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(54) **SYSTEM AND METHOD FOR MEASURING LEAD IMPEDANCE IN AN IMPLANTABLE STIMULATION DEVICE EMPLOYING PULSE-TRAIN WAVEFORMS**

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**A61N 1/36** (2006.01)

(52) **U.S. Cl.** ..... **607/8; 607/28; 607/74**

(58) **Field of Classification Search** ..... **607/8, 607/28, 68, 70, 72, 74**  
See application file for complete search history.

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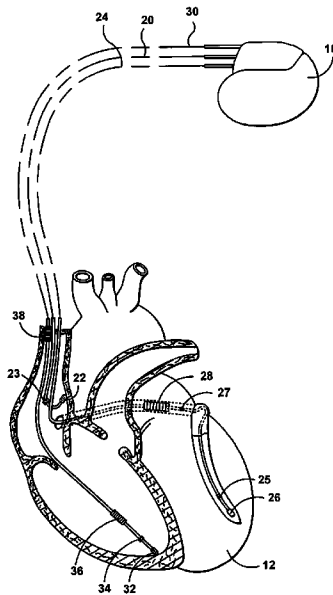
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(57) **ABSTRACT**

A leakage detection system for use in an implantable cardiac stimulation device, such as a cardioverter defibrillator. The leakage detection system includes a switch bank and a controller that regulates the switching arrangements of various switches. The leakage detection system causes pulse generators to generate a pulse-train waveform comprised of a sequence of pulses of opposite polarities, and to deliver these pulses in a preselected temporal relation. The controller detects the current leakage from the pulse generator to the tissues by sensing and analyzing the voltage or current of the pulse generator, leads, and electrodes. The pulsatility and alternating polarities of biphasic pulse-train waveforms increase the stimulation threshold of the motor or sensory nerves and excitable tissues.

**25 Claims, 5 Drawing Sheets**



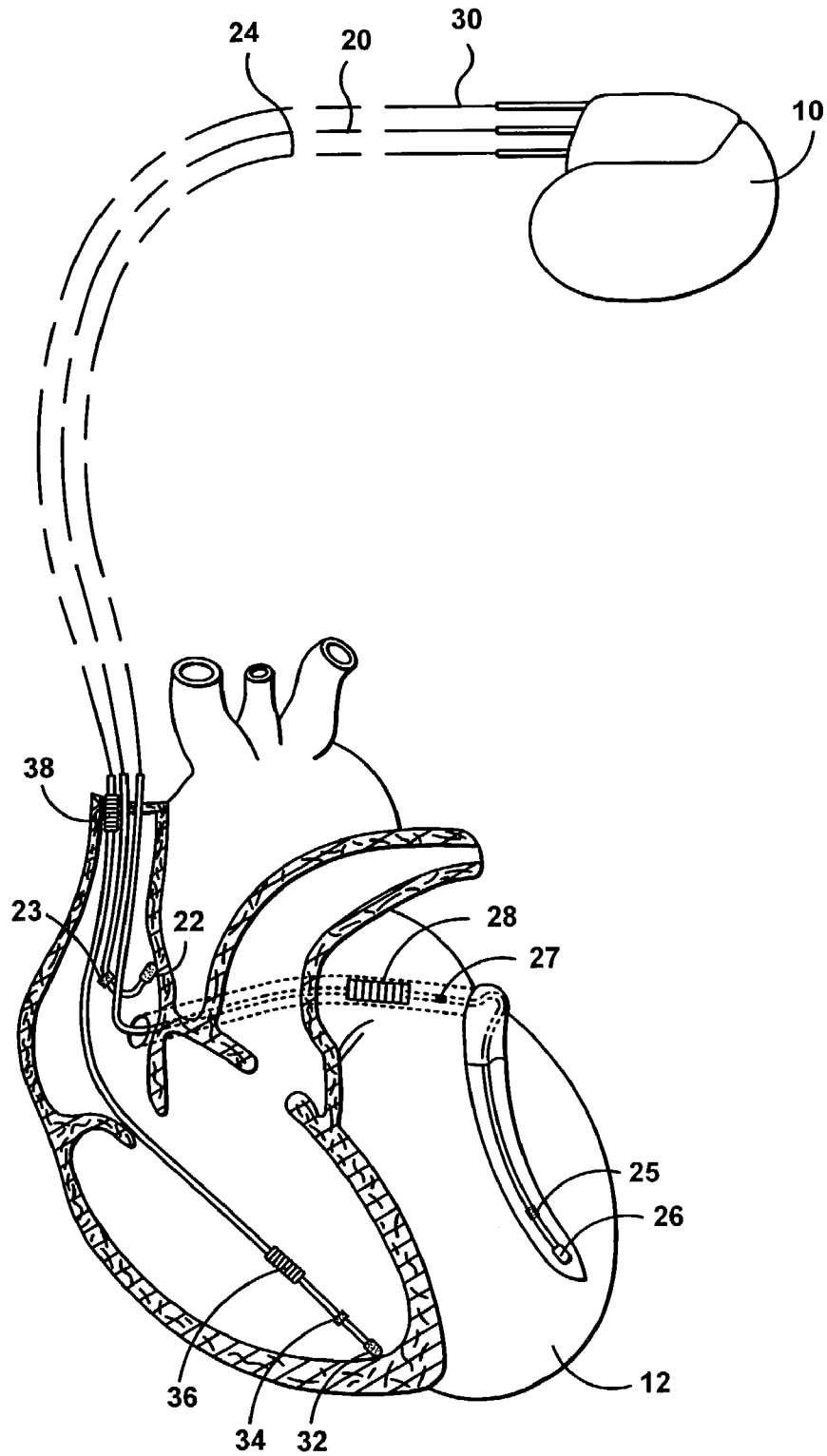


FIG. 1

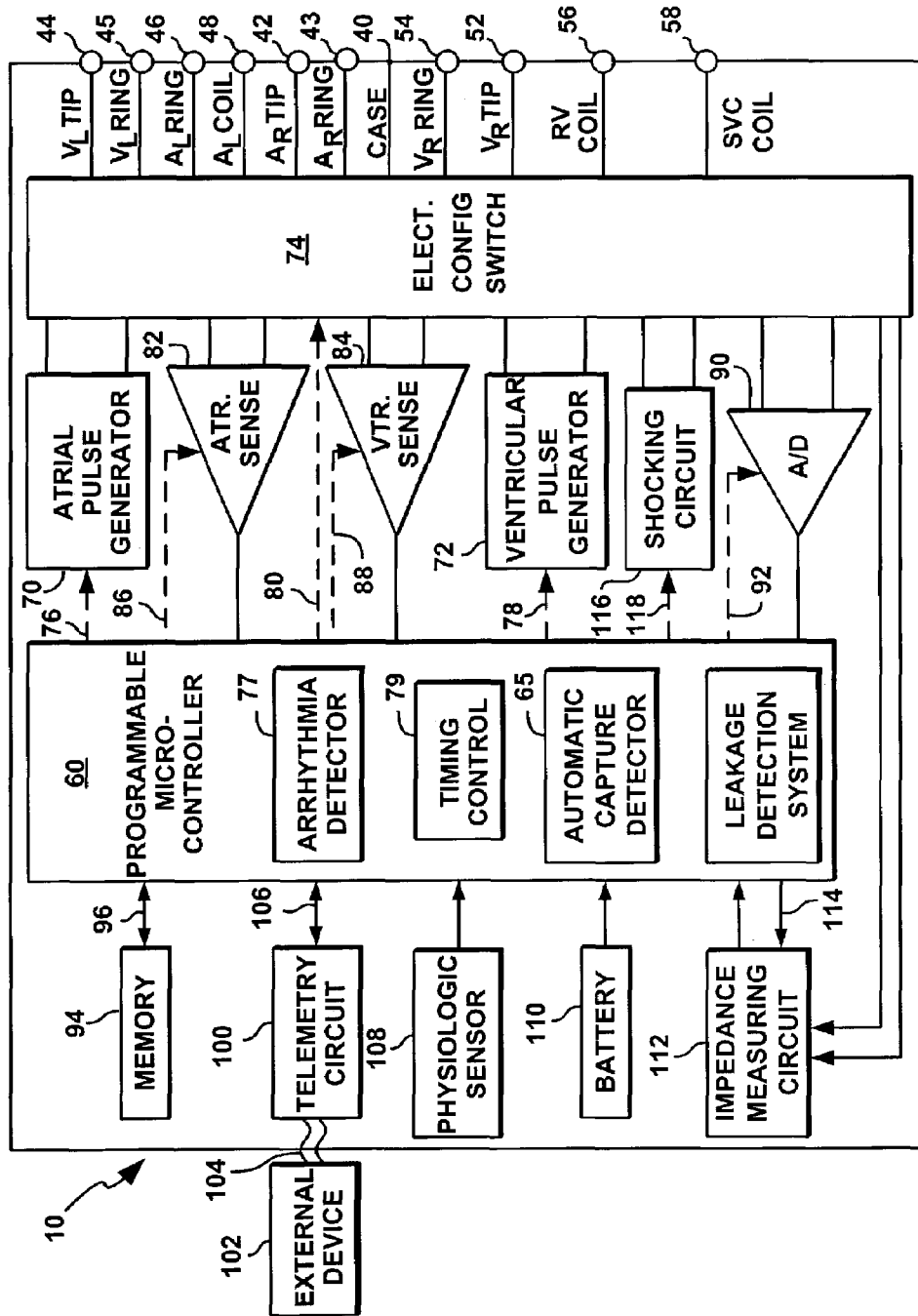
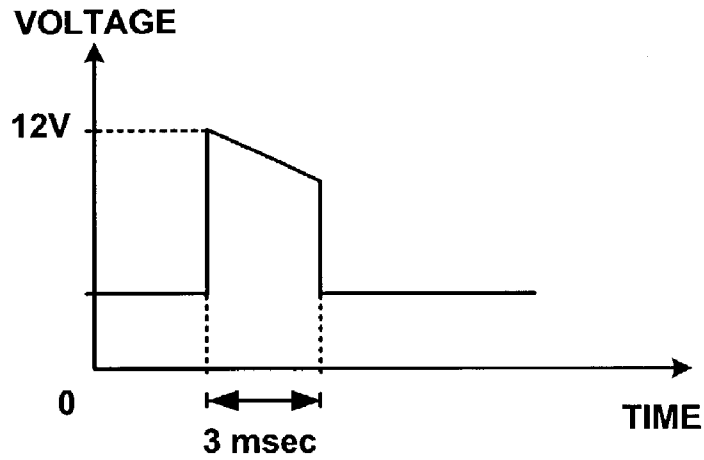
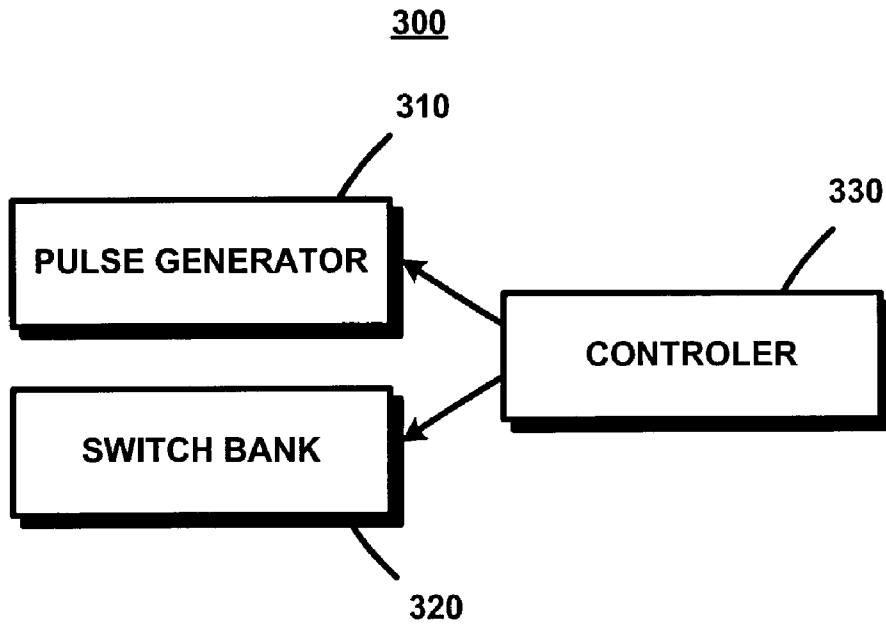


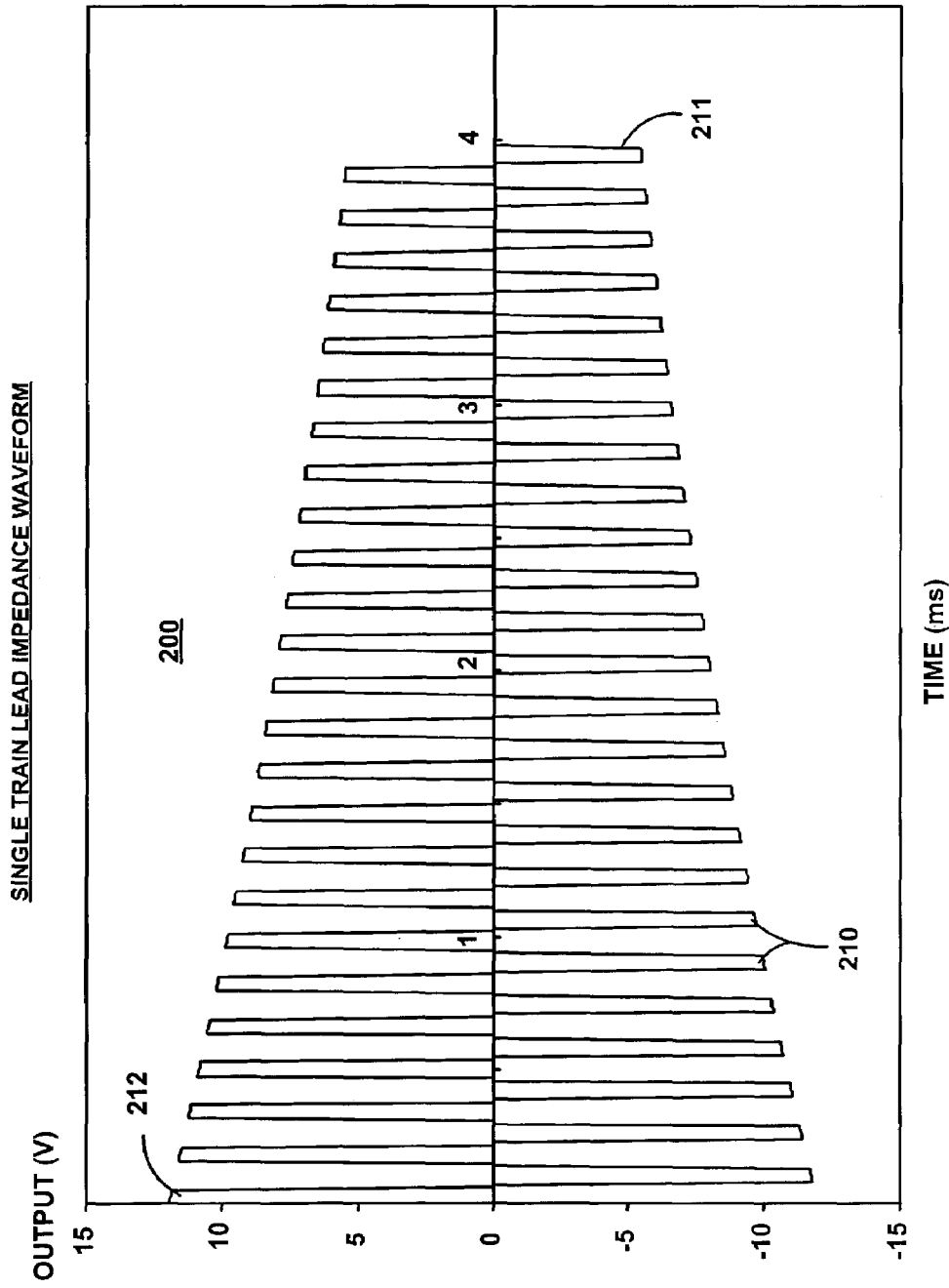
FIG. 2



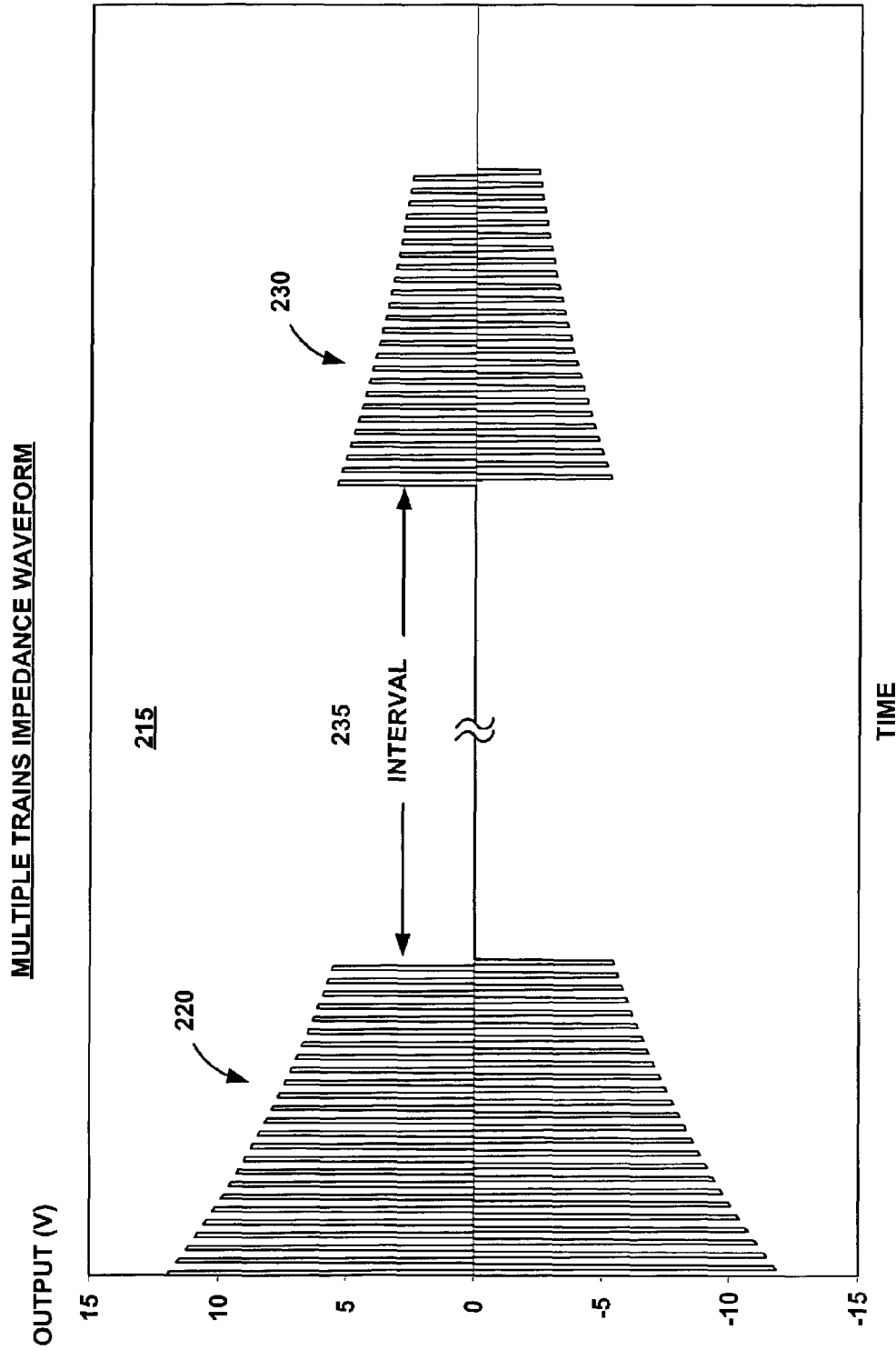
(PRIOR ART)  
**FIG. 3**



**FIG. 6**



**FIG. 4**



TIME

FIG. 5

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**SYSTEM AND METHOD FOR MEASURING  
LEAD IMPEDANCE IN AN IMPLANTABLE  
STIMULATION DEVICE EMPLOYING  
PULSE-TRAIN WAVEFORMS**

PRIORITY CLAIM

This application claims the priority of copending U.S. provisional patent application, titled "System and Method for Imperceptible Lead Integrity Checking in an Implantable Stimulation Device," Ser. No. 60/337,410, filed on Dec. 3, 2001, which is assigned to the same assignee as the present invention and which is incorporated herein by reference in its entirety.

FIELD OF THE INVENTION

The present invention generally relates to implantable cardiac stimulation devices. More specifically, this invention relates to an implantable cardioverter defibrillator and associated method for measuring the patient impedance. The impedance measuring system employs pulse-train waveforms for checking the integrity of various leads implanted in a patient's dysfunctional heart.

BACKGROUND OF THE INVENTION

In the normal human heart, the sinus node, that is generally located near the junction of the superior vena cava and the right atrium, constitutes the primary natural pacemaker initiating rhythmic electrical excitation of the heart chambers. Disruption of the heart's natural pacemaker and conduction system, as a result of aging and/or disease, can be successfully treated using various implantable cardiac stimulation devices, including pacemakers and implantable cardioverter defibrillators. A pacemaker is generally arranged to deliver rhythmic electrical pulses to the heart to maintain a normal rhythm in patients having bradycardia, which is too slow of heart rate, or other conduction abnormalities. In contrast, an implantable cardioverter defibrillator, commonly referred to as an "ICD", can recognize tachycardia and/or fibrillation and deliver electrical therapy in order to terminate such arrhythmias. In addition, such ICDs may often be configured to perform pacemaking functions (or pacing) as well.

Depending upon the patients' needs, the ICDs generate pacing, cardioverting, and/or defibrillating pulses, and deliver them to excitable cardiac tissues of the patients' heart by means of implanted electrical leads and electrodes. Since the lead is an essential part of the therapy a lead failure renders the device ineffective.

To detect lead failure, the cardiac stimulation devices, such as ICDs, monitor the impedance of the implanted leads. For high-voltage leads, a sudden rise of the lead impedance above 100 ohms is generally considered a sign of lead failure. To this end, certain conventional stimulation devices incorporate a high-voltage lead integrity check (HVLIC) system that generates a detection waveform, delivers the waveform through the implanted leads, and checks the integrity of the leads based on the delivered waveform parameters measured by the device.

In a conventional method of performing high-voltage lead integrity check a 12V, 3 msec truncated exponential pulse illustrated in FIG. 3, is delivered from the high voltage capacitors through the defibrillation leads. The low amplitude of this pulse is an attempt to get below perception thresholds of sensory and motor nerves and muscle tissue.

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The 3 msec duration of this pulse is chosen to allow enough time to enable the measurement of a voltage change across the high voltage capacitors of the implantable device. Several problems are associated with the monophasic detection waveform of FIG. 3. First, the duration of 3 msec is generally much longer than the time constants of the sensory and/or motor nerves that are generally on the order of 200  $\mu$ sec to 500  $\mu$ sec. In fact, such a duration almost approaches the time constant for stimulation of de-innervated muscles, and could thus cause muscle twitches and sensation.

In addition, the ICD is designed to charge its high voltage capacitors to about 800 volts with 2% accuracy. However, this accuracy degrades when charging to, or measuring lower voltages. This loss of accuracy is compounded by measurement errors associated with even lower voltages, and results in an inaccurate high-voltage lead integrity check of the lead impedance.

Another problem is that approximately 3 volts of the monophasic detection waveform is consumed in polarizing of the electrode-electrolyte interface at the electrodes and body fluids boundary. This voltage drop occurs, for example, between the blood and a polished platinum electrode, obscuring the delivered signal and compounding the inaccuracy of the measurement of the lead impedances.

Accordingly, it would be desirable to provide a more reliable impedance measurement system for the cardiac stimulation device, which need has heretofore remained unsatisfied.

SUMMARY

The present invention addresses the above needs by providing an implantable stimulation device, such as a cardioverter defibrillator (ICD), which is equipped with a lead impedance measuring circuit that employs pulse-train waveforms to check the integrity of various leads implanted in a patient's dysfunctional heart.

A feature of this invention is to provide a cardiac stimulation device that comprises at least one pulse generator for generating electrical pulses; a plurality of electrodes that are positioned in electrical contact with excitable cardiac tissues; and a plurality of leads that deliver the electrical pulses from the pulse generator to the cardiac tissues.

An impedance measurement system generally comprises at least one switch bank and a controller. The switch bank comprises of multiple switches that connects the pulse generator to the leads to permit multiple switching arrangements. The controller actuates the switches of the switch bank to select an optimal switching arrangement, to generate a waveform composed of a first set of pulses with a first polarity, and a second set of pulses with a second polarity that is opposite to the first polarity. With such a switching arrangement, the first and second pulses are delivered in a pre-selected temporal relation, the ICD measures the voltage before and after the delivery of the pulse and calculates the resulting tissue impedance across the leads.

The switch bank comprises an H-bridge that includes at least two of switches along each leg of the H-bridge. The use of such an H-bridge is known in the field.

The waveform comprises first and second pulses that are delivered in an alternating order. The first and second set of pulses have alternating polarity. Each of these pulses has a duration less than about 15% or 10% of a time constant of stimulation of the tissues. Preferably, each pulse has a duration of less than 50  $\mu$ sec. At least one of the first and second pulses may have a voltage higher than 12 volts, wherein the voltages of each pulse decreases exponentially.

The waveform is comprised of a train of pulses. The train is comprised of more than 10 pulses (or pairs of pulses of different polarities).

The temporal relation of the pulses that are delivered by the selected switching arrangement preferably relate to a cardiac event.

The pulse generator may generate multiple waveforms for delivery via the leads, each waveform including an initial pulse and a terminal (or last) pulse. These waveforms can be identical or similar, and they can be separated by a pre-selected period of time. As stated earlier, the voltages of the pulses within each waveform decrease exponentially. In the event of a sequence of waveforms, the terminal pulse voltage of the preceding waveform is substantially equal to the initial pulse voltage of the succeeding waveform.

The impedance measuring system includes a method to measure the leading and trailing waveform voltage in the pulse generator. The pulse generator or the external programmer can analyze the measured leading and trailing voltages and calculate the patient's lead impedance. Starting with the equation for exponential decay:

$$V_{trailing} = V_{leading} \cdot e^{-\frac{d}{RC}}$$

where,  $V_{trailing}$  is the waveform's trailing voltage,  $V_{leading}$  is the initial waveform voltage,  $d$  is the effective duration (on time of the switches),  $C$  is the generator capacitance and  $R$  is the patient impedance, the patient impedance  $R$  can be solved using the following relationship between the patient impedance and the other waveform parameters:

$$R = \frac{d}{\left( \ln \left( \frac{V_{leading}}{V_{trailing}} \right) \right) \cdot C}$$

This impedance measuring system offers various benefits by using pulse-train detection waveforms. For example, the pulsatility and alternating polarities of the biphasic pulse-train waveform will result in a higher stimulation threshold of the motor or sensory nerves and excitable tissues. This results in reducing the patient's sensation associated with the delivery of a conventional waveform. In addition, this impedance measuring system can employ pulse-train waveforms with higher amplitudes to improve accuracy of measurement of the patient lead impedance.

Moreover, this system can deliver a pulse-train waveform for a prolonged duration so that the trailing pulse of the waveform has a smaller amplitude than the leading pulse, thereby generating a greater voltage drop between the leading and trailing pulses. A larger drop improved the signal to noise ratio of the measurement further improving its accuracy.

Furthermore, the alternating biphasic feature of the pulse-train waveform as well the shorter duration of each pulse (i.e., higher frequency) avoid or at least minimize polarization voltage across the electrode electrolyte interface (i.e., the interface between the electrode surfaces and the body fluids). Polarization voltage subtracts from the voltage delivered to the patient. This loss of signal represent another source of inaccuracy. By reducing the polarization loss further improves the accuracy of the measured impedance.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Various features of the present invention and the manner of attaining such will now be described in greater detail with reference to the following description, claims, and drawings, wherein reference numerals are reused when appropriate, to indicate a correspondence between the referenced items, and wherein:

FIG. 1 is a simplified, partly cut-away view of an exemplary implantable cardiac stimulation device in electrical communication with at least three leads implanted into a patient's heart for delivering multi-chamber stimulation and shock therapy according to the present invention;

FIG. 2 is a functional block diagram of the exemplary implantable cardiac stimulation device of FIG. 1, illustrating the basic elements providing pacing stimulation, cardioversion, and defibrillation in four chambers of the heart, and incorporating a patient lead impedance measuring circuit of the present invention;

FIG. 3 illustrates a prior art monophasic waveform used to measure a patient lead impedance;

FIG. 4 is a graph of a biphasic pulse-train waveform used to measure the patient lead impedance according to the present invention;

FIG. 5 is a graph of a sequence of biphasic pulse-train waveforms used by the impedance measuring circuit according to the present invention; and

FIG. 6 is a high level block diagram of the lead impedance measuring circuit of the present invention.

#### DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

The following description is of a best mode presently contemplated for practicing the present invention. This description is not to be taken in a limiting sense but is made merely for the purpose of describing the general principles of the invention. The present invention is directed at an improved patient impedance measuring system for implantable cardiac stimulating devices with pacemaking, cardioversion, and/or defibrillation capabilities.

A cardiac stimulation device will thus be described in conjunction with FIGS. 1 and 2, in which the features included in this invention could be implemented. It is recognized, however, that numerous variations of such a device exist in which various methods included in the present invention can be implemented without deviating from the scope of the present invention.

FIG. 1 illustrates a stimulation device 10 in electrical communication with a patient's heart 12 by way of three leads 20, 24 and 30 suitable for delivering multi-chamber stimulation and/or shock therapy. To sense atrial cardiac signals and to provide right atrial chamber stimulation therapy, the device 10 is coupled to an implantable right atrial lead 20 including at least one atrial tip electrode 22 that typically is implanted in the patient's right atrial appendage. The right atrial lead 20 may also include an atrial ring electrode 23 to allow bipolar stimulation or sensing in combination with the atrial tip electrode 22.

To sense the left atrial and left ventricular cardiac signals and to provide left-chamber stimulation therapy, the stimulation device 10 is coupled to a "coronary sinus" lead 24 designed for placement in the "coronary sinus region" via the coronary sinus ostium in order to place a distal electrode adjacent to the left ventricle and additional electrode(s) adjacent to the left atrium. As used herein, the phrase "coronary sinus region" refers to the venous vasculature of



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the left ventricle, including any portion of the coronary sinus, great cardiac vein, left marginal vein, left posterior ventricular vein, middle cardiac vein, and/or small cardiac vein or any other cardiac vein accessible by the coronary sinus.

Accordingly, the coronary sinus lead **24** is designed to: receive atrial and/or ventricular cardiac signals; deliver left ventricular pacing therapy using at least one left ventricular tip electrode **26** for unipolar configurations or in combination with left ventricular ring electrode **25** for bipolar configurations; deliver left atrial pacing therapy using at least one left atrial ring electrode **27** as well as shocking therapy using at least one left atrial coil electrode **28**.

The stimulation device **10** is also shown in electrical communication with the patient's heart **12** by way of an implantable right ventricular lead **30** including, in this embodiment, a right ventricular (RV) tip electrode **32**, a right ventricular ring electrode **34**, a right ventricular coil electrode **36**, a superior vena cava (SVC) coil electrode **38**, and so on. Typically, the right ventricular lead **30** is inserted transvenously into the heart **12** so as to place the right ventricular tip electrode **32** in the right ventricular apex such that the RV coil electrode **36** is positioned in the right ventricle and the SVC coil electrode **38** will be positioned in the right atrium and/or superior vena cava. Accordingly, the right ventricular lead **30** is capable of receiving cardiac signals, and delivering stimulation in the form of pacing and shock therapy to the right ventricle.

FIG. 2 illustrates a simplified block diagram of the multi-chamber implantable stimulation device **10**, which is capable of treating both fast arrhythmia and slow arrhythmia with stimulation therapy, including cardioversion, defibrillation, and pacing stimulation. While a particular multi-chamber device is shown, this is for illustration purposes only, and one of ordinary skill in the pertinent art could readily duplicate, eliminate or disable the appropriate circuitry in any desired combination to provide a device capable of treating the appropriate chamber(s) with cardioversion, defibrillation, and/or pacing stimulation.

The stimulation device **10** includes a housing **40** which is often referred to as "can", "case," or "case electrode," and which may be programmably selected to act as the return electrode for all "unipolar" modes. The housing **40** may further be used as a return electrode alone or in combination with one or more of the coil electrodes **28**, **36**, or **38**, for defibrillation shocking purposes. The housing **40** further includes a connector having a plurality of terminals **42**, **43**, **44**, **45**, **46**, **48**, **52**, **54**, **56**, and **58** (shown schematically and, for convenience, the names of the electrodes to which they are connected are shown next to corresponding terminals). As such, in order to achieve right atrial sensing and stimulation, the connector includes at least one right atrial tip terminal ( $A_R$  TIP) **42** adapted for connection to the atrial tip electrode **22**. The connector may also include a right atrial ring terminal ( $A_R$  RING) **43** for connection to the right atrial ring electrode **23**.

To achieve left chamber sensing, pacing, and/or shocking, such a connector includes a left ventricular tip terminal ( $V_L$  TIP) **44**, a left ventricular ring terminal ( $V_L$  RING) **45**, a left atrial ring terminal ( $A_L$  RING) **46**, and a left atrial shocking coil terminal ( $A_L$  COIL) **48**, that are adapted for connection to the left ventricular tip electrode **26**, the left ventricular ring electrode **25**, the left atrial ring electrode **27**, and the left atrial coil electrode **28**, respectively.

To support right ventricular sensing, pacing, and/or shocking, the connector may further include a right ventricular tip terminal ( $V_R$  TIP) **52**, a right ventricular ring

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terminal ( $V_R$  RING) **54**, a right ventricular shocking coil terminal (RV COIL) **56**, and an SVC shocking coil terminal (SVC COIL) **58**, which are adapted for connection to the right ventricular (RV) tip electrode **32**, the RV ring electrode **34**, the RV coil electrode **36**, and the SVC coil electrode **38**, respectively.

At the core of the stimulation device **10** is a programmable microcontroller **60** that controls the various modes of stimulation therapy. The microcontroller **60** typically includes a microprocessor, or equivalent control circuitry, designed specifically for controlling the delivery of stimulation therapy, and may include RAM or ROM memory, logic and timing circuitry, state machine circuitry, and/or I/O circuitry. Typically, the microcontroller **60** may have the ability to process or monitor various input signals (data) as controlled by a program code stored in a designated block of memory.

FIG. 2 illustrates an atrial pulse generator **70** and ventricular pulse generator **72** which generate stimulation pulses for delivery by the right atrial lead **20**, the right ventricular lead **30**, and/or the coronary sinus lead **24** via a switch **74**. It is understood that, to provide the stimulation therapy in each of the four chambers of the heart, the atrial pulse generator **70** and the ventricular pulse generator **72** may include, e.g., dedicated pulse generators, independent pulse generators, multiplexed pulse generators, and/or shared pulse generators. The atrial pulse generator **70** and the ventricular pulse generator **72** are generally controlled by the microcontroller **60** via appropriate control signals **76** and **78**, respectively, to trigger or inhibit the stimulation pulses.

The microcontroller **60** may further include timing control circuitry **79** which may be used to control timing of the stimulation pulses such as, e.g., pacing rate, atrio-ventricular (AV) delay, atrial interchamber (A-A) delay, and/or ventricular interchamber (V-V) delay. Such timing control circuitry **79** may also be used to keep track of the timing of refractory periods, noise detection windows, evoked response windows, alert intervals, marker channel timing, and so on.

The switch **74** includes a plurality of switches for connecting the desired electrodes to the appropriate I/O circuits, thereby providing complete electrode programmability. Accordingly, the switch **74**, in response to a control signal **80** from the microcontroller **60**, determines the polarity of the stimulation pulses (e.g., unipolar, bipolar, cross-chamber, and the like) by selectively closing the appropriate combination of switches. Atrial sensing circuits **82** and ventricular sensing circuits **84** may also be selectively coupled to the right atrial lead **20**, coronary sinus lead **24**, and the right ventricular lead **30** through the switch **74**, for detecting the presence of cardiac activity in each of the four chambers of the heart.

Accordingly, the atrial sensing circuit **82** and the ventricular sensing circuit **84** may include dedicated sense amplifiers, multiplexed amplifiers or shared amplifiers. The switch **74** determines the "sensing polarity" of the cardiac signal by selectively closing the appropriate switches. In this way, the clinician may program the sensing polarity independent of the stimulation polarity.

Each of the atrial and ventricular sensing circuits **82**, **84** preferably employs one or more low power, precision amplifiers with programmable gain, automatic gain or sensitivity control, band-pass filtering, and threshold detection circuit, to selectively sense the cardiac signal of interest. The automatic sensitivity control enables the stimulation device

**10** to deal effectively with the difficult problem of sensing the low amplitude signal characteristics of atrial or ventricular fibrillation.

The outputs of the atrial sensing circuit **82** and ventricular sensing circuits **84** may be connected to the microcontroller **60** for triggering or inhibiting the atrial and ventricular pulse generators **70** and **72**, respectively, in a demand fashion, in response to the absence or presence of cardiac activity, respectively, in the appropriate chambers of the heart. The atrial and ventricular sensing circuits **82** and **84**, in turn, may receive control signals over signal lines **86** and **88** from the microcontroller **60**, for controlling the gain, threshold, polarization charge removal circuitry, and the timing of any blocking circuitry coupled to the inputs of the atrial and ventricular sensing circuits **82** and **84**.

For arrhythmia detection, the stimulation device **10** includes an arrhythmia detector **77** that utilizes the atrial and ventricular sensing circuits **82** and **84** to sense cardiac signals, for determining whether a rhythm may be physiologic or pathologic. As used herein, "sensing" generally refers to the process of noting an electrical signal, while "detection" generally refers to the step of confirming the sensed electrical signal as the signal being sought by the detector. As an example, "detection" applies to the detection of both proper rhythms (i.e., "P wave" or "R wave") as well as improper dysrhythmias including arrhythmia and bradycardia (e.g., detection of the absence of a proper rhythm).

The timing intervals between sensed events (e.g., P-waves, R-waves, and depolarization signals associated with fibrillation which are sometimes referred to as "F-waves" or "Fib-waves") are then classified by the arrhythmia detector **77** by comparing them to a predefined rate zone limit (e.g., bradycardia, normal, low rate ventricular tachycardia, high rate ventricular tachycardia, fibrillation rate zones, and so on) and various other characteristics (e.g., sudden onset, stability, physiologic sensors, morphology, and so on), in order to determine the type of remedial therapy required (e.g., bradycardia pacing, anti-tachycardia stimulation, cardioversion shocks or defibrillation shocks, collectively referred to as "tiered therapy").

Cardiac signals are also applied to the inputs of a data acquisition system **90** which is depicted as an analog-to-digital (A/D) converter for simplicity of illustration. The data acquisition system **90** is configured to acquire intracardiac electrogram (EGM) signals, convert the raw analog data into digital signals, and store the digital signals for later processing and/or telemetric transmission to an external device **102**. Such a data acquisition system **90** may be coupled to the right atrial lead **20**, the coronary sinus lead **24**, and the right ventricular lead **30** through the switch **74** to sample the cardiac signals across any pair of desired electrodes.

Advantageously, such a data acquisition system **90** may be coupled to the microcontroller **60** and/or another detection circuitry, for detecting an evoked response from the heart **12** in response to an applied stimulus, thereby aiding in the detection of "capture." In the embodiment of FIG. **2**, the microcontroller **60** may include an automatic capture detector **65** which searches for an evoked response signal following a stimulation pulse during a "detection window" set by timing control circuitry **79**. The microcontroller **60** enables the data acquisition system **90** via control signal **92** to sample the cardiac signal which falls in the capture detection window. The sampled signal is evaluated by the automatic capture detector **65** to determine if it is an evoked response signal based on its amplitude, peak slope, morphology or another signal feature or combination of the

features. Detecting the evoked response during the detection window may indicate that capture has occurred.

The microcontroller **60** may further be coupled to a memory **94** by a suitable data/address bus **96**, wherein the programmable operating parameters used by the microcontroller **60** are stored and modified, as required, so as to customize the operation of the stimulation device **10** to suit the needs of particular patients. Such operating parameters may define, e.g., stimulation pulse amplitude, pulse duration, polarity of electrodes, rate, sensitivity, automatic features, arrhythmia detection criteria, and/or the amplitude, shape of waves, and/or vector of each stimulation pulse to be delivered to the patient's heart **12** within each respective tier of therapy.

The stimulation device **10** may additionally include a power source that may be illustrated as a battery **110** for providing operating power to all the circuits of FIG. **2**. For the stimulation device **10** employing shocking therapy, the battery **110** must be capable of operating at low current drains for long periods of time, preferably less than 10  $\mu$ A, and also be capable of providing high-current pulses when the patient requires a shock pulse, preferably in excess of 2 A, at voltages above 2V, for periods of 10 seconds or more.

The implantable cardiac stimulation device **10** is equipped with an impedance measuring circuit **112** for measuring impedance between the high-voltage (HV) leads **40**, **56** and **58** of the stimulation device **10**. The impedance measuring circuit **112** employs pulse-train waveforms to decrease the patient sensation associated with the delivery of the impedance measuring waveform. It could also be used with higher amplitudes and prolonged durations to increase accuracy of the impedance measurement.

FIGS. **4** and **5** illustrate exemplary embodiments of pulse-train waveform used by the impedance measuring circuit **112** to achieve the objectives of the present invention. FIG. **6** illustrates the circuit used to generate the waveform of FIG. **4**.

In one embodiment of the present invention, the impedance measuring circuit **112** generates a variety of biphasic pulse-train waveforms. As an example, FIG. **4** illustrates an exemplary biphasic pulse-train waveform **200** formed of a plurality of successive electrical pulses **210** with alternating polarities mode. In this example, the pulses **210** have substantially identical durations, with exponentially decreasing amplitudes.

The impedance measuring circuit **112** sets the duration of the pulses **210** to a minimal value so that the electrical stimulation of the nerves and cardiac tissues by the pulse-train waveform **200** may be prevented or at least minimized. In general, the time constant ( $\tau_s$ ) of most motor and sensory nerves are in the range of approximately 200  $\mu$ sec to 500  $\mu$ sec, and those of the excitable cardiac tissues range from approximately 1000  $\mu$ sec to 5000  $\mu$ sec.

Accordingly, the impedance measuring system **112** sets the duration of each pulse **210** to only a fraction of the time constant ( $\tau_s$ ) of most motor and sensory nerves, e.g., ranging from about 1% of  $\tau_s$  to about 20% of  $\tau_s$ , or more particularly, about 10% of  $\tau_s$  or about 50  $\mu$ s. The total duration of the waveform **200** extends between approximately 1 and 10 milliseconds.

It is understood that the minimum durations of the pulses **210** achievable in a given stimulation device **10** are generally determined by the hardware characteristics of the stimulation device **10**, such as the switching speed of the high voltage output stage devices and/or discharging dynamics of the capacitors. The temporal characteristics of the pulse-train measuring waveform **200** can avoid or minimize the

twitches and/or patient sensation due to a reduction of the motor and sensory nerve stimulation.

The impedance measuring circuit 112 may also cause the voltage amplitudes of the pulses 210 of the pulse-train waveform 200 to exceed pre-selected levels. In general, errors in measuring impedance drastically increase as the charging and/or operating voltage levels decrease. As an example, the pulse generators 70, 72 of the stimulation device 10 are generally designed to charge up to 800 volts within a  $\pm 2\%$  error range. However, such errors could increase to  $\pm 20\%$  when the operating voltage falls to about 12 volts. The loss of accuracy may further be compounded by the errors in measuring the low voltage signals, resulting in inaccurate measurements of lead impedances.

Therefore, the impedance measuring circuit 112 is preferably arranged to maintain the amplitudes of the pulses 210 above 10 volts or, more particularly, above 5 volts but preferably below 50 volts.

The total duration of the pulse-train waveform 200 may be determined by a variety of factors. As an example, the impedance measuring circuit 112 may cause the generation of pulses 210 for a preset period so that the impedance measuring circuit 112 can generate pulse-train waveforms that include the same number of pulses as long as the pulse duration (or pulse frequency) is maintained at the same value (i.e., fixed or constant). In this example, the amplitudes of the initial and terminal pulses of the waveform 200 can be determined primarily by the charging status and/or the amount of energy stored in the pulse generators 70, 72, the switching device characteristics, the discharging capacitor characteristics, and the patient's lead impedance.

It should be clear that the fixed duration is not an essential requirement for the implementation of the present the invention, but is just a matter of design simplicity and mathematical convenience. As long the effective on-time of the waveform is known, the impedance can be calculated. This means that all variations are allowed in the pulse width and pulse spacing.

Accordingly, depending upon the charging status of the pulse generators 70, 72, the impedance measuring circuit 112 may generate pulse-train waveforms 200 with different shapes, even though their constituent pulses 210 have the same duration or frequency. Alternatively, the impedance measuring circuit 112 may terminate the generation of the pulses 210 when the voltage of the terminal pulse 211 of the waveform 200 reaches or falls below a preset percentage (or ratio) of the voltage of the initial pulse 212, when the voltage of the terminal pulse 211 reaches or falls below a preset threshold, or when the pulses 210 of the waveform 200 deliver a preset amount of electrical energy to the surrounding tissues. Although this embodiment does not require the pulse-train waveform 200 to have a preset duration, it may allow the waveform 200 to maintain at least substantially similar shapes, regardless of the charging status and discharging characteristics of the pulse generators 70, 72.

In addition, because the pulsatile biphasic waveform could be made not to cause stimulation of cardiac tissues, the impedance measuring circuit 112 may generate the pulse-train waveform 200 asynchronously, without having to synchronize the waveform 200 to the cardiac events such as the R-waves, the refractory periods of the cardiac tissues, or other similar events. However, if cardiac stimulation is unavoidable, the impedance measuring circuit 112 may generate the waveform 200 synchronously with the cardiac events.

The exponentially decreasing amplitudes of the pulses 210 of the pulse-train waveform 200 are primarily attributed

to the nature of capacitive discharges, that is the output energies of the pulse generators 70, 72 are incrementally depleted while generating the successive pulses 210. This decrease allows for the estimation of the discharging time constant. From which, and by knowing the capacitance value of the generator, it is possible to calculate the patient lead impedance.

The impedance measuring circuit 112 may also regulate the durations of each pulse 210 of the pulse-train waveform 200 such that pre-selected amounts of electrical energy are delivered to the surrounding tissues through the leads 40, 56, 58 during each pulse 210 of the waveform 200.

The impedance measuring circuit 112 also causes a pulse 210 to be followed by a succeeding pulse with an opposite polarity. In general, approximately 3 volts of monophasic pulses are consumed through the polarization of the electrodes 40, 56 and 58, in particular between the polished surfaces of these electrodes and the surrounding body fluid such as blood. This undesirable voltage drop not only obscures the signals, but also compounds the inaccuracy in measuring the lead impedance.

The biphasic pulse-train waveform 200 of the present invention advantageously cancels the polarization voltage drops that would otherwise be present across the electrodes 40, 56 and 58 for two reasons. The biphasic pulse-train has a better charge balance (i.e., a net charge of approximately 0) and further has a higher frequency content than the monophasic waveform. Since the electrode/electrolyte interface has a capacitive components (helmholtz capacitor), the charge balance results in less voltage remaining on that capacitor. Also the higher frequency content of the waveform passes easier through this capacitor.

In addition, the alternating polarities of the biphasic pulse-train waveform 200 may further cancel or neutralize the stimulation of the nerves and/or excitable cardiac tissues. To this end, the impedance measuring circuit 112 preferably delivers the pulses 210 in alternating pairs or, in other words, deliver a pulse-train waveform 200 with the same number of positive and negative pulses 210. It being understood that each pulse 210 of the pulse-train waveform 200 may preferably be immediately followed by a succeeding pulse 210 with an opposite polarity, so that the tissue sees them as a single biphasic pulse.

The foregoing biphasic pulse-train waveforms 200 offers various benefits over conventional monophasic and monotonous waveforms. The pulsatility and alternating polarity of the biphasic pulse-train waveform 200 has a higher stimulation threshold of the motor or sensory nerves and excitable tissues. Thus, the impedance measuring circuit 112 of the present invention can employ pulse-train waveforms 200 with higher amplitudes, and can further improve the accuracy in measuring the lead impedance of the electrodes and/or leads.

In addition, the impedance measuring circuit 112 can deliver the pulse-train waveform 200 for a prolonged duration so that the terminal pulse 211 of the waveform 200 has a lower amplitude than the initial pulse 212, thereby generating a greater voltage drop between the initial pulse 212 and the terminal pulse 211. This also contributes to an improvement in the measurement accuracy. Furthermore, the alternating biphasic feature of the pulse-train waveform 200 as well as a much shorter duration of each pulse (i.e., higher frequency) avoid, or at least minimize the polarization between the surfaces of the electrodes and the surrounding body fluid.

FIG. 5 is a graph of another exemplary biphasic pulse-train waveform 215 that is formed of a sequence of two or

more relatively short biphasic pulse-train waveforms, e.g., **220**, **230**. The pulse-train waveform **215** is used by the impedance measuring circuit **112** for impedance measurement according to an alternative embodiment of the present invention.

Each of the pulse-train waveforms **220**, **230** has a generally similar shape to that of the waveform **200** of FIG. 4, but has a shorter duration so that it is not felt by the patient. The pulse-train waveforms **220**, **230** are separated by an interval **235**, that could be for example one cardiac cycle. One feature of this alternative embodiment is that the effective pulse delivery time, or effective on-time, is used for impedance measurement.

The alternative embodiment of FIG. 5 illustrates that the waveform **215** may be time-split into several groups of pulse-pairs. As an example, five pulse pairs may be delivered in a single train **220**, followed by five more pairs that are similarly delivered in a single train **230**, at a programmable delay or interval **235**. Alternatively, the second train **230** may be synchronized to a specific cardiac event or to a sensed biological event. Several pulse trains may deliver a larger number of total pulses, such that the total energy discharge is spread over a longer effective on-time pulse delivery period. By increasing the total delivery energy, the accuracy of the impedance calculation can be improved.

For both exemplary biphasic waveforms **200** and **215** (FIGS. 4 and 5) the patient impedance "R" can be measured by the following expression:

$$R = \frac{d}{\left( \ln \left( \frac{V_{\text{leading}}}{V_{\text{trailing}}} \right) \cdot C \right)},$$

where  $V_{\text{trailing}}$  is the end or trailing voltage after pulse delivery;  $V_{\text{leading}}$  is the starting or leading voltage of the biphasic waveforms **200** and **215**, such as initial waveform **212** (FIG. 4),  $d$  is the effective on-time which is the effective duration of the pulses where the effective on-time is equal to the sum of all individual pulse durations; and  $C$  is the capacitance of the generator or ICD that is predetermined. The only variable in the above expression, is the impedance "R" that can be readily computed knowing the other values. The foregoing expression is calculated for the entire train.

FIG. 6 illustrates an ICD output switch configuration **300** comprised of a pulse generator **310** (such as the atrial and ventricular pulse generators **70**, **72**), a switch bank **320** (such as the electrical configuration switch **74**), and a controller (such as the microcontroller **60**). The pulse generator **310** receives power from the energy cells and generates the pulse-train waveforms **200** (or **220** and **230**). The switch bank **320** is coupled to the pulse generator **310** and generally has a plurality of switches to connect or disconnect the pulse generator **310** to and from the electrodes **40**, **56** and **58**. More particularly, the switch bank **320** may include at least one H-shaped bridge (or "H-bridge") **100** (FIG. 7) in which at least two switches are implemented in each leg.

The microcontroller **60** controls the normal operation of the stimulation device **10**, and further regulates the actuation (i.e., opening and closing of) the switches within the switch bank **330**. More particularly, the microcontroller **60** is preferably provided with complete electrode programmability (e.g., switching operation and connection arrangements) so that it may regulate the timing for generating and/or terminating the pulse-train waveforms **200**, **220**, **230**, the durations, frequencies and amplitudes of the pulses of these

pulse-train waveforms **200**, **220**, **230**, the intervals between the waveforms **200**, **220**, **230** when multiple waveforms are delivered to the electrodes **40**, **56** and **58**.

Thus, various aspects and embodiments of impedance measuring systems and methods thereof for the implantable cardiac stimulation devices have been described in which the pulse-train waveforms that has a higher stimulation threshold of various nerves and excitable tissues, thereby making it less perceptible by the patient while also enhancing the measurements accuracy. While detailed descriptions of the specific embodiments of this invention have been provided, it would be apparent to those skilled in the art that numerous variations of the systems and methods described herein may be possible in which the concepts of this invention may readily be applied. The descriptions provided herein are for the sake of illustration and in no aspect intended to be limiting.

What is claimed is:

1. In an implantable cardiac stimulation device, a method of measuring lead impedance comprising:

generating a biphasic pulse train comprised of a first set of pulses of a first polarity and a second set of pulses of a second polarity that is opposite to the first polarity; delivering the biphasic pulse train through the lead in a preselected temporal relation that minimizes tissue stimulation and polarization between the tissue and the lead; and

calculating a lead impedance as a function of an initial measured voltage and a post-delivery measured voltage.

2. The method of claim 1, wherein the first and second sets of pulses are grouped in a paired arrangement of alternating polarities.

3. The method of claim 2, wherein at least some of the first and second sets of pulses are of equal duration.

4. The method of claim 3, wherein the duration of the pulses ranges between approximately 10% and 15% of a time constant of stimulation of the tissue.

5. The method of claim 4, wherein the duration of each of the pulses is less than approximately 50  $\mu\text{sec}$ .

6. The method of claim 5, wherein at least one pulse of the first and second sets of pulses has a voltage higher than 12 volts.

7. The method of claim 6, wherein the first set of pulses has a voltage that decreases exponentially over time.

8. The method of claim 7, wherein the second set of pulses has a voltage that decreases exponentially over time.

9. The method of claim 1, wherein generating the biphasic pulse train comprises generating a waveform that is formed of a sequence of two or more short biphasic pulse-trains.

10. The method of claim 9, wherein the sequence of two or more short biphasic pulse-trains comprises at least a first pulse train and a second pulse train; and

wherein the first and second pulse trains are synchronized to cardiac events.

11. The method of claim 9, wherein the sequence of two or more short biphasic pulse-trains comprises at least a first pulse train and a second pulse train; and

wherein the first and second pulse trains are synchronized to a predetermined sensed biological event.

12. The method of claim 1 wherein at least one pulse in the pulse train has an amplitude sufficient to cause tissue stimulation and the preselected temporal relation minimizes the tissue stimulation that would otherwise be caused by the at least one pulse.

13. A system for measuring lead impedance, for use with a stimulation device, comprising:

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- a pulse generator that generates a biphasic pulse train comprised of a first set of pulses of a first polarity and a second set of pulses of a second polarity that is opposite to the first polarity;
  - a lead that delivers the biphasic pulse train in a preselected temporal relation that minimizes tissue stimulation and polarization between the tissue and the lead; and
  - an impedance measuring circuit that calculates a lead impedance as a function of an initial measured voltage and a post-delivery measured voltage.
14. The system of claim 13, wherein the first and second sets of pulses are grouped in a paired arrangement of alternating polarities.
15. The system of claim 13, wherein at least some of the first and second sets of pulses are of equal duration.
16. The system of claim 15, wherein the duration of the pulses ranges between approximately 10% and 15% of a time constant of stimulation of the tissue.
17. The system of claim 16, wherein the duration of each of the pulses is less than approximately 50  $\mu$ sec.
18. The system of claim 15, wherein at least one pulse of the first and second sets of pulses has a voltage higher than 12 volts.
19. The system of claim 13, wherein the biphasic pulse train comprises a waveform that is formed of a sequence of two or more short biphasic pulse-trains.
20. The system of claim 19, wherein the sequence of two or more short biphasic pulse-trains comprises at least a first pulse train and a second pulse train; and  
 wherein the first and second pulse trains are synchronized to cardiac events.

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21. The system of claim 19, wherein the sequence of two or more short biphasic pulse-trains comprises at least a first pulse train and a second pulse train; and  
 wherein the first and second pulse trains are synchronized to a predetermined sensed biological event.
22. The system of claim 13 wherein at least one pulse in the pulse train has an amplitude sufficient to cause tissue stimulation and the preselected temporal relation minimizes the tissue stimulation that would otherwise be caused by the at least one pulse.
23. A system for measuring lead impedance, for use with a stimulation device, the system comprising:  
 means for generating a pulse train comprising a first set of pulses of a first polarity and a second set of pulses of a second polarity that is opposite to the first polarity, the pulse train formed of a sequence of two or more short biphasic pulse-trains;  
 means for delivering the pulse train in a way that minimizes tissue stimulation and polarization between the tissue and the lead; and  
 means for calculating a lead impedance.
24. The system of claim 23, wherein each of the short biphasic pulse-trains contains a series of consecutive pulses of opposite polarities.
25. The system of claim 24, wherein each of the pulses in the series of consecutive pulses has a duration and an amplitude set to avoid a generation of stimulation sensation.

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