, St. Louis, MO) was inserted approximately 2.0 cm into the balloon. The hemostatic valve was tightened to seal the balloon, and was then attached to a Balloon
35 Development Station Model 210A (Beahm Designs, Inc., Campbell, CA). The nozzle airflow was set to 25-30 units and the temperature was set to 140°C, air pressure to 2.58 atmospheres. The air pressure was turned on, the center 40

mm long region to be inflated was subjected to heat for about 2-3 minutes resulting in a balloon with a diameter of 2.85 mm. The diameter was checked with a Mitutoyo Laser Scan Micrometer Model LSM-3100 (Mitutoyo America Corp, Aurora, IL) while in the inflated state. The resulting balloon had a
5 diameter of 2.85 mm and an inflated length of 27 mm.

Using a Monoject blunt needle with Aluminum luer lock hub (model # 8881-202389, Sherwood Medical, St. Louis, MO) dispensing needle, the balloon was subjected to an internal pressure of 5.44 atmospheres at room temperature for approximately 1 hour.

10 The 2.85 mm inflated diameter by 27 mm long balloon was mounted to a 0.36 mm diameter stainless steel hypotube (Creganna Medical Devices, Parkmore West Galway, Ireland) that had been helically wrapped with approximately three layers of expanded PTFE reinforcing polymer and EFEP fluoroplastic composite with the EFEP layer facing the stainless steel tube. The
15 balloon was attached and sealed to the catheter shaft by wrapping an approximately 5 mm wide ePTFE/eFEP film circumferentially around the balloon approximately five times. One band was wrapped on each end of the balloon and was centered over the end of the balloon and the catheter such that it made a seal by contacting both the hypotube shaft and the balloon.

20

Example 4 – Material Properties

All of the experimental runs were performed using Mayer Bar coating technology and direct solution feed to the coating surface.

The Mayer Bar is simply a metal bar with wire windings.

25 Bars with windings of different wire sizes are used to achieve the desired thickness in coating. The Mayer Bar is used to apply the wet coating to the ePTFE membrane. The coating dries with the aid of an inline oven. The finished coated membrane receives a second coat directly to the membrane surface. This process provides an even coating and offers flexibility in the
30 laydown design.

Example 5

The Tecothane 1085 (TT1085) elastomer, used in the coating, is readily solvated in Tetrahydrofuran (THF). THF is characterized by a low vapor
35 pressure, and as expected, a fast evaporation rate. Using this material the following results were obtained:

Test Samples:

	Sample 1	Single Sided Coat "2 Passes"
	Sample 2	Single Sided Coat "4 Passes"
5	Sample 3	Double Sided Coat "2 Passes"
	Sample 4	Double Sided Coat "4 Passes"

Results: Gross Testing @ ambient temperatures:

10	Sample 1:	Inflated to 30 atm – no weeping for two minutes.
	Sample 2:	Inflated to 30 atm – no weeping for three minutes.
	Sample 3:	Inflated to 30 atm - no weeping observed until burst at 3 minutes.
15	Sample 4:	Inflated to 30 atm - no weeping observed until burst at 7 minutes.

Multiple Inflation Testing: The following procedure was used for this test. Each unit was preconditioned at 37°C for 2 minutes. At 37°C, nine inflations were made to 18 atm and held for 30 seconds. On the 10th inflation, the unit was removed from the bath, wiped off, and inspected for weeping.

	Sample 1:	Weeping observed on the 10 th inflation.
	Sample 2:	Weeping observed on the 10 th inflation.
25	Sample 3:	No weeping observed on 10 th inflation. Balloon was pressurized for 4 minutes.
	Sample 4:	No weeping observed on 10 th inflation. Balloon was pressurized for 45 minutes.

30 While particular embodiments of the present invention have been illustrated and described herein, the present invention should not be limited to such illustrations and descriptions. It should be apparent that changes and modifications may be incorporated and embodied as part of the present invention within the scope of the following claims.

35

The invention claimed is:

1. A stretchable material comprising a reinforcing polymer having a porous matrix with void spaces and a sealing material imbibed into the reinforcing polymer substantially sealing the porous matrix void spaces and extending beyond the reinforcing polymer matrix to form a surface coating.
2. The stretchable material of claim 1 wherein the surface coating possesses a greater strain capability than the sealing material.
3. The stretchable material of claim 1 wherein the sealing material is an elastomer.
4. The stretchable material of claim 1 wherein the sealing material is a nylon.
5. The stretchable material of claim 1 wherein the sealing material is a polyether block amide.
6. The stretchable material of claim 1 wherein the sealing material is a fluoropolymer.
7. The stretchable material of claim 1 wherein the polymer matrix is anisotropic material stretched in only one direction.
8. The stretchable material of claim 1 wherein the polymer matrix is isotropic.
9. A balloon catheter comprising a tubular catheter shaft having a longitudinal axis and an inflatable bladderless wrapped balloon affixed to the catheter shaft wherein the balloon comprises the stretchable material of claim 1.
10. The balloon catheter of claim 9 wherein a surface coating is formed on both sides of the reinforcing polymer layer.

11. The balloon catheter of claim 9 wherein said surface coating maintains a watertight matrix when the sealing material is stressed.
- 5 12. The balloon catheter of claim 9 wherein the sealing material is an elastomer.
13. The balloon catheter of claim 9 wherein the sealing material is an urethane.
- 10 14. The balloon catheter of claim 9 wherein the sealing material is a fluoropolymer.
- 15 15. The balloon catheter of claim 9 wherein the sealing material is a viscous flow material.
- 16 16. The balloon catheter of claim 9 wherein the sealing material is a nylon.
- 17 17. The balloon catheter of claim 9 wherein the sealing material is a polyether block amide.
- 20 18. The balloon catheter of claim 9 wherein the surface coating thickness is controlled to allow for controlled porosity when strained due to inflation.
- 25 19. The balloon catheter of claim 18 wherein the controlled porosity delivers a liquid in therapeutic quantities.
20. The balloon catheter of claim 19 wherein the therapeutic liquid weeps only when the balloon is inflated to high pressure.
- 30 21. A wrapped balloon wherein the strain on the wrap layers is lower than the radial strain on the balloon upon inflation.
- 35 22. A balloon of claim 21 wherein the balloon is wrapped at an angle less than 54 degrees and the wrap angle approaches 54 degrees upon inflation.

23. A balloon of claim 21 wherein the final diameter is determined by the change between the wrap angle and the diameter wherein the wrap angle approaches 54 degrees upon inflation.

FIGURE 1B

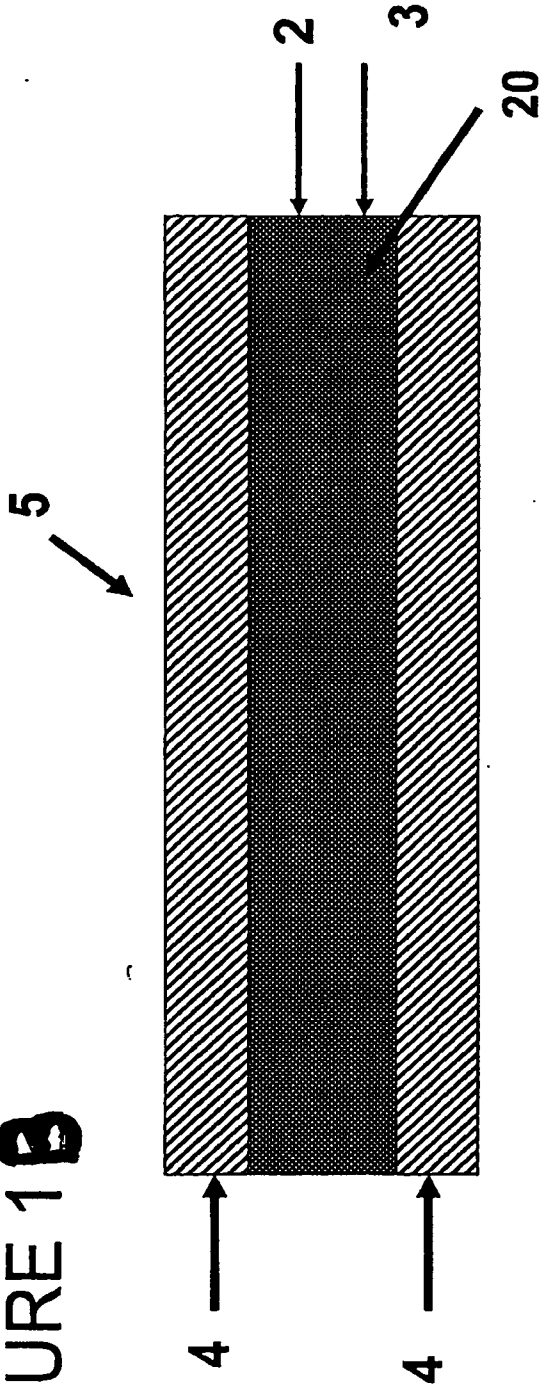


FIGURE 1A

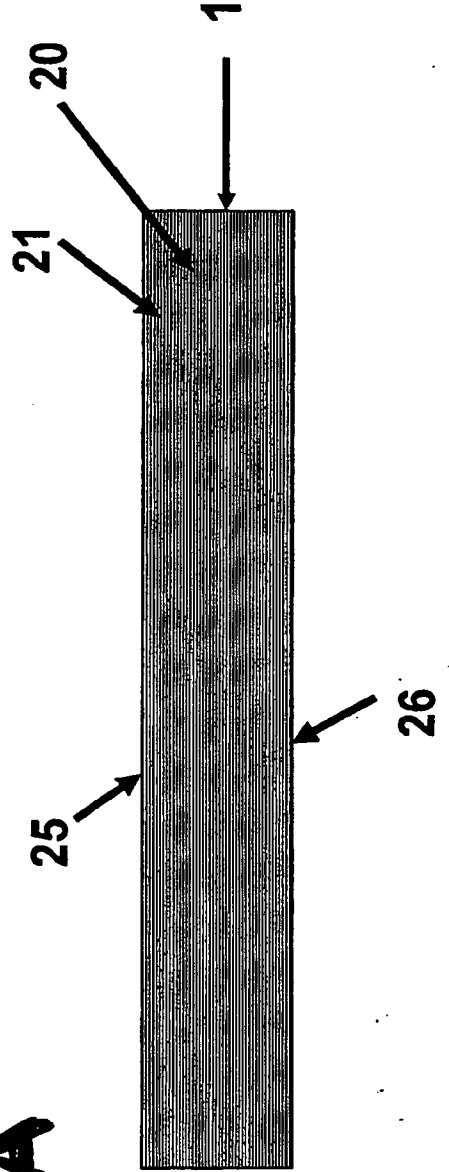
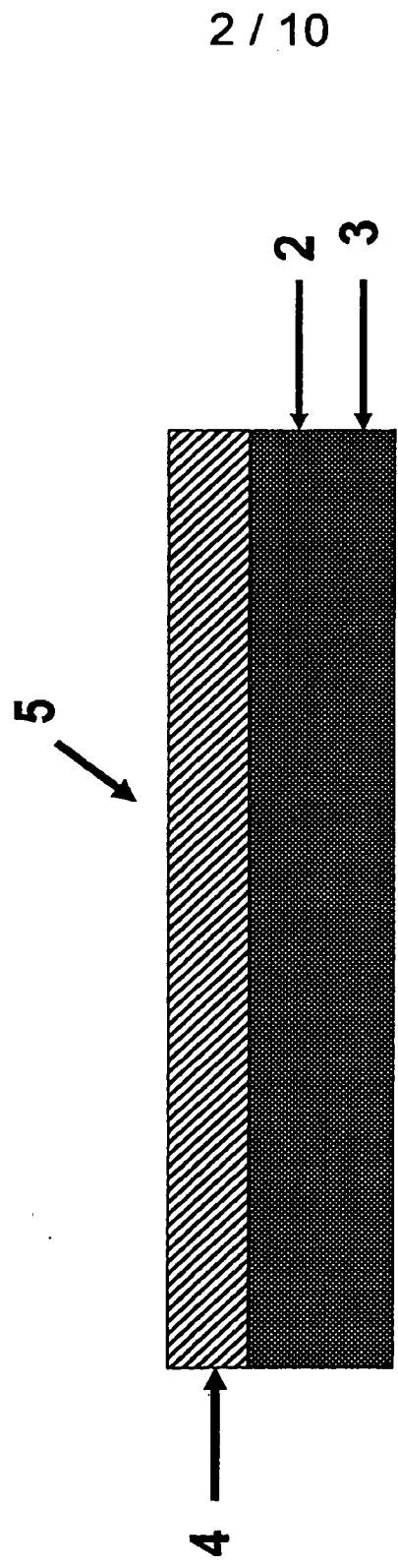
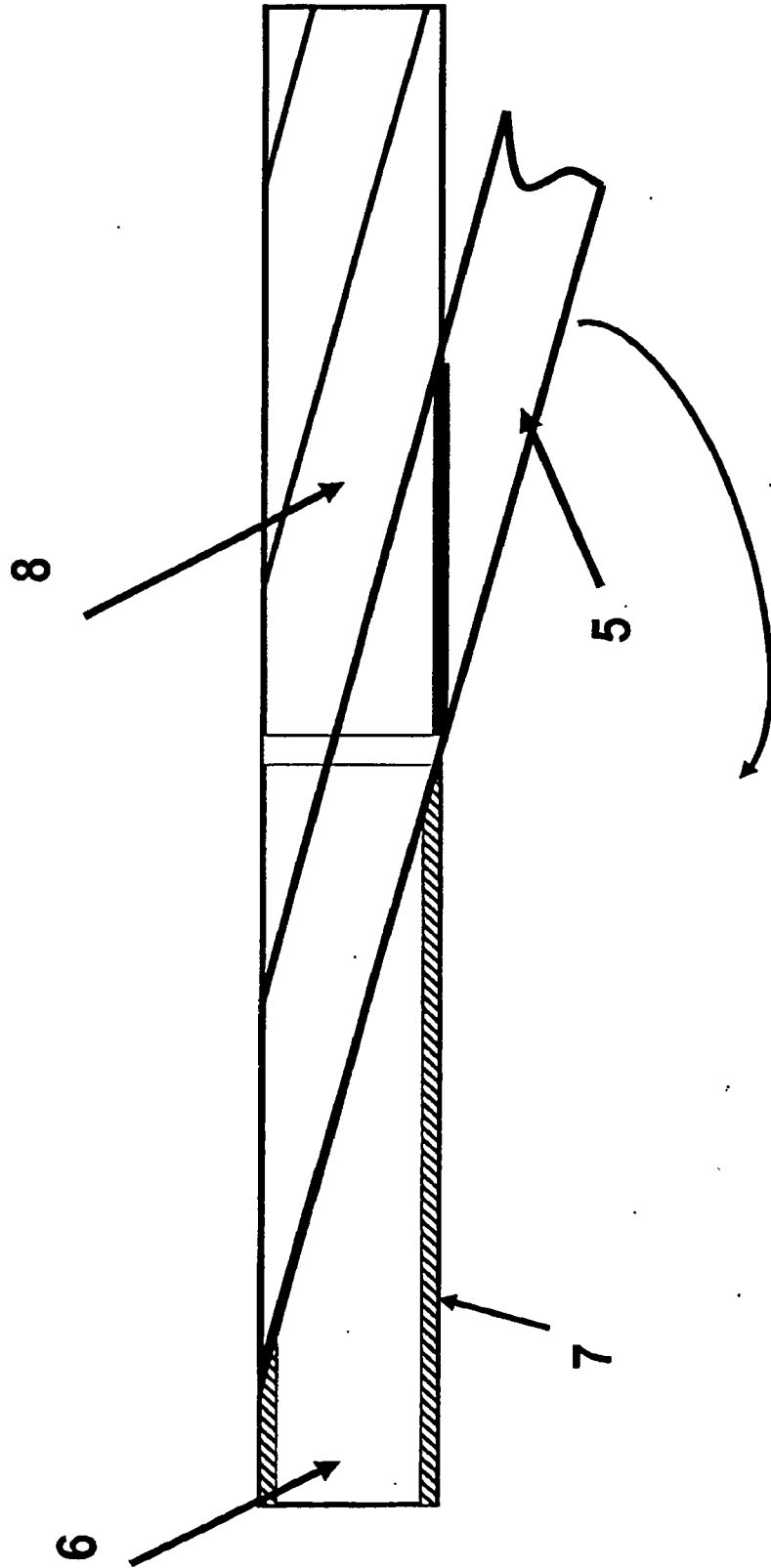


FIGURE 2



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FIGURE 3



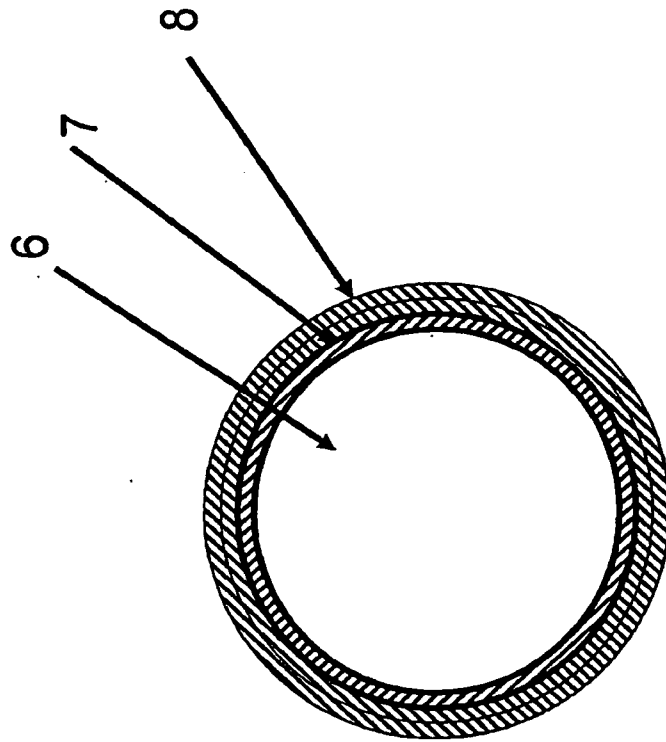


FIGURE 4

5 / 10

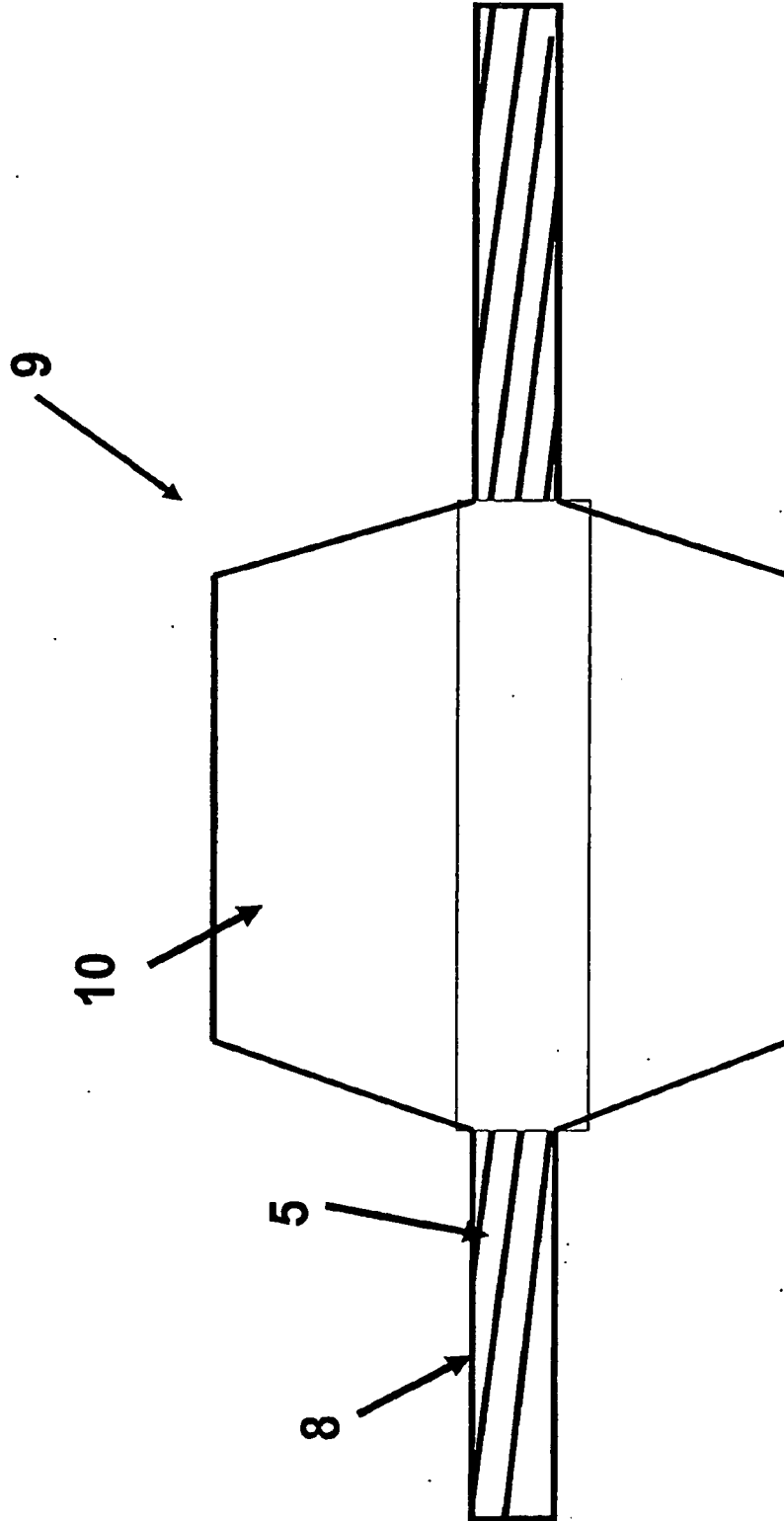


FIGURE 5

6 / 10

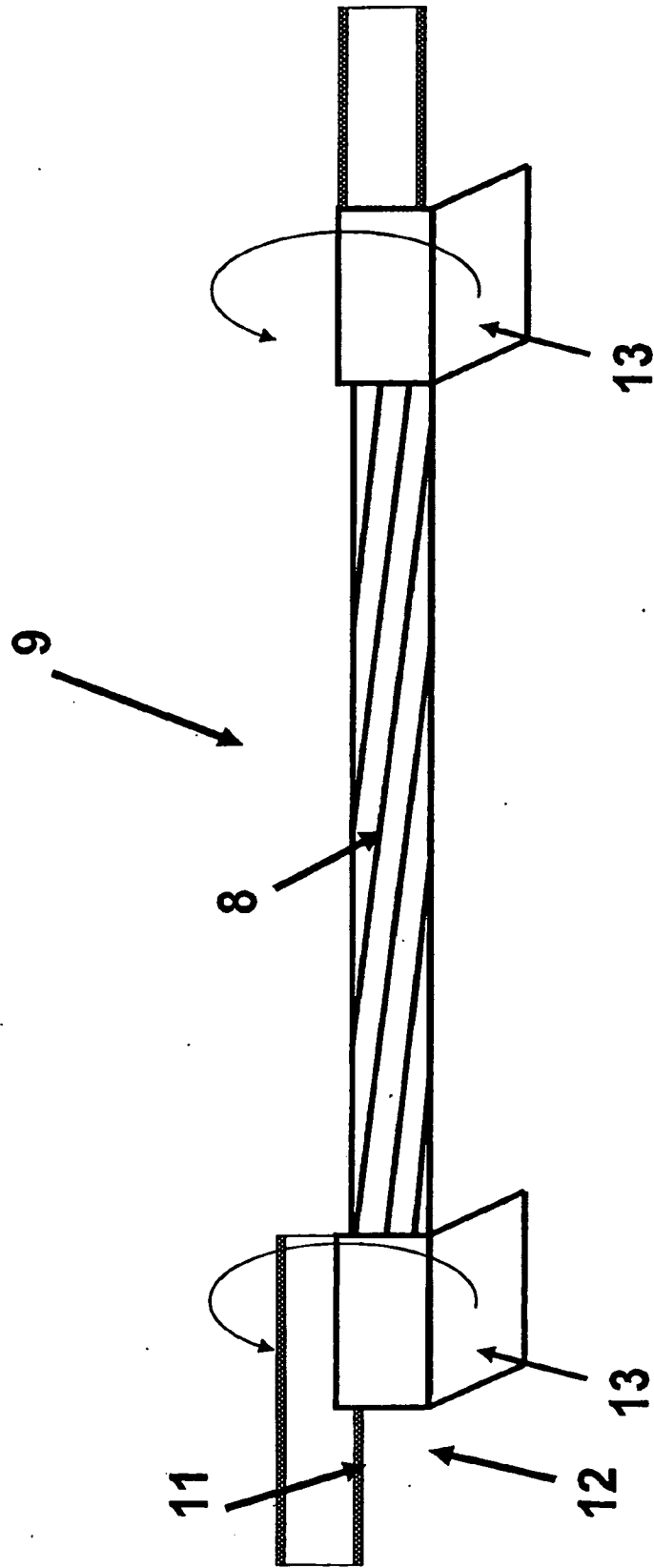


FIGURE 6

FIGURE 7

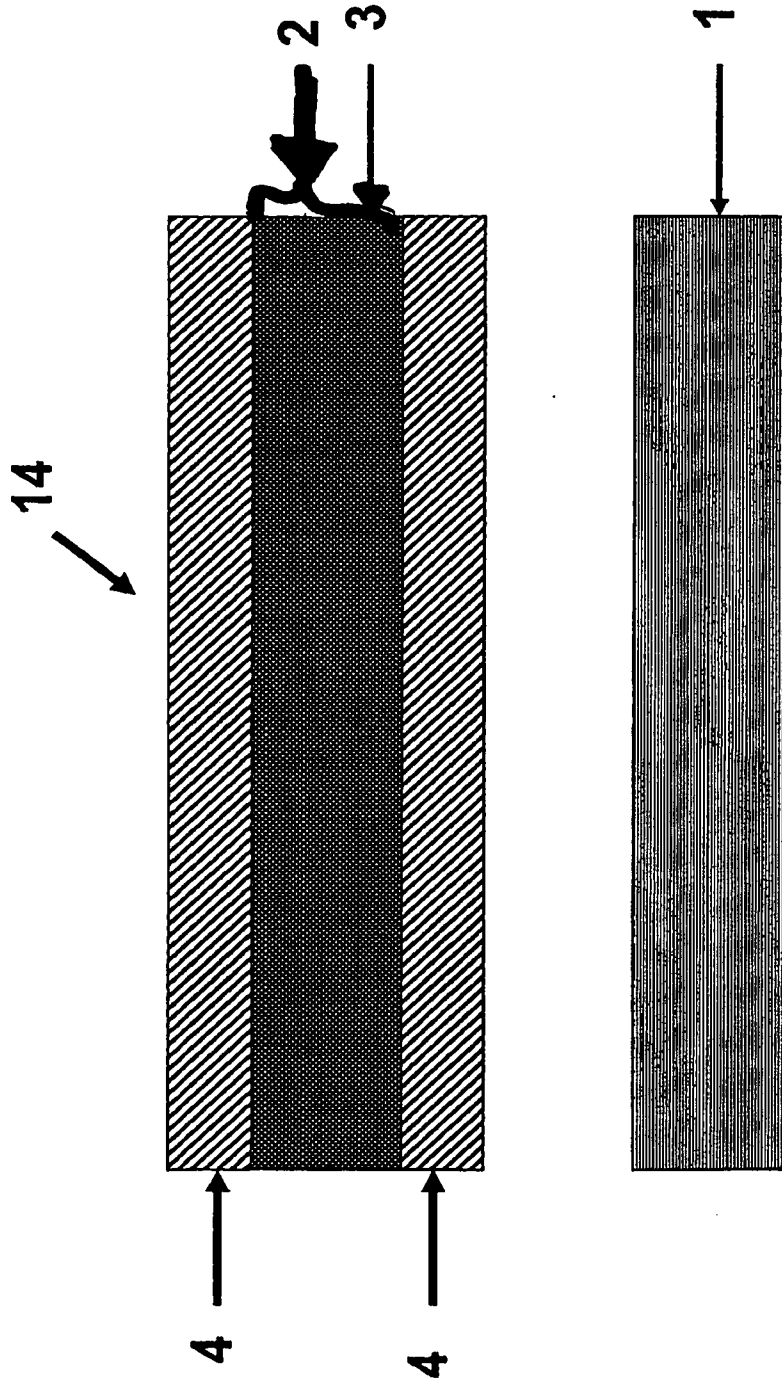


FIGURE 8

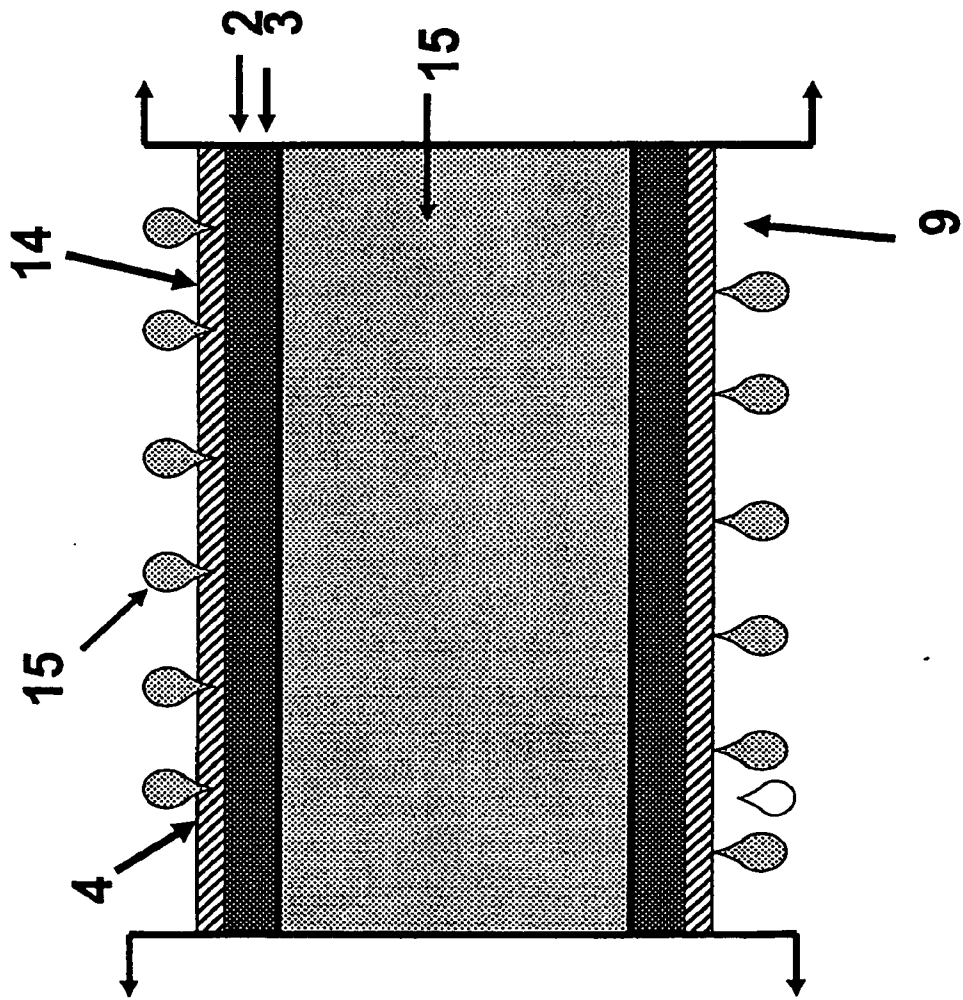
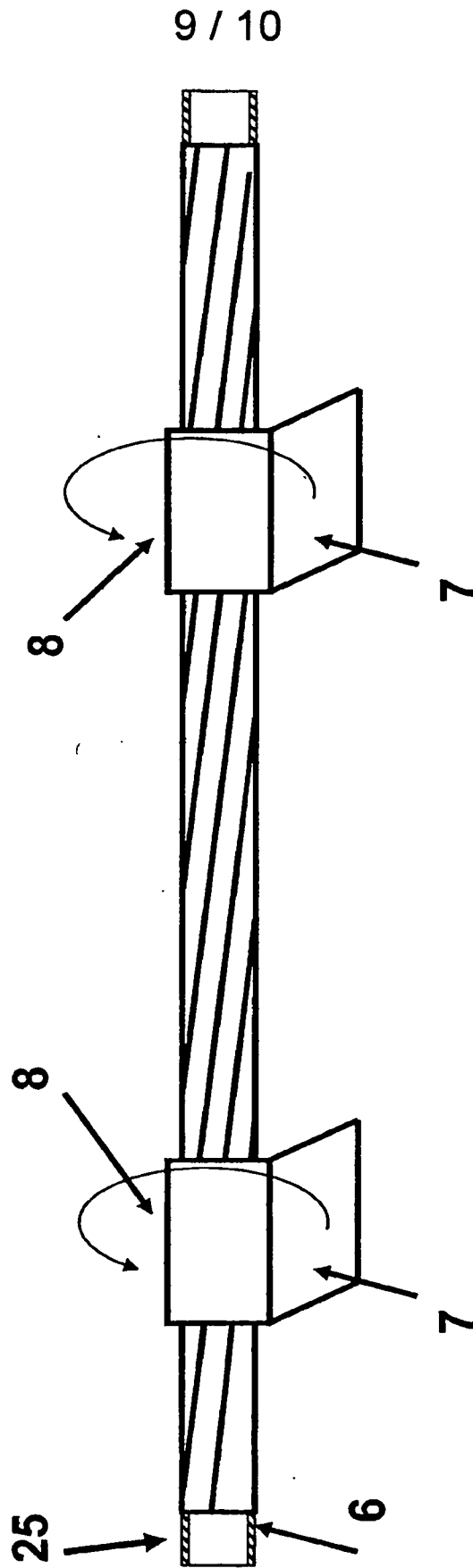


FIGURE 9



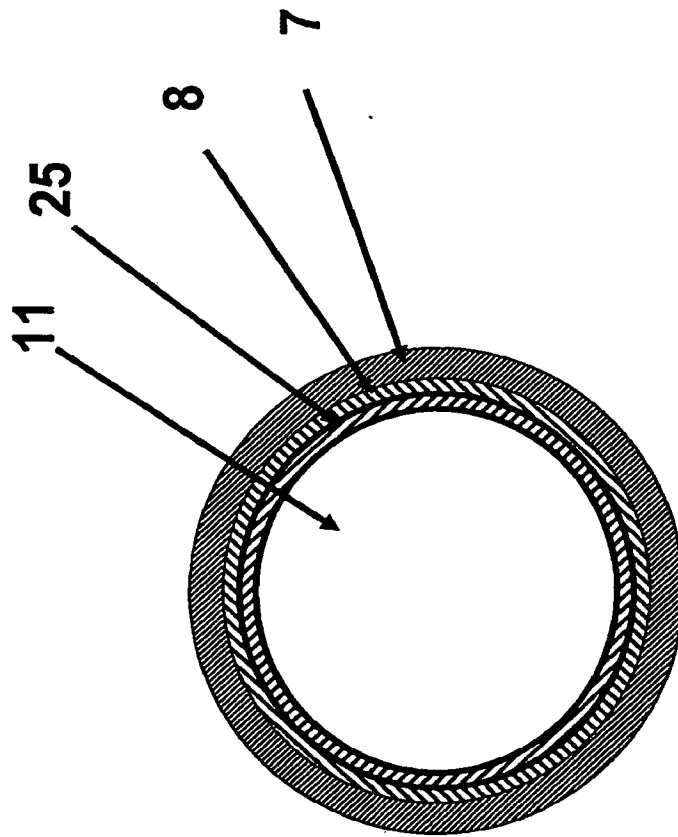


FIGURE 10