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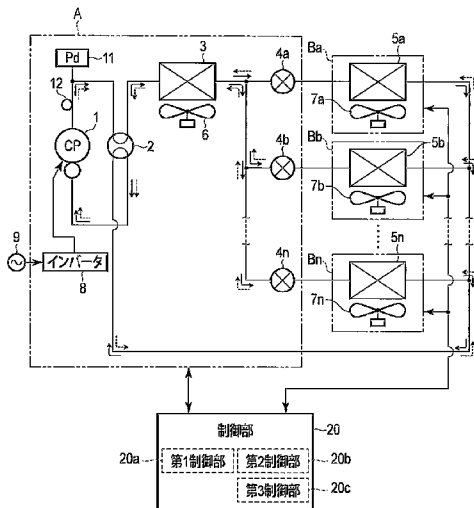


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(54) Title: REFRIGERATION CYCLE DEVICE

(54) 発明の名称: 冷凍サイクル装置



(57) Abstract: Through the present invention, a compressor is stopped in response to operation of a high-pressure switch, and subsequently, the compressor is restarted in response to returning of the high-pressure switch, and the lower-limit value of opening degree control for an expansion valve is also shifted to an increased value during the restarting.

(57) 要約: 高圧スイッチの作動に応じて圧縮機を停止し、その後、高圧スイッチの復帰に応じて圧縮機を再起動するとともに、この再起動に際し膨張弁に対する開度制御の下限值を増大側にシフトする。

- 8 Inverter
- 20 Control unit
- 20a First control unit
- 20b Second control unit
- 20c Third control unit

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D E S C R I P T I O N

REFRIGERATION CYCLE APPARATUS

5

Technical Field

Embodiments described herein relate generally to a refrigeration cycle apparatus coping with a rise in the pressure on the high-pressure side.

Background Art

10

A refrigeration cycle apparatus incorporated in an air-conditioning apparatus or the like is provided with a high-pressure switch responding to the pressure on the high-pressure side of a refrigeration cycle, when the pressure on the high-pressure side rises and the high-pressure switch operates, the compressor is stopped, and when thereafter the pressure on the high-pressure side lowers and the high-pressure switch is restored, the compressor is restarted. When the high-pressure switch operates, the compressor is stopped, whereby the pressure on the high-pressure side is prevented from abnormally rising, and the safety of the refrigeration cycle equipment including the compressor is secured.

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A reference herein to a patent document or any other matter identified as prior art, is not to be taken as an admission that the document or other matter was known or that the information it contains was part of the common general knowledge as at the priority date of any of the claims.

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Summary of Invention

Even when the compressor is restarted in response to the restoration of the high-pressure switch, the pressure on the high-pressure side soon rises again, and the high-pressure switch operates in some cases.

35

In this case, the compressor frequently repeats a stop

and restart to thereby cause a variation in the indoor temperature and deteriorate the comfort of air conditioning.

5 Further, as a refrigerant for the refrigeration cycle, in place of the R410A refrigerant, a changeover to the refrigerant R32 excellent in ability and energy efficiency is advancing. However, as for the refrigerant R32, the pressure thereof at the time when it is discharged from the compressor becomes higher
10 than the case of the refrigerant R410A, and hence a state where the high-pressure switch is liable to operate is brought about.

Embodiments of the present invention may provide a refrigeration cycle apparatus capable of preventing the pressure on the high-pressure side after a restart of
15 the compressor from rising, and thereby preventing frequent repetitions of a stop and restart of the compressor from occurring.

According to one aspect of the invention, there is provided a refrigeration cycle apparatus comprising a
20 refrigeration cycle including a compressor, a condenser, an expansion valve, and an evaporator; a high-pressure switch responding to the pressure on the high-pressure side of the refrigeration cycle; and a control unit configured to control the degree of
25 opening Q of the expansion valve to be within a range of a predetermined upper-limit value Q_{max} to a predetermined lower-limit value Q_{min} in order that the degree of superheat of the evaporator or the degree of subcooling of the condenser becomes a constant value,
30 wherein the control unit stops the compressor in response to an operation of the high-pressure switch, thereafter restarts the compressor in response to restoration of the high-pressure switch, and at the
35 time of the restart, shifts the lower-limit value Q_{min}

of opening degree control for the expansion valve toward the increase side by a predetermined value ΔQ .

Brief Description of Drawings

5 FIG. 1 is a block diagram showing the configuration of an embodiment.

FIG. 2 is a flowchart showing the control of the embodiment.

10 FIG. 3 is a view showing a relationship between the capacity of a refrigeration cycle at the time of cooling and the pressure on the high-pressure side in the embodiment.

15 FIG. 4 is a view showing a relationship between the capacity of a refrigeration cycle at the time of heating and the pressure on the high-pressure side in the embodiment.

FIG. 5 is a view showing examples of changes in the pressure on the high-pressure side, expansion valve opening, discharged refrigerant temperature, and compressor rotational speed.

20 Detailed Description of Example Embodiment(s)

Hereinafter, an embodiment will be described with reference to the drawings.

25 As shown in FIG. 1, one end of an outdoor heat exchanger 3 is piping-connected to an discharge port of a compressor 1 through a four-way valve 2. One end of each of a plurality of indoor heat exchangers 5a, 5b, ... 5n is piping-connected to the other end of the outdoor heat exchanger 3 through each of a plurality of expansion valves 4a, 4b, ... 4n, and the other end of
30 each of the plurality of indoor heat exchangers 5a, 5b, ... 5n is piping-connected to an inlet port of the compressor 1 through the four-way valve 2. These piping connections constitute a heat pump refrigeration cycle. This heat pump refrigeration cycle system is
35 filled with a refrigerant including the refrigerant R32

in an amount of, for example, 50% or more.

At the time of cooling, as indicated by solid line
arrows, the refrigerant discharged from the compressor
1 flows into the indoor heat exchangers (evaporators)
5 5a, 5b, ... 5n through the four-way valve 2, outdoor
heat exchanger (condenser) 3, and expansion valves 4a,
4b, ... 4n, and the refrigerant flowing out of the

indoor heat exchangers 5a, 5b, ... 5n is sucked into the compressor 1 through the four-way valve 2. At the time of heating, as indicated by broken line arrows, the flow paths in the four-way valve 2 are changed, whereby the refrigerant discharged from the compressor 1 flows into the indoor heat exchangers (condenser) 5a, 5b, ... 5n, and the refrigerant flowing out of the indoor heat exchangers 5a, 5b, ... 5n is sucked into the compressor 1 through expansion valves 4a, 4b, ... 4n, outdoor heat exchanger (evaporator) 3, and four-way valve 2.

An outdoor fan 6 is arranged in the vicinity of the outdoor heat exchanger 3, and indoor fans 7a, 7b, ... 7n are arranged in the vicinities of the indoor heat exchangers 5a, 5b, ... 5n. An inverter 8 is connected to a motor of the compressor 1. The inverter 8 converts a voltage of an AC source 9 into a DC voltage, and further converts the DC voltage into an AC voltage of a predetermined frequency F to output the AC voltage. The motor of the compressor 1 operates at a rotational speed corresponding to this output frequency F.

A high-pressure switch 11 and refrigerant temperature sensor 12 are attached to the high-pressure side piping between the discharge port of the compressor 1 and the four-way valve 2. The high-pressure switch 11 operates when the pressure (called the pressure on the high-pressure side) P_d of the refrigerant discharged from the compressor 1 rises to a value greater than a set value P_{d2} , and is restored when the pressure P_d on the high-pressure side lowers to a value smaller than a set value P_{d1} ($<P_{d2}$). The refrigerant temperature sensor 12 detects the temperature T_d of the refrigerant discharged from the compressor 1.

Each of the expansion valves 4a, 4b, ... 4n is a so-called pulse-motor valve in which the degree of opening continuously changes according to the number of pulses of a drive pulse signal input thereto.

5 In an outdoor unit A, the compressor 1, four-way valve 2, outdoor heat exchanger 3, expansion valves 4a, 4b, ... 4n, outdoor fan 6, and inverter 8 are incorporated. In a plurality of indoor units Ba, Bb, ... Bn, the indoor heat exchangers 5a, 5b, ... 5n, 10 and indoor fans 7a, 7b, ... 7n are respectively incorporated. A control unit 20 is connected to the outdoor unit A and indoor units Ba, Bb, ... Bn.

The control unit 20 is constituted of a microcomputer and peripheral circuit thereof, and 15 includes, as main functions, a first control section 20a, second control section 20b, and third control section 20c.

The first control section 20a stops the compressor 1 in response to an operation of the high-pressure 20 switch 11, and thereafter restarts the compressor 1 in response to the restoration of the high-pressure switch 11.

The second control section 20b controls, at the 25 time of the operation of the heat pump refrigeration cycle, the degree of opening Q of each of the expansion valves 4a, 4b, ... 4n to be within a range of a predetermined upper-limit value Q_{max} to a predetermined lower-limit value Q_{min} in order that the degree of 30 superheat (at the time of cooling) or the degree of subcooling (at the time of heating) of the indoor heat exchangers 5a, 5b, ... 5n may become a constant value.

The third control section 20c shifts (opening-narrowing control), at the time of a restart of the compressor 1 based on the restoration of the

high-pressure switch 11, the lower-limit value Q_{min} of the opening degree control for each of the expansion valves 4a, 4b, ... 4n toward the increase side by a predetermined value ΔQ .

5 It should be noticed that the second control section 20b sets the predetermined value ΔQ which is the shift amount to different values ($\Delta Q_1, \Delta Q_2, \dots \Delta Q_n$) according to the capacity (the number of indoor units Ba, Bb, ... Bn in operation) of the heat pump refrigeration cycle. More specifically, the second control section 20b sets the predetermined value ΔQ to a value proportional to the capacity of the heat pump refrigeration cycle at the time of cooling, and to a value inversely proportional to the capacity of the heat pump refrigeration cycle at the time of heating. Further, the second control section 20b selectively executes the opening-narrowing control of shifting the lower-limit value Q_{min} on the basis of a comparison between the discharged refrigerant temperature T_d to be detected by the refrigerant temperature sensor 12 and a set value T_{ds} . Furthermore, the second control section 20b cancels the selective execution of the opening-narrowing control concomitantly with shutdown of the heat pump refrigeration cycle.

20 Next, the control to be executed by the control unit 20 will be described below with reference to the flowchart of FIG. 2.

25 At the time of a start of an operation of at least one of the indoor units Ba, Bb, ... Bn (YES in step S1), the control unit 20 starts the compressor 1 (step S2). Concomitantly with the start, the control unit 20 confirms whether or not an opening degree limiting flag f is "0" (step S3).

30 When the opening degree limiting flag f is "0" (YES in step S3), the control unit 20 controls the

degree of opening Q of each of the expansion valves 4a, 4b, ... 4n to be within the range of the predetermined upper-limit value Q_{\max} to the predetermined lower-limit value Q_{\min} in order that the degree of superheat (at the time of cooling) or the degree of subcooling (at the time of heating) of the indoor heat exchangers 5a, 5b, ... 5n may become a constant value (step S4).

The control unit 20 monitors the operation of the high-pressure switch 11 concomitantly with the opening degree control (step S7). When the high-pressure switch 11 does not operate (NO in step S7), the control unit 20 monitors a shutdown of the indoor units Ba, Bb, ... Bn (step S14).

When a shutdown of the indoor units Ba, Bb, ... Bn is not needed (NO in step S14), the control unit 20 returns to the flag determination of step S3. When a shutdown of the indoor units Ba, Bb, ... Bn is needed (YES in step S14), the control unit 20 stops the compressor 1 (step S15). Further, the control unit 20 resets the opening degree limiting flag f to "0" (step S16), and returns to the operation start determination of first step S1.

On the other hand, when the high-pressure switch 11 operates (YES in step S7), the control unit 20 stops the compressor 1 (step S8). By this stop, the pressure on the high-pressure side is prevented from abnormally rising. Further, the control unit 20 starts time measurement t (step S9), and monitors the restoration of the high-pressure switch 11 (step S10). When the restoration of the high-pressure switch 11 is not obtained (NO in step S10), the time measurement t is continued (step S9).

When the pressure on the high-pressure side lowers, and the high-pressure switch 11 is restored (YES in step S10), the control unit 20 determines

whether or not the time measurement t has reached a fixed time t_s (step S11). The fixed time t_s is a restart limiting time for preventing the damage or the like of the compressor 1.

5 When the time measurement t has not reached the fixed time t_s (NO in step S11), the control unit 20 continues the time measurement t (step S9). When the time measurement t has reached the fixed time t_s (YES in step S11), the control unit 20 restarts the
10 compressor 1 (step S12), and sets the opening degree limiting flag f to "1" (step S13). Further, the controller 20 monitors a shutdown of the indoor units $B_a, B_b, \dots B_n$ (step S14).

 When a shutdown of the indoor units $B_a, B_b, \dots B_n$
15 is not needed (NO in step S14), the control unit 20 returns to the flag determination of step S3. At this time, the opening degree limiting flag f is "1" (NO in step S3), and hence the control unit 20 compares the discharged refrigerant temperature (detected
20 temperature) T_d detected by the refrigerant temperature sensor 12 and the set value T_{ds} with each other (step S5).

 When the discharged refrigerant temperature T_d is lower than the set value T_{ds} (NO in step S5), the
25 control unit 20 controls the degree of opening Q of each of the expansion valves $4_a, 4_b, \dots 4_n$ to be within the range of the upper-limit value Q_{max} to the normal lower-limit value Q_{min} (step S4).

 When the discharged refrigerant temperature T_d is
30 higher than or equal to the set value T_{ds} (YES in step S5), the control unit 20 shifts the lower-limit value Q_{min} of the opening degree control toward the increase side by a predetermined value ΔQ , and controls the degree of opening Q of each of the expansion valves $4_a,$
35 $4_b, \dots 4_n$ to be within the range of the upper-limit

value Q_{max} to the lower-limit value " $Q_{min}+\Delta Q$ " (step S6).

5 A relationship between the outdoor air temperature and the pressure P_d on the high-pressure side, and a relationship between the outdoor air temperature and the discharged refrigerant temperature T_d are respectively proportional relations. When the outdoor air temperature rises, the pressure P_d on the high-pressure side and the discharged refrigerant
10 temperature T_d also rise. In this state, when the degree of opening Q of each of the expansion valves 4a, 4b, ... 4n is narrowed to the lower-limit value Q_{min} , there is a possibility of the high-pressure switch 11 operating after an elapse of not so long a time from
15 the restart of the compressor 1, and thereby stopping the compressor 1.

Thus, when the discharged refrigerant temperature T_d is higher than or equal to the set value T_{ds} , the opening-narrowing control of shifting the lower-limit
20 value Q_{min} of the opening degree control toward the increase side is executed, whereby it is possible to prevent the pressure P_d on the high-pressure side after the restart of the compressor 1 from rising. Particularly, even when the refrigerant with which the
25 heat pump refrigeration cycle system is filled is the refrigerant R32, by carrying out the opening-narrowing control as in the case of the refrigerant R410A, it is possible to prevent the pressure P_d on the high-pressure side after the restart of the compressor 1
30 from rising.

Accordingly, it is possible to prevent the operation of the high-pressure switch 11 at the time of the restart of the compressor 1 from being carried out, and by extension, to prevent frequent repetitions of a
35 stop and restart of the compressor 1 from occurring.

Thereby, the indoor temperature which is the load can be stabilized, and the comfort of air conditioning is improved.

5 It should be noted that when the outdoor air temperature lowers, the pressure P_d on the high-pressure side and the discharged refrigerant temperature T_d also lower, and hence there is a possibility of the opening-narrowing control becoming unnecessary. When the opening-narrowing control is
10 furthermore carried out under such circumstances, there is a possibility of the operational state of the heat pump refrigeration cycle becoming unable to be held appropriate, and thereby causing a shortage of air-conditioning capability. In consideration of these
15 circumstances, when the discharged refrigerant temperature T_d is lower than the set value T_{ds} (NO in step S5), the control unit 20 controls the degree of opening Q to be within the range of the upper-limit value Q_{max} to the normal lower-limit value Q_{min} without
20 executing the opening-narrowing control (step S4).

Thereafter, when a state where a shutdown of the indoor units $B_a, B_b, \dots B_n$ is needed is brought about (YES in step S14), the control unit 20 stops the compressor 1 (step S15). Then, the control unit 20
25 resets the opening degree limiting flag f (=1) to "0" (step S16), and returns to the operation start determination of first step S1. By resetting the opening degree limiting flag f to "0", the selective execution of the opening-narrowing control
30 corresponding to the discharged refrigerant temperature T_d is canceled.

Incidentally, the pressure P_d on the high-pressure side changes according to the capacity (the number of indoor units $B_a, B_b, \dots B_n$ in operation) of the heat
35 pump refrigeration cycle. That is, at the time of

cooling, as shown in FIG. 3, the larger the capacity, the higher the pressure P_d on the high-pressure side rises. Conversely, at the time of heating, as shown in FIG. 4, the smaller the capacity, the higher the pressure P_d on the high-pressure side rises.

In consideration of these circumstances, the control unit 20 sets the predetermined value ΔQ which is the shift amount of the opening-narrowing control to different values ($\Delta Q_1, \Delta Q_2, \dots, \Delta Q_n$) according to the number of indoor units B_a, B_b, \dots, B_n in operation. That is, at the time of cooling, in consideration of the fact that the larger the number of indoor units in operation, the higher the pressure P_d on the high-pressure side rises, the control unit 20 sets the predetermined value ΔQ_1 when the number of indoor units in operation is 1, sets the predetermined value ΔQ_2 ($>Q_1$) when the number is 2, sets the predetermined value ΔQ_3 ($>Q_2$) when the number is 3, and sets the predetermined value ΔQ_n ($\dots >Q_3$) when the number is the largest number n . At the time of heating, in consideration of the fact that the smaller the number of indoor units in operation, the higher the pressure P_d on the high-pressure side rises, the control unit 20 sets the predetermined value ΔQ_n when the number of indoor units in operation is 1, and sets the predetermined values $\Delta Q_3, \Delta Q_2,$ and ΔQ_1 in sequence with the increase in the number of indoor units in operation. In short, on the side on which the rise in the pressure P_d on the high-pressure side is remarkable, the predetermined value ΔQ is made large.

Further, concomitantly with the switching of the predetermined values $\Delta Q_1, \Delta Q_2, \dots, \Delta Q_n$, the control unit 20 switches the set value T_{ds} which is the criterion of the selective execution of the opening-narrowing control. That is, the control unit 20

selects a set value $Tds1$ when the predetermined value $\Delta Q1$ is set, selects a set value $Tds2$ ($>Tds1$) when the predetermined value $\Delta Q2$ is set, selects a set value $Tds3$ ($>Tds2$) when the predetermined value $\Delta Q3$ is set, and selects a set value $Tdsn$ ($\dots >Tds3$) when the predetermined value ΔQn is set.

As described above, the predetermined value ΔQ which is the shift amount of the opening-narrowing control is set to different values according to the number of indoor units $Ba, Bb, \dots Bn$ in operation, and the set value Tds which is the criterion of the selective execution of the opening-narrowing control is switched according to the predetermined value ΔQ , whereby it is possible to prevent frequent repetitions of a stop and restart of the compressor 1 from occurring irrespective of a change in the number of indoor units $Ba, Bb, \dots Bn$ in operation, i.e., irrespective of a change in the capacity of the heat pump refrigeration cycle.

Examples of changes in the pressure Pd on the high-pressure side, degree of opening Q of the expansion valve, discharged refrigerant temperature Td , and compressor rotational speed are shown in FIG. 5. As the degree of opening Q is narrowed, the pressure Pd on the high-pressure side rises, and when the pressure Pd on the high-pressure side rises to a set value $Pd2 \approx 4.1$ MPa, the high-pressure switch 11 operates to thereby stop the compressor 1. Thereafter, when the pressure Pd on the high-pressure side lowers to a set value $Pd1 \approx 3.2$ MPa, the high-pressure switch 11 is restored, and the compressor 1 is restored, however the discharged refrigerant temperature Td exceeds a set value $Tds \approx 65$ °C, and hence narrowing of the degree of opening Q is limited to the minimum value $Q_{min} \approx 200$ pls

which is the value after the shift, and concomitantly with this, the rise in the pressure Pd on the high-pressure side is held to about 3.7 MPa.

5 It should be noticed that although in the above embodiment, a description has been given by taking the refrigeration cycle apparatus to be incorporated in the air-conditioning apparatus as an example, the embodiment is also similarly applicable to a refrigeration cycle apparatus to be incorporated in other apparatuses.

10 The above embodiment and modification examples have been presented by way of example only, and are not intended to limit the scope of the inventions. Indeed, the novel embodiment and modification examples described herein may be embodied in a variety of other forms; 15 furthermore, various omissions, substitutions and changes in the form of the embodiment and modification examples described herein may be made without departing from the spirit of the inventions. The accompanying claims and their equivalents are intended to cover such 20 forms or modifications as would fall within the scope and spirit of the inventions.

Reference Signs List

1 ... compressor, 2 ... four-way valve, 3 ... 25 outdoor heat exchanger, 4a, 4b, ... 4n expansion valve, 5a, 5b, ... 5n indoor heat exchanger, 8 ... inverter, 9 ... AC source, and 20 ... control unit

Where any or all of the terms "comprise", "comprises", "comprised" or "comprising" are used in this specification (including the claims) they are to be 30 interpreted as specifying the presence of the stated features, integers, steps or components, but not precluding the presence of one or more other features, integers, steps or components.

C L A I M S

1. A refrigeration cycle apparatus comprising:
a refrigeration cycle including a compressor, a
condenser, an expansion valve, and an evaporator;

5 a high-pressure switch responding to the pressure
on the high-pressure side of the refrigeration cycle;
and

a control unit configured to control the degree of
opening Q of the expansion valve to be within a range of
10 a predetermined upper-limit value Q_{max} to a
predetermined lower-limit value Q_{min} in order that the
degree of superheat of the evaporator or the degree of
subcooling of the condenser becomes a constant value,
wherein

15 the control unit stops the compressor in response
to an operation of the high-pressure switch, thereafter
restarts the compressor in response to restoration of
the high-pressure switch, and at the time of the
restart, shifts the lower-limit value Q_{min} of opening
20 degree control for the expansion valve toward the
increase side by a predetermined value ΔQ .

2. The refrigeration cycle apparatus of Claim 1,
wherein

the control unit sets the predetermined value ΔQ to
25 different values according to the capacity of the
refrigeration cycle.

3. The refrigeration cycle apparatus of Claim 2,
wherein

the refrigeration cycle is a heat pump
30 refrigeration cycle capable of carrying out cooling and
heating, and

the control unit sets the predetermined value ΔQ to
a value proportional to the capacity of the
refrigeration cycle at the time of cooling, and to a
35 value inversely proportional to the capacity of the

refrigeration cycle at the time of heating.

4. The refrigeration cycle apparatus of any one of Claim 1 to Claim 3, further comprising temperature detecting section for detecting a temperature of a refrigerant discharged from the compressor, wherein

the control unit selectively executes shifting of the lower-limit value Q_{min} according to whether or not a detected temperature of the temperature detecting section is higher than or equal to a set value.

5. The refrigeration cycle apparatus of Claim 4, wherein

the control unit cancels the selective execution of the shifting of the lower-limit value Q_{min} concomitantly with a shutdown of the refrigeration cycle.

6. The refrigeration cycle apparatus of any one of Claim 1 to Claim 3, wherein

the refrigerant of the refrigeration cycle contains the refrigerant R32 in an amount of 50% or more.

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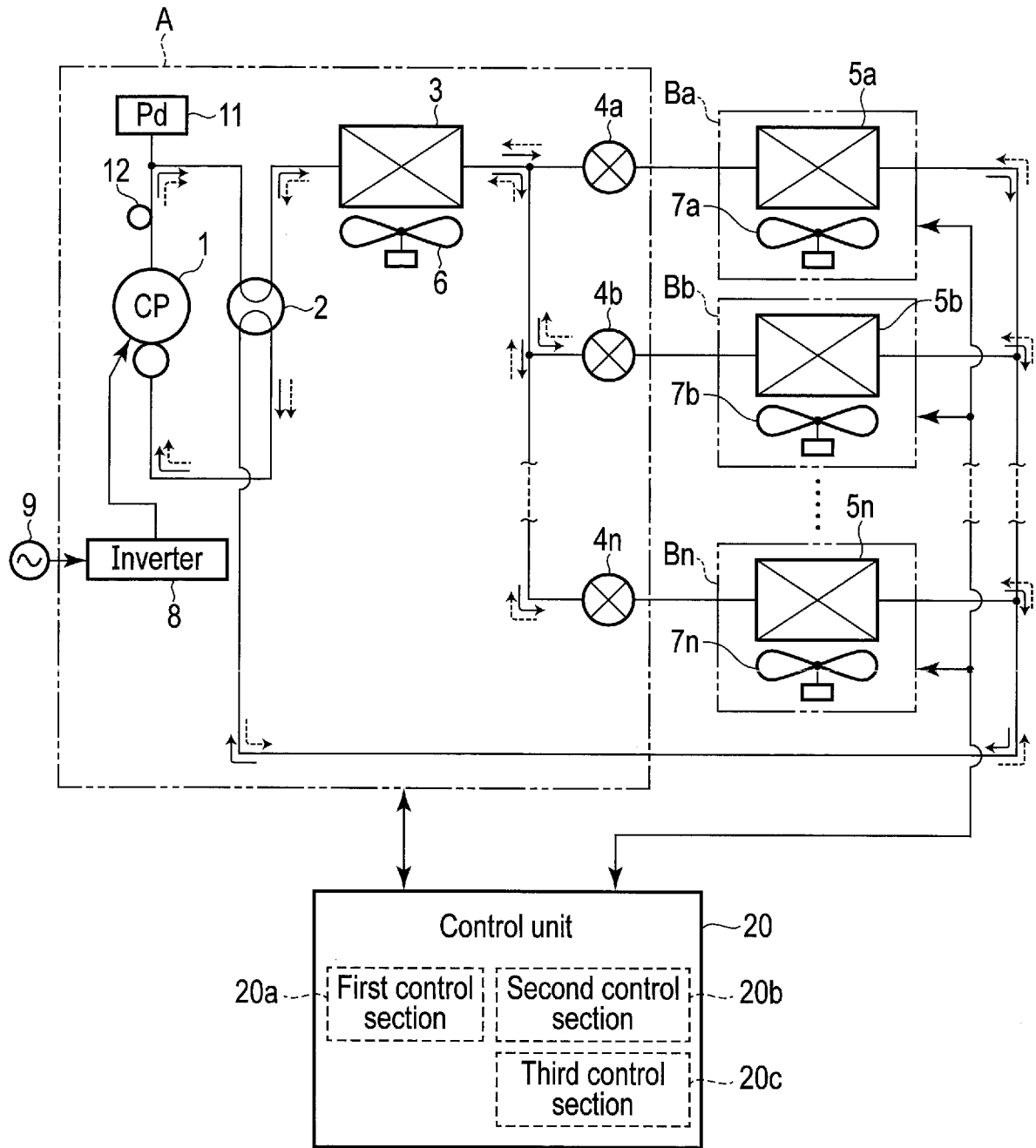


FIG. 1

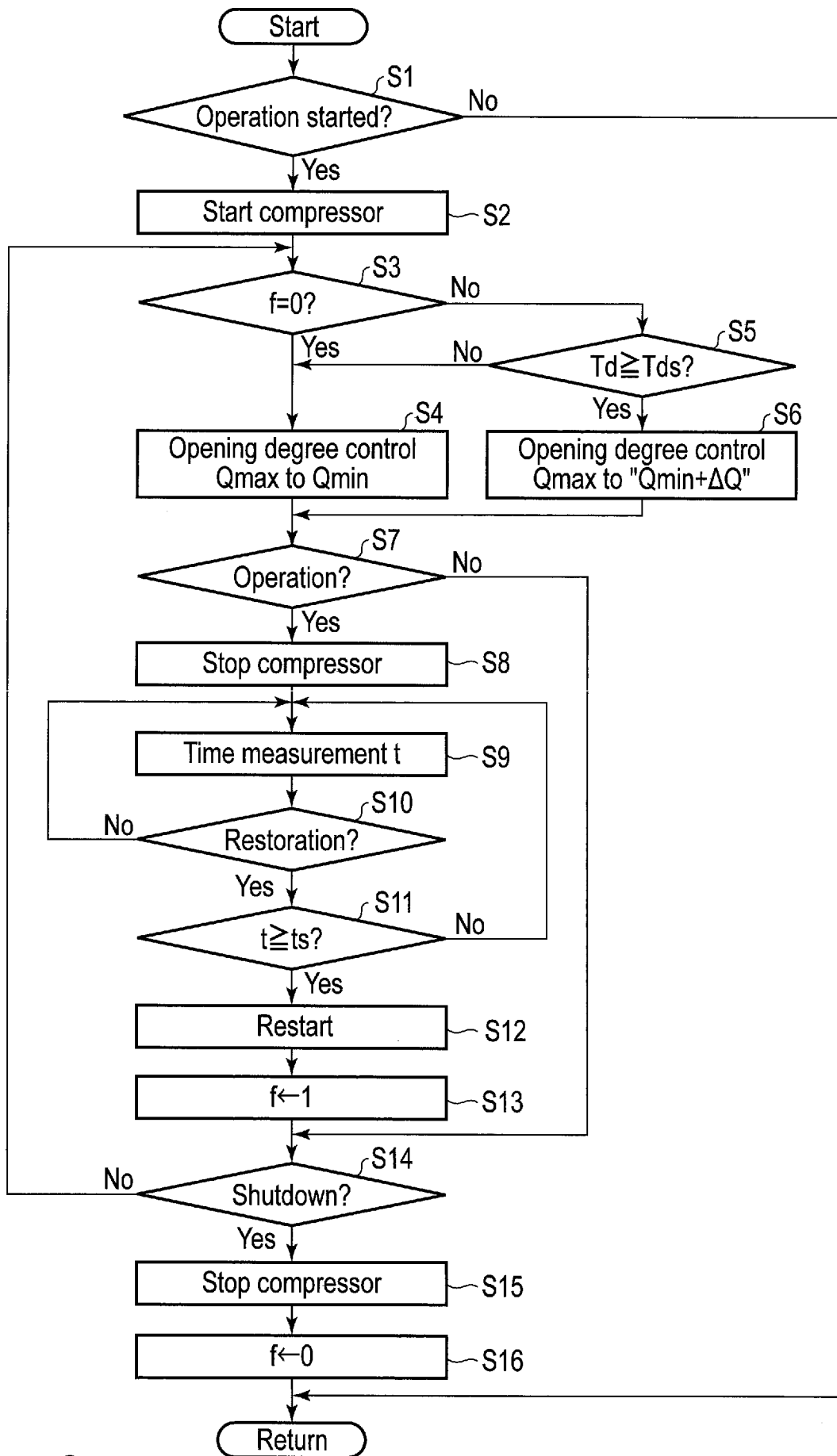


FIG. 2

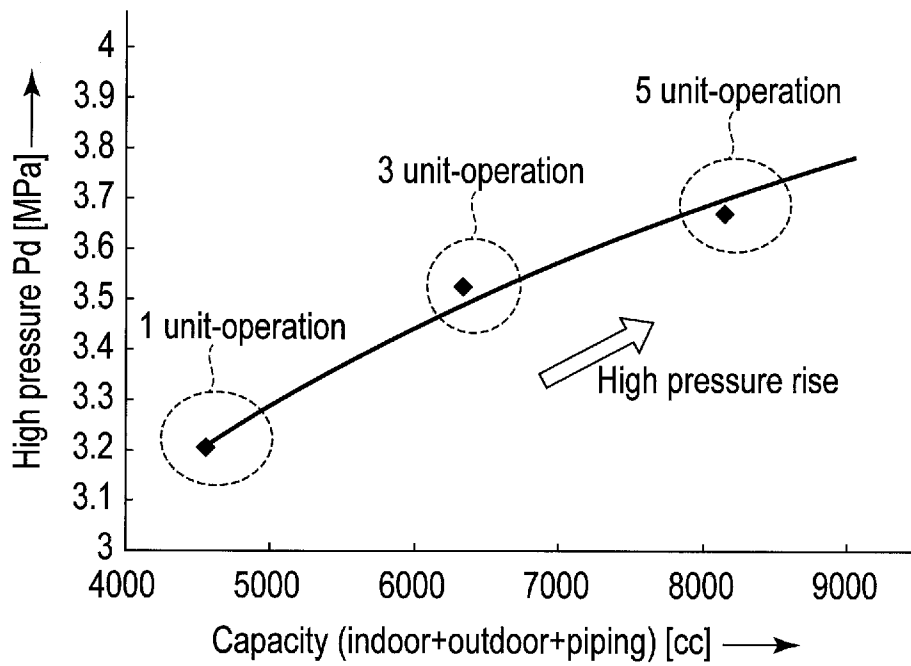


FIG. 3

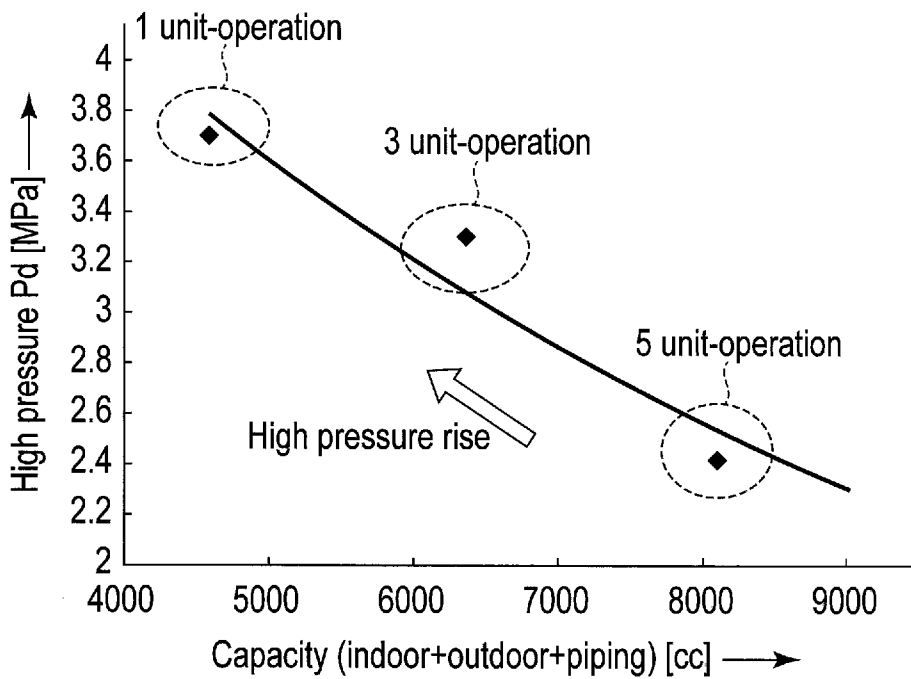


FIG. 4

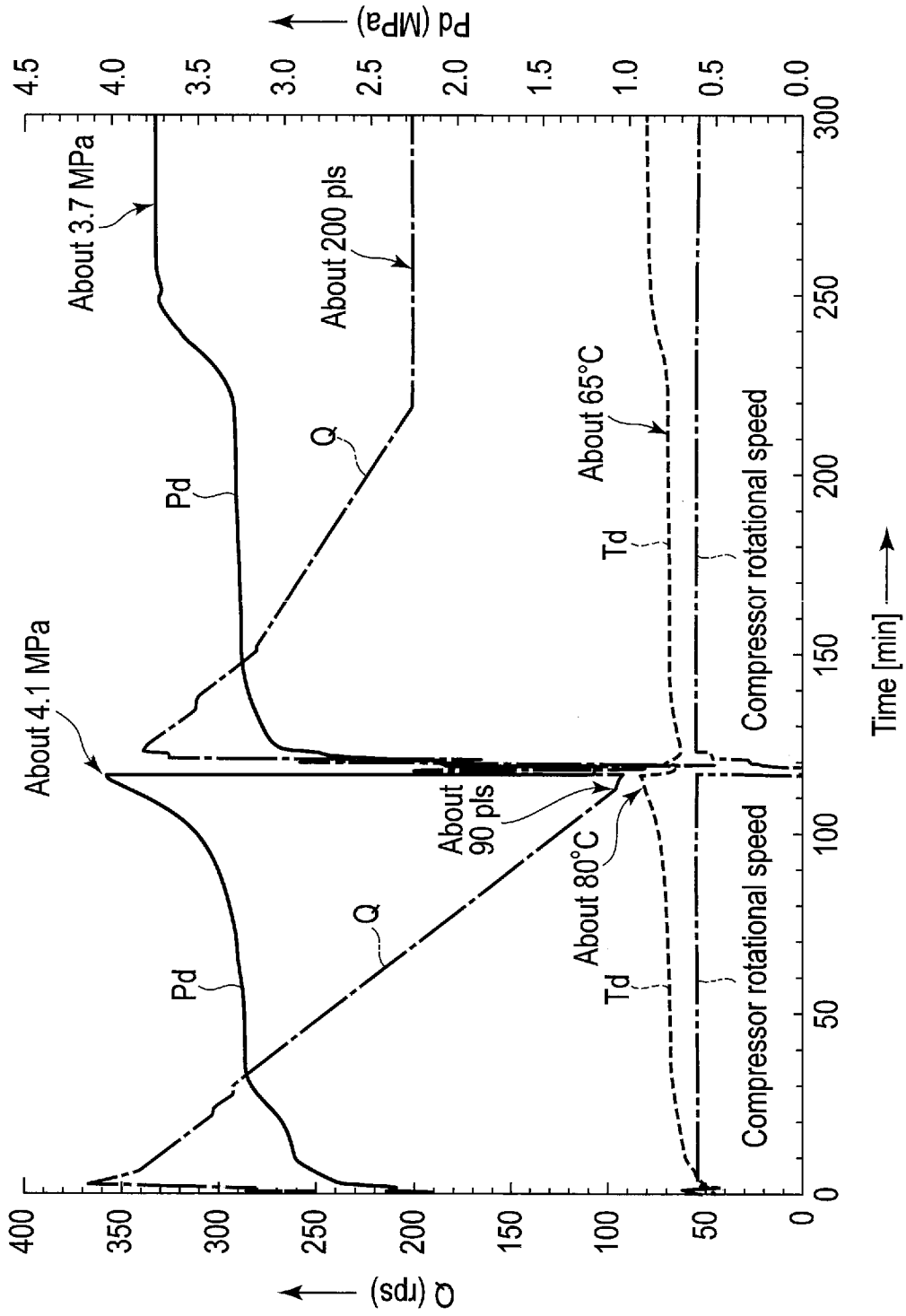


FIG. 5