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(54) Title: GLASS YARN SIZING COMPOSITION, ME		

# 4) Title: GLASS YARN SIZING COMPOSITION, METHOD USING SAME AND RESULTING PRODUCTS

(54) Titre: COMPOSITION D'ENSIMAGE POUR FILS DE VERRE, PROCEDE UTILISANT CETTE COMPOSITION ET PRODUITS RESULTANTS

#### (57) Abstract

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A glass yarm sizing composition consisting of a solution having a viscosity no higher than 400 cP and including a solvent in an amount of less than 5 wt.%, and at least one heat-polymerisable basic system, is disclosed. Said basic system includes at least 60 wt.% of components having a molecular weight of less than 750 and at least 60 wt.% of a mixture of one or more components having at least one epoxy reactive function, and one or more components having at least one anhydride reactive function. A method using said composition and the resulting yams coated with said composition are also disclosed.

#### (57) Abrégé

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La présente invention concerne une composition d'ensimage pour fils de verre constituée d'une solution de viscosité inférieure ou égale à 400 cP comprenant moins de 5 % en poids de solvant et comprenant au moins un système de base polymérisable thermiquement, ledit système de base comprenant au moins 60 % en poids de composants de masse moléculaire inférieure à 750 et comprenant au moins 60 % en poids d'un mélange: de composant(s) présentant au moins une fonction réactive époxy, et de composant(s) présentant au moins une fonction réactive anhydride. L'invention concerne également un procédé utilisant cette composition et les fils obtenus selon ce procédé et revêtus de ladite composition.

### PATENT

SIZING COMPOSITION FOR GLASS STRANDS, PROCESS USING THIS COMPOSITION AND RESULTING PRODUCTS

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#### ABSTRACT

The present invention relates to a sizing composition for glass strands composed of a solution with a viscosity of less than or equal to 400 cP comprising less than 5% by weight of solvent and comprising at least one thermally polymerizable base system, the said base system comprising at least 60% by weight of components with a molecular mass of less than 750 and comprising at least 60% by weight of a mixture: . of component(s) exhibiting at least one epoxy reactive functional group,

• and of component(s) exhibiting at least one anhydride reactive functional group.

The invention also relates to a process using this composition and to the strands obtained according to this process and coated with the said composition.



# SIZING COMPOSITION FOR GLASS STRANDS, PROCESS USING THIS COMPOSITION AND RESULTING PRODUCTS

The present invention relates to a sizing composition for glass strands, this composition reacting to heat. The present invention also relates to a process for the production of reinforcing glass strands using this composition as well as to the glass strands obtained and to the composites produced from the strands.

In the continuation of the text, "polymerization", "to polymerize", "polymerizable" and the like are understood to mean "polymerization and/or crosslinking", "to polymerize and/or to crosslink", "polymerizable and/or crosslinkable" and the like respectively.

Reinforcing glass strands are manufactured in a known way from molten glass streams flowing from die orifices. These streams are drawn in the form of continuous filaments and then these filaments are gathered into base strands, which are then collected.

Before they are gathered together in the form of strands, the filaments are coated with a size by passing over a sizer device. This deposition is necessary for the production of the strands and makes it possible to combine them with other organic and/or inorganic materials to produce composites.

The size serves, in the first place, as lubricant and protects the strands from the abrasion resulting from the high-speed friction of the strands over various devices during the abovementioned process.

The size can also ensure, in particular after polymerization, the integrity of the abovementioned strands, that is to say the binding of the filaments to one another within the strands. This integrity is in particular sought after in textile applications where the strands are subjected to strong mechanical stresses. Indeed, if the filaments show little attachment to one another, they break more readily and disrupt the operation of the textile machinery. Non-

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integrated strands are moreover regarded as difficult to handle.

The size also facilitates the wetting and/or impregnation of the strands by materials to be the reinforced and helps in the creation of bonds between the said strands and the said materials. The mechanical properties of the composites obtained from the material and the strands depend in particular on the quality of the adhesion of the said material to the said strands and on the ability of the said strands to be wetted 10 and/or to be impregnated by the said material.

compositions The sizing used must be sufficiently stable and compatible with the drawing . rates of the filaments which have to pass through them 15 (several tens of metres per second). They must in particular resist the shearing induced by the passage of the filaments and properly wet their surface at the said rates. In the case where they thermally polymerize, they must exhibit a reaction temperature 20 which is sufficiently high to remain stable at the die. It is also desirable for these compositions to exhibit, after polymerization, a maximum degree of conversion (this degree corresponding to the ratio of the level of functional groups which have reacted in the size after 25 heat treatment to the level, in the size, before heat treatment of reactive functional groups capable of reacting), in order to guarantee in particular that sized strands of constant quality are obtained (a size exhibiting a degree of conversion which is much below 30 the theoretical degree expected being capable of changing over time).

The majority of sizes currently used are aqueous sizes which are easy to handle but which have to be deposited in large amounts on the filaments in order to be effective. The water generally represents 90% by weight of these sizes (in particular for reasons of viscosity), which necessitates the drying of the strands before they are used as reinforcers, it being possible for the water to be harmful to the good

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adhesion between the strands and the materials to be These drying operations are lengthy and reinforced. expensive, must be adapted to the manufacturing conditions of the strands and their efficiency is not always optimum. When they are carried out during the 5 (that fibre-drawing operation is to say before collecting the strands obtained by gathering together the filaments), on the filaments (WO 92/05122) or on the strands (US-A-3,853,605), they require the installation of drying devices at each die and when 10 they are carried out on the strand wound packages, they bring about risks of uneven and/or selective migration of the components of the size within the wound packages (aqueous sizes already having a tendency to spread 15 themselves unevenly over the strands because of their nature) and optionally phenomena of colouring of the strands or of deformation of the wound packages. The deformation of the wound packages is also observed, in the absence of drying, on straight-edged wound packages (rovings) of fine strands (that is to say exhibiting a 20 "count" or "mass per unit length" of 300-600 tex (g/km) or less) coated with aqueous sizes.

A few exceptional patents describe non-aqueous sizes sizes but these generally involve organic solvents which are problematic to handle and which can, 25 because of their toxicity, harm the health of people in the vicinity and/or pose problems of viscosity which it is appropriate to solve by heating these sizes (US 4,604,325) or by adding suitable agents (US 4,609,591). 30 These sizes also often require the installation of specific devices below each die; it is in particular necessary, when the strands are collected in the form wound of packages, to treat the strands before obtaining the wound packages in order to prevent the 35 turns of each wound package from sticking to one another, this sticking phenomenon making it difficult unwind the strands. to These treatments, the effectiveness of which depends on operating the conditions, consist, for example, in polymerizing the

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size by subjecting the sized strands to the effect of ultraviolet radiation in order to confer on them a satisfactory integrity and to make it possible to handle them (US-A-5,049,407). The polymerized size, however, prevents the filaments from sliding with respect to one another, this absence of mobility resulting in the shattering, by mechanical degradation of the size, of the strands when they are cut and it being possible for this absence of mobility to cause problems in textile applications where the strands used must be both integrated and flexible.

The subject of the present invention is an improved sizing composition which does not exhibit the . abovementioned disadvantages, this composition being intended to coat glass strands and being capable of 15 polymerizing under the effect of heat, this composition making it easy to handle the sized strands, even before polymerization, and conferring on them a flexibility compatible with their subsequent treatments, this 20 composition conferring good integrity on the strands after polymerization and exhibiting a high degree of conversion, this composition in addition efficiently protecting the strands from abrasion, conferring on them the possibility of being combined with various 25 materials to be reinforced for the purpose of producing composite items exhibiting good mechanical properties, being particularly stable, in particular at the die, and being compatible with the drawing rates of the filaments.

Another subject of the present invention is an improved process for the manufacture of sized glass strands as well as sized glass strands which are easy to handle and which exhibit improved characteristics, the said strands being capable of efficiently reinforcing organic and/or inorganic materials for the preparation of composites.



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According to the present invention there is provided a glass strand coated with a sizing composition composed of a solution with a viscosity of less than or equal to 400 cP including less than 5% by weight of solvent and at least one thermally polymerizable and/or

crosslinkable base system, the said base system including at least 60% by weight of components with a molecular mass of less than 750 and at least 60% by weight of a mixture: of component(s) exhibiting at least one epoxy

10 reactive functional group, and

of component(s) exhibiting at least one anhydride reactive functional group.

The sizing composition according to the invention 15 is composed of a solution with a viscosity of less than or equal to 400 cP comprising less than 5% by



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weight of solvent and comprising а thermally the said polymerizable base system, base system comprising at least 60% by weight of components with a molecular mass of less than 750 and comprising at least 60% by weight of a mixture:

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of component(s) exhibiting at least one epoxy
 reactive functional group,

and of component(s) exhibiting at least one anhydride reactive functional group.

The invention also relates to a process for the 10 production of sized glass strands according to which a multiplicity of molten glass streams, flowing from a multiplicity of orifices arranged at the base of one or a number of dies, is drawn in the form of one or a number of sheets of continuous filaments and then the 15 filaments are gathered together in one or a number of strands which are collected on a moving support, the said process comprising the deposition at the surface of the filaments, during drawing and before gathering 20 together the filaments into strands, of the sizing composition defined above.

The invention further relates to strands coated with a size exhibiting the composition defined above and/or obtained according to the process mentioned above.

Subsequently, "epoxy component(s)" and "anhydride component(s)" is understood to mean "component(s) exhibiting at least one epoxy reactive functional group" and "component(s) exhibiting at least one anhydride reactive functional group" respectively.

In the composition according to the invention, the possible solvents are essentially organic solvents necessary for dissolving certain polymerizable compounds. The presence of these solvents in a limited amount does not require specific treatments to remove them; in the majority of cases, the sizes according to the invention are, moreover, entirely free of solvent,



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that is to say of compounds which act solely as solvent in the solution.

Due to its low viscosity (less than or equal to 400 cP and preferably less than or equal to 200 cP), the sizing composition according to the invention is 5 compatible with the conditions for producing glass strands imposed by the direct process, the viscosity of the composition being chosen as a function of the drawing rate and of the diameter of the filaments caused to pass through it. The composition according to 10 the invention also exhibits a wetting rate on the strand compatible with the drawing rate of the strands.

"Thermally polymerizable base system" according to the invention should be understood as meaning the compound or compounds essential to the sizing 15 and having the essential function of participating in the structure of the polymerized size, these compounds being capable of thermally polymerizing. As a general rule, the base system represents between 60 and 100% by 20 weight of the sizing composition according to the invention, mainly between 70 and 99.5% by weight of the composition and, in the majority of cases, between 75 and 90% by weight of the composition.

The base system is mostly composed (preferably 25 to 80% by weight and up to 100% by weight in the majority of cases) of epoxy component(s) and of anhydride component(s), the use of this mixture of components making it possible to obtain, after polymerization, epoxy-anhydride (polyester) copolymers as the major participants in the structure of the 30 polymerized size, the properties of the sized strands depending directly on this structure.

addition, the In base system comprises а majority (preferably at least 70-75% by weight and up to 100% by weight) of component(s) with a molecular mass of less than 750, this/these component(s) normally mostly (and in the majority of cases, entirely) forming abovementioned epoxy part of the and anhydride components.

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Preferably and in general according to the invention, the components with a molecular mass of less than 750 mentioned above have molecular masses of less than 500. Likewise, in the majority of cases according to the invention and preferably, these components are (monoor polyfunctional, monomers as explained subsequently) but the base system can also comprise components with a molecular mass of less than 750 in the form of oligomers or of polymers containing partially polymerized functional groups.

According to certain embodiments, the base system according to the invention can optionally comprise а small proportion of component(s) participating in the structure of the polymerized size but not exhibiting epoxy or anhydride functional groups and/or exhibiting a higher molecular mass.

According to the preferred embodiment of the invention which makes it possible to obtain particularly satisfactory results, the base system is composed solely of components exhibiting at least one epoxy or anhydride reactive functional group and/or, optionally, is composed solely of components with a molecular mass of less than 750.

The epoxy or anhydride components which can be used in the base system can exhibit one (monofunctional 25 or number of identical components) а reactive functional groups (polyfunctional components) among epoxy and anhydride functional groups.

The epoxy component or components of the base system can be in particular one or a number of the 30 following components: alkyl glycidyl ether with a C4- $C_{16}$  aliphatic chain or the like; cresyl- or phenyl- or nonylphenyl- or p-tert-butylphenyl- or 2-ethylhexylglycidyl ether and the like; limonene epoxide; cyclohexene monoxide; glycidyl ester of versatic acid 35 neodecanoic acid; or of and the like (the above components being monofunctional components); 1,4butanediol or neopentyl glycol or resorcinol or cyclohexanedimethanol or 1,6-hexanediol or



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dibromoneopentyl glycol diglycidyl ether and the like; diepoxidized derivative of bisphenols A or F; 3,4epoxycyclohexylmethyl 3,4-epoxycyclohexanecarboxylate; bis(3,4-epoxycyclohexyl) adipate, polyglycol diepoxide; hexahydrophthalic diglycidyl ester of anhydride; diglycidylhydantoin; 2-(3,4-epoxycyclohexyl)-5,5-spiro-(3,4-epoxycyclohexyl)-m-dioxane, vinylcyclohexene dioxide; trimethylolethane or trimethylolpropane or trisphenylolmethane triglycidyl ether and the like; triglycidyl ether of palm oil; triglycidyl ether of para-aminophenol; tetra (para-glycidoxyphenyl) ethane; 4,4'-(diglycidylamino)diphenylmethane; polyglycidyl ether of an aliphatic polyol, epoxidized polybutadiene; epoxyphenol novolak epoxycresol or novolak resin; triglycidyl isocyanurate; N, N, N', N'-tetraglycidyl- $\alpha, \alpha'$ bis(4-aminophenyl)or N, N, N', N'-tetraglycidyl- $\alpha, \alpha'$ bis(4-amino-3,5-dimethylphenyl)-p-diisopropylbenzene

and the like; and the like (these components being polyfunctional components).

20 As a general rule according to the invention, the proportion of epoxy component(s) of the base system is between 15 and 85% by weight of the sizinq composition, mainly between 25 and 70% by weight approximately of the sizing composition. In the 25 majority of cases, it is between 35 and 60% by weight of the sizing composition.

The anhydride component or components of the base system can be in particular one or a number of the following components: methylbicyclo[2.2.1]heptene-2,3dicarboxylic anhydride; hexahydrophthalic anhydride; dodecylsuccinic anhydride; phthalic anhydride; 1,4,5,6,7,7-hexachlorobicyclo[2.2.1]hept-5-ene-2,3dicarboxylic anhydride; endo-cis-bicyclo[2.2.1]heptene-2,3-dicarboxylic anhydride; tetrachlorophthalic anhydride; pyromellitic dianhydride; 1,2,3,4cyclopentanetetracarboxylic dianhydride; polyazelaic polyanhydride; polysebacic anhydride; glutaric anhydride; or alternatively polyester anhydride; bromodibromophthalic anhydride; cyclic sulphopivalic or



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anhydride; bicyclodicarboxylic anhydride; diphenoxyphosphinylsuccinic anhydride; anhydride of 2alkyleneglutaric acid; poly(cycloaliphatic anhydride); anhydride; cyclooctadiene-maleic styrene-maleic anhydride; perchlorocoumalin-maleic anhydride; myrcene monoepoxide-maleic anhydride; cyclohexadienedicarboxylic-maleic anhydride; poly(cyclopentadienyl) anhydride; trimellitic anhydride derivative maleic (bistrimellitic anhydride of neopentyl glycol, product of the acidolysis of a tricarboxylic anhydride and of an ester or of an amine, oxyalkylated derivative of trimellitic anhydride); anhydride of phenylenebis(3butanedicarboxylic acid); dianhydride of benzophenoneacid; of tetracarboxylic dianhydride phenylalkylpentanetetracarboxylic acid; dianhydride of alkylsubstituted tricyclodecanecarboxylic acid; dianhydride of dicarboxytetrahydronaphthalenesuccinic acid; and the like.

As a general rule according to the invention, 20 the proportion of anhydride component(s) of the base system is between 5 and 65% by weight of the sizing composition, mainly between 10 and 55% by weight approximately of the composition. In the majority of cases, it is between 15 and 45% by weight of the sizing 25 composition.

Preferably, according to the invention, the components of the base system and their levels within the base system are chosen so that the ratio r of the number of anhydride reactive sites to the number of 30 contrasting epoxy reactive sites is between 0.2 and 6 epoxy functional group counting (an as one epoxy reactive site and an anhydride functional group counting as two anhydride reactive sites), so as to make possible satisfactory polymerization of the sizing 35 composition, in particular by formation of epoxyanhydride (polyester) copolymers, during the polymerization heat treatment. In the majority of cases according to the invention, this ratio r is between 0.3 and 4 and, preferably, it is greater than 0.4 and less



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than or equal to 2.0 approximately, so as to promote the formation of more stable epoxy-anhydride copolymers of diester type (the formation of copolymers of monoester type not, however, being excluded when the ratio r is greater than 1 and it being possible for the formation of copolymers of monoester type to exhibit advantages in the reinforcement of certain matrices).

In one embodiment of the invention, the sizing composition comprises, in addition to the base system, least one specific catalyst which promotes 10 at the polymerization of the size under the effect of heat by facilitating the opening of the anhydride and/or epoxy functional groups, mainly in the case where the . anhydride component or components of the base system have little reactivity and/or optionally in the case 15 where the base system is devoid of cycloaliphatic epoxy components. This catalyst is preferentially chosen from derivatives. amino such as trialkylamines, hexamethylenetetramine, aniline/formaldehyde conden-

20 sation products, substituted aniline/aliphatic aldehyde (anhydrobutyraldehyde/toluidine) condensates, epoxyamines (N-(2,3-diepoxypropyl)aniline), basic tertiary amines, N,N-dialkylalkanolamines, amino salts of polyacids, quaternary ammonium salts, quaternary 25 imidazoline salts, dicyanodiamide, and the like, or from derivatives of boron and of phosphorus, such as ammonium organoboron salts, trialkanolamine borates, fluoroborates, organosubstituted phosphines, and the like, or from metal derivatives, such as tin 30  $(SnCl_4)$ , tin tetrachloride divalent salts, metal chelates containing epoxide groups, magnesium, barium,

chelates containing epoxide groups, magnesium, barium, zinc or cadmium oxides, and the like, or alternatively from alcohols.

The polymerization of the epoxy and anhydride 35 components can also be initiated by the presence of water (even in the form of traces), by the hydroxyl or carboxyl groups of components of the size (presence, for example, of hydrolysed silanes), by the moisture in the surrounding air, and the like. In the absence of



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catalyst(s) as defined above, the ratio r is in addition generally less than 3 and preferably less than 2.

The level of specific components defined above which act solely as catalysts in the sizing composition 5 is less than 3% by weight of the sizing composition, in the majority of cases less than 1% by weight and, preferably, is less than or equal to 0.5% by weight of the sizing composition. The presence of a catalyst which promotes the opening of the anhydride components 10 makes it possible to use less reactive anhydrides and to lower the polymerization temperature of the size, as explained subsequently. In the case of highly reactive components, such phthalic anhydride as anhydride, 15 maleic anhydride or succinic anhydride, the presence of a catalyst is, in contrast, generally avoided.

In addition to the base structure and the specific catalyst(s), the composition according to the invention can comprise additives in small amounts, additives giving specific properties to 20 these the sizing composition but not being essential participants in the structure of the size, in contrast to the base system. Even if these additives are to be distinguished from the base system, they may nevertheless be 25 thermally polymerizable, like the compounds of the base system.

The composition according to the invention can thus comprise, as additive, at least one coupling agent which makes it possible to attach the size to the glass, the proportion of the coupling agent or agents being between 0 and 25% by weight of the size and preferably being less than or equal to 20% by weight of the size. These agents can be one or a number of the following components: silanes, such as  $\gamma$ -glycidoxypropyltrimethoxysilane, γ-methacryloyloxypropyltrimethoxysilane, polyethoxylated-propoxylated trimethoxysilane,  $\gamma$ -acryloyloxypropyltrimethoxysilane, vinyltrimethoxysilane, phenylaminopropyltrimethoxy-



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silane, and the like; or titanates, zirconates, siloxanes, and the like.

The composition according to the invention can also comprise, as additive, at least one film-forming which acts solely as slip agent and which 5 agent facilitates fibre-drawing, in proportions of between 0 and 10% by weight and preferably less than or equal to 5% by weight. The presence of this agent or agents prevents significant friction of the filaments on the sizing device when the filaments are drawn at a high 10 rate (more than 40 m/s) and/or when they are very fine, these agents being, however, expensive and it being possible for these agents to result in a diminuation in . the mechanical characteristics of the composites. These fibre-drawing agents can be one or a number of the 15 following components: silicones, siloxanes or polysiloxanes, such as glycidyl(n)polydimethylsiloxane,  $\omega$ ,  $\omega$ -acryloyloxypolydimethylsiloxane, and the like. silicone derivatives, such as silicone oils, and the 20 like.

The composition according to the invention can also comprise, as additive, at least one textile processing agent acting essentially as lubricant, in between 0 and 15% by weight proportions of and 25 preferably of between 0 and 8% by weight. These textile agents can be one or a number of the following components: fatty esters (optionally ethoxylated or propoxylated), glycol derivatives (in particular of ethylene or of propylene glycol), such as isopropyl or cetyl palmitates, isobutyl stearates, decyl laurates, 30 ethylene glycol adipates, polyethylene glycols or polypropylene glycols with a molecular weight of less than 2000, isopropyl stearates, and the like.

The size can also comprise, as additive, at 35 least one agent for adapting to the materials to be reinforced, in the case of cement materials in particular.

The sizing composition according to the invention efficiently protects the strands from



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is stable, in particular at the die (the abrasion, according to the invention not truly composition polymerizing before 100°C and being subjected at the die to temperatures not exceeding 70°C), is compatible with the drawing rates of the filaments and does not require recourse to а drying operation before polymerization or recourse to a specific treatment between the deposition on the strand and the operation of collecting the sized strands.

10 Moreover, when the composition according to the invention is deposited on the filaments during drawing, it spreads out very quickly over the whole of their surface and forms a true protective film for each of The strand obtained by gathering together the them. filaments and which is coated with the thermally untreated composition (that say is τo not yet polymerized) is thus composed of a bundle of sheathed filaments which can slide over one another, this strand then exhibiting high flexibility, which is particularly 20 advantageous in the case where this strand is intended to be cut, the sheathing of the filaments in addition offering additional protection against abrasion. Such a strand does not exhibit integrity in the ordinary meaning of the term, that is to say that it is not 25 composed of filaments attached to one another by virtue in particular of an adhesive binding caused by one or a number of constituents of the size, such as can be sticky film-forming agents caused by present in significant amounts in a size. Despite this, this 30 strand coated with the not yet polymerized composition is easy to handle and, when it is wound in the form of wound packages, can easily be extracted from the wound packages without having subjected the size beforehand to a polymerization treatment. The strands coated with 35 have, the not yet polymerized sizing composition moreover, a very good aptitude towards wetting and towards impregnation by materials to be reinforced, it thus being possible for the impregnation to take place more rapidly (gain in productivity) and the composites



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obtained thus exhibiting a more homogeneous appearance and some improved mechanical properties.

The integrity proper of the strands by adhesive binding of the filaments constituting them is obtained after polymerization of the sizing composition by the 5 effect of heat. This integrity is sought for with respect to the strands which have to be subjected to strong mechanical stresses, for example in textile applications ratio r of the composition (the is preferentially between 0.5 and 2 approximately when the 10 strands are intended to be woven), or, if appropriate, after cutting, with respect to the cut strands intended to reinforce organic and/or inorganic materials. It is preferable, in such cases, to carry out the 15 polymerization of the size before, respectively, using the strands in textile applications or combining the cut strands with a material to be reinforced.

The integrity obtained after polymerization of the size is particularly important when the level of 20 size on the strands is relatively low (the loss on ignition of strands the coated with the sizing composition and/or obtained according to the process of the invention not exceeding 3% by weight). The amount of sizing composition which has to be deposited on the strands in order to be effective is advantageously of 25 little importance and makes it possible, however, to obtain strands exhibiting very good characteristics, including integrity (the integrity obtained being high even for levels of size on the filaments of the order 30 of 0.6% by weight).

The sizing composition according to the invention also exhibits, after polymerization, a maximum degree of conversion, the degree of conversion of the anhydride components being, for example, close to 100% when the ratio r is less than approximately 1.

Moreover, it is observed, surprisingly, that properties such as the tensile strength of the strands according to the invention are better, after the



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beginning of ageing in a humid environment, than those obtained before ageing of the strands.

strands according to the invention The can advantageously be combined with various materials to be 5 reinforced for the purpose of producing composite items exhibiting good mechanical properties. The composition invention the makes the strands according to particularly compatible with the materials to he reinforced, in particular with organic materials and in also with inorganic 10 particular epoxy materials but

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- materials such as cement materials. possible the impregnation of the sized strands by the material be reinforced. to This particularly suitable for the production of continuous
- 15 strands collected in the form of rovings, cakes, cops, mats, the like or for the production of and cut strands, these different strands being composed of filaments with a diameter which can range from 5 to approximately 24 microns. The sizing composition 20 according to the invention is in particular suited to the production of fine strands (with a count of less

than 600 tex) collected in the form of rovings, in contrast to conventional aqueous sizes.

The sizing composition according to the 25 invention is advantageously deposited during the process according to the invention on filaments intended to be collected into strands and is then polymerized under the effect of a heat treatment, the said treatment taking place independently of the fibre-30 drawing operation (devices thus not being necessary below each die) and it being possible for the said treatment to be carried out at different stages of the process after fibre-drawing.

The heat treatment can in particular be carried out on the collected strands or during the preparation of a composite by combining the sized strands with an organic material. In the case where the strands obtained are collected in the form of wound packages, the heat treatment can be carried out on the strand

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wound packages prior to the use of the strands, in textile applications. If the heat particular in treatment is carried out with respect to the strand wound packages before unwinding the strands, it is desirable for the strand turns constituting the said wound packages to exhibit a crossing angle at least equal to 1.5° in order to prevent adhesive bonding between turns via the polymerized size, these adhesive bondings making it difficult to unwind the strands.

The strands obtained after gathering together filaments can also be collected on receiving the supports in translational motion. They can indeed be projected, by a device which is also used to draw them, towards the collecting surface moving transversely to the direction of the projected strands, for the purpose 15 of obtaining a sheet of intermixed continuous strands, known as a "mat", in which case the heat treatment can be carried out on the strands spread out over the collecting surface. If appropriate, a binder (it being 20 possible for this binder optionally to comprise and to contribute to the size the catalyst(s) mentioned above) may have been projected onto the mat before heat treatment of the combination and the heat treatment may make it possible to polymerize the binder and the size at the same time. 25

The strands can also be cut before collecting by a device which is also used to draw them, the cut being collected on receiving strands supports in translational motion, in which case the heat treatment is preferentially carried out with respect to the cut strands spread out over the receiving supports.

The treatment times for strands collected in the form of rovings weighing several kilograms are at least 1 hour at temperatures greater than approximately 140°C, preferably of the order of 160°C, when the strands are coated with a composition according to the invention not comprising specific catalyst(s) (a high temperature promoting the formation of more stable compounds), the treatment time varying according to the

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shape and the weight of the roving and most of this time being dedicated to raising the temperature of the mass of glass contained in the wound package. When the strands coated with a composition according to the comprising specific catalyst(s) 5 invention not are number of collected on one or а supports in translational motion and when the heat treatment is carried out on the support or supports, the treatment of 15 time is of the order to 20 minutes at temperatures generally greater than approximately 10 140°C. The treatment temperature, whatever the method of collecting the strands, can be lowered by a few tens of degrees (it can decrease by 10 to 30°C for example . 120 and 140°C approximately) and the and be between treatment time reduced when the composition coating the 15 strands comprises at least one specific catalyst as mentioned above.

The strands can also be collected without being subjected to heat treatment, the heat treatment being carried out subsequently. In particular, the strands 20 can be collected in the form of wound packages and can then be extracted from the said wound packages in order to be subjected to additional treatments (for example in order to be cut by a device which is also used to carry them along mechanically), it being possible for 25 the heat treatment to be carried out on the strands before, during or after the additional treatment or treatments (in particular, for the cutting, the heat treatment can be carried out on the device for 30 collecting the cut strands, and the like).

The sized strands can also be collected without having been heat-treated and can then be heat-treated after combining with an organic material during the preparation of а composite, the said material optionally comprising at least one as catalyst mentioned above. Depending on the organic material used, the heat treatment can be accompanied by a treatment with ultraviolet radiation, by a treatment with an electron beam, and the like. The heat treatment



time during the preparation of a composite is generally at least 2 hours, at temperatures greater than approximately 130°C and preferably of the order of 180-200°C.

5 The glass strands coated with the size according to the invention and/or obtained according to the process of the invention are coated with a nonpolymerized size or with a size polymerized after heat treatment. These strands exhibit a loss on ignition 10 advantageously of less than 3% by weight and preferably of less than 1.5%. The small amount of size deposited on the strand makes it possible to greatly reduce the problems of adhesive bonding between strands, in . particular when they are collected in the form of wound packages, also makes possible better opening of the 15 by a material strand during impregnation to be reinforced and is economically advantageous.

The strands obtained according to the invention are easy to handle and can, after collecting, be found 20 in different forms which may or may not require additional stages of treatment of the strands, these stages being carried out before or after the heat treatment and/or the collecting of the strands. The glass strands can thus be provided in the form of continuous strands, of 25 cut strands, may have been combined in the form of braids, tapes, mats or networks, which may or may not be woven, and the like. The strands according to the invention exhibit in particular good tensile strength properties.

The composites advantageously obtained by combining at least glass strands according to the invention and at least one organic and/or inorganic material (the level of glass within these composites generally being between 30 and 70% by weight) exhibit good mechanical properties, as illustrated in the examples below.

Other advantages and characteristics of the invention will become apparent in the light of the following examples giving, by way of illustration but

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without implied limitation, sizing compositions according to the invention and characteristics of the strands coated with these compositions or characteristics of the composites comprising the said strands.

### EXAMPLE 1

Filaments with a diameter of 14 microns obtained by drawing molten glass streams according to the process of the invention are coated with the size with the following composition, expressed as

percentages by weight:

Components of the base system with a molecular mass of less than 750:

•	Trimethylolpropane triglycidyl ether <sup>(1)</sup>	34.0%
•	Diglycidyl ether of 1,4-butanediol <sup>(2)</sup>	18.4%
. •	1,2-Epoxyhexadecane <sup>(3)</sup>	29.1%
•	Methyltetrahydrophthalic anhydride $^{(4)}$	10.0%
<u>Cata</u>	alyst:	
•	1-Methylimidazole <sup>(5)</sup>	0.5%

### 20 <u>Additives:</u>

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Polyethoxylated alkylsilane coupling agent<sup>(6)</sup>

The ratio r in this composition is 0.24.

The filaments are gathered together into 25 strands, which are wound in the form of rovings exhibiting an approximate mass of 13.5 kg, and then the rovings are heated at 140°C for 6 hours.

The strands are then extracted from the wound packages in order to measure their tensile strength and their tenacity at break under the conditions defined by 30 ISO Standard 3341. The results on 8 to 10 test specimens (with the standard deviations shown in brackets) are reported in the appended Comparative Table I, which also gives the count and the loss on ignition of the strands obtained. 35

### EXAMPLE 2

Filaments with a diameter of 14 microns obtained according to the invention are coated with the



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8.0%

size with the following composition (percer	ntages by
weight):	
<u>Components of the base system with a molecula:</u>	<u>r mass of</u>
<u>less than 750</u> :	
3,4-Epoxycyclohexylmethyl 3,4-epoxycyclohe	exane-
carboxylate <sup>(7)</sup>	28%
• Mixture based on vinylcyclohexene	
monoxide <sup>(8)</sup>	28%
• Mixture of phthalic anhydride, of	
hexahydrophthalic anhydride and of	
tetrahydrophthalic anhydride <sup>(9)</sup>	28%
Additives:	
γ-Methacryloyloxypropyltrimethoxysilane	
coupling agent <sup>(10)</sup>	10%
Isopropyl palmitate textile agent	6%
The ratio r in this composition is 0.7	and this
composition exhibits a viscosity of 64 cP at 20	D°C.

The filaments are gathered into strands, which are wound in the form of rovings exhibiting an 20 approximate mass of 13.5 kg. The strands thus collected are not heat-treated.

Composite panels with parallel strands are prepared, in accordance with NF Standard 57152, from the strands obtained exhibiting a count of 320 tex. The 25 reinforced resin is "Epoxy LY 556" resin sold under this reference by the company Ciba-Geigy, to which are added, per 100 parts by weight of epoxy resin, 90 parts of a curing agent sold under the reference "HY 917" by the company Ciba-Geigy and 0.5 parts of an accelerator 30 sold under the reference "DY 070" by the company Ciba-Geigy.

The panels prepared are then heat-treated and the mechanical properties exhibited by these panels, with respect to flexion and shearing, are respectively measured according to ISO Standard 178 and ISO Standard 4585, before ageing and after immersion of these panels in water at 98°C for 24 hours. The results obtained on 8 to 10 test specimens are reported in the appended Comparative Table II, which gives the type of resin



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used for the panels, the flexural strength at break for a level of glass adjusted to 100%, before and after ageing, and the shear strength at break before and after ageing. The standard deviations are shown in brackets.

### EXAMPLE 3

The procedure is the same as in Example 2, the heat treatment, however, being carried out with respect to the strand wound packages and not with respect to the composite panels. The strand rovings obtained in Example 2 are thus heated, in the present example, at 160°C for 8 hours. No deformation of these rovings is observed. The results obtained with respect to composite panels in the present example are reported in Table II.

The tensile strength and tenacity at break of the heat-treated strands extracted from the wound packages are also measured, as in Example 1. The results are reported in Table I.

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#### EXAMPLE 4

Filaments with a diameter of 14 microns obtained according to the invention are coated with the size with the following composition (percentages by weight):

25 <u>Components of the base system with a molecular mass of</u> <u>less than 750:</u>

- 3,4-Epoxycyclohexylmethyl 3,4-epoxycyclohexanecarboxylate<sup>(7)</sup> 25.0%
- Diglycidyl ether of 1,4-butanediol<sup>(2)</sup>
   2-Ethylhexyl glycidyl ether<sup>(11)</sup>
   20.0%
  - Methyl-5-norbornene-2,3-dicarboxylic
     anhydride<sup>(12)</sup> 36.5%

<u>Catalyst:</u>

# 1-Methylimidazole<sup>(5)</sup>

35 <u>Additives:</u>

Polyethoxylated alkylsilane coupling agent<sup>(6)</sup>

8.0%

0.5%

The ratio r in this composition is 1.3 and this composition exhibits a viscosity of 72 cP at 20°C.

- 22 are

gathered together

into

strands, which are wound in the form of rovings weighing approximately 13.5 kg, and are then heated at 160°C for 6 hours. The tensile strength and tenacity at break of the strands are then measured, as in Example 1 (Table I). The resistance to abrasion of the strands is

The

filaments

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also evaluated by weighing the amount of flock formed after passing the strands over a series of rods. For different strands coated with the polymerized size described in the present example, the amount of flock on conclusion of the test is of the order of 1 mg per kg of strand tested.

By way of comparison, strands coated with an aqueous size based on an emulsion containing epoxy resin, silanes and surfactants, these strands being dried according to normal methods, can form 200, indeed 500, mg of flock per kg of strand.

### EXAMPLE 5

Filaments with a diameter of 10 microns 20 obtained according to the invention are coated with the size with the following composition (percentages by weight):

<u>Components of the base system with a molecular mass of</u> <u>less than 750:</u>

25	Diglycidyl ether on a novolak phenol			
	base <sup>(13)</sup>		25.	0%
	Diglycidyl ether of 1,4-butanediol <sup>(2)</sup>		10.	0%
	· 2-Ethylhexyl glycidyl ether <sup>(11)</sup>		16.	5%
	• Methyltetrahydrophthalic anhydride <sup>(4)</sup>		40.	0%
30	<u>Catalyst:</u>			
	<ul> <li>1-Methylimidazole<sup>(5)</sup></li> </ul>		0.5	58
	Additives:			
	• Polyethoxylated alkylsilane coupling			
	agent <sup>(6)</sup>		8.0	)%
35	The ratio r in this composition	is	1.57	and

this composition exhibits a viscosity of 104 cP at 20°C.

The filaments are gathered together into strands, which are wound in the form of cakes weighing

PRISTRALINE PRINT OFFICE approximately 7 kg, and are then heated at  $140 \,^{\circ}$ C for 6 hours. The tensile strength and tenacity at break of the strands are then measured, as in Example 1 (Table I).

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# EXAMPLE 6

Filaments obtained according to the invention are coated with a size with the following composition (percentages by weight):

<u>Components of the base system with a molecular mass of</u> <u>less than 750:</u>

•	Trimethylolpropane triglycidyl ether <sup>(1)</sup>	24%
•	2-Ethylhexyl glycidyl ether <sup>(11)</sup>	24%
	Mather 5 markers and 0 2 disambar lis	

Methyl-5-norbornene-2,3-dicarboxylic
 anhydride<sup>(12)</sup>
 40%

15 <u>Additives:</u>

γ-Methacryloyloxypropyltrimethoxysilane coupling agent<sup>(10)</sup> 12%

The ratio r in this composition is 1.9.

The filaments are gathered together into 20 strands, which are wound in the form of rovings. The collected strands are not heat-treated.

Composite panels are prepared from these strands, which are easily extracted from the wound packages obtained, in the same way as in Example 2 and 25 are then heat-treated and the mechanical properties of these panels, measured under the same conditions as in Example 2, are reported in Table II.

### EXAMPLE 7

The procedure is the same as in Example 6, use 30 being made of an identical sizing composition but which comprises a lower level of coupling agent (11.6% instead of 12%) and which additionally comprises a in the form catalyst of а 2,4,6tridimethylaminomethylphenol, sold under the reference 35 "Protex NX3" by the company Protex, at levels of 0.4% by weight of the composition.

The results are reported in Table II.

EXAMPLE 8



Filaments obtained according to the invention are coated with the size with the following composition (percentages by weight):

Components of the base system with a molecular mass of

•	Tetraglycidyl ether of 4,4'-diamino-	
	diphenylmethane <sup>(14)</sup>	20.0%
•	Cresyl glycidyl ether <sup>(15)</sup>	15.0%
•	Diglycidyl ether of cyclohexane-	
	dimethanol <sup>(16)</sup>	8.0%
•	Methylhexahydrophthalic anhydride <sup>(17)</sup>	42.0%

2-Propylimidazole<sup>(18)</sup> 0.3%

<u>Additives:</u>

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15 γ-Methacryloyloxypropyltrimethoxysilane coupling agent<sup>(10)</sup> 8.7% γ-Glycidoxypropyltrimethoxysilane coupling

agent<sup>(19)</sup>

The ratio r in this composition is 1.68.

6.0%

The procedure is then as in Example 6, use being made in the composite panels prepared, in place of the epoxy resin, of a polyester resin "M 402", sold under this reference by the company Ciba-Geigy, to which are added, per 100 parts by weight of polyester resin, 20 parts of a softening agent sold under the reference "F 8010 C" by the company Ciba-Geigy, 16.5 parts of styrene and 1.5 parts of an accelerator sold under the reference "THM 60" by the company Ciba-Geigy.

The results are reported in Table II.

## EXAMPLE 9

The procedure is the same as in Example 6, the sizing composition used being replaced by the following composition (percentages by weight):

<u>Components of the base system with a molecular mass of less than 750:</u>

•	Bisphenol A diglycidyl ether <sup>(20)</sup>	21.0%
•	Cresyl glycidyl ether <sup>(15)</sup>	25.0%

Methylhexahydrophthalic anhydride<sup>(17)</sup> 42.0%

<u>Catalyst:</u>

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- 25 -	,
• Organometallic amine in polyglycols <sup>(21)</sup>	0.4%
Additives:	
<ul> <li>γ-Methacryloyloxypropyltrimethoxysilane coupl</li> </ul>	ling
agent <sup>(10)</sup>	11.6%
The ratio r in this composition is 1.98.	
The procedure is then as in Example	6. The
results are reported in Table II.	
EXAMPLE 10	
Filaments obtained according to the inv	vention
are coated with the size with the following compo	osition
(percentages by weight):	
Components of the base system with a molecular m	<u>nass of</u>
less than 750:	
• Diglycidyl ether of cyclohexanedi-	
methanol <sup>(16)</sup>	10.0%
2-Ethylhexyl glycidyl ether <sup>(11)</sup>	14.0%
Methylhexahydrophthalic anhydride <sup>(17)</sup>	40.0%
<u>Components of the base system with a molecula</u>	
Components of the base system with a molecula	r mass
<u>Components of the base system with a molecula</u> greater than 750:	r mass
Components of the base system with a molecula greater than 750: • Triglycidyl ether on an aliphatic polyol bas	<u>r mass</u> e
<u>Components of the base system with a molecula</u> <u>greater than 750:</u> <ul> <li>Triglycidyl ether on an aliphatic polyol bas with an average molecular mass of 1950<sup>(22)</sup></li> </ul>	<u>r mass</u> e

- 25 · γ-Methacryloyloxypropyltrimethoxysilane coupling agent<sup>(10)</sup> 11.6%
  - Isopropyl palmitate textile agent4.0%The ratio r in this composition is 2.96.

The filaments are gathered together into 30 strands, which are wound in the form of rovings, and are then heated at 145°C for 8 hours. The tensile strength and tenacity at break of the strands are then measured as in Example 1 (Table I).

Composite panels are prepared from the strands obtained, which are easily extracted from the wound packages, in the same way as in Example 3, use being made, however, as resin, in place of the epoxy resin LY 556, of an epoxy resin "CY 205", sold under this reference by the company Ciba-Geigy, to which are



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added, per 100 parts by weight of epoxy resin, 32 parts by weight of a curing agent sold under the reference "HT 972" by the company Ciba-Geigy.

The mechanical properties of the panels 5 obtained are measured as in Example 2, before ageing and after immersion of the panels in water at 98°C for, this time, 72 hours (Table II)

#### EXAMPLE 11

The procedure is as in Example 2, use being 10 made of an identical sizing composition but which comprises a lower level of 3,4-epoxycyclohexylmethyl 3,4-epoxycyclohexanecarboxylate (9.3% instead of 28%), a lower level of the mixture based on vinylcyclohexene monoxide (18.7% instead of 28%) and a higher level of 15 the mixture of phthalic anhydride, of hexahydrophthalic anhydride and of tetrahydrophthalic anhydride (58% instead of 28%). The ratio r in this composition is 2.84 and this composition exhibits a viscosity of 76 cP at 20°C.

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The results are reported in Table II.

# EXAMPLE 12

The procedure is as in Example 3, the sizing composition explained in Example 11 being used.

The results are reported in Tables I and II.

The resistance to abrasion of the strands is also measured as in Example 4. The amount of flock weighed on conclusion of the test is 99 mg per kg of strand.

#### EXAMPLE 13

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Filaments with a diameter of 14 microns obtained according to the invention are coated with the size with the following composition (percentages by weight):

<u>Components of the base system with a molecular mass of less than 750:</u>

- 3,4-Epoxycyclohexylmethyl 3,4-epoxycyclohexanecarboxylate<sup>(7)</sup> 9.25%
- Mixture based on vinylcyclohexene monoxide<sup>(8)</sup>



9.25%

Mixture of phthalic anhydride, of hexahydrophthalic anhydride and of tetrahydrophthalic anhydride<sup>(9)</sup>

γ-Methacryloyloxypropyltrimethoxysilane coupling agent<sup>(10)</sup> 20%

55.5%

6%

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Isopropyl palmitate textile agent

The ratio r in this composition is 4.19 and this composition exhibits a viscosity of 62 cP at 20°C.

The filaments are gathered together into strands, which are wound in the form of rovings weighing approximately 13.5 kg, and are then heated at 160°C for 8 hours. The tensile strength and tenacity at break of the strands are then measured, as in Example 1 (Table I).

The resistance to abrasion of the strands is also measured as in Example 4. The amount of flock weighed on conclusion of the test is 57 mg per kg of strand.

#### COMPARATIVE EXAMPLE

The mechanical characteristics of the composites obtained using the strands described in Examples 2, 3 and 6 to 12 are compared with the mechanical characteristics of the composites obtained using reference strands coated with an aqueous size 25 based on an emulsion containing epoxy resin, silanes and surfactants, the latter composites being prepared in the same way as in Examples 8 (the heat treatment, however, being carried out with respect to the strand 30 wound packages and not with respect to the composite panels) and 10 (the heat treatment of the strands being, however, carried out at a higher temperature) respectively, and the mechanical properties of the latter composites, measured as in Examples 2 and 10 35 respectively, being reported in Comparative Table II.

It is observed, in the preceding examples, that the strands coated with size according to the invention are easy to handle, whether or not they had been heattreated, and exhibit good tensile strength properties.

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Remarkably and advantageously, the tensile strength properties of the strands coated with size according to the invention are better after the beginning of ageing in a humid environment than those obtained before ageing of the sized strands.

The strands obtained according to the invention moreover exhibit a low loss on ignition and good resistance to abrasion and make it possible to efficiently reinforce organic and/or inorganic materials.

The low levels of flock obtained during the tests of resistance to abrasion of the strands and the good tensile strength properties of the strands also make it possible to say that the strands obtained according to the invention exhibit good integrity. The strands obtained also give good texturing results.

The strands coated with size according to the invention moreover make it possible to obtain composites exhibiting mechanical properties which are as good as those of the composites obtained from strands coated with conventional aqueous sizes.

The glass strands according to the invention can be used in various applications, for example in textile applications, such as the manufacture of warps 25 by warping, or directly in reinforcing applications, such as the reinforcement of organic materials (for example plastics) or inorganic materials (for example cement materials), in order to obtain composite products.

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(1)	Sold under	the	reference	"Heloxy	5048"	by	the	company	Shel
(1)	Sora mider	CHE	TELETENCE	neroxy	2040	DY	CITE	company	She

- (2) Sold under the reference "Heloxy 67" by the company Shell
- (3) Sold under the reference "UVR 6216" by the company Union Carbide
- 35 (4) Sold under the reference "HY 917" by the company Ciba-Geigy
  - (5) Sold under the reference "DY 070" by the company Ciba-Geigy
  - (6) Sold under the reference "Silquest A 1230" by the company OSI
  - (7) Sold under the reference "UVR 6110" by the company Union

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		Carbide
	(8)	Sold under the reference "UVR 6200" by the company Union
		Carbide
	(9)	Sold under the reference "HY 905" by the company Ciba-Geigy
5	(10)	Sold under the reference "Silquest A 174" by the company OSI
	(11)	Sold under the reference "Heloxy 116" by the company Shell
	(12)	Sold under the reference "HY 906" by the company Ciba-Geigy
	(13)	Sold under the reference "Araldite PY 307" by the company
		Ciba-Geigy
10	(14)	Sold under the reference "Araldite MY 722" by the company
		Ciba-Geigy
	(15)	Sold under the reference "Heloxy 62" by the company Shell
	(16)	Sold under the reference "Heloxy 107" by the company Shell
	(17)	Sold under the reference "HY 1102 BD" by the company
15		Ciba-Geigy
	(18)	Sold under the reference "Actiron NXJ 60" by the company
		Protex
	(19)	Sold under the reference "Silquest A 187" by the company OSI
	(20)	Sold under the reference "Araldite GY 250" by the company
20		Ciba-Geigy
	(21)	Sold under the reference "DY 071" by the company Ciba-Geigy
	(22)	Sold under the reference "Heloxy 84" by the company Shell



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COMPARATIVE	TABLE I	
 · · · · · · · · · · · · · · · · · · ·		

1		Ex.1	Ex.3	Ex.4	Ex.5	Ex.10	Ex.12	Ex.13
5	Count (tex)	320	320	320	84	320	320	320
	Loss on							
	ignition (%)	0.93	0.58	0:82	0.56	0.42	0.39	0.40
	Tensile							
	strength at							
10	break (kgf)	16.5	18.2	19.0	4.7	17.2	18.7	18.1
	σ	(0.8)	(1.1)	(0.7)	(0.2)	(0.6)	(0.8)	(1.4)
	Tenacity							
	(g/tex)	48.6	57.8	57.0	53.3	53.6	55.2	56.1
	σ	(2.3)	(3.4)	(2.0)	(2.8)	(2.0)	2.3)	(4.4)

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# COMPARATIVE TABLE II

	Ex.2	Ex.3	Ex.6	Ex.7	Ex.8	Ex.9	Ex.10	Ex.11	Ex.12	Compa- rative Ex.	Compa- rative Ex.
Resin used	Epox	у Ероху	Ероху	Ероху	Poly- ester	Ероху	Ероху	Ероху	Ероху	Poly- ester	Ероху
Flexur streng at bre for 10	th ak			<u> </u>							
glass (MPa) ·Befor	-										
ageing σ ·After	(65)	2122 (62)	2207 (46)	2361 (63)	2268 (68)	2274 (66)	2022 (83)	2379 (43)	2334 (49)	2440 (70)	2280 (40)
ageing ø	2241 (89)	1767 (65)	1822 (29)	1758 (81)	1406 (38)	1883 (69)	1408 (67)	2211 (99)	1977 (85)	1370 (40)	1400 (20)
Shear streng at bre											
(MPa) ·Befor agein	-	86.0	56.0	69.4	59.8	48.8	56.3	85.1	68.6	56.5	69.5
σ After agein			(0.9) 49.4	(0.8) 50.8	(0.4) 28.6	(0.8) 49.0	(0.9) <b>4</b> 1.2	(1.4) 64.7	(1.8) 49.0	(1.0) 25.0	(1.0)
σ	(5.1		(1.3)	(1.4)	(0.2)	(0.5)		(2.1)	-	(0.5)	(0.4)

*...* 



THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:

 A glass strand coated with a sizing composition composed of a solution with a viscosity of less than or
 equal to 400 cP including less than 5% by weight of solvent and at least one thermally polymerizable and/or crosslinkable base system, the said base system including at least 60% by weight of components with a molecular mass of less than 750 and at least 60% by weight of a mixture:
 of component(s) exhibiting at least one epoxy

reactive functional group, and

of component(s) exhibiting at least one anhydride reactive functional group.

15 2. A glass strand according to claim 1, in which the base system represents between 60 and 100% by weight of the sizing composition.

3. A glass strand according to claim 1 or 2, in which the base system is composed solely of component(s) exhibiting at least one epoxy reactive functional group and of component(s) exhibiting at least one anhydride reactive functional group.

A glass strand according to any one of claims 1 to 3, in which the sizing composition additionally includes at least one catalyst which facilitates the opening of the anhydride or epoxy functional groups under the effect of heat.

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5. A glass strand according to any one of claims 1 to 4, in which the sizing composition additionally includes at least one coupling agent in an amount of between 0 and 25% by weight.

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6. A glass strand according to any one of claims 1 to 5, in which the sizing composition additionally includes

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at least one film-forming agent in an amount of between 0 and 10% by weight.

7. A glass strand according to any one of claims 1
5 to 6, in which the sizing composition additionally includes at least one textile agent in an amount of between 0 and 15% by weight.

8. A sizing composition for a glass strand composed
10 of a solution with a viscosity of less than or equal to 400 cP including less than 5% by weight of solvent and at least one thermally polymerizable and/or crosslinkable base system, in which the base system includes at least 60% by weight of components with a molecular mass of less than 750
15 and at least 60% by weight of a mixture:

of component(s) exhibiting at least one epoxy reactive functional group, and

of component(s) exhibiting at least one anhydride reactive functional group.

9. A sizing composition according to claim 8 in which the base system represents between 60 and 100% by weight of the sizing composition.

25 10. A sizing composition according to claim 8 or 9 in which the base system is composed solely of component(s) exhibiting at least one epoxy reactive functional group and of component(s) exhibiting at least one anhydride reactive functional group.

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11. A sizing composition according to any one of claims 8 to 10 further including at least one catalyst which facilitates the opening of the anhydride or epoxy functional groups under the effect of heat.

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12. A sizing composition according to any one of claims 8 to 11 further including at least one coupling

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DSTRALIAN P agent in an amount of between 0 and 25% by weight.

13. A sizing composition according to any one of claims 1 to 12 further including at least one film-forming
5 agent in an amount of between 0 and 10% by weight.

14. A sizing composition according to any one of claims 8 to 13 further including at least one textile agent in an amount of between 0 and 15% by weight.

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15. A process for the production of sized glass strands including drawing a multiplicity of molten glass streams, flowing from a multiplicity of orifices arranged at the base of one or a number of dies, in the form of one or a number of sheets of continuous filaments and then gathering the filaments together in one or a number of strands, collecting the strands on a moving support, and depositing a sizing composition according to any one of claims 8 to 14 on the surface of the filaments during 20 drawing and before gathering together the filaments into strands.

16. A process according to claim 15, in which the strands are collected in the form of wound packages on a rotating support, and wherein the crossing angle of the wound packages is at least equal to 1.5°.

17. A process according to claim 15 or 16, in which the sizing composition is subjected to a heat treatment during or after collecting the strands coated with the said composition.

18. A process according to any one of claims 15 to
17, in which the sized strands collected are brought into
35 contact with an organic material to be reinforced, before subjecting the combination to a heat treatment, so as to obtain a composite.

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19. A composite including at least one organic and/or inorganic material and sized glass strands, in which at least a part of the sized glass strands are in accordance
5 with any one of claims 1 to 7.

20. A glass strand coated with a sizing composition substantially as herein described with reference to the accompanying examples apart from the comparative examples.

21. A sizing composition for a glass strand substantially as herein described with reference to the accompanying examples apart from the comparative examples.

15 22. A process for the production of sized glass strands substantially as herein described with reference to the accompanying examples apart from the comparative examples.

20 23. A composite substantially as herein described with reference to the accompanying examples apart from the comparative examples.

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