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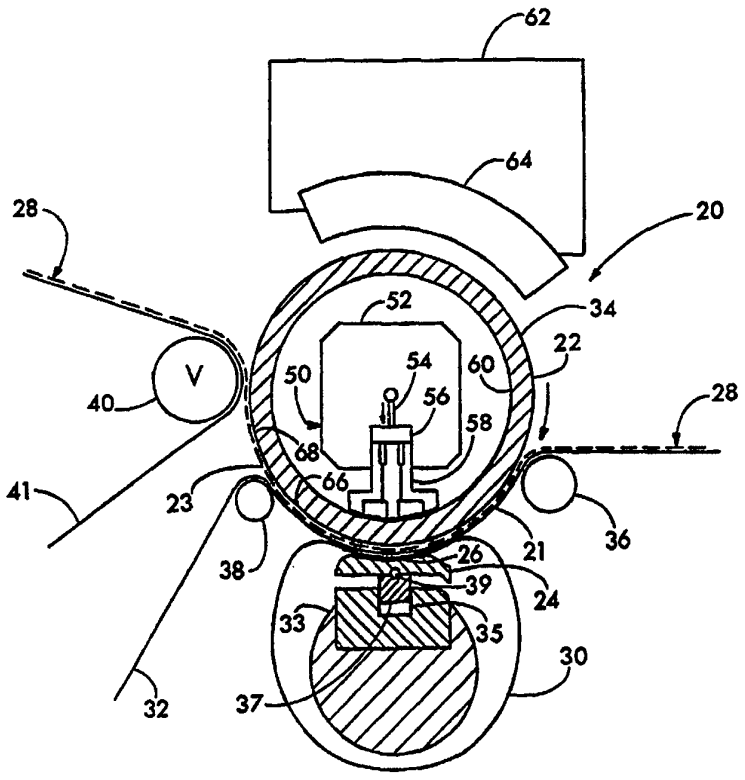
(54) Title: HEAVY-WEIGHT HIGH-TEMPERATURE PRESSING APPARATUS

(57) Abstract

An extended nip press has a heated backing roll (22), on the surface of which a paper web (28) is preheated before it passes through the extended nip. The paper web is restrained on the surface of the backing roll (22) to achieve post-pressing drying. During a portion of the post-pressing drying, the extended nip press may be arranged so that the paper web is not backed by the pressing/drying felt, thus allowing free venting from the web to occur. In some cases, this zone will be augmented by a vacuum assist unit to draw steam away. This high temperature press is capable of outgoing dryness in the range of sixty-five percent versus fifty percent for conventional technology. This combination of high temperature pressing and drying can be expected to improve the maximum strength of the web by approximately 20 percent or more over conventional pressing methods. Two high temperature press dryers of this invention may be combined to achieve outgoing dryness of approximately seventy percent.



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PATENT APPLICATION

TITLE: HEAVY-WEIGHT HIGH-TEMPERATURE PRESSING APPARATUS

FIELD OF THE INVENTION

This invention relates to papermaking machines in general. More particularly, this invention relates to paper web presses and dryers. Still more particularly, this invention relates to paper web dryers which employ an extended nip press.

BACKGROUND OF THE INVENTION

Over the years, many advances have been made in the process of converting wood pulp into paper. The papermaking art includes depositing a layer of fibrous pulp, or stock, onto a moving screen and draining excessive water from the fibrous stock to form a relatively thin, fibrous web on the surface of the screen. In order to dry the web as well as increase its strength, the web is removed from the screen and passed through various pressing rolls to reduce the amount of water remaining in the web. After passage through the press section of a papermaking machine, where the web's density has been increased, the web is conducted around multiple heated drums, or dryers, such that excess water remaining in the web is removed.

In a modern papermaking machines, it is not uncommon to have in the drying section eighty or more dryer drums, with each drum having a diameter of five feet and a length of up to 33 feet. Of necessity, these dryer drums take up an enormous floor area which greatly exceeds the floor area required for the installation of the forming and pressing section combined. Additionally, with escalating fuel costs, it is evident that if more water can be removed in the press section, less energy will be required in the drying section. Consequently, much research has been carried out in an attempt to remove ever greater quantities of water from the paper web before it leaves the press section. This

reduces the number of dryer drums required and the amount of energy and steam required to drive off any remaining moisture within the web.

A breakthrough in press section design was commercialized in 1980 by the introduction of the so-called "extended nip press" (herein referred to as an ENP), which successfully increases the percent fiber in the web after pressing from 35 present to approximately fifty percent. The main features of the ENP, as compared to the prior conventional pressing technique, may be outlined as follows..

In conventional pressing, the web passes through the nip defined by counter-rotating rolls, whereas in the ENP, one of the rolls is replaced by a concave shoe. The concave surface of the shoe cooperates with the outer surface of a press roll to define therebetween an elongated or extended pressing section, such that the web is pressed with a moderate pressure for an extended period of time between the press roll and the shoe. In order to permit the web to pass through the extended nip, a moveable blanket is disposed between the concave surface and the web, so that the web is pressed between the blanket and the pressing roll during passage through the press section.

More recent improvements in the ENP have involved solving a problem of oil leakage from the nip blanket by extending the blanket beyond the ends of the backing roll where the ends may be made to take a circular shape and sealing them to rotating heads.

Further improvements in the function of the ENP have been achieved by induction heating the surface of the backing, or press roll, in the temperature range of 200 to 600 degrees Fahrenheit. The addition of heat to the ENP to form a so-called impulse dryer has resulted not only in better drying of the web, but also increased mechanical properties, such as web strength. Increased

web strength can have tremendous pay-back in reducing the cost of paper production.

The ability to manufacture increased strength paper or paperboard can allow changes in the furnish, the fibers used to construct the paper. The ability to develop greater strength in a paper or paperboard web allows the use of lower-cost, and lower-strength fibers, or the use of a lower-weight paper for a particular application. Using less fiber, or fiber of lower cost, can yield a dramatic cost savings, particularly for heavy-weight paper or paperboard materials.

What is needed is a combination press dryer which can provide improved drying and strength development, particularly for heavier weight paper webs.

SUMMARY OF THE INVENTION

The dryer of the present invention achieves more effective drying by engaging the web against the dryer backing roll both before it enters the extended nip and after it leaves the extended nip. The web is thus preheated on the surface of the backing roll before it passes through the extended nip. Further, the web is retained on the surface of the backing roll to achieve post-pressing drying. During a portion of the post-pressing drying, the apparatus of this invention may be arranged so that the paper web is not backed by the pressing/drying felt, thus allowing free venting from the web to occur. In some cases, this zone will be augmented by a vacuum assist unit to draw the steam away.

In a conventional ENP, if a 42 pound sheet enters at twenty to thirty percent dryness, just one pass will generally increase dryness some ten to twenty points. With a combination of preheating, hot-pressing, and post-drying through a high temperature pressing unit, outgoing dryness can be bettered by

ten to fifteen more percentage points. Thus, this high temperature pressing can be capable of outgoing dryness in the range of sixty-five percent versus current, conventional technology which is capable of outgoing dryness in the range of fifty percent. This combination of high temperature pressing and drying can be expected to improve the maximum strength of the web by approximately 20 percent or more over conventional pressing methods.

Two high temperature press dryers of this invention may be combined to achieve outgoing dryness in excess of seventy percent. The dryers may both rotate in the same direction, so that the web presents a single surface to both dryers, and the open draw between the dryers being parallel to a plane containing the axes of rotations of both dryer rolls. The open draw of the web between the dryer drums may be enclosed in vacuum assists for the removal of steam. This further increases drying of the web as it transits from one drum to the other. Alternatively, the drums may rotate in opposite directions, with the paper web presenting a different side to each drum, with the open draw crossing the plane containing the axes of rotation of the two drums.

The dryer press of this invention consists of a backing roll, the surface of which is heated by an induction heater. A backing felt transports a formed web containing twenty to thirty percent dry weight fibers. The backing felt is wrapped together with the web around approximately ninety to one-hundred degrees of the circumferential surface of the roll. After which, the backing felt is led away from the roll and the web alone continues to be wrapped for approximately another forty-five degrees around the roll until it is removed by a second drying felt. Approximately half way along its travels on the surface of the backing roll, the first felt in the web is passed through an ENP. The combination of the first felt being wrapped around a portion of the circumference of the backing roll and being more or less centered about the portion of the backing roll forming the ENP, is to create a preheat zone which warms the web

before it enters the ENP, and a post-heat zone which transits into a drying zone where the web is allowed free venting before being removed from the backing roll.

It is an object of the present invention to provide an apparatus for reducing the length of a dryer section in a papermaking machine.

It is another object of the present invention to provide an apparatus for increasing the strength of a paper or a paperboard web.

It is a further object of the present invention to provide a papermaking apparatus which requires less stock or stock of a lower cost to manufacture a particular strength or grade of paper or paperboard.

It is yet another object of the present invention to provide a papermaking apparatus which can improve the surface finish on a paper web.

It is a still further object of the present invention to provide a combination press dryer which in one press can increase the dryness of a paper web by fifteen to thirty-five percentage points.

Further objects, features, and advantages of the invention will be apparent from the following detailed description when taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a somewhat schematic, side-elevational view of a single drum press dryer of this invention.

FIG. 2 is a somewhat schematic, side-elevational view of two press dryers of this invention, wherein both dryer rolls rotate in the same direction.

FIG. 3 is a somewhat schematic, side-elevational view of two press dryers of this invention wherein the dryer drums rotate in opposite directions.

FIG. 4 is a somewhat schematic, side-elevational view of an alternative embodiment of this invention having two press dryers.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring more particularly to FIGS. 1-4, wherein like numbers refer to similar parts, an improved type of impulse dryer **20** is shown in FIG. 1. The impulse dryer **20** employs a preheat zone **21**, a pressing zone or extended nip **26**, and a post-heat zone **23**. The zones **21**, **26**, **23** are defined on a press roll **22** which forms the nip **26** with a shoe **24**. The shoe **24** is provided with a concave surface which faces the roll **22** and is mounted so that it is urged towards the roll **22**. The press nip 26 is formed between the roll **22** and the shoe **24**. A web of paper **28** is brought into contact with the surface **34** of the roll **22** by an infeed roll **36** where it is preheated by the hot surface **34** of the roll **22**. The web **28** then passes through the nip **26** and is subjected to the pressing zone **26**. A press felt **32** underlies the web **28** and moves beneath the web **28** and over a looped belt **30**. The web **28**, the felt **32** and the belt **30** together pass through the nip **26** between the shoe **24** and the roll **22**.

Oil is supplied between the shoe **24** and the belt **30**. The oil causes a hydrodynamic wedge of fluid to build up between the belt **30** and the shoe **24**. The fluid wedge transmits pressure to the web while at the same time lubricating the movement of the web **28** through the nip **26**. The press felt **32** passes through the nip **26** while underlying the paper web **28** and riding on the belt **30**. The paper web **28**, the press felt **32**, and the belt **30**, as well as the roll

22, are in engagement and so driven at the same speed. Thus the paper web 28 does not experience significant sheer force because there is no relative motion in the plane of the web 28 and the press felt 32 and the surface 34 of the press roll 22. Thus the paper web 28 is subject to principally compressive forces as it moves through the extended nip 26. The effect of this compressive force is to bring the web into intimate contact with the surface 34 of the press roll 22.

The intimate engagement of the web 28 with the press roll surface 34 under pressure facilitates the rapid heat exchange between the surface 34 of the roll 22 and the web 28. The rapid heat transfer between the roll 22 and the web 28 produces a not completely understood drying mechanism which is characteristic of the impulse dryer. The rapid heating of the paper web vaporizes some of the water contained in the web. The steam which has been produced from the water in the web is trapped between the surface 34 of the roll 22 and the paper web 28. Its only route of escape is through the paper web 28 into the press felt 32. The rapid downward movement of the steam from the upper surface of the paper web 28 downwardly into the press felt 32 has the effect of blowing water contained in the web 28 into the felt 32. This process, impulse drying, results in the rapid removal of water from the paper web 28.

After the nip or pressing zone 26 the web 28 moves through a post-heat zone. In the post-heat zone the web 28 is backed by the felt for a distance, after which the felt 32 is stripped away by a stripping roll 38 and the web 28 is free to vent from its back side. After vented post-heating, the web 28 is removed from the press roll 22 by a transfer felt 41 which is fed around out the feed roll 40.

As will be appreciated by those versed in the art of papermaking, the cross-machine width of the paper web 28 will normally be between one-hundred and four-hundred inches, with the components of the impulse dryer such as the

roll **22** being in general somewhat longer, as necessitated by their particular function.

The looped belt **30** and its method of support are conventional and are described more fully in U.S. Patent Number 4,673,461 to Roerig et al. The belt **30** is a continuous loop. It has a cross-machine width greater than the press roll **22**, so that the ends of the belt (not shown) may be sealed to circular closures (not shown) which seal the ends of the belt, thus containing the nip lubricating oil within the sealed belt **30**. A stationary beam **33** is contained within the belt **30**. The beam adjustably supports the shoe **24** by means of a hydraulic piston chamber **35** in which is positioned a piston **37**. The shoe **24** is pivotally supported on a roller pin **39**, seated in a downward facing groove in the shoe **24** and an upward facing groove in the piston **37**. The piston is urged upward by fluid pressure beneath the piston in the chamber **35**, which is in the form of an elongated slot, slidably receiving the piston, and extending the full width of the machine beneath the shoe **24**. The belt **30** may be guided by means of curved guides (not shown) or by internal air pressure which serves to stabilize the belt **30** during start-up. The guides or air pressure also stabilize the belt **30** if any fluttering or instability should occur during normal operation.

Once the belt **30** has reached operational speed, centrifugal force will cause the belt **30** to assume a naturally circular shape, except where traversing the nip **26** between the shoe **24** and the press roll **22**.

The press felt **32** is supported on the infeed roll **36** and the outfeed roll **38**. The infeed press felt roll **36** and outfeed roll **38** will typically have a diameter of two feet, where the corresponding diameter of the press roll **22** is five feet. The rolls **36**, **38** serve to bring the press felt into position to be fed through the nip **26** of the impulse dryer **20**. The press felt **32**, after leaving the outfeed roller **38**, is processed by a felt dryer (not shown), which removes water

and excess moisture from the felt **32** before it returns for reuse over the infeed roller **36**.

The press roll **22** in FIG. 1 is shown employing a hydraulic crown control mechanism **50** which has a non-rotating crown support beam **52**. The crown support beam has an oil supply port **54** which supplies oil to piston cavities **56** which drive pistons **58** against the inner surface **60** of the metallic base shell **38**. Pistons **58** which are spaced along the central beam or shaft **50** serve to apply a constant pressure between the press roll **22** and the shoe **24**.

In FIG. 1, an induction heater **62** is shown schematically. It has coils **64** which are energized with high frequency current. The induction heater **62** is conventional in nature. It employs oscillating magnetic fields caused by the high frequency alternating current, which create eddy currents in the surface **34** of the roll **22**. The currents induced produce resistance heating in the surface **34** thereby heating it to the desired temperature. The temperature of the roll surface is preferably raised to between 400 degrees and 500 degrees Fahrenheit.

High temperature pressing studies conducted with heavy-weight linerboard grades indicate that web preheating in the preheat zone **21**, hot pressing in the nip **26**, and post drying in the post-heat zone **23**, if conducted while the web **28** is restrained on the surface **34** of the drum **22**, offer higher water removal capabilities and improved product strength over conventional pressed, then dried, sheets.

It is important that the web **28** be restrained without sticking to the surface **24** in order to avoid the delamination that will occur when sticking occurs. It is equally important that the web **28** be restrained against the surface

34 during the pressing and drying process in order to maximize water removal and strength development.

The impulse dryer 20 presses and dries the paper web 28 in three zones, a preheat zone 21, a hot-pressing zone (or extended nip) 26, and a post-heat zone 23, as shown in FIG. 1. The post-heat zone 23 is divided into a web-backed zone 66 and a free-venting zone 68.

The web 28 is carried to the heated cylinder 22 by a hot press felt 32. The cylinder 22 is typically heated to a temperature of 400 degrees Fahrenheit; however, temperatures in the range of 300 degrees to 900 degrees Fahrenheit are well within the realm of this process, provided that other technological barriers can be overcome. A 300 degrees to 500 degrees Fahrenheit system is currently feasible. The function of the three zones, 21, 26, 23 are described as follows:

In the preheat zone 21, the web 28 is held in contact with the roll surface 34 so that its temperature may be raised to 212 degrees Fahrenheit or higher.

In the nip, or hot press zone, 26, the web 28 is subjected to high pressure to facilitate water removal by venting flashing stream into the hot felt. This zone 26 will develop the most strength.

In the post-heat drying zone 23, the web 28 is constrained against the hot surface 34 of the roll 22. An important function of the drying zone 23 is the free drying zone 68 which allows free venting from the web 28 to occur while the web is constrained on the surface 34. The free venting zone 68 could be augmented by a vacuum assist unit (not shown) to draw the steam away from the web 28.

In a conventional extended nip press, if a 42-pound sheet enters at twenty to thirty percent dryness, just one pass through the press will generally increase dryness some ten to twenty percentage points. Percent dryness is the percent of the web **28** which constitutes dry fiber by weight. With the combination of preheating, hot pressing, and post drying through a high temperature pressing unit **20**, the outgoing dryness can be bettered by five to fifteen percentage points over a conventional dryer. Thus, this high temperature pressing with pre- and post-heating can be capable of outgoing drynesses in the range of sixty-five percent versus current conventional technology in the fifty percent range.

Pressing along with drying improves product strength versus drying only. The high temperature pressing unit described should maximize strength development some twenty percent or more over conventional pressing, depending on the product furnish (fiber content) and bonding characteristics. Strength development may be best achieved by multiple hot pressing steps during the post drying cycle.

To achieve even greater solid content in a web, two press rolls **70**, **72** may be combined in a dryer **74**, as shown in FIG. 2. Backing rolls **70**, **72** are heated by induction heaters **76**, **78**. The backing roll **70** is employed with an extended nip press **80** which is shown in FIG. 2 as an open-ended type where the blanket **82** is supported by blanket rolls **84** and wherein one blanket roll **86** also functions as a press felt **32** outfeed roller. Similarly, the backing roll **72** has an extended nip press **88**.

As will be understood by those skilled in the art of papermaking, the extended nip presses **80**, **88** could be of the apple type shown in FIG. 1. Although the particular type of extended nip is a design choice, in many circumstances the apple-type extended nip is preferable because the end seals

contain the lubricating oil which reduces friction between the shoe **24** and the looped belt **82**.

The extended nip **80** on the first roll **70** is arranged with an infeed roller **36** which brings the heated press felt **32** together with the web **28** into contact with the surface of the roll **70**. Thus, in a way similar to the impulse dryer **20**, preheat zones **21**, pressing zones **26**, and post-heat zones **23** are defined. The web **28** backed by the felt **32** then enters a draw between the rolls **70**, **72**. The web **28** and the felt **32** pass in the draw **90** between an upper vacuum assist **92** and a lower vacuum assist **94**, which vent and remove steam from the felt **32** and the web **28**, thus drying the web **28**.

After passing through the draw **90**, the web **28**, and the felt **32**, are brought into contact with the surface **34** of the roll **72** by an infeed roller **96**. The web **28** then progresses through the second preheat zone **98** into a second pressing zone **100**, which is followed by a second post-heat zone **102**. Thus the dryer **74** increases web dryness and strength by adding a vacuum assist steam removal zone formed by the draw **90** as well as the second preheat, pressing, and post-heat zones **98**, **100**, **102**. The second roll **72** may be at a higher temperature than the first roll **70**.

Too much drying of the web **28** on a single roll can lead to adhesion of the web **28** to the roll surface **34**. This leads to delamination in the web **28** as it is removed from the roll. The dryer **74** advantageously allows increased drying while preventing adhesion of the web **28** to the roll surfaces **34**. The second post-heat zone **102** could include a free venting zone similar to the zone **68** shown on FIG. 1. However, by the time the web **28** reaches the second post-heat zone **102**, the web **28** should be sufficiently dry, so that venting into the felt will not impede the drying process.

With webs of certain fiber composition (furnishes), especially those which are multi-ply in composition, the web strength may be optimized by pressing and drying both sides of the web. An impulse dryer **104** shown in FIG. 3 employs a first press roll **70** and a second press roll **72** which rotate in opposite directions. The first roll **70** is heated by a first induction heater **76**. A second roll **72** is heated by a second induction heater **78**. A web **28** on a press felt **32** is wrapped onto the first roll **70** by an infeed roller **36** where it passes through a preheat zone **21**, a pressing zone **26** formed by the extended nip press **80**, and a post-heat zone **23**. Upon leaving the post-heat zone **23**, the press felt **32** is stripped away by a stripping roller **38**, leaving the unbacked web to enter an open draw **106** formed between the two rolls, **70**, **72**. Between where the felt **32** is stripped from the first roll **70** and where the web **28** enters the open draw **106**, a first side **108** of the web **28** enters a free venting region **110**. Then the web enters the open draw **106**, where both sides of the web are vented. Next, the web enters a free venting zone **112** where the second side **114** of the web **28** may dry by freely venting.

A second press felt **116** is brought into contact with the web **28** on the surface **34** of the roll **72** by a second infeed roller **118**. After the second infeed roll **118**, the web **28** enters the second preheat zone **98**. From the second preheat zone **98**, the web travels to the second pressing zone **100** formed by the second extended nip press **88**, finally exiting through the second post-heat zone **102**.

The impulse dryer **104** shown in FIG. 3 is capable of longer post-drying zones **23**, **102**. It has a stream venting zone comprised of the free-venting zones **110**, **112**, and the open draw **106**, where both sides of the web **28** are vented. It may also be possible to optimize web surface properties during the second and final pressing step before exiting from the dryer **104**. Once the solid content of the web approaches 70 plus percent solids, heated pressing

offers potential surfacing finishing means. Since this unit may dewater the web to dryness in the seventy plus percent range, surface finish could be initiated in the second nip **100**. The surface finish could proceed further by the addition of a third heated nip and/or a hot calender. The shoe**24** of the dryer **104** is shown in FIG. 3 in position to have an increased pressure profile at the inlet to the extended nip press with pressure tapering off toward the exit. The high rise in pressure at entrance may provide improved surface finishing. However, the shoe may alternatively be set to have a high peak pressure at the extended nip exit. Which configuration is desirable will depend upon entering solids. For example, if entering solids is near 75 percent, the peak should be near the nip entrance. If entering solids is 65 percent, the peak should be near the exit. This takes into account finishing or precalendering the sheet when it has just about the right amount of water content to be of benefit to the web--35 percent to 15 percent.

An alternative impulse dryer **120** is shown in FIG. 4 which employs a steam shower **122** to preheat the web **28** before pressing and drying. The dryer **120** has two rolls **70**, **72** which are arranged in tandem and rotate in the same direction, similar to the dryer **74**, shown in FIG. 2. The dryer **120** employs a double felt employing an upper felt **124** and a lower felt **126**. The upper felt **124** must be very open and made from heat resistant fibers.

A felt meeting these conditions is available from Albany International by the designation "R40" or "Albany Felt R." The upper felt **124** should be hydrophobic to resist water and thus resist rewetting the web **28**. A lower felt **126** underlies the upper felt and receives moisture from the web **28**. To facilitate the reception of steam and water from the web **28** through the upper felt **124**, the lower felt will preferably be hydrophilic, an exemplary felt being the type available from Albany International under the designation "BXC5" or "Albany Felt B."

The upper felt **124** is brought over an infeed felt roll **128** and overlies and joins the lower felt **126** over a first vacuum roll **130** where it also joins the web **28**. The web **28** overlying the upper felt **124** and the lower felt **126** then enters a steam shower **122** while being restrained by a vacuum box **132**. The steam shower **122** heats the web to approximately **212** degrees Fahrenheit, the boiling point of water. After this, the web and the upper felt **124** and lower felt **126** are wrapped by a second vacuum roller **134** onto the roll surface **34** of the roll **70**.

Once wrapped onto the roll **70**, the web is preheated in the preheat zone **21**, passes through the pressing zone or nip **26** formed by the extended nip **80**, and then continues on to the post-heat zone **23**. From the post-heat zone **23**, the web **28** and the backing felts **124**, **126** enter the draw **136** between the first roll **70** and the second roll **72**. A mid-draw vacuum roll **138** serves to constrain the web **28** against the felts **124**, **126**. The vacuum roll **138** also increases the wrap of the web **28** around the first roll **70** and the second roll **72**. The increased wrap increases the post-heat zone **23** and the preheat zone **98**.

A second steam shower **140** prevents the web from cooling in the draw **136**. The second steam shower **140** may be omitted if significant cooling is not found to take place in the draw **136**. It is, however, important that the web remain restrained and heated as it traverses the dryer **120** in order to maximize the strength developed in the web **28**. The blankets **82** of the extended nips **80**, **88** will preferably be of the vented type to maximize the amount of water removed from the web as it transits the pressing zone **26** of the first extended nip **80** and the pressing zone **100** formed by the second extended nip press **88**. The felt **124** is turned away from the web **28** and the felt **126** at final outfeed vacuum roll **103**.

Best properties in the web **28** are developed while the sheet is hot, pressed, and restrained during the heating and pressing process. This restrained pressing system must have adequate venting of the water and steam to inhibit sheet damage by delamination. This restrained hot pressing system should achieve solids and property development without causing sheet delamination.

It is also important to utilize hot release roll surfaces (non-sticking) and a hot release felt surface on the upper felt **124** to assure that the sheet will separate from the last heated roll **72** and the felt **124**, and not delaminate at the exit from the press **120**. The press **120** will preferably utilize ten to twenty inch extended nip press shoes **24**, and forty-eight to sixty inch diameter press rolls **70**, **72**. This should allow operation in the 1,500 to 3,000 feet per minute range for forty-two pound linerboard and achieve outgoing solids in the range of sixty to seventy percent, with the press operating at temperatures from 400 degrees to 500 degrees Fahrenheit.

Sheet presteaming is utilized at the entrance of the press, but may be optional or not necessary between the two heated rolls **70**, **72**. Vacuum as applied by vacuum rolls **130**, **134** and vacuum box **132** is necessary to assure proper presteaming in web restraint. Although the objective is to operate the press **120** at temperatures of 500 degrees or less, the press is not restricted in temperature. Higher temperatures may be desirable in some circumstances.

It should be understood that wherein two rolls are shown employed with presteaming of a paper web, a single roll press of this invention could be employed with a steam shower preheat.

It should be understood that where open, extended nip presses employing rolls are shown, closed ended, apple-type extended nip presses

could be used. Furthermore, where an apple-type extended nip press is shown, an open-ended roll type press could be used.

It should also be understood that where one or two press rolls with induction heaters and extended nip presses are shown, three or more rolls in tandem or counter-rotating could be employed.

It should also be understood that although the temperature of a particular backing roll is suggested to be 400 to 500 degrees Fahrenheit, other individual roll temperatures or combination of roll temperatures could be used to develop specific properties in a particular paper web of a given furnish.

It should also be understood that where a first felt which is open and hydrophobic is shown in use with a second felt which is hydrophilic, the properties of the two felts could be combined in a single felt. Furthermore, where a single felt is shown, two or more felts could be used.

It should also be understood that where induction heaters are shown and described, other types of heaters including but not limited to infrared heaters, direct flame impingement heaters, hot gas heaters, or steam heaters could be employed.

It should further be understood that wherein the impulse dryers **20**, **74**, **104** and **120** are described as particularly advantageous for the processing of linerboard, paper webs of varying weight and furnish could be advantageously processed by the disclosed apparatus.

It should be understood that the invention is not confined to the particular construction and arrangement of parts herein illustrated and described, but

embraces such modified forms thereof as come within the scope of the following claims.

CLAIMS

I claim:

1. An apparatus (20) for pressing and drying a formed web (28), comprising:

a first roll (22) mounted for rotation in a given direction and having a cylindrical surface (34);

a first felt (32) which underlies a portion of the web (28);

a shoe (24) which engages the first felt (32) and the web (28) against the first roll cylindrical surface (34), forming an extended nip press;

a heater (62) which heats portions of the first roll surface (34) prior to entry into the extended nip press;

a second roll (36) upstream of the first roll (22), wherein the felt and the web pass over the second roll (36) and are engaged by the second roll (36) against the first roll surface (34) at a position ahead of the extended nip press, thereby defining a preheating region between the second roll (36) and the extended nip press;

a third roll (38) downstream of the first roll (22), wherein the first felt (32) and the web (28) pass over the third roll (38) and are engaged by the third roll (38) against the first roll surface (34) at a position downstream of the nip press, and where the first felt (32) is separated from the web; and

a fourth roll (40) downstream of the third roll (38), wherein a second felt (41) wraps around portions of the fourth roll (40), and the web (28) extends from the third roll (38) to the fourth roll (40), and is engaged against the first roll (22) by the second felt (41) and the fourth roll (40), such that the web extends without backing between the third roll (38) and the fourth roll (40), providing a post-heat zone.

2. The apparatus of Claim 1 further comprising:

a fifth roll having a cylindrical surface, located upstream of the first roll;

a second heater which heats the fifth roll cylindrical surface;

a second shoe which engages the first felt and the web against the fifth roll cylindrical surface, forming a second extended nip press through which the web passes prior to engagement with the first roll; and

a sixth roll downstream of the second shoe, wherein the first felt and the web pass over the sixth roll and thence to the second roll.

3. The apparatus of Claim 2 further comprising:

an upper vacuum assist positioned above the web, between the second roll and the sixth roll; and

a lower vacuum assist positioned below the first felt, between the second roll and the sixth roll, wherein the vacuum assists vent and remove steam from the first felt and the web contributing to the drying of the web.

4. The apparatus of Claim 1 wherein the heater is an induction heater which heats a portion of the cylindrical surface not wrapped by a web.

5. An apparatus for pressing and drying a formed web, comprising:

a first roll mounted for rotation in a given direction and having a cylindrical surface;

a first felt which underlies a portion of the web;

a shoe which engages the first felt and the web against the first roll cylindrical surface, forming an extended nip press;

a heater which heats portions of the first roll surface prior to entry into the extended nip press;

a second roll upstream of the first roll, wherein the felt and the web pass over the second roll and are engaged by the second roll against the first roll surface at a position ahead of the extended nip press, thereby defining a preheating region between the second roll and the extended nip press;

a third roll downstream of the first roll, wherein the first felt and the web pass over the third roll and are engaged by the third roll against the first roll surface at a position downstream of the nip press, and where the first felt is separated from the web; and

a fourth roll downstream of the third roll, wherein a second felt wraps around portions of the fourth roll, and the web extends from the third roll to the fourth roll, and engages with the felt such that the web extends without backing between the third roll and the fourth roll, providing a post-heat zone.

6. The apparatus of Claim 5 further comprising:

a fifth roll having a cylindrical surface, located downstream of the first roll, wherein the web and the second felt are engaged against the fifth roll by the fourth roll, such that the unbacked web in the post-heat zone extends between the first roll and the fifth roll;

a second heater which heats the fifth roll cylindrical surface; and

a second shoe which engages the second felt and the web against the fifth roll cylindrical surface, forming a second extended nip press through which the web passes after engagement with the first roll.

7. The apparatus of Claim 6 further comprising:

a sixth roll downstream of the fourth roll, wherein a second felt and the web engage and pass over the sixth roll against the fifth roll surface at a position ahead of the second extended nip press; and

a seventh roll downstream from the sixth roll, wherein the second felt and the web pass over the seventh roll and are engaged by the seventh roll against the fifth roll surface at a position downstream of the second extended nip press and where the second felt is separated from the web and the web is separated from the fifth roll.

8. The apparatus of Claim 5 wherein the heater is an induction heater which heats a portion of the cylindrical surface not wrapped by a web.

9. An apparatus for pressing and drying a formed web, comprising:

a first dryer roll mounted for rotation and having a cylindrical surface;

a felt which underlies the web;

a shoe which engages the felt and the web against the first dryer roll cylindrical surface, forming an extended nip press;

a heater which heats portions of the first dryer roll surface;

a second roll upstream of the first dryer roll, wherein the felt and the web pass over the second roll and are engaged against the first dryer roll surface at a position ahead of the extended nip press, thereby defining a preheating region between the second roll and the extended nip press;

a third roll downstream of the first dryer roll, wherein the felt and the web pass over the third roll and are engaged by the third roll against the first dryer roll surface at a position downstream of the nip press to define a post-heat zone; and

a steam shower positioned ahead of the second roll to discharge heated water steam onto the web in advance of the first dryer roll.

10. The apparatus of Claim 9 wherein the first felt is comprised of:

an upper felt formed of an open felt; and

a lower felt which backs the upper felt, wherein the lower felt is hydrophilic.

11. The apparatus of Claim 9 further comprising:

a second dryer roll having a cylindrical surface, located downstream of the first dryer roll, wherein the felt and the web pass over the third roll and thence to the second dryer roll;

a second heater which heats the second dryer roll cylindrical surface;

a second shoe which engages the felt and the web against the second dryer roll cylindrical surface, forming a second extended nip press through which the web passes subsequent to engagement with the first dryer roll; and

an outfeed roll downstream of the second shoe, over which the felt and the web pass.

12. The apparatus of Claim 11 further comprising a second steam shower positioned to discharge heated water steam onto the web as it travels over the third roll.

13. The apparatus of Claim 9 wherein the second roll is a vacuum roll.

14. The apparatus of Claim 9 wherein the third roll is a vacuum roll.

15. The apparatus of Claim 9 wherein the heater is an induction heater.

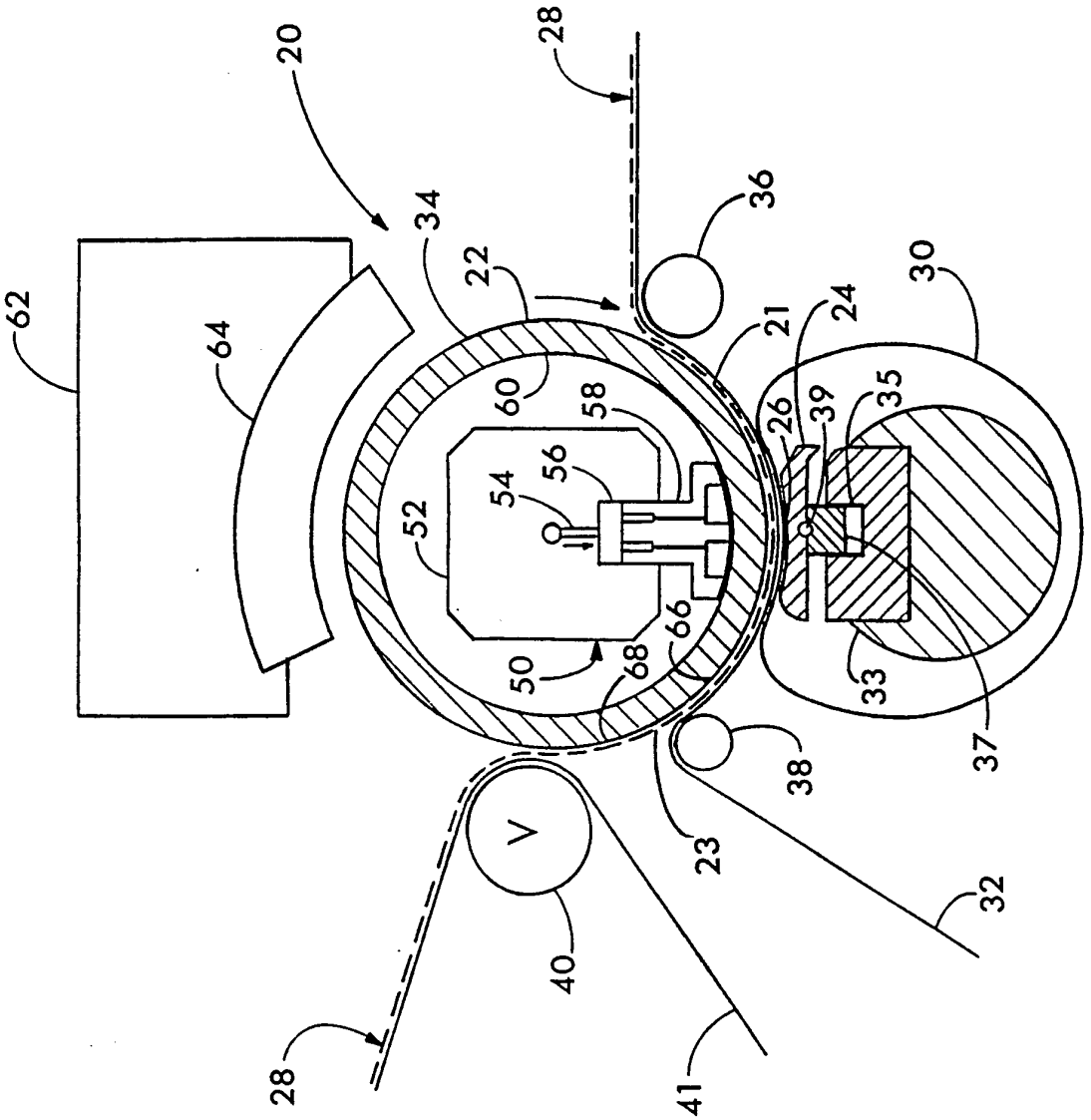
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FIG. 1

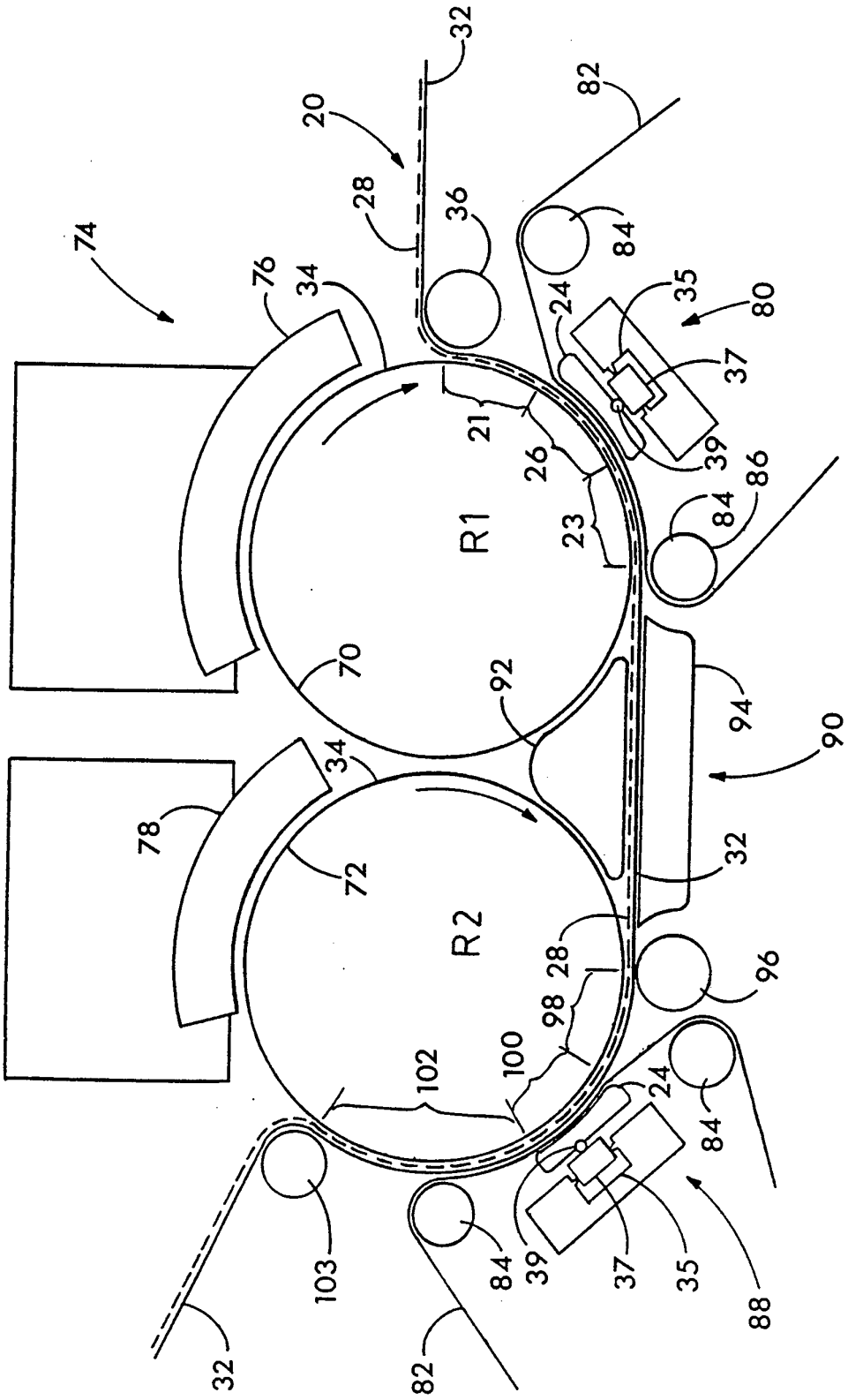
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FIG. 2

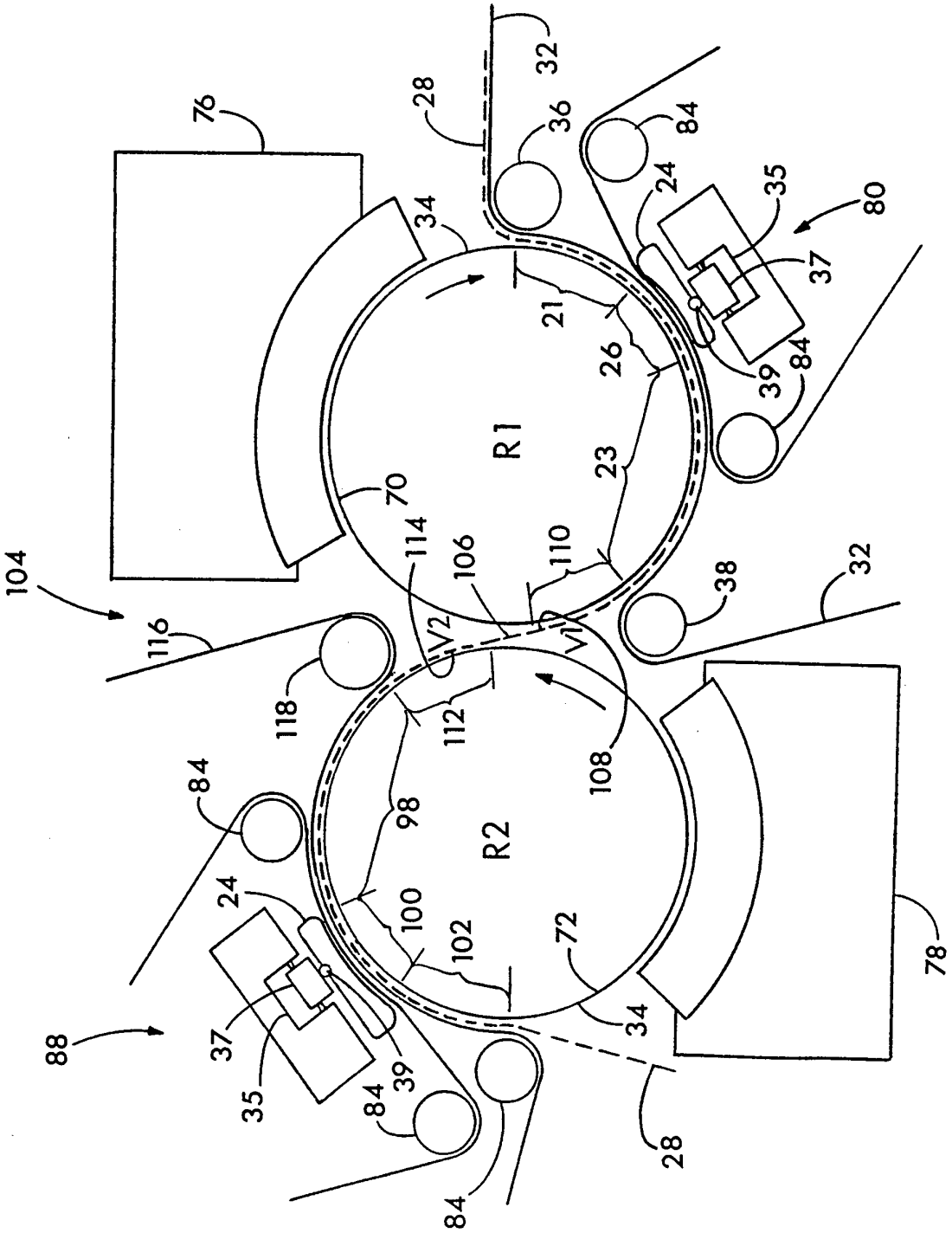
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FIG. 3

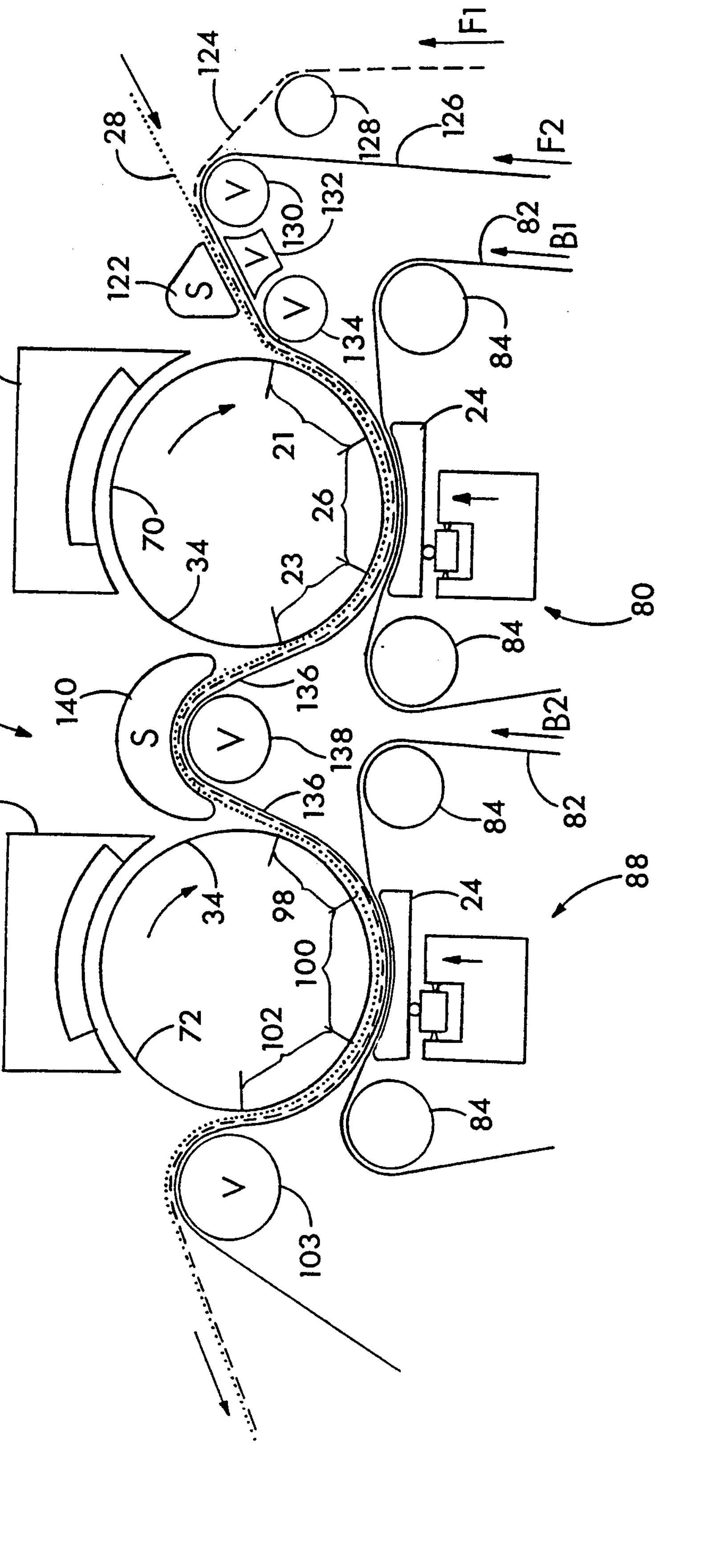
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FIG. 4

INTERNATIONAL SEARCH REPORT

Interna il Application No
PCT/US 94/14808

A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 D21F3/02 D21F3/04

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 6 D21F

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A	WO,A,91 08339 (BELOIT) 13 June 1991 see the whole document	9,10 1,4,5,8
A	EP,A,0 258 169 (BELOIT) 2 March 1988 see the whole document	1,4,5,8, 9
A	EP,A,0 289 477 (VALMET PAPER MACHINERY INC.) 2 November 1988 see the whole document	1,4,5,8, 9
A	WO,A,92 08003 (BELOIT) 14 May 1992 see the whole document	1,5,9
A	WO,A,93 23613 (SULZER-ESCHER WYSS) 25 November 1993	

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

° Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

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"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

1

Date of the actual completion of the international search	Date of mailing of the international search report
27 April 1995	09.05.95

Name and mailing address of the ISA	Authorized officer
European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016	De Rijck, F

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INTERNATIONAL SEARCH REPORT

Intern. al Application No
PCT/US 94/14808

Patent document cited in search report	Publication date	Patent family member(s)		Publication date
WO-A-9108339	13-06-91	AU-A-	6274690	26-06-91
EP-A-258169	02-03-88	US-A-	4738752	19-04-88
		AU-B-	597404	31-05-90
		AU-A-	7677987	18-02-88
		FI-B-	92942	14-10-94
		JP-A-	63050594	03-03-88
		US-A-	4874469	17-10-89
		ZA-A-	8705911	12-02-88
EP-A-289477	02-11-88	CA-A-	1325546	28-12-93
		JP-A-	1052897	28-02-89
		US-A-	4976820	11-12-90
WO-A-9208003	14-05-92	NONE		
WO-A-9323613	25-11-93	DE-A-	4216264	18-11-93
		EP-A-	0640158	01-03-95