

19



**Octrooi Centrum
Nederland**

11

2034255

12 B1 OCTROOI

21

Aanvraagnummer: **2034255**

51

Int. Cl.:
A61L 9/20 (2023.01)

22

Aanvraag ingediend: **2 maart 2023**

62

30

Voorrang:

-

73

Octrooihouder(s):
Ubed B.V. te Amsterdam

41

Aanvraag ingeschreven:
9 september 2024

72

Uitvinder(s):
Frans de la Haye te Den Haag

43

Aanvraag gepubliceerd:

-

74

Gemachtigde:
dr. R.C. van Duijvenbode c.s. te Den Haag

47

Octrooi verleend:
9 september 2024

45

Octrooischrift uitgegeven:
19 september 2024

54

Antimicrobial Air Ventilation Unit with Integral LED UV Light Source

57

This invention relates to an antimicrobial air ventilation unit (10) for treating air with UVC light comprising:
- at least one centrifugal fan unit (20) comprising an impeller (21) and a ducted fan housing (22); and
- at least one UVC radiation unit (31) comprising (i) at least one UVC-LED (32) and optionally (ii) at least one UVC directing lens (34),
- wherein the UVC radiation unit(s) (31) are configured to allow irradiation of air passing through the antimicrobial air ventilation unit (10),
wherein the at least one UVC radiation unit (31) is configured to illuminate at least a part of the interior of the ducted fan housing (22) with UVC light.

Antimicrobial Air Ventilation Unit with Integral LED UV Light Source

This invention relates to an antimicrobial air ventilation unit (10) for treating air with UVC light comprising:

- 5 - at least one centrifugal fan unit (20) comprising an impeller (21) and a ducted fan housing (22); and
- at least one UVC radiation unit (31) comprising (i) at least one UVC-LED (32) and optionally (ii) at least one UVC directing lens (34),
- wherein the UVC radiation unit(s) (31) are configured to allow irradiation of air passing through the antimicrobial air ventilation unit (10),
- 10 wherein the at least one UVC radiation unit (31) is configured to illuminate at least a part of the interior of the ducted fan housing (22) with UVC light.

Background

15 Air contamination is a long-standing problem, which has drawn considerable attention over the years. Typically, untreated air comprises bacteria, mould spores and viruses, which can cause health problems if inhaled. This is a particular problem in interior spaces where air may be recirculated by air ventilation units, such as elevators and hospital wards. Airborne bacterial infections that may be spread via an air ventilation unit include whooping cough, diphtheria and tuberculosis. Airborne bacterial infections that

20 may be spread via an air ventilation unit include the common cold, COVID-19, measles morbillivirus, chickenpox virus, influenza virus, enterovirus, norovirus and less commonly adenovirus. In an enclosed space, such as an office space, hospital ward or an elevator, recirculated air can increase the residence time of microbes in the air, hence the increase the probability that a susceptible person in that space will be infected by the microbe.

25 UVC light is well known to possess a very powerful germicidal effect capable of inactivating a wide spectrum of microorganisms, such as viruses, bacteria, protozoa, fungi, yeasts, and algae, through the formation of pyrimidine dimers, the photoproducts of genetic materials. Dimerization of pyrimidine disturbs DNA replication and transcription, which may lead to cell death. However, cell death is not required to anti-microbially treat

30 air, as long as sufficient damage to the cells has been caused so as to inhibit reproduction is required to render the microbes entrained in the air anti-microbially treated. A minimum residence time under UVC illumination is required to render microbes incapable of reproduction. This residence time is dependent on the wavelength of light, and the strength

of illumination. To provide compact air ventilation units, high light intensity is required, and the state-of-the-art systems use UV bulbs with high wattage (6 W).

Such antimicrobial air conditioning systems have been provided that anti-microbially treat the air that transits through the air ventilation unit. US 5,925,230 discloses an air purification system comprising a plurality of noisy axial fans and an ultraviolet (UV) light source (UV lamp bulb) within an air ventilation housing. One disadvantage of systems of this type is that the air flow must be brought close to the UV lamp, in this case with air being deviated around a UV lamp placed across the middle of C-shaped airflow ducting. This is bulky and causes turbulence in the airflow, and consequently causes noise. This also causes energy inefficiencies due to the turbulent flow. This prior art solution is therefore unsuitable for compact air ventilation units that rely on laminar air-flows to reduce noise and energy consumption. Until now, UV irradiation has mostly been performed with conventional low-pressure mercury UV lamps (LP lamps), which emit UV light with peak wavelength of 254 nm.

A further consideration is that UVC light is damaging to people's skin and eyes, which may cause cancer in the long term. Therefore, where UVC light sources are used in air ventilation units, care is taken to ensure that UVC light does not escape such systems. This is achieved in known systems by employing a series of baffles within the air ducting or bends within the air ducting (typically, V-, W-, U-, C- or S-shaped) to occlude light. These light occluding elements typically render such air ventilation units bulky and loud to operate, with the baffles and/or bends in the air ducting causing turbulence, which created disadvantageous noise and is energy inefficient. An example of an S-shaped air ducting assembly is seen in US 5,925,230.

It therefore remains a challenge to provide antimicrobial air ventilation units for treating air with UVC light that operate quietly, at greater energy efficiency (lower power, in Watts) and without bulky, light-occluding elements that induce turbulent air-flow.

Brief summary of the disclosure

In accordance with the present inventions there is provided an antimicrobial air ventilation unit (10) for treating air with UVC light comprising:

- at least one centrifugal fan unit (20) comprising an impeller (21) and a ducted fan housing (22); and
- at least one UVC radiation unit (31) comprising (i) at least one UVC-LED (32) and optionally (ii) at least one UVC directing lens (34),
- wherein the UVC radiation unit(s) (31) are configured to allow irradiation of air passing through the antimicrobial air ventilation unit (10),

wherein the at least one UVC radiation unit (31) is configured to illuminate at least a part of the interior of the ducted fan housing (22) with UVC light.

Brief description of the drawings

5 Embodiments of the invention are further described hereinafter with reference to the accompanying drawings, in which:

 Figure 1 depicts a perspective view of a first embodiment of an antimicrobial air ventilation unit according to the invention.

10 Figure 2 is a cut-away view of the first embodiment of an antimicrobial air ventilation unit according to the invention.

 Figure 3 is a horizontal, top-down, cross-section view of the first embodiment of an antimicrobial air ventilation unit according to the invention.

 Figure 4 is top-down, horizontal cross-sectional view of a non-limiting example of the first embodiment of an antimicrobial air ventilation unit according to the invention.

15 Figure 5 depicts a lamb-type UVC LED suitable for use in the invention.

 Figure 6 depicts a chip-type UVC LED suitable for use in the invention.

 Figure 7 depicts a UVC radiation unit (31) comprising 9 chip-type LEDs as depicted in Figure 6 suitable for use in the invention.

20 Figure 8 depicts the light occluding nature of a light occluding baffle assembly according to the invention.

 Figure 9 depicts the non-limiting example of Figure 4, with the dotted lines depicting direct emission paths of UVC photons from the UVC radiation units (31) being absorbed by the plates (51) of the light occluding baffle assembly (50).

25 Figure 10 is a cartoon of use of an antimicrobial air ventilation unit (10) according to the first embodiment of the present invention to antimicrobially treat air.

 Figure 11 is a cartoon of use of an example of an antimicrobial air ventilation unit (10) according to the first embodiment of the present invention to antimicrobially treat air, in which the ducted fan housing (22) comprises a portion of mirrored interior surface of the ducted fan housing (22M).

30 Figure 12 depicts in cartoon fashion antimicrobial treating air using a unit as depicted in Figures 4, 8 and 9.

Figure 13 depicts in cartoon fashion antimicrobial treating air using a particularly preferred embodiment unit broadly corresponding to that depicted in Figures 4, 8 and 9, wherein the ducted fan housing (22) is mirrored.

5 Figure 14 depicts in cartoon fashion antimicrobial treating air using a particularly preferred embodiment unit broadly corresponding to that depicted in Figure 2 combined with Figure 12.

Figure 15 depicts in cartoon fashion antimicrobial treating air comprising microbes (depicted as rings) and dust particles (pentagons) in an embodiment according to Figure 1

10 Figure 16 depicts a particularly preferably embodiment of the present invention, in which the unit (10) additionally comprises a filter unit (80).

Figure 17 depicts a non-limiting example corresponding to that of Figure 9, in which the ducted fan housing (22) is mirrored.

Detailed description

15 In a first aspect, the invention concerns antimicrobial air ventilation unit (10) for treating air with UVC light comprising:

- at least one centrifugal fan unit (20) comprising an impeller (21) and a ducted fan housing (22); and
- at least one UVC radiation unit (31) comprising at least one UVC-LED (32);

20 wherein the at least one UVC radiation unit (31) is configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that mechanical axis of the UVC-LED(s) (33) intersects the ducted fan housing (22).

The present invention achieves the goal of antimicrobially treating air with improved energy efficiency over the prior art by synergistically:

- (i) moving air with greater energy efficiency;
- 25 (ii) generating photons with greater energy efficiency;
- (iii) maximising the probability that a photon generated will impinge on a microbe in the moved air; and
- (iv) maximising the probability that when a photon generated hits a microbe, it stops the microbe from reproducing.

30

A centrifugal fan unit (20) is a mechanical device for moving air or other gasses in a direction at an angle to the incoming air, typically expelling air in a direction at 90° to the

incoming air. Centrifugal fan units (20) encompass fan units that may be referred to as “cross-flow fan” units (120) and “tangential fan” units (220). Centrifugal fan units (20) do not encompass fan units referred to as “axial fan” units or “axial blower” units. Centrifugal fan units (20) are not positive-displacement devices (pumps). Centrifugal fans comprise a ducted fan housing (22) and an impeller (21) (air moving means). The impeller (21) (air moving means) are typically provided by an axially symmetric rotor impeller (121) or cylindrical impeller (221), which rotate about their axes of rotation (26). The centrifugal fan unit (20) uses the centrifugal power supplied from the rotation of the impeller (21) (air moving means) to increase the kinetic energy of air or other gasses.

10 The impeller (21) (air moving means) may optionally be a fan wheel impeller (321) comprising an impeller hub (23) along the axis of rotation (26) and a number of impeller fan blades (24) attached to the periphery of the hub (23).

I Impeller fan blades (24) may be arranged around an impeller (21) in three different ways: (i) forward-curved/inclined impeller fan blades (24a); (ii) backward-curved/backward inclined impeller fan blades (24b) or (iii) straight radial impeller fan blades (24c).

 The impeller fan blades (24) may optionally be forward-curved impeller fan blades (24b), that is the curve of the blade is configured to be in the direction of the fan wheels rotation. For small diameter fan wheels, the blade may be straight, in which case the blade is referred to as forward inclined. Antimicrobial air ventilation units (10) comprising an impeller (21), wherein the impeller (21) comprises forward-curved impeller fan blades (24b) are particularly advantageous in providing laminar air flows with minimal noise production.

 The impeller fan blades (24) may optionally be backward-curved, that is the curve of the blade is against the direction of the fan wheel’s rotation. For particularly small diameter fan wheels, the blade may be straight, in which case the blade is referred to as backward-inclined. Antimicrobial air ventilation units (10) comprising an impeller (21), wherein the impeller (21) comprises backward-curved or backward-inclined blades are particularly advantageously energy efficient air moving means. They are more energy efficient than comparable air ventilation units comprising forward-curved or inclined impeller fan blades (24a), but at the disadvantage of operating with slightly more noise pollution. The noise pollution generated by air ventilation units (10) comprising backward-curved or backward-inclined blades are still advantageously quieter and more energy efficient than comparable “axial fan” units or “axial blower” units. Antimicrobial air ventilation units (10) comprising an impeller (21), wherein the impeller (21) comprises backward-curved/backward inclined impeller fan blades (24b) are advantageously resistant

to the solid accumulation/fouling and may be advantageously used for ventilating gasses with moderate to high particulate loadings.

The impeller fan blades (24) may optionally be straight radial impeller fan blades (24c), which extend straight out from the centre of the hub. Antimicrobial air ventilation units (10) comprising an impeller (21), wherein the impeller (21) comprises straight radial blades are the least sensitive to solid accumulation and are particularly advantageous for ventilation of airs with high to very high particulate loadings (as would be encountered with filter free operation in dusty conditions, such as in grain silos or kitchen environments).

Preferably, the impeller (21) (air moving means) is a hollow cylindrical impeller (421) with a hollow (25) aligned along the axis of rotation (26). The ends of the hollow cylindrical impeller (421) may be capped with solid end walls (27), as is typically the case for tangential fan units (220). By ends is meant an end region comprising the last 10% of the length of the impeller along the axis of rotation at either end of the impeller. The hollow cylindrical impeller (421) features impeller fan blades (24), which may be (i) forward-curved/inclined impeller fan blades (24a), (ii) backward curved/inclined impeller fan blades (24b) or (iii) straight radial impeller fan blades (24c). Dependent on the length of the hollow cylindrical impeller (421) along the axis of rotation (26), there may optionally be impeller fan blade support disks (28) to ensure impeller fan blade (24) rigidity and dimensional integrity. These impeller fan blade support disks (28) may be arranged so that their walls (29) are orthogonal to the axis of rotation (26), so that they do not impede the tangential flow of air.

In the absence of a ducted fan housing (22), when a hollow cylindrical impeller (421) or a fan wheel impeller (321) is rotated an equilibrium is created. Throughout the whole cross section of the impeller (21), air is being stirred in concentric circles with a stable vortex located in the centre of the impeller (21). In the absence of a ducted fan housing (22), minimal effective ventilation work is done, as little volume of air would transit through such a putative fan.

To produce work, air must travel through the impeller (21) (air rotation means), such as a hollow cylindrical impeller (421) or a fan wheel impeller (321). This is achieved by interaction of the impeller (21) with the ducted fan housing (22), which are configured to provide a laminar flow of air through the centrifugal fan unit (20).

In the case of an impeller (21) comprising a number of impeller fan blades (24), the ducted fan housing (22) is configured so that when the impeller fan blades (24) rotate about the axis of rotation (26), the gas particles near the impeller fan blades (24) are displaced radially outward and move towards the ducted fan housing (22). As a result, the kinetic energy of gas results in an increased pressure near the ducted fan housing (22),

because of the system resistance offered by the ducted fan housing (22). The gas is then rotationally displaced within the ducted fan housing (22) to the second (outlet) side (20b) of the centrifugal fan unit, where the gas exits the centrifugal fan unit (20). As the gas is radially displaced by the impeller fan blades (24), the gas pressure near the axis of rotation decreases. The external gas from the first (inlet) side of the centrifugal fan unit (20a) rushes in to the centrifugal fan unit (20) to normalize the pressure. This cycle repeats and therefore the gas can be continuously transferred through the centrifugal fan unit (20).

For tangential centrifugal fan units (220), this means that air must enter from at least one first (inlet) side of the tangential centrifugal fan unit (220a), which may be at a large range of tangential angles with respect to the second (outlet) side of the cross-flow centrifugal fan unit (220b), which is what "tangential" refers to. For tangential centrifugal fan units (220) this works by offsetting the position of the vortex from the axis of rotation to create an imbalance in pressures. Shifting the position of the vortex is accomplished by a non-axially symmetric (with respect to the axis of rotation of the impeller (21)) ducted fan housing (22a). This may be achieved by configuring the ducted fan housing (23a) so as to form an obstruction (22b) near the outer diameter of the impeller (21), which impedes rotation of gas (e.g. air) around the outside of the impeller (21).

The obstruction (22b) in the ducted fan housing (22a) is commonly known as a "vortex tongue" and its shape and position determines the performance characteristics of the tangential centrifugal fan unit (220) as well as the change in direction of the air flow. This shifting of the vortex creates high gas velocity in the centre of the impeller increasing the dynamic pressure, reducing static pressure. This creates suction on the first (inlet) side of the tangential centrifugal fan unit (220a). As the air exits through the second (outlet) side of the tangential centrifugal fan unit (220b) the gas velocity slows, decreasing the dynamic pressure and increasing static pressure. This causes the gas to exit the tangential centrifugal fan unit (220) via the second (outlet) side of the tangential centrifugal fan unit (220b). Thus, a fast, smooth laminar flow out of the tangential centrifugal fan unit (220) is established at a particularly advantageous high velocity for a given motor speed.

For cross-flow centrifugal fan units (120), this means that air must enter from at least one first (inlet) side of the cross-flow centrifugal fan unit (120a), which is appropriately orthogonal to the second (outlet) side of the cross-flow centrifugal fan unit (120b). This is what "cross-flow" refers to.

The size and shape of the centrifugal fan unit (20) and the size and shape of the fan housing are mutually dependent and are preferably configured so as to allow a laminar air flow to be formed in use.

The first aspect of the invention requires that the antimicrobial air ventilation unit (10) for treating air with UVC light comprises at least one UVC radiation unit (31) comprising (i) at least one UVC-LED (32), and optionally (ii) at least one UVC lens (34).

5 Suitable UVC radiation units (31) are capable of producing light with one or more wavelengths in the range of from 100 to 280 nm, more preferably in the range of from 225 to 280 nm, even more preferably in the range of from 255 to 270 nm and most preferably with a wavelength of 265 (± 0.5) nm. Using a wavelength of from 100 to 280 nm maximizes the probability that when a photon generated with this wavelength hits a microbe, it stops the microbe from reproducing. The more preferable wavelength ranges are particularly
10 advantageous as this is most destructive to bacteria and virus DNA and/or RNA, hence most efficacious at antimicrobial treatment of air.

UVC radiation units (31) comprising UVC-LEDs (32) are more energy efficient at generating photons with a wavelength of from 100 to 280 nm than conventional low-pressure mercury UV lamps (LP lamps), thereby generating photons with greater energy
15 efficiency.

UVC radiation units (31) comprising UVC-LEDs (32) are also much faster at generating sufficient UVC radiation, doing so within seconds, compared to the minutes required by conventional low-pressure mercury UV lamps (LP lamps) to “warm up”. This provides the benefit that an antimicrobial air ventilation unit (10) according to the present
20 invention does not needlessly circulate air for up to 15 minutes before antimicrobially treating air, and is consequently more energy efficient.

UVC radiation units (31) comprising UVC-LEDs (32) generate directionally focused light, rather than random direction of light generated by gas-discharge within a conventional mercury vapour lamp. This provides the benefit that an antimicrobial air
25 ventilation unit (10) according to the present invention maximizes the probability that a photon generated will impinge on a microbe in the moved air, as the directionally focused light may be directed across the path through which the air is moved.

UVC radiation units (31) comprising UVC-LEDs (32) are smaller than conventional mercury vapor lamp capable of outputting the same amount of UVC radiation.
30 The effect of this difference is that the smaller UVC radiation units (31) may be located within the ducted fan housing (22) without significantly objecting the air flow path. This results in an apparatus capable of (i) moving air with greater energy efficiency and (ii) moving air more quietly than an apparatus with a conventional mercury vapour lamp located within the ducted fan housing (22).

UVC radiation units (31) comprising UVC-LEDs (32) are believed to have a longer lifespan of approximately 25,000 hours, compared to the shorter lifespan of 5,000 hours of a typical low pressure mercury lamp. This means that an antimicrobial air ventilation unit (10) according to the present invention may be advantageously operated for longer periods than known antimicrobial UVC ventilation units without maintenance.

Suitable UVC-LEDs (32) are capable of producing light with a wavelength of 100-280 nm, more preferably in the range of from 225 to 280 nm, even more preferably in the range of from 255 to 270 nm and most preferably with a wavelength of 265 (± 0.5) nm. For example, suitable UVC-LEDs may optionally be NCSU334B LED lights commercially available from Nichia (2021). UVC-LEDs are particularly advantageous in providing high flux of light with a wavelength of from 100 to 280 nm in an energy efficient manner.

Preferably, the UVC-LED(s) (32) emit light with a peak wavelength (λ_P) of from 250 to 280 nm. More preferably, the UVC-LED(s) (32) have a peak wavelength (λ_P) of from 225 to 270 nm, which is deemed particularly lethal to most microorganisms and which is herein referred to as ultraviolet germicidal irradiation (UVGI). Most preferably, the UVC-LED(s) (32) have a peak wavelength (λ_P) of 265 (± 0.5) nm. This wavelength is particularly advantageous as this is most destructive to bacteria and virus DNA.

Preferably, the UVC-LED(s) (32) have a maximum irradiance flux density of from 0.5 to 50 mW/cm² at a distance of 50 mm from the UVC-LED, more preferably 1.0 to 25 mW/cm², even more preferably 1.5 to 15 mW/cm².

Preferably, the UVC radiation unit(s) (31) have a directivity angle $2\theta_{1/2}$ of from 180° to 5°, more preferably of from 160° to 10°, even more preferably of from 140° to 20°, yet more preferably of from 120° to 30° and most preferably of from 70° to 50°. A directivity angle that is too small (smaller than 5°) is less preferable as little of the air moved through the ducted fan housing (22) may be irradiated by a single UVC-LED, leading to less energy efficiency. A directivity angle that is too large (greater than 180°) is less preferable as a significant part of the radiant flux of UVC-light hits the ducted fan housing (22) before passing through the air to be treated which is being moved through the centrifugal fan unit (20), leading to less energy efficiency.

Where the UVC radiation unit(s) (31) do not comprise at least one UVC converging lens, the UVC-LED(s) (32) preferably have a directivity angle $2\theta_{1/2}$ of from 180° to 5°, more preferably of from 160° to 10°, even more preferably of from 140° to 20° and most preferably of from 120° to 30°. The preferable directivity angles allow for maximising the probability that a photon generated will impinge on a microbe in the moved air.

The UVC radiation unit(s) (31) preferably additionally comprise at least one UVC lens. The UVC lens is made of a material that is optically transmissive to light with a wavelength in the range of from 100 to 280 nm that is resistant to photodegradation at this wavelength. Suitable materials include UV-resistant plastics and quartz glass. The function of the UVC lens(es) (34) is to modify the directivity angle $2\theta_{1/2}$ of the light emitted by the UVC-LED(s) (32). The UVC lens(es) (34) and UVC-LED(s) (32) may be configured such that the UVC radiation emitted by each UVC-LED impinges a UVC lens (34), which results in an overall change in the directivity angle $2\theta_{1/2}$. The UVC lens (34) may be a converging lens or a diverging lens, more preferably a converging lens. Particularly preferable UVC radiation unit(s) (31) comprise a combination of a converging UVC lens and a UVC-LED (32), to afford UVC radiation unit(s) (31) with a directivity angle $2\theta_{1/2}$ of from 180° to 5° , more preferably of from 160° to 10° , even more preferably of from 140° to 20° , yet more preferably of from 120° to 30° and most preferably of from 70° to 50° . Preferably, the UVC radiation unit(s) (31) is(are) configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that optical axis(axis) of the UVC radiation unit(s) (31) is(are) approximately co-axial with the axis of rotation of the impeller (26). By approximately co-axial, it is meant that the axes are within 25° of co-axial. An advantage of this configuration is that this allows light from the UVC radiation unit(s) (31) to travel along the length of the ducted fan housing (22L), approximately orthogonal (within 25° of orthogonal) to the flow of air. This allows the UVC photons to travel for a maximal distance through microbe-containing air, which increases the probability that any one photon of UVC light will impinge on a microbe travelling through the ducted fan housing. The effect of this is that lower irradiance flux, and consequently less energy is required to achieve the same degree of antimicrobial treatment. This arrangement is described in this patent application as enfilading UVC illumination.

More preferably, the UVC radiation unit(s) (31) is(are) configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that the optical axis(es) of the UVC radiation unit(s) (31) is(are) approximately co-axial with the axis of rotation of the impeller (26), wherein by approximately co-axial, it is meant that the axes are within 15° of co-axial, even more preferably it is meant that the axes are within 10° of co-axial, most preferably it is meant that the axes are within 5° of co-axial.

Most preferably, the UVC radiation unit(s) (31) is(are) configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that all air flowing through the antimicrobial air ventilation unit (10) is exposed to UVC radiation.

In a preferable embodiment, the UVC radiation unit(s) (31) is(are) configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that mechanical

axis(axis) of the UVC-LED(s) (33) is(are) approximately co-axial with the axis of rotation of the impeller (26). By approximately co-axial, it is meant that the axes are within 25° of co-axial. An advantage of this configuration is that this allows light from the UVC-LED to travel along the length of the ducted fan housing (22L), which increases the probability that any one photon of UVC light will impinge on a microbe travelling through the ducted fan housing and consequently lower irradiance flux and less energy is required to achieve the antimicrobial treatment. This could be considered to be enfilading UVC illumination of a laminar air flow.

More preferably, the UVC radiation unit (31) is configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that mechanical axis of the UVC-LED(s) (33) is approximately co-axial with the axis of rotation of the impeller (26), wherein by approximately co-axial, it is meant that the axes are within 15° of co-axial, even more preferably it is meant that the axes are within 10° of co-axial, most preferably it is meant that the axes are within 5° of co-axial.

Most preferably, the UVC radiation unit (31) is configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that all air flowing through the antimicrobial air ventilation unit (10) is exposed to UVC radiation.

In a preferable embodiment, the antimicrobial air ventilation unit (10) for treating air with UVC light comprises:

- at least one centrifugal fan unit (20) comprising an impeller (21) and a ducted fan housing (22); and
- at least two UVC radiation units (31), each UVC radiation unit comprising at least one UVC-LED (32);

wherein the at least two UVC radiation units (31) are configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that mechanical axis of the UVC-LED(s) (33) intersects the ducted fan housing (22).

Preferably, the at least two UVC radiation units (31) are located on or at opposite sides of the ducted fan housing (22) and are configured to simultaneously illuminate a volume of the ducted fan housing (22K). This simultaneously illuminated volume of the ducted fan housing is termed the enfilading microbial kill-zone of the ducted fan housing (22K). The advantage of this configuration is that higher radiant flux of UVC light can be achieved for low energy costs compared to other configurations, which in use allow high energy efficiency antimicrobial treatment of air moved through the ducted fan housing (22).

Most preferably, the at least two UVC radiation units (21) are located on or at opposite sides of the ducted fan housing (22), are configured to simultaneously illuminate

a volume of the ducted fan housing (22K) and are configured such that mechanical axes of the UVC-LED(s) (33) are approximately co-axial with the axis of rotation of the impeller (26). By approximately co-axial, it is meant that the axes are within 45° of co-axial. An advantage of this configuration is that this allows light from the UVC-LED to travel along the length of the ducted fan housing (22L), from two directions, which increases the probability that any one photon of UVC light will impinge on a microbe travelling through the ducted fan housing and consequently lower irradiance flux and less energy is required to achieve the antimicrobial treatment. This means that higher UVC photon flux can be achieved in the enfiling microbial kill-zone of the ducted fan housing (22K), and consequently higher flow rates can be realised without comprising the antimicrobial treatment. Even more preferably, the UVC radiation units (31) are configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that mechanical axes of the UVC-LEDs (33) are approximately co-axial with the axis of rotation of the impeller (26), wherein by approximately co-axial, it is meant that the axes are within 30° of co-axial, yet more preferably it is meant that the axes are within 10° of co-axial, most preferably it is meant that the axes are within 5° of co-axial. The closer to co-axial the axes of the UVC-LEDs (33) are to the axis of rotation of the impeller, the higher the flux of UVC photons in the enfiling microbial kill-zone of the ducted fan housing (22K) can be achieved for the same UVC-LEDs (32).

In an equally preferable alternative embodiment, the antimicrobial air ventilation unit (10) for treating air with UVC light comprises:

- at least one centrifugal fan unit (20) comprising an impeller (21) and a ducted fan housing (22);
- at least one UVC radiation unit (31) comprising at least one UVC-LED (32); and
- at least one mirrored interior surface of the ducted fan housing (22M),

wherein the at least one UVC radiation unit (31) is configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that mechanical axis of the UVC-LED(s) (33) intersects the mirrored interior surface of the ducted fan housing (22M).

This embodiment advantageously allows higher UVC photon flux to be achieved within the ducted fan housing (22) than a comparable antimicrobial air ventilation unit without at least one mirrored interior surface of the ducted fan housing (22M) or configured such that mechanical axis of the UVC-LED(s) (33) intersects the mirrored interior surface of the ducted fan housing (22M).

By mirrored interior surface of the ducted fan housing (22M) is meant a surface that reflects at least 15% of incident light radiation with a wavelength of from 100 to 280

nm. A suitable mirrored interior surface would be stainless steel sheet, which reflects approximately 20-30% of incident UVC light with a wavelength of 100-280 nm, or untreated aluminium, which reflects approximately 40-60% of incident UVC light with a wavelength of 100-280 nm, or chromium plating, which reflects approximately 39% of incident UVC light with a wavelength of 100-280 nm, or aluminium paint, which reflects approximately 10-75% of incident UVC light with a wavelength of 100-280 nm. Preferably, the mirrored interior surface of the ducted fan housing (22M) reflects at least 70% of incident light radiation with a wavelength of 100-280 nm. Such a surface could suitably be made of aluminium foil, which reflects approximately 73% of incident light radiation with a wavelength of 100-280 nm, or magnesium oxide which reflects approximately 75-88% of incident light radiation with a wavelength of 100-280 nm. More preferably the mirrored interior surface of the ducted fan housing (22M) reflects at least 75% of incident light radiation with a wavelength of 100-280 nm. Such a surface could suitably be made of polished aluminium sheet (alzak), which reflects approximately 80% of incident light radiation with a wavelength of 100-280 nm. Even more preferably the mirrored interior surface of the ducted fan housing (22M) reflects at least 90% of incident light radiation with a wavelength of 100-280 nm. Such a surface could suitably be made of expanded Polytetrafluoroethylene (e-PTFE), which reflects approximately 95% of incident light radiation with a wavelength of 100-280 nm.

Preferably, the at least one UVC radiation unit (31) and at least one mirrored interior surface of the ducted fan housing (22M) are located on or at opposite sides of the ducted fan housing (22) and are configured such that un-reflected light from the at least one UVC radiation unit (31) and reflected light from the mirrored interior surface of the ducted fan housing (22M) simultaneously illuminate a volume within the ducted fan housing (22K). This simultaneously illuminated volume of the ducted fan housing is termed the enfiling microbial kill-zone (reflected) of the ducted fan housing (22KR). The advantage of this configuration is that higher radiant flux of UVC light can be achieved for low energy costs compared to other configurations, which in use allow high energy efficiency antimicrobial treatment of air moved through the ducted fan housing (22), in particular air moved through the enfiling microbial kill-zone (reflected) of the ducted fan housing (22

More preferably, the at least one UVC radiation units (31) and at least one mirrored interior surface of the ducted fan housing (22M) are configured to simultaneously illuminate a volume of the ducted fan housing (22KR) and are configured such that mechanical axis(axis) of the UVC-LED(s) (33) is (are) approximately co-axial with the axis of rotation of the impeller (26) and substantially orthogonal to the at least one mirrored

interior surface of the ducted fan housing (22M). By approximately co-axial, it is meant that the axes are within 45° of co-axial. By substantially orthogonal, it is meant that the axis is within 20° of normally incident. An advantage of this configuration is that this allows light from the UVC-LED to travel along the length of the ducted fan housing (22L), from two
5 directions, which increases the probability that any one photon of UVC light will impinge on a microbe travelling through the ducted fan housing and consequently lower irradiance flux and less energy is required to achieve the antimicrobial treatment. This means that higher UVC photon flux can be achieved in the enfiling microbial kill-zone (reflected) of the ducted fan housing (22KR), and consequently higher flow rates can be realised without
10 comprising the antimicrobial treatment.

Even more preferably, the at least one UVC radiation unit (31) is configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that mechanical axis (axes) of the UVC-LED(s) (33) is (are) approximately co-axial with the axis of rotation of the impeller (26), wherein by approximately co-axial, it is meant that the axes are within
15 30° of co-axial, yet more preferably it is meant that the axes are within 10° of co-axial, most preferably it is meant that the axes are within 5° of co-axial. The closer to co-axial the axis (axes) of the UVC-LED(s) (33) is (are) to the axis of rotation of the impeller, the higher the flux of UVC photons in the enfiling microbial kill-zone (reflected) of the ducted fan housing (22KR) can be achieved for the same number of UVC-LED(s) (32) in alternative
20 configurations.

Even more preferably, the at least one UVC radiation unit (31) is configured to illuminate the interior of the ducted fan housing (22) with UVC light, such that mechanical axis (axes) of the UVC-LED(s) (33) is (are) substantially orthogonal to the at least one mirrored interior surface of the ducted fan housing (22M), wherein by substantially
25 orthogonal is meant that the axis is (axes are) within 10° of normally incident, yet more preferably within 5° of normally incident and most preferably are within 2° of normally incident.

A favourable combination of features is an the antimicrobial air ventilation unit according to this embodiment wherein:

- 30
- the mirrored interior surface of the ducted fan housing (22M) reflects at least 20% of incident light radiation with a wavelength of 100-280 nm;
 - mechanical axis(axis) of the UVC-LED(s) (33) is (are) approximately co-axial with the axis of rotation of the impeller (26), wherein approximately co-axial means that the axes are within 45° of co-axial; and

- mechanical axis(axis) of the UVC-LED(s) (33) is (are) substantially orthogonal to the at least one mirrored interior surface of the ducted fan housing (22M), wherein substantially orthogonal means that the axis is within 20° of normally incident.

5 Another, particularly favourable combination of features is an the antimicrobial air ventilation unit according to this embodiment wherein:

- the mirrored interior surface of the ducted fan housing (22M) reflects at least 70% of incident light radiation with a wavelength of 100-280 nm;
- mechanical axis(axis) of the UVC-LED(s) (33) is (are) approximately co-axial with the axis of rotation of the impeller (26), wherein approximately co-axial means that
10 the axes are within 30° of co-axial; and
- mechanical axis(axis) of the UVC-LED(s) (33) is (are) substantially orthogonal to the at least one mirrored interior surface of the ducted fan housing (22M), wherein substantially orthogonal means that the axis is within 10° of normally incident.

15 Another, more particularly favourable combination of features is an the antimicrobial air ventilation unit according to this embodiment wherein:

- the mirrored interior surface of the ducted fan housing (22M) reflects at least 75% of incident light radiation with a wavelength of 100-280 nm;
- mechanical axis(axis) of the UVC-LED(s) (33) is (are) approximately co-axial with the axis of rotation of the impeller (26), wherein approximately co-axial means that
20 the axes are within 5° of co-axial; and
- mechanical axis(axis) of the UVC-LED(s) (33) is (are) substantially orthogonal to the at least one mirrored interior surface of the ducted fan housing (22M), wherein substantially orthogonal means that the axis is within 10° of normally incident.

25 Another, even more particularly favourable combination of features is an the antimicrobial air ventilation unit according to this embodiment wherein:

- the mirrored interior surface of the ducted fan housing (22M) reflects at least 80% of incident light radiation with a wavelength of 100-280 nm;
- mechanical axis(axis) of the UVC-LED(s) (33) is (are) approximately co-axial with the axis of rotation of the impeller (26), wherein approximately co-axial means that
30 the axes are within 10° of co-axial; and
- mechanical axis(axis) of the UVC-LED(s) (33) is (are) substantially orthogonal to the at least one mirrored interior surface of the ducted fan housing (22M), wherein substantially orthogonal means that the axis is within 5° of normally incident.

Another, most favorable combination of features is an antimicrobial air ventilation unit according to this embodiment wherein:

- the mirrored interior surface of the ducted fan housing (22M) reflects at least 90% of incident light radiation with a wavelength of 100-280 nm;
- 5 - mechanical axis(axis) of the UVC-LED(s) (33) is (are) approximately co-axial with the axis of rotation of the impeller (26), wherein approximately co-axial means that the axes are within 5° of co-axial; and
- mechanical axis(axis) of the UVC-LED(s) (33) is (are) substantially orthogonal to the at least one mirrored interior surface of the ducted fan housing (22M), wherein
10 substantially orthogonal means that the axis is within 2° of normally incident.

The more the incident light radiation with a wavelength of 100-280 nm the mirrored interior surface of the ducted fan housing (22M) reflects at least 90% of, the higher the flux of UVC photons in the enfilading microbial kill-zone (reflected) of the ducted fan housing (22KR) can be achieved than for alternative configurations utilizing less
15 reflective mirrored interior surface of the ducted fan housings (22M).

The closer to co-axial the axis (axes) of the UVC-LED(s) (33) is (are) to the axis of rotation of the impeller, the higher the flux of UVC photons in the enfilading microbial kill-zone (reflected) of the ducted fan housing (22KR) can be achieved than for alternative configurations utilizing the same UVC-LED(s) (32).

20 The closer to normally incident the axis (axes) of the UVC-LED(s) (33) is (are) to the at least one mirrored interior surface of the ducted fan housing (22M), the higher the flux of UVC photons in the enfilading microbial kill-zone (reflected) of the ducted fan housing (22KR) can be achieved than for alternative configurations utilizing the same UVC-LED(s) (32).

25 The antimicrobial air ventilation unit (10) according to the first aspect of the invention, according to any of the embodiments above, may optionally additionally comprise an air ventilation housing (40).

The air ventilation housing (40) is preferably configured to enclose the at least one centrifugal fan unit (20) and the UVC radiation unit (31), whilst still allowing fluid
30 communication of air from the outside of the antimicrobial air ventilation unit (10) to the first (inlet) side of the at least one centrifugal fan unit (20a) and the second (outlet) side of the at least one centrifugal fan unit (20). The air ventilation housing (40) advantageously protects the antimicrobial air ventilation unit (10) from accidental damage and external environmental factors.

The antimicrobial air ventilation unit (10) according to the first aspect of the invention, according to any of the embodiments above, may optionally additionally comprise a light occluding baffle assembly (50) comprising a plurality of light occluding baffle assembly slits (51).

5 Where present, the light occluding baffle assembly (50) is configured to fit the second (outlet) side of the at least one centrifugal fan unit (20b). The light occluding baffle assembly advantageously protects the centrifugal fan unit from accidental ingress of large objects into the ducted fan housing (22).

In a preferable embodiment, the light occluding baffle assembly (50) comprises:

- 10 - a plurality of light occluding baffle assembly slits (51); and
 - a plurality of light occluding baffle assembly plates (52),

 wherein the plurality of light occluding baffle assembly slits (51) and the plurality of light occluding baffle assembly plates (52) are configured to visibly occlude the UVC radiation unit(s) (31) whilst still allowing free fluid communication of air from the interior of the centrifugal fan unit (20) with the exterior of the antimicrobial air ventilation unit (10) via the second (outlet) side of the at least one centrifugal fan unit (20). Visibly occluding the UVC radiation unit(s) (31) means that no UVC light emitted by the UVC radiation units (31) has a direct path to the exterior of the antimicrobial air ventilation unit (10).

15

A suitable light occluding baffle assembly (50) so configured could be a light occluding baffle assembly (50) wherein the plurality of light occluding baffle assembly plates (52) are arranged to be substantially orthogonal to the axis of rotation of impeller (26) [and consequently substantially parallel to direction of air flow out of the second (outlet) side of the at least one centrifugal fan unit (20)].

20

An effect of this embodiment is that little to no UVC-light exits the antimicrobial air ventilation unit (10), which confers the advantage of being safer (less to no harmful radiation exposure). Another effect is that this obviates the need for additional light occluding elements, such as a series of baffles within the air ducting or bends within the air ducting (typically, V-, W-, U-, C- or S-shaped). These light occluding elements typically render such air ventilation units bulky and loud to operate, thus this advantageously allows for the provision of more compact antimicrobial air ventilation units.

25

30

Preferably, the plurality of light occluding baffle assembly plates (52) are coated in a material that reflects less than 30% of incident light radiation with a wavelength of 100-280 nm. A suitable surface would be polished steel, which reflects approximately 20-28% of incident UVC light with a wavelength of 100-280 nm. More preferably, the plurality of light occluding baffle assembly plates (52) are coated in a material that reflects less than

35

10% of incident light radiation with a wavelength of 100-280 nm. Even more preferably, the plurality of light occluding baffle assembly plates (52) are coated in a material that reflects less than 2% of incident light radiation with a wavelength of 100-280 nm. Most preferably, the plurality of light occluding baffle assembly plates (52) are coated in a material that reflects less than 2% of incident light radiation with a wavelength of 100-280 nm.

The less that the plurality of light occluding baffle assembly plates (52) reflect incident light radiation with a wavelength of 100-280 nm, the less potentially harmful UVC light that may escape the antimicrobial air ventilation unit (10) by reflecting off the light occluding baffle assembly plates (52), and hence safer the antimicrobial air ventilation unit (10) is in use.

The antimicrobial air ventilation unit (10) according to the first aspect of the invention, according to any of the embodiments above, may optionally additionally comprise a filtration unit (80). The optional filtration unit (80) is preferably proximal to the first (inlet) side of the at least one centrifugal fan unit (20a). The filtration unit (80) may be selected from a high-efficiency particulate air (HEPA) filter (80a).

The HEPA filter (80a) is preferably configured to remove at least 99.95% of particles whose diameter is equal to 0.3 μm from the air that passes through the HEPA filter, measured according to method described in European Standard EN 1822-1:2019, and references cited therein.

A second aspect of the invention concerns a method for the antimicrobial treatment of air comprising the steps of:

- i. Providing air comprising microbes to an antimicrobial air ventilation unit (10) according to any of the embodiments according to the first aspect of the invention;
- ii. Causing the air comprising microbes to move through the centrifugal fan unit (20);
- and
- iii. Irradiating the moving air comprising microbes with UVC light within the ducted fan housing (22) of the antimicrobial air ventilation unit (10).

In the context of the current invention antimicrobial treatment is a reduction in the active microorganism concentration. This may be quantified by an inactivation rate, which is a measurement in the reduction in active microorganism concentration is expressed as $N_0/N(\%)$ or $\log(N_0/N)$, in which:

- N_0 is the original active microorganism concentration, and
- N is the active microorganism concentration after microbial treatment.

Another useful parameter is the fractional kill after time t , which is defined as $1-N_t/N_0$, wherein:

- N_0 is the original active microorganism concentration; and
- N_t is the active microorganism concentration after time t .

5 The method according to the second aspect of the invention is advantageous in that it provides almost instantaneous UVC radiation time compared to methods that employ conventional mercury lamps which typically require a warm up time of up to 15 minutes.

Preferably, the method is a method for the antimicrobial treatment of air, wherein the microbes are selected from fungal spores, bacterial spores, mycobacteria, vegetative
10 bacteria and viruses. More preferably, the method is a method for the antimicrobial treatment of air, wherein the microbes are selected from bacterial spores, mycobacteria, vegetative bacteria and viruses. Even more preferably, the method is a method for the antimicrobial treatment of air, wherein the microbes are selected from mycobacteria, vegetative bacteria and viruses. Yet more preferably, the method is a method for the
15 antimicrobial treatment of air, wherein the microbes are selected vegetative bacteria and viruses. Most preferably, the method is a method for the antiviral treatment of air.

Preferably, the method is one wherein the air is moved through the centrifugal fan unit (20) at a rate of from [values] m^3/s .

Preferably, the method comprises the additional step of:

20 (iv) filtering the air comprising microbes using a filter unit (80) before causing the air comprising microbes to move through the centrifugal fan unit (20)

A third aspect of the invention relates to a method for the antimicrobial treatment of air comprising the steps of:

- 25 i. providing air comprising microbes to an antimicrobial air ventilation unit according to any of the embodiments above;
- ii. causing the air comprising microbes to move through the centrifugal fan unit;
- iii. irradiating the moving air comprising microbes with UVC light within the ducted fan housing of the antimicrobial air ventilation unit.

A fourth aspect of the invention relates to the use of the antimicrobial air
30 ventilation unit (10) according to any of embodiments according to the first aspect in controlling the air quality of an internal space, preferably for controlling the air quality of a room or vehicle cabin space, most preferably a room.

A fifth aspect of the invention relates to an air-conditioning unit comprising an antimicrobial air ventilation unit (10) according to any of embodiments according to the first aspect.

5 A sixth aspect of the invention relates to a mattress comprising an antimicrobial air ventilation unit (10) according to any of embodiments according to the first aspect.

A seventh aspect of the invention relates to an elevator comprising an antimicrobial air ventilation unit (10) according to any of embodiments according to the first aspect.

Definitions

10 In the context of the current invention, the following definitions are used:

UVC: ultraviolet C, light with a wavelength of 100-280 nm. This usage is in accordance with ISO standard ISO-21348:2007.

LED: A light-emitting diode (LED) is a semiconductor light source that emits light when current flows through it.

15 Irradiance flux density is the radiant flux (power) received by a surface per unit area. The SI unit of irradiance is the watt per square meter ($\text{W}\cdot\text{m}^{-2}$). A point source of light produces spherical wave-fronts, in which case irradiance flux density varies inversely with the square of the distance from the source.

20 The directivity angle indicates the range the light emitted from a LED radiates, expressed in degrees. Directivity is determined by viewing the change in light output when rotating the package, measuring from the output peak value up to what angle the light is still visible. Numerically, since directivity is normally symmetrical and covers the left and right sides when viewed from the front, it is indicated by twice the angle (\pm) at which the light output is half the maximum output, denoted $2\theta_{1/2}$.

25 LED front tip: the LED front tip is the center point of the LED light emitting surface on the outer surface of the emitter.

LED optical axis. This is the axis through the LED emitter front tip in the direction of the centroid of the optical radiation pattern.

30 LED peak intensity axis. This is the axis through the LED emitter front tip in the direction of the maximum intensity.

LED mechanical axis. This is the axis through the LED emitter front tip in the direction of the axis of symmetry of the emitter body for lamb-type LEDs. For chip-type LEDs the mechanical axis corresponds to the axis about which the lens element (i) has the

highest rotational symmetry, and (ii) if two or more axes possess the same rotational symmetry, then the axis with the highest mirror symmetry is selected.

Peak wavelength (λ_P) is defined as the single wavelength where the radiometric emission spectrum of the light source reaches its maximum.

5 Normally incident to a surface is at 90° with respect to the surface.

An optical axis is a line along which there is some degree of rotational symmetry in an optical system.

UV susceptibility is the extent to which a microorganism is sensitive to UVC light or how easily it can be inactivated by UV irradiation. UV susceptibility depends on the species and character of the microorganism. It can be described by a UV susceptibility constant (k) with the unit of m^2/J .

UV dose (D) is the product of UV irradiance and specific exposure time on a given microorganism (expressed in millijoules per square centimetre, mJ/cm^2). The longer the time a microbe is exposed to UV light, the higher the UV dose it will receive. In a device with evenly distributed UV irradiation and airflow, the UV dose can be calculated based on the definition above.

Average UV dose (AD). In the current invention, the average UV dose is determined by the inactivation rate and a known microbial susceptibility.

Inactivation rate: reduction in active microorganism concentration is expressed as N_0/N (%) or $\log(N_0/N)$,

in which:

- N_0 is the original active microorganism concentration, and
- N is the active microorganism concentration after antimicrobial treatment.

UV dose-response curve is quantified relationship between the inactivation rate of a specific microorganism and the average UV dose (AD) it received

The relationship typically follows the equation as below:

$$(1) \ln(N_0/N) = k AD$$

in which AD, k and $\ln(N_0/N)$ are as described above. In Formula (1), N/N_0 or AD can be calculated with the other parameters known. In other cases, the relationship may not strictly follow Formula (1), but N/N_0 or AD can also be determined according to the specific curve.

ISO 15714:2019(en) "Method of evaluating the UV dose to airborne microorganisms transiting in-duct ultraviolet germicidal irradiation devices" provides the method by which this inactivation rate may be determined from the UV dose-response curve.

5

Description of the embodiments

Figure 1 depicts a perspective view of a first embodiment of an antimicrobial air ventilation unit (10) according to the invention. In the embodiment depicted here, the antimicrobial air ventilation unit (10) is suitable for treating air with UVC light. The antimicrobial air ventilation unit (10) comprises a centrifugal fan unit (20), which itself comprises an impeller (21) and a ducted fan housing (22). In the embodiment depicted in Figure 1, the antimicrobial air ventilation unit (10) comprises at least one UVC radiation unit (31), which is configured to reside within the antimicrobial air ventilation unit (10) and thus not depicted. The UVC radiation unit(s) (31) comprise at least one UVC-LED (32). The UVC radiation unit(s) may optionally additionally comprise at least one UVC directing lens. Such a UVC directing lens may optionally be used to obtain a source of UVC light with a narrower directivity angle $2\theta_{1/2}$ than from a commercially available UVC-LED. This optional UVC directing lens can be advantageous used in producing a higher flux of UVC light across a flow of air comprising microbes, with a resultant higher energy efficiency for antimicrobially treating air with the antimicrobial air ventilation unit (10). The UVC radiation units (31) are configured to allow irradiation of air passing through the antimicrobial air unit (10). The at least one UVC radiation unit (31) is configured to illuminate at least a part of the interior of the ducted fan housing with UVC light.

Figure 1 additionally depicts optional features of the present invention. The depicted embodiment may optionally feature a light occluding baffle assembly (50). The optional light occluding baffle assembly is configured to allow air to flow the baffle assembly and to occlude direct rays of UVC light emitted by the UVC LED unit(s) (31). The optional light occluding baffle assembly (50) therefore prevents direct emission of the UVC light generated by the UVC LED unit(s) to the exterior of the antimicrobial air ventilation unit (10). In a particularly preferred configuration, the light occluding baffle assembly (50) is configured to allow air to pass through without generating more than 40 decibels of sound, more preferably less than 30 decibels of sound, even more preferably less than 20 decibels of sound, most preferably less than 10 decibels of sound. In a particularly preferable configuration, the light occluding baffle assembly (50) comprises a series of light occluding baffle plates, where the plates are preferably substantially orthogonal to the rotational axis(axis) of the impeller(s) (26). By substantially orthogonal is means that the

axis is within 20° of normally incident. In an even more preferably configuration, the light occluding baffle assembly (50) comprises a series of light occluding baffle plates, where the plates are substantially orthogonal to the rotational axis(axis) of the impeller(s) (26), wherein by substantially orthogonal is meant that the axis is (axes are) within 10° of normally incident, yet more preferably within 5° of normally incident and most preferably are within 2° of normally incident.

Figure 1 further depicts the optional feature of an air ventilation housing (40). Figure 1 additionally depicts the optional feature of an integrated motor within a motor housing (71). The means of moving the impeller may also be externally provided to the antimicrobial air ventilation unit (10), such as by a chain drive or gear mechanism. The advantage of incorporating an optional motor within the antimicrobial air ventilation unit (10) is that no external moving means is required, making installation of a complete unit easier.

Figure 2 depicts an antimicrobial air ventilation unit (10) according to an embodiment of the present invention in a cut away view, with both the optional air ventilation housing (40) and essential ducted fan housing (22) partially cut away. By way of a non-limiting example, the centrifugal fan unit (20) comprises a tangential cross-flow centrifugal fan. By way of non-limiting example, the tangential cross-flow centrifugal fan comprises a hollow cylindrical impeller (421). For this non-limiting example, the tangential cross-flow centrifugal fan is located within the ducted fan housing (22), and the ducted fan housing (22) has been configured so as to form an obstruction (22b) near the outer diameter of the impeller (21), which impedes rotation of gas (e.g., air) around the outside of the impeller (21, 421). The obstruction (22b) proximal to the hollow cylindrical impeller (421) is typically called a "vortex tongue". For tangential cross-flow centrifugal fans, the ducted fan housing (22) needs to be axially asymmetric (not-axially symmetric) with respect to the axis of rotation of the impeller.

In this non-limiting example, the hollow cylindrical impeller (421) features two solid end walls (27) delimited radially in the impeller hubs (23), with the impeller fan blades (24) attached to the solid end walls (27) proximal to the impeller hubs (23). In this example, the hollow cylindrical impeller (421) further features two optional impeller fan blade support disks (28), which are attached to the impeller fan blades (24), and each impeller fan blade support disk (28) comprises an impeller fan blade support disk wall (29). The optional feature of impeller fan blade support disks is conferring additional structural rigidity and hence may beneficially extend operational lifetime. By way of non-limiting example, the blades are arranged with rotational symmetry around the rotational axis of the impeller. The skilled person will readily appreciate that minor deviation from rotational symmetry,

such as by omitting a blade or minor structural modification of a blade, will not diminish the efficacy of the impeller. In this particular example, the blades of the impeller (24) are configured to occlude direct rays of UVC light emitted by the UVC LED unit(s) (31) passing through the impeller (21). This feature of the blades being configured in a light occluding configuration is not limiting, and the skilled person can readily envisage alternative configurations. One advantage of a light occluding configuration of the impeller blades (24) is that UVC light is not emitted from the antimicrobial air ventilation unit (10) through the impeller (21), obviating any need for a further light occluding baffle assembly. The embodiment is depicted with the optional feature of a light occluding baffle assembly (50). By way of non-limiting example. The light occluding baffle assembly (50) may consist of parallel plates (51), which are configured substantially orthogonal to the axis of rotation of the impeller. Figure 2 additionally depicts the optional features of an integrated motor within a motor housing (71) and an air ventilation housing (40).

Figure 2 depicts a UVC radiation unit (31) comprising a UVC-LED (32). By way of non-limiting example, it is attached to an interior wall of the antimicrobial air ventilation unit (10) and is configured to emit UVC radiation substantially parallel to the rotational axis of the impeller (21). In this non-limiting example, the UVC radiation unit (31) is configured to illuminate a space defined by the (i) the ducted fan housing (22) and (ii) between the impeller (21) and (iii) the light occluding baffle assembly (50) as described above, in particular in the space "down-wind" from the impeller when the antimicrobial air ventilation unit (10) is in use. This confers the advantage that most UVC light generated cannot directly exit the antimicrobial air ventilation unit (10), obviating the need for any further light occluding winds/turns in the ducted fan housing. This beneficially results in a more compact antimicrobial air ventilation unit (10), which operates with less noise pollution from air turbulence. The skilled person will readily appreciate that the UVC radiation unit (31) may be configured to illuminate a space defined by the (i) the ducted fan housing (22) and (ii) between the impeller (21) and (iii) the light occluding baffle assembly (50) as described above, either "up-wind" or "down-wind" from the impeller when the antimicrobial air ventilation unit (10) is in use, with substantially the same result.

Figure 3 depicts a vertical cross-section view of the first embodiment of an antimicrobial air ventilation unit according to the invention. In this non-limiting example, a cross section of the hollow cylindrical impeller (421) depicts the impeller fan blades (24) as curved fan blades arranged in a rotationally symmetric manner around the rotational axis of the impeller (26). The hollow space (25) defined by the by end walls (not depicted, 27) and the impeller fan blades (24) is rotationally symmetric around the rotational axis of the

impeller (26). By way of non-limiting example, the UVC radiation unit (31) in this example comprises both (i) an essential UVC LED (32) and (ii) an optional UVC directing lens (34).

When in use, the air comprising microbes enters the antimicrobial air ventilation unit (10) from below (vertical arrow, 90). The air is moved through the unit (10) by rotation of the impeller (21, 421) around its axis of rotation (26). The impeller (21), in conjunction with the "vortex junction" constituted by the obstruction (22b) causes a substantially laminar flow of air through/past the impeller substantially orthogonal to the rotational axis of the impeller. This is advantageously quiet compared to rotary fan units known in the art for moving air in ventilation systems. As the air exits the impeller, a substantial fraction of the laminar air flow passes through a volume illuminated by UVC radiation emitted by the UVC radiation unit (31). For each photon of UVC light that impinges on a microbe within the moving laminar air column, there is a probability that the UVC will to the microbe so as to inhibit the microbe from reproducing. The antimicrobial treated laminar air column then exits the unit (10), as depicted by the horizontal arrow (90). Optionally, the air may pass through a light obstructing baffle assembly (i) prior to passing through/past the impeller (21) and/or (ii) after passing through/past the impeller (21).

Figure 4 is a top-down, horizontal cross-sectional view of a non-limiting example of the first embodiment of an antimicrobial air ventilation unit (10) according to the invention. In this example, two UVC radiation units (31), each comprising a UVC LED (32) and a UVC directing lens (34), are located on opposite faces of the ducted fan housing (22). By way of non-limiting example, the optical axes of both UVC radiation units are substantially parallel to the rotational axis of the impeller (not depicted, 26). The two UVC radiation units (31) are configured to allow illumination of substantially all of the air passed through the unit (10) during use, allowing more rapid antimicrobial treatment of an enclosed space ventilated by the unit (10), such as an elevator or hospital room. One possible configuration of a light occluding baffle assembly (50) is depicted, comprising a set of substantially parallel plates (51), which are configured substantially orthogonal to the rotational axis of the impeller (21). When in use, the air comprising microbes exits the impeller (21) and substantially all of the laminar air flow passes through a volume illuminated by UVC radiation emitted by the two UVC radiation units (not labelled here, 31). For each photon of UVC light that impinges on a microbe within the moving laminar air column, there is a probability that the UVC will to the microbe so as to inhibit the microbe from reproducing. The antimicrobial treated laminar air column then exits the unit (10), as depicted by the arrow (90).

Figures 5-7 depict three representative types of suitable UVC radiation units. Figure 5 depicts a UVC radiation unit (31) consisting of a typical lamb-type UVC-LED. The

unit comprises two electrically conductive wires (38) and the LED emitter body (32). The mechanical axis of the LED (33) is the axis through the LED emitter body front tip (right hand side of 32) in the direction of the axis of symmetry (in this depiction an infinite rotational axis, C^∞) of the emitter body for lamb-type LEDs. The mechanical axis of the LED (33) is depicted as coincident with the optical axis / peak intensity axis (θ_{MAX}). The peak intensity axis is the axis corresponding to the maximum light output at a given distance from the LED emitter body (32). Lamb type LEDs typically exhibit minor deviations of the peak intensity axis (θ_{MAX}) from the mechanical axis in the range of 0-15°. Figure 5 also depicts the first angle at which the light output is half the maximum output (36) (with respect to the peak intensity axis, θ_{MAX}) and the second angle at which the light output is half the maximum output (37) (with respect to the peak intensity axis, θ_{MAX}). The angle from the peak intensity axis, θ_{MAX} to depicts the first angle at which the light output is half the maximum output (36) (with respect to the peak intensity axis, θ_{MAX}) defines θ . Numerically, since directivity is normally symmetrical and covers the left and right sides when viewed from the front, it is indicated by twice the angle (\pm) at which the light output is half the maximum output, denoted $2\theta_{1/2}$.

Figure 6 depicts a UVC radiation unit (31) consisting of a chip-type LED. The chip-type LED typically comprises an LED emitter body (32) attached to a circuit board. In this instance, the LED emitter body (32) is housed in a housing (35). Attached to the housing (35) is a lens (34). The lens (34) may be suitably selected from glass or plastic resistant to UVC-radiation degradation. The mechanical axis of the LED (33) is the axis about which the lens element (34) has the highest rotational symmetry (in this depiction an infinite rotational axis, C^∞). The mechanical axis of the LED (33) is depicted as coincident with the optical axis / peak intensity axis (θ_{MAX}). The peak intensity axis is the axis corresponding to the maximum light output at a given distance from the LED emitter body (32). Figure 6 also depicts the first angle at which the light output is half the maximum output (36) (with respect to the peak intensity axis, θ_{MAX}) and the second angle at which the light output is half the maximum output (with respect to the peak intensity axis, θ_{MAX}). The angle from the peak intensity axis, θ_{MAX} too the first angle at which the light output is half the maximum output (36) (with respect to the peak intensity axis, θ_{MAX}) defines θ . Numerically, since directivity is normally symmetrical and covers the left and right sides when viewed from the front, it is indicated by twice the angle (\pm) at which the light output is half the maximum output, denoted $2\theta_{1/2}$. The UVC radiation unit (31) is configured such that, when in use, UVC radiation is emitted by the light emitter body (32), which is then focused by the lens (34) to give a $2\theta_{1/2}$ value in the range of 0.05 to 10°.

Figure 7 depicts a UVC radiation unit (31) consisting of 9 chip-type LEDs as depicted in Figure 6. This is a non-limiting representative example of a UVC radiation unit (31) comprising a plurality of either (i) lamb-type LEDs, (ii) chip-type LEDs or (iii) a mixture of lamb-type LEDs and chip-type LEDs. The left-hand side of Figure 7 depicts a cross-section of the UVC radiation unit (31). The right-hand side depicts a front-on perspective of the UVC unit (31).

Figure 8 corresponds to Figure 4, with the optical axis of the two UVC radiation units (not labelled, 31, comprising 32 and 34) depicted as the arrow " θ_{MAX} " and the $2\theta_{1/2}$ cone for each UVC radiation unit depicted between the first angle at which the light output is half the maximum output (36) (with respect to the peak intensity axis, θ_{MAX}) and the second angle at which the light output is half the maximum output (37) (with respect to the peak intensity axis, θ_{MAX}).

Figure 9 corresponds to Figure 4, with the dotted lines depicting direct emission paths of UVC photons from the UVC radiation units (31) being absorbed by the plates (51) of the light occluding baffle assembly (50).

Figure 10 is a cartoon of use of an antimicrobial air ventilation unit (10) according to the first embodiment of the present invention to antimicrobially treat air. Air comprising microbes, depicted in cartoon form as rings, enters a part of the unit (10) with a UVC radiation unit (31) attached to the ducted fan housing (22). The direction of the air flow is from bottom to top, as denoted by arrow (90). As the air comprising microbes passes through the volume illuminated by UVC radiation emitted by the UVC radiation unit (31), photons of UVC light impinge at least some of the microbes present in the air column. For each photon of UVC light that impinges on a microbe within the moving laminar air column, there is a probability that the UVC will to the microbe so as to inhibit the microbe from reproducing. Destruction of the microbe is depicted by the cartoon "lightning strike". The antimicrobially treated laminar air column then exits the unit (10), as depicted by the horizontal arrow (90), which comprises a lower concentration of microbes.

Figure 11 broadly corresponds to Figure 10, but ducted fan housing (22) comprises a portion of mirrored interior surface of the ducted fan housing (22M), which is located such that at least some UVC light from at least one UVC radiation unit (31) may be incident with the mirrored interior surface of the ducted fan housing (22M) during use. By way of non-limiting example. By way of non-limiting example, the mirrored interior surface of the ducted fan housing (22M) may be configured to be substantially orthogonal to the optical axis of at least one UVC radiation unit (31). Such a configuration allows a substantial portion of the incident UVC photons to be reflected, increasing their path length and increasing the probability that any one UVC photon will impinge on a microbe. This

increases the probably that any one microbe will be stuck by a UVC photon and thereby inhibited from reproducing. An additional benefit of such a configuration is that substantially all air passing though such a unit (10) may be antimicrobial treated using only one UVC radiation unit.

5 Figure 12 depicts in cartoon fashion antimicrobial treating air using a unit as depicted in Figures 4, 8 and 9.

 Figure 13 depicts in cartoon fashion antimicrobial treating air using a particularly preferred embodiment unit broadly corresponding to that depicted in Figures 4, 8 and 9, wherein the ducted fan housing (22) is mirrored. Such a configuration allows a substantial
10 portion of the UVC photons incident on the ducted fan housing (22) to be reflected, increasing their path length and increasing the probability that any one UVC photon will impinge on a microbe. This increases the probably that any one microbe will be stuck by a UVC photon and thereby inhibited from reproducing.

 Figure 14 depicts in cartoon fashion antimicrobial treating air using a particularly
15 preferred embodiment unit broadly corresponding to that depicted in Figure 2 combined with Figure 12. Such a configuration allows a substantial portion of the UVC photons incident on the ducted fan housing (22) to be reflected, increasing their path length and increasing the probability that any one UVC photon will impinge on a microbe. This
20 increases the probably that any one microbe will be stuck by a UVC photon and thereby inhibited from reproducing. This particularly favored embodiment confers the advantage that most UVC light generated cannot directly exit the antimicrobial air ventilation unit (10), obviating the need for any further light occluding winds/turns in the ducted fan housing. This beneficially results in a more compact antimicrobial air ventilation unit (10), which operates with less noise pollution from air turbulence and maximal energy efficiency.

25 Figure 15 depicts in cartoon fashion antimicrobial treating air comprising microbes (depicted as rings) and dust particles (pentagons) in an embodiment according to Figure 1. UVC photons impinging dust particles may be absorbed, lowering the probability that any one UVC photon will impinge with a microbe. This reduces the probably that any one
30 microbe will be stuck by a UVC photon and thereby inhibited from reproducing. The more dust is present, the less energy efficient the antimicrobial treatment is.

 Figure 16 depicts a particularly preferably embodiment of the present invention, in which the unit (10) additionally comprises a filter unit (80). Preferably, the filter unit is a high-efficiency particulate air (HEPA) filter (80a). The figure depicts, in cartoon form, the
35 effect of the filter (80) in removing dust particles (pentagons) from the air to be microbially treated, thereby increasing the probability that any one UVC photon will impinge a microbe and damage it sufficiently to inhibit its reproduction. Thereby, the probability that any one

microbe is inhibited from reproduction is increased and the efficiency of the apparatus for antimicrobial treating air thereby increased.

Throughout the description and claims of this specification, the words “comprise” and “contain” and variations of them mean “including but not limited to”, and they are not intended to (and do not) exclude other moieties, additives, components, integers or steps. Throughout the description and claims of this specification, the singular encompasses the plural unless the context otherwise requires. In particular, where the indefinite article is used, the specification is to be understood as contemplating plurality as well as singularity, unless the context requires otherwise.

Features, integers, characteristics, compounds, chemical moieties or groups described in conjunction with a particular aspect, embodiment or example of the invention are to be understood to be applicable to any other aspect, embodiment or example described herein unless incompatible therewith. All of the features disclosed in this specification (including any accompanying claims, abstract and drawings), and/or all of the steps of any method or process so disclosed, may be combined in any combination, except combinations where at least some of such features and/or steps are mutually exclusive. The invention is not restricted to the details of any foregoing embodiments. The invention extends to any novel one, or any novel combination, of the features disclosed in this specification (including any accompanying claims, abstract and drawings), or to any novel one, or any novel combination, of the steps of any method or process so disclosed.

The reader's attention is directed to all papers and documents which are filed concurrently with or previous to this specification in connection with this application and which are open to public inspection with this specification, and the contents of all such papers and documents are incorporated herein by reference.

List of reference numerals

Similar reference numbers used in the description to indicate similar elements (but only differences in hundreds) are implicitly included.

- 10 Antimicrobial air ventilation unit.
- 30 20 Centrifugal fan unit.
- 20a First (inlet) side of the at least one centrifugal fan unit (20).
- 20b Second (outlet) side of the at least one centrifugal fan unit (20).
- 21 Impeller.
- 21L Length of impeller.

- 21D Diameter of impeller.
- 22 Ducted fan housing.
- 22a Non-axially symmetric ducted fan housing, with respect to the axis of rotation of impeller (26).
- 5 22b Deformation of the ducted fan housing (22a).
- 22H Height of the ducted fan housing (22).
- 22K Enfilading microbial kill-zone of the ducted fan housing (22).
- 22KR Enfilading microbial kill-zone (reflected) of the ducted fan housing (22).
- 22L Length of the ducted fan housing (22).
- 10 22M Mirrored interior surface of the ducted fan housing (22).
- 22W Width of the ducted fan housing (22).
- 23 Impeller hubs.
- 24 Impeller fan blades.
- 24a Forward-curved/inclined impeller fan blades.
- 15 24b Backward-curved/backward inclined impeller fan blades.
- 24c Straight radial impeller fan blades.
- 25 Hollow space.
- 26 Axis of rotation of impeller (21, 121, 221, 321).
- 27 Solid end walls.
- 20 28 Impeller fan blade support disks.
- 29 Impeller fan blade support disk walls.
- 31 UVC radiation unit.
- 32 UVC-LED(s).
- 33 Mechanical axis of the LED(s).
- 25 34 UVC directing lens.
- 35 LED housing.
- 36 First angle at which the light output is half the maximum output.
- 37 Second angle at which the light output is half the maximum output.
- 40 Air ventilation housing.

- 50 Light occluding baffle assembly.
- 51 Light occluding baffle assembly slits.
- 52 Light occluding baffle assembly plates.
- 80 Filter unit.
- 5 80a High-efficiency particulate air (HEPA) filter.
- 90 Direction of air flow.
- 120 cross-flow centrifugal fan unit
- 120a first (inlet) side of the cross-flow centrifugal fan unit (120).
- 120b second (outlet) side of the cross-flow centrifugal fan unit (120).
- 10 121 axially symmetric rotor impeller.
- 220 tangential centrifugal fan unit.
- 220a first (inlet) side of the tangential centrifugal fan unit (200).
- 220b second (outlet) side of the tangential centrifugal fan unit (200).
- 221 cylindrical impeller.
- 15 321 fan wheel impeller.
- 421 hollow cylindrical impeller.

Conclusies

1. Antimicrobiële luchtventilatie-eenheid (10) voor het behandelen van lucht met UVC-licht, omvattende:
 - ten minste één centrifugale ventilatoreenheid (20) die een waaier (21) en een gekanaliseerde ventilatorbehuizing (22) omvat; en
 - ten minste één UVC-stralingseenheid (31) die (i) ten minste één UVC-led (32) en optioneel (ii) ten minste één UVC-richtende lens (34) omvat,
 - waarbij de UVC-stralingseenheid of -eenheden (31) geconfigureerd is of zijn om een bestraling mogelijk te maken van lucht die door de antimicrobiële luchtventilatie-eenheid (10) stroomt,waarbij de ten minste ene UVC-stralingseenheid (31) geconfigureerd is om ten minste een deel van het inwendige van de gekanaliseerde ventilatorbehuizing (22) te belichten met UVC-licht.
2. Antimicrobiële luchtventilatie-eenheid (10) volgens conclusie 1, waarbij de ten minste ene centrifugale ventilatoreenheid (20) is geselecteerd uit een dwarsstromende centrifugale ventilatoreenheid (120) of een tangentiële centrifugale ventilatoreenheid (220), waarbij bij voorkeur de ten minste ene centrifugale ventilatoreenheid (20) een tangentiële centrifugale ventilatoreenheid (220) is.
3. Antimicrobiële luchtventilatie-eenheid (10) volgens conclusie 1 of 2, waarbij de waaier (21) een axiaal symmetrische rotorwaaier (12), een cilindrische waaier (221), een ventilatorwielwaaier (321), en/of een holle cilindrische waaier (421) is.
4. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de waaier (21) een ventilatorwielwaaier (321) is, bij voorkeur waarbij de ventilatorwielwaaier (321) waaierventilatorbladen (24) omvat die geselecteerd zijn uit voorwaarts gekromde/hellende waaierventilatorbladen (24a), achterwaarts gekromde/hellende waaierventilatorbladen (24b), of rechte radiale waaierventilatorbladen (24c), beter waarbij de ventilatorwielwaaier (321) voorwaarts gekromde/hellende waaierventilatorbladen (24a) omvat, en bij voorkeur waarbij de ventilatorwielwaaier (321) voorwaarts gekromde waaierventilatorbladen omvat.
5. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de waaier (21) een holle cilindrische waaier (421) is, bij voorkeur waarbij de holle cilindrische waaier (421) waaierventilatorbladen (24) omvat die geselecteerd zijn uit voorwaarts gekromde/hellende waaierventilatorbladen (24a), achterwaarts gekromde/hellende waaierventilatorbladen (24b), of rechter radiale waaierventilatorbladen (24c), beter waarbij de holle cilindrische waaier (421) voorwaarts gekromde/hellende waaierventilatorbladen (24a) omvat, bij voorkeur waarbij de holle cilindrische waaier (421) voorwaarts gekromde waaierventilatorbladen (24a) omvat.
6. Antimicrobiële luchtventilatie-eenheid (10) volgens conclusie 5, waarbij de ten minste ene centrifugale ventilatie-eenheid (20) een tangentiële centrifugale ventilatie-eenheid (220) is, waarbij de waaier (21) een holle cilindrische waaier (421) is, en waarbij de einden van de holle cilindrische waaier (421) afgedopt zijn met vaste eindwanden (27).
7. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de UVC-stralingseenheden (31) in staat zijn om licht te produceren met één of meerdere golf lengtes die gelegen zijn

in het bereik van 100 nm tot en met 280 nm, die beter gelegen zijn in het bereik van 225 nm tot en met 280 nm, die nog beter in het bereik gelegen zijn van 255 nm tot en met 270 nm, en bij voorkeur met een golflengte van 265 ($\pm 0,5$) nm.

- 5 8. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de UVC-leds (32) in staat zijn om licht te produceren met een golflengte van 100-280 nm, beter met een golflengte die gelegen is het bereik van 225 nm tot en met 280 nm, nog beter met een golflengte die gelegen is in het bereik van 255 nm tot en met 270 nm, en bij voorkeur met een golflengte van 265 ($\pm 0,5$) nm.
- 10 9. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de UVC-led(s) (32) licht uitzendt of uitzenden met een piekgolflengte (λ_p) van 250-280 nm, waarbij de UVC-led(s) (32) beter licht uitzendt of uitzenden met een piekgolflengte (λ_p) van 225-270 nm, en waarbij bij voorkeur de UVC-led(s) (32) licht uitzenden met een piekgolflengte (λ_p) van 265 ($\pm 0,5$) nm.
- 15 10. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de UVC-led(s) (32) in het bezit is of zijn van een stralingsfluxdichtheid van 0,5 mW/cm² tot en met 50 mW/cm² op een afstand van 50 mm ten opzichte van de UVC-led, beter van een stralingsfluxdichtheid 1,0 mW/cm² tot en met 25 mW/cm², en nog beter van een stralingsfluxdichtheid 1,5 mW/cm² tot en met 15 mW/cm².
- 20 11. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de UVC-led(s) (32) in het bezit is of zijn van een richthoek $2\theta_{1/2}$ die gelegen is tussen 180° en 5°, die nog beter gelegen is tussen 160° en 10°, die nog beter gelegen is tussen 140° en 20°, en die bij voorkeur gelegen is tussen 120° en 30°.
- 25 12. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de UVC-stralingseenheid (31) geconfigureerd is om het inwendige van de gekanaliseerde ventilatorbehuizing (22) te verlichten met UVC-licht, op een zodanige wijze dat de mechanische as van de UVC-led(s) (33) ongeveer coaxiaal is met de rotatieas van de waaier (26), waarbij de term "ongeveer coaxiaal" verwijst naar het feit dat de assen binnen een hoek van 45° ten opzichte van coaxiaal gelegen zijn, beter waarbij dit betekent dat de assen binnen een hoek van 30° van coaxiaal gelegen zijn, nog beter dat het betekent dat de assen binnen een hoek van 10° van coaxiaal gelegen zijn, en bij voorkeur dat het betekent dat de assen binnen 5° een hoek van coaxiaal gelegen zijn.
- 30
- 35 13. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de antimicrobiële luchtventilatie-eenheid (10) omvat:
- ten minste één centrifugale ventilatoreenheid (20) die een waaier (21) en een gekanaliseerde ventilatorbehuizing (22) omvat; en
 - minste twee UVC-stralingseenheden (31), waarbij elke UVC-stralingseenheid ten minste één UVC-led (32) omvat;
 - waarbij de ten minste twee UVC-stralingseenheden (31) geconfigureerd zijn om het inwendige van de gekanaliseerde ventilatorbehuizing (22) te verlichten met UVC-licht, op een zodanige wijze dat de mechanische as van de UVC-led(s) (33) de gekanaliseerde ventilatorbehuizing (22) snijdt.
- 40
- 45 14. Antimicrobiële luchtventilatie-eenheid (10) volgens een der voorgaande conclusies, waarbij de antimicrobiële luchtventilatie-eenheid (10) bovendien een licht-afsluitend schotgeheel omvat.

15. Antimicrobiële luchtventilatie-eenheid (10) volgens een der conclusies 1 tot en met 12, waarbij de antimicrobiële luchtventilatie-eenheid (10) voor het behandelen van lucht met UVC-licht omvat:

- 5
- ten minste één centrifugale ventilatie-eenheid (20) die een waaier (21) en een gekanaliseerde ventilatorbehuizing (22) omvat;
 - ten minste één UVC-stralingseenheid (31) die ten minste één UVC-led (32) omvat; en
 - ten minste één gespiegeld inwendig oppervlak van de gekanaliseerde ventilatorbehuizing (22M),

10

waarbij de ten minste ene UVC-stralingseenheid (31) geconfigureerd is om het inwendige van de gekanaliseerde ventilatorbehuizing (22) te verlichten met UVC-licht, op een zodanige wijze dat de mechanische as van de UVC-led(s) (33) het gespiegelde inwendige oppervlak van de gekanaliseerde ventilatorbehuizing (22M) snijdt.

16. Werkwijze voor het antimicrobieel behandelen van lucht, de stappen omvattende met:

- 15
- i. het aanleveren van lucht die microben omvat, aan een antimicrobiële luchtventilatie-eenheid volgens een der conclusies 1 tot en met 15;
 - ii. het ervoor zorgen dat de lucht die de microben omvat, doorheen de centrifugale ventilatoreenheid wordt verplaatst;
 - iii. het bestralen van de bewegende lucht die de microben omvat, met UVC-licht in de gekanaliseerde ventilatorbehuizing van de antimicrobiële luchtventilatie-eenheid.
- 20

17. Gebruik van een apparaat volgens een der conclusies 1 tot en met 15, voor het onder controle houden van de luchtkwaliteit van een inwendige ruimte, bij voorkeur voor het onder controle houden van de luchtkwaliteit in een kamer of in een cabineruimte van een voertuig, bij voorkeur in een kamer.

25

18. Airconditioningeenheid, omvattende een apparaat volgens een der conclusies 1 tot en met 15.

19. Matras, omvattende een apparaat volgens een der conclusies 1 tot en met 15.

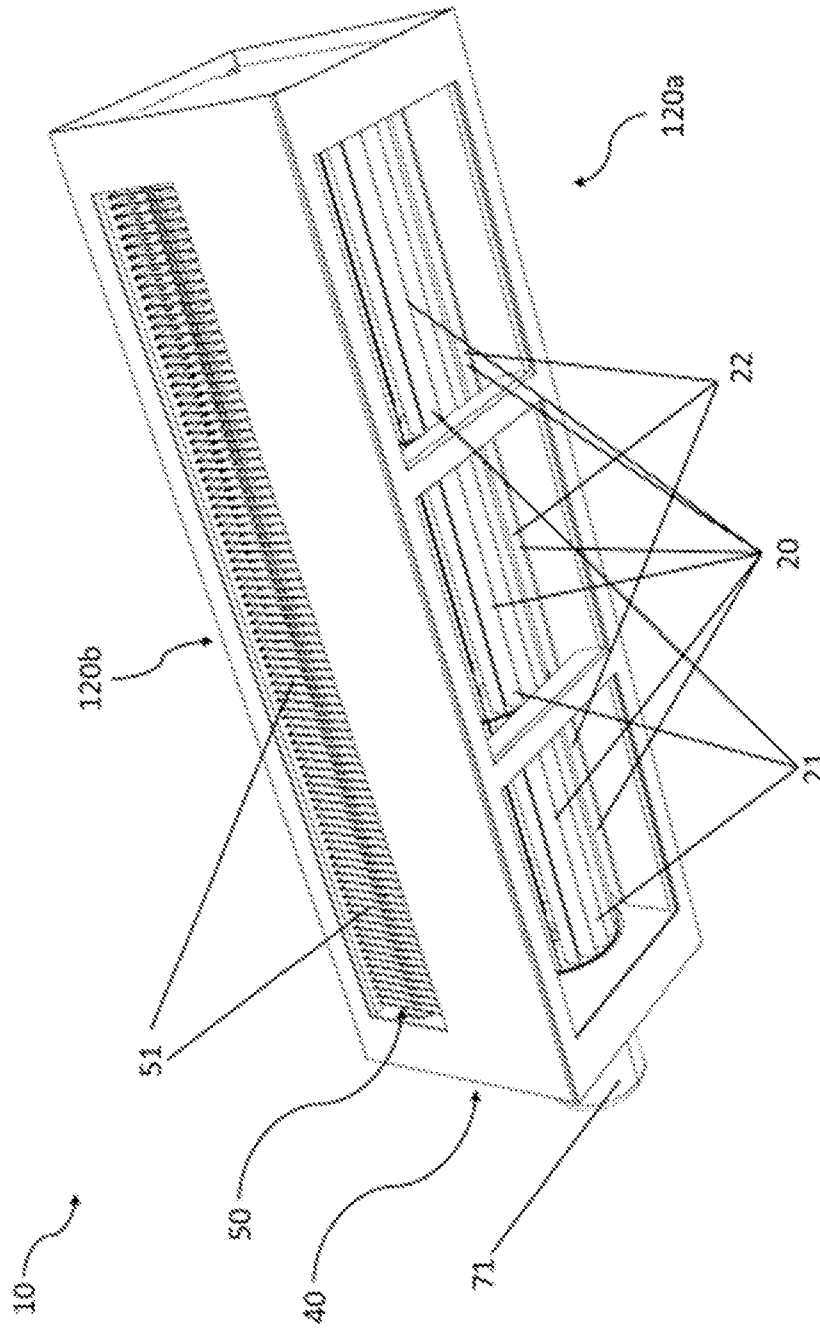


Figure 1

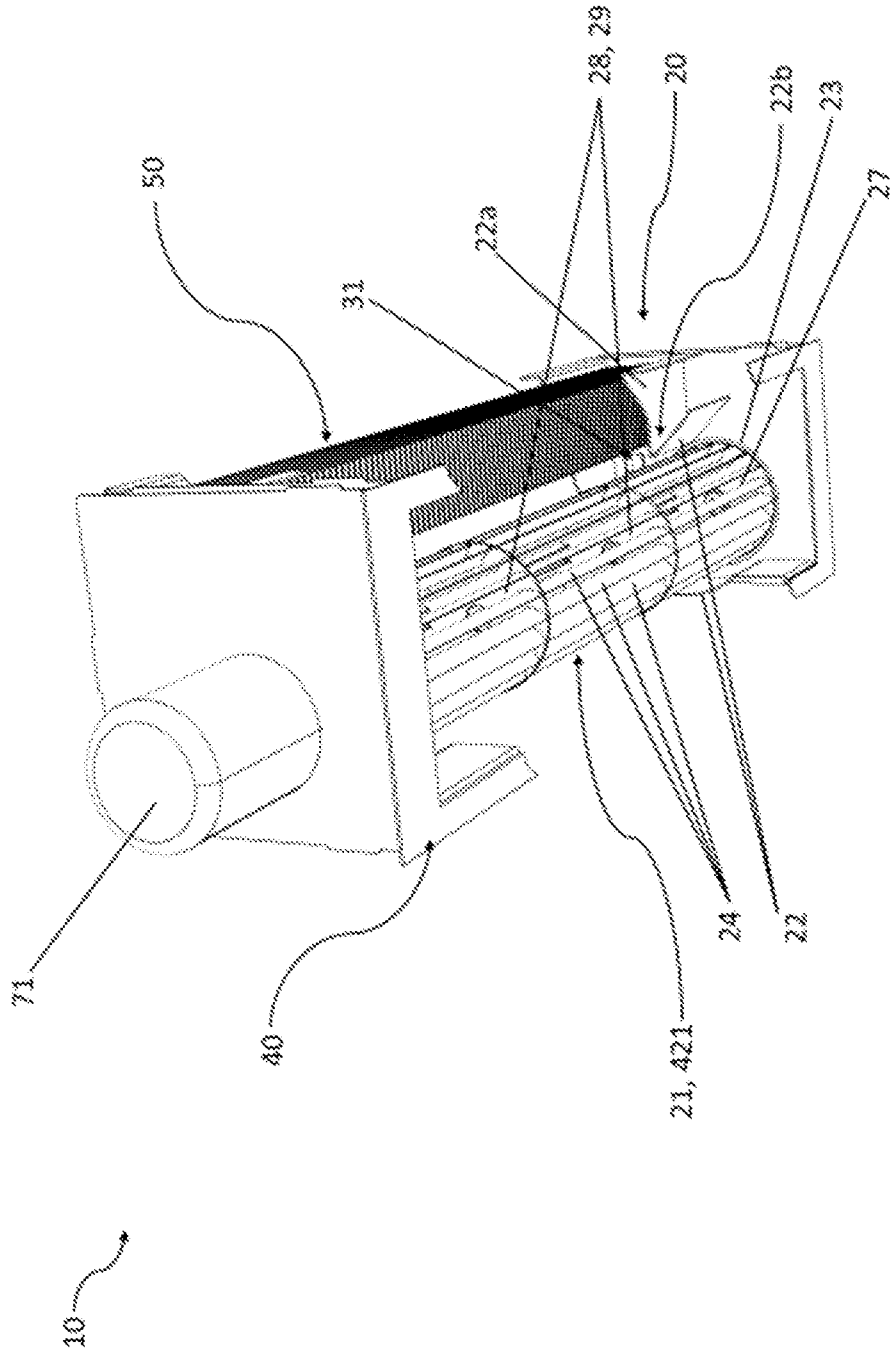


Figure 2

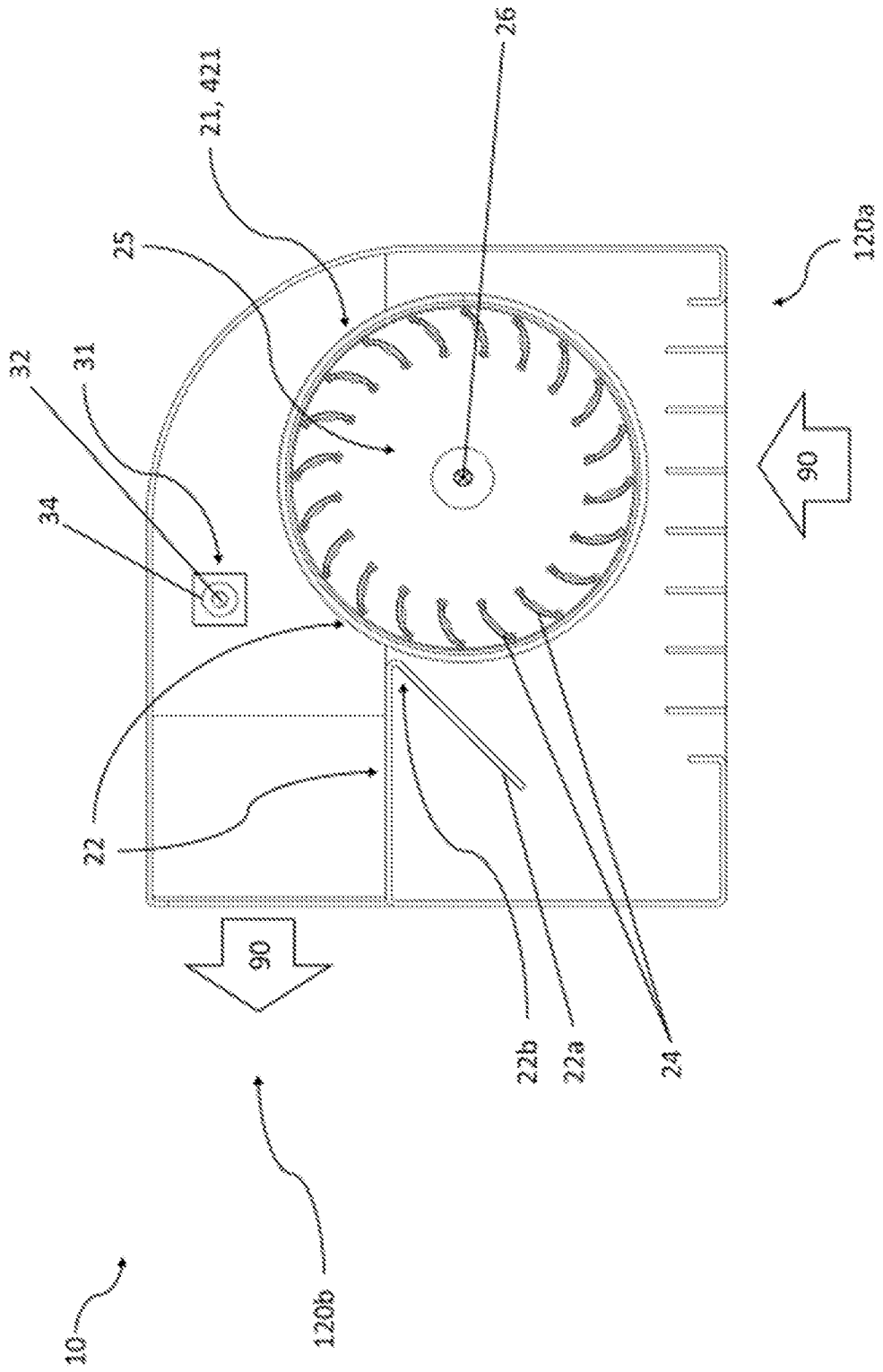


Figure 3

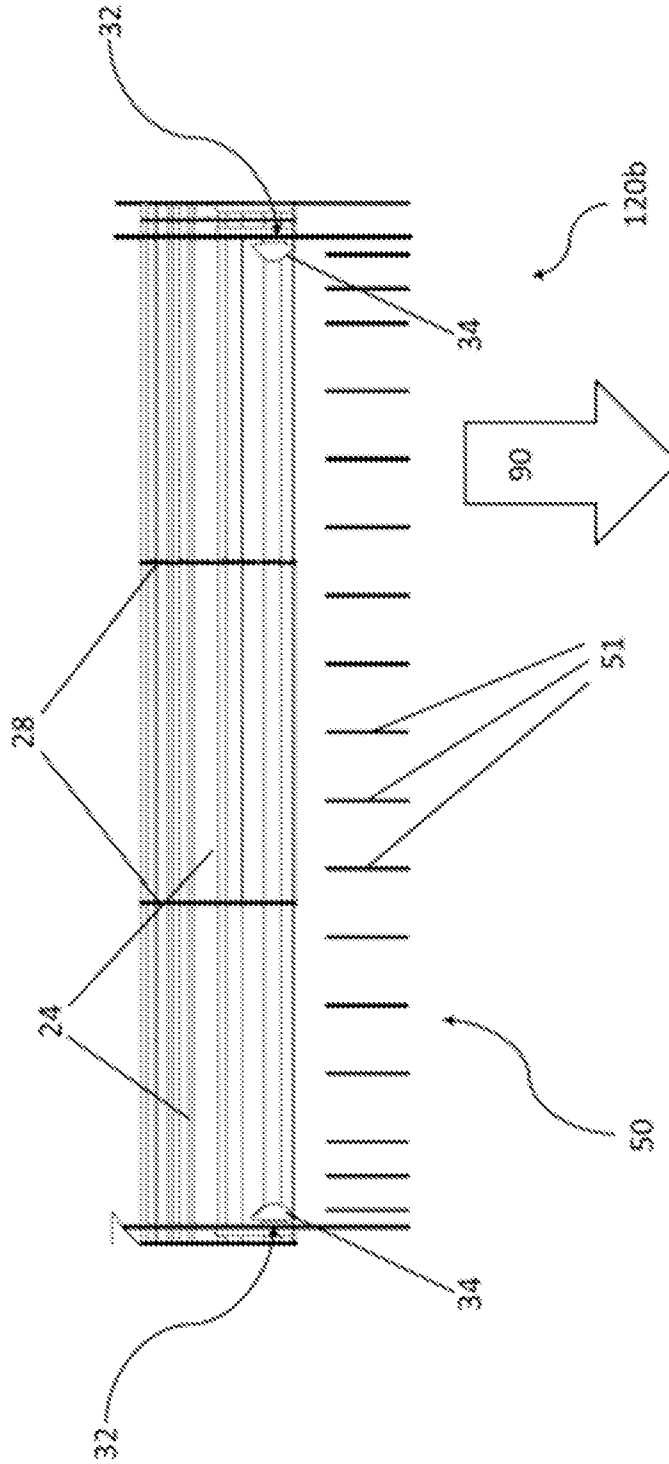


Figure 4

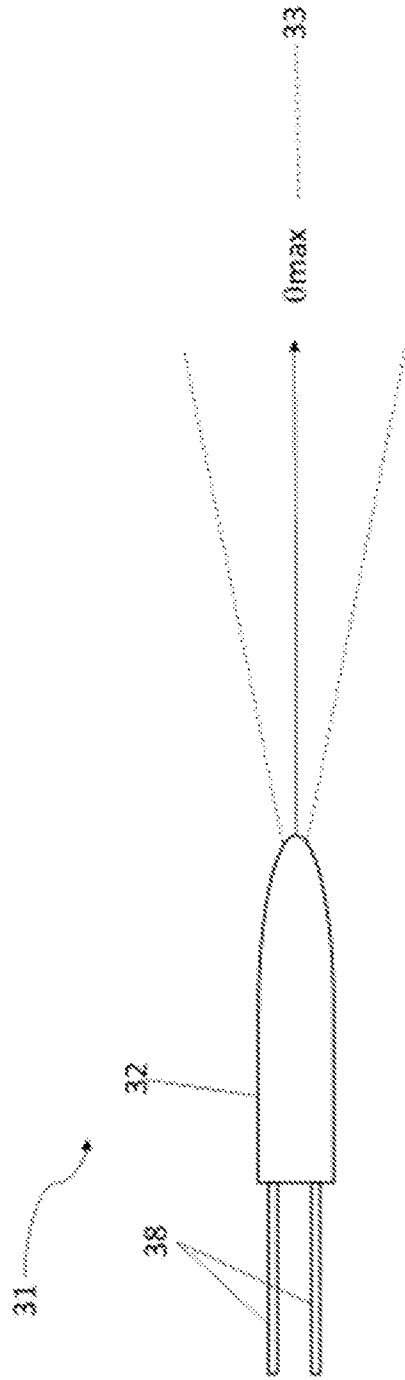


Figure 5

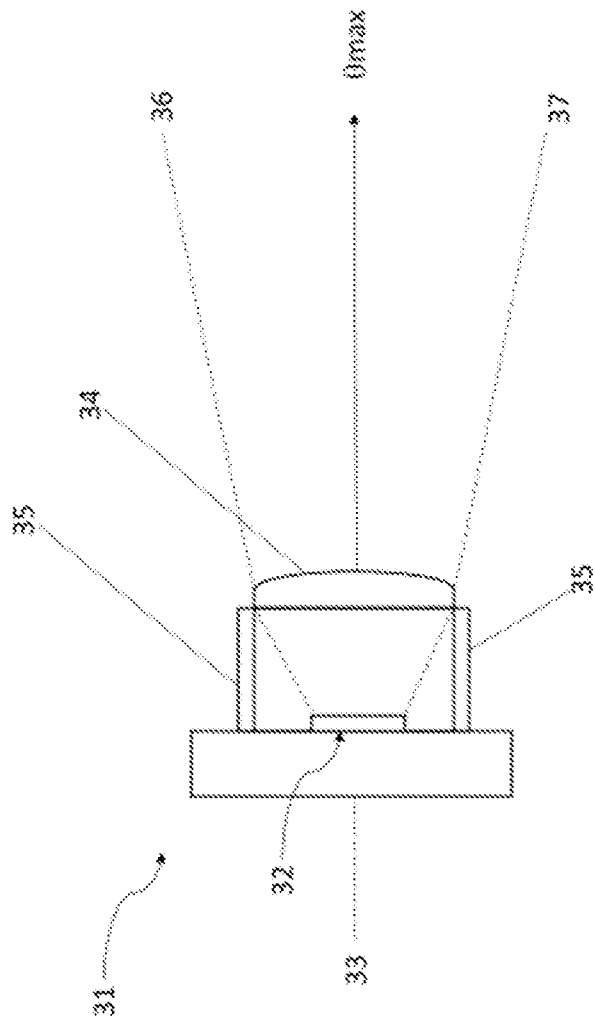


Figure 6

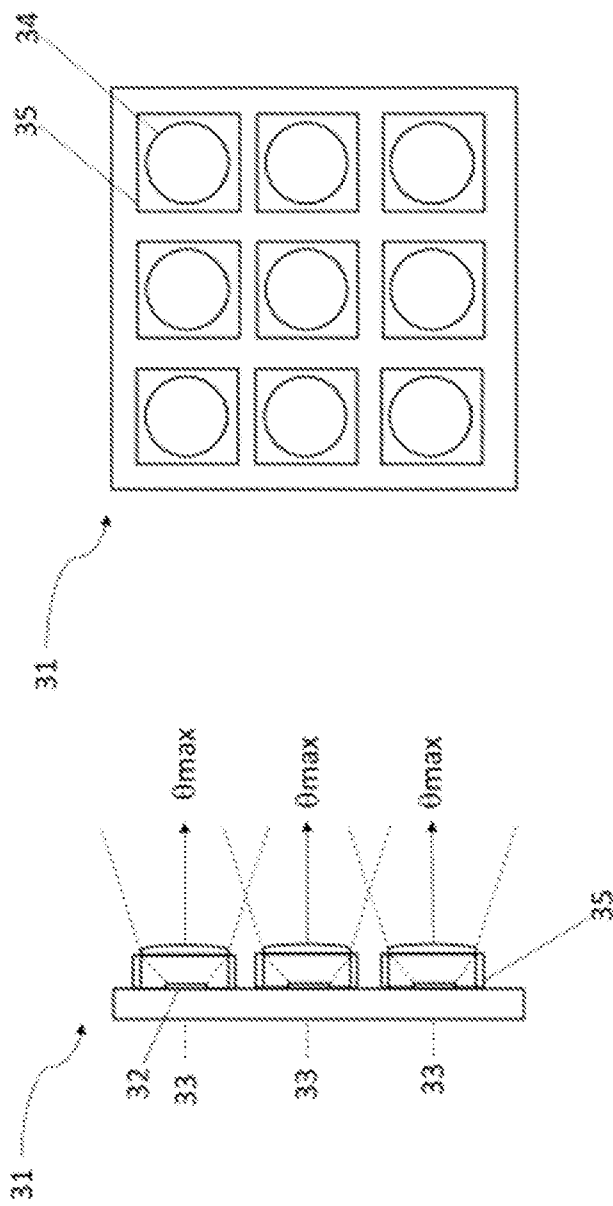


Figure 7

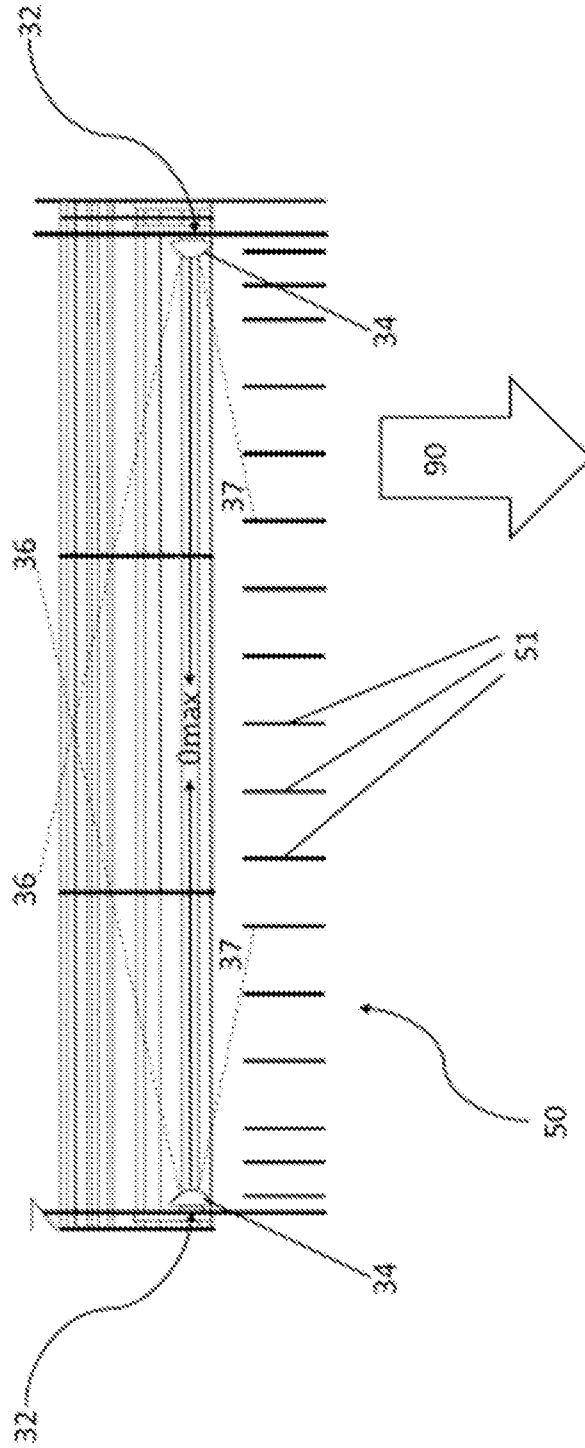


Figure 8

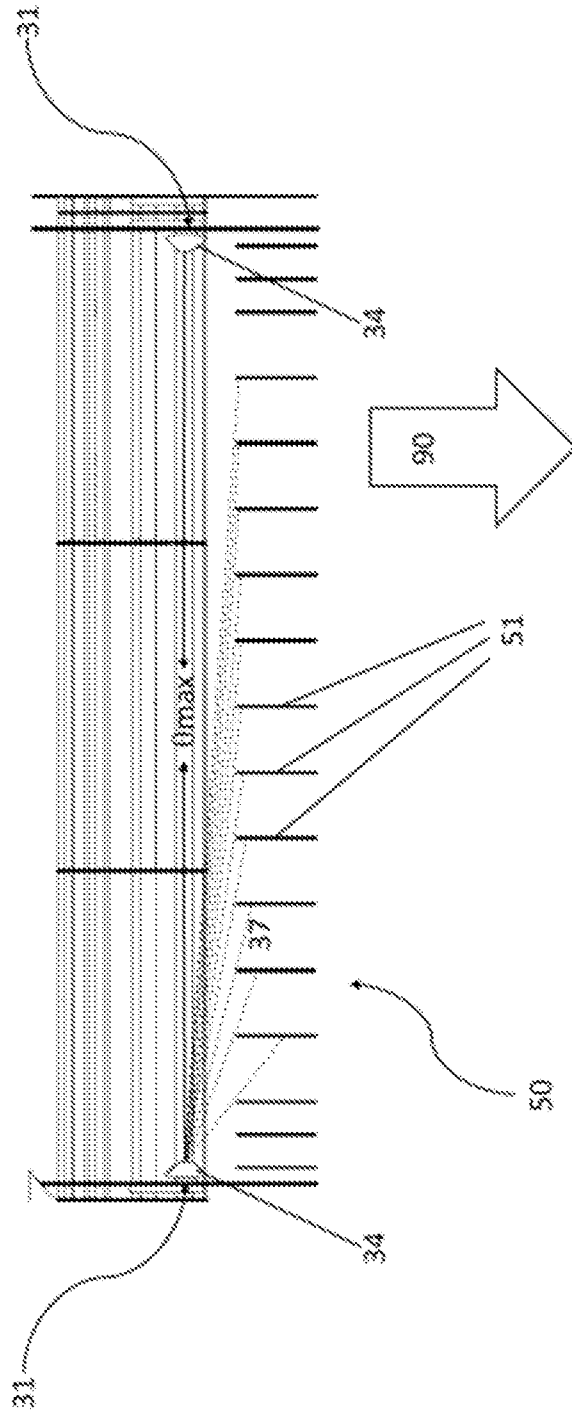


Figure 9

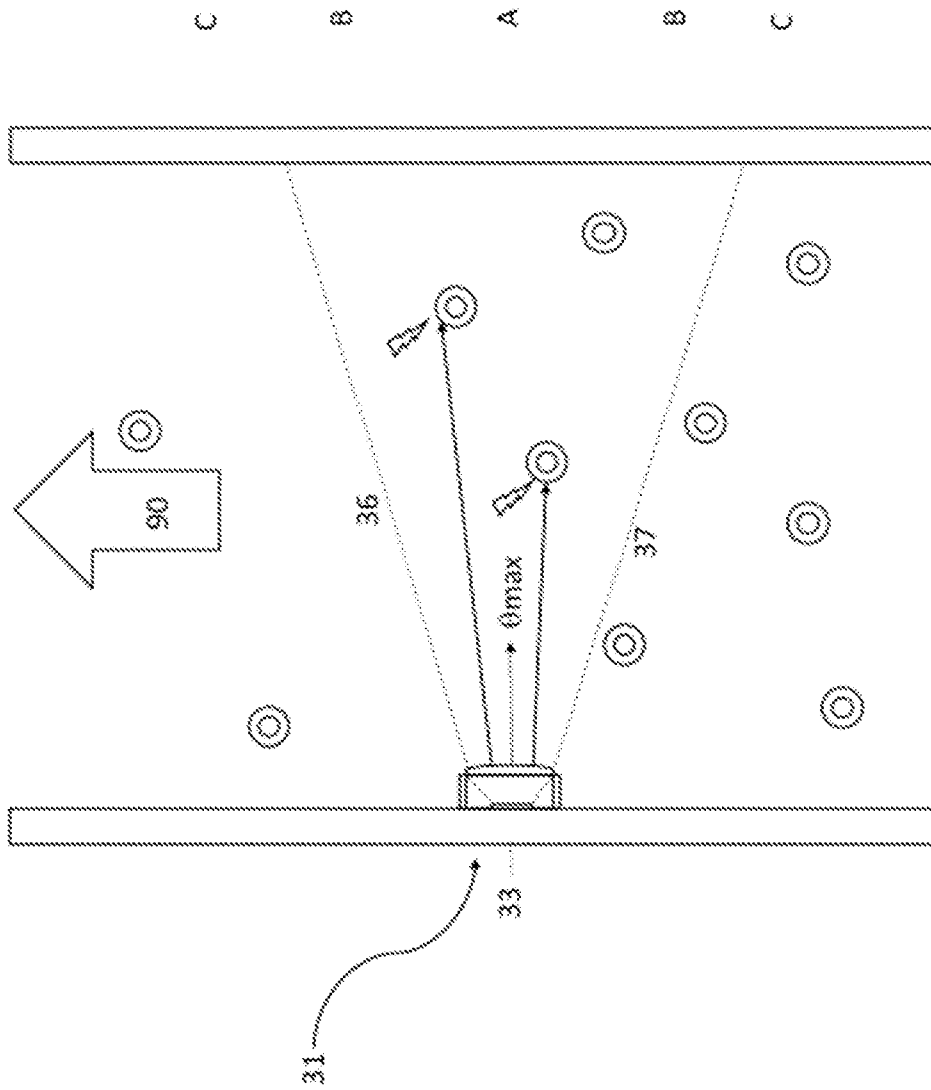


Figure 10

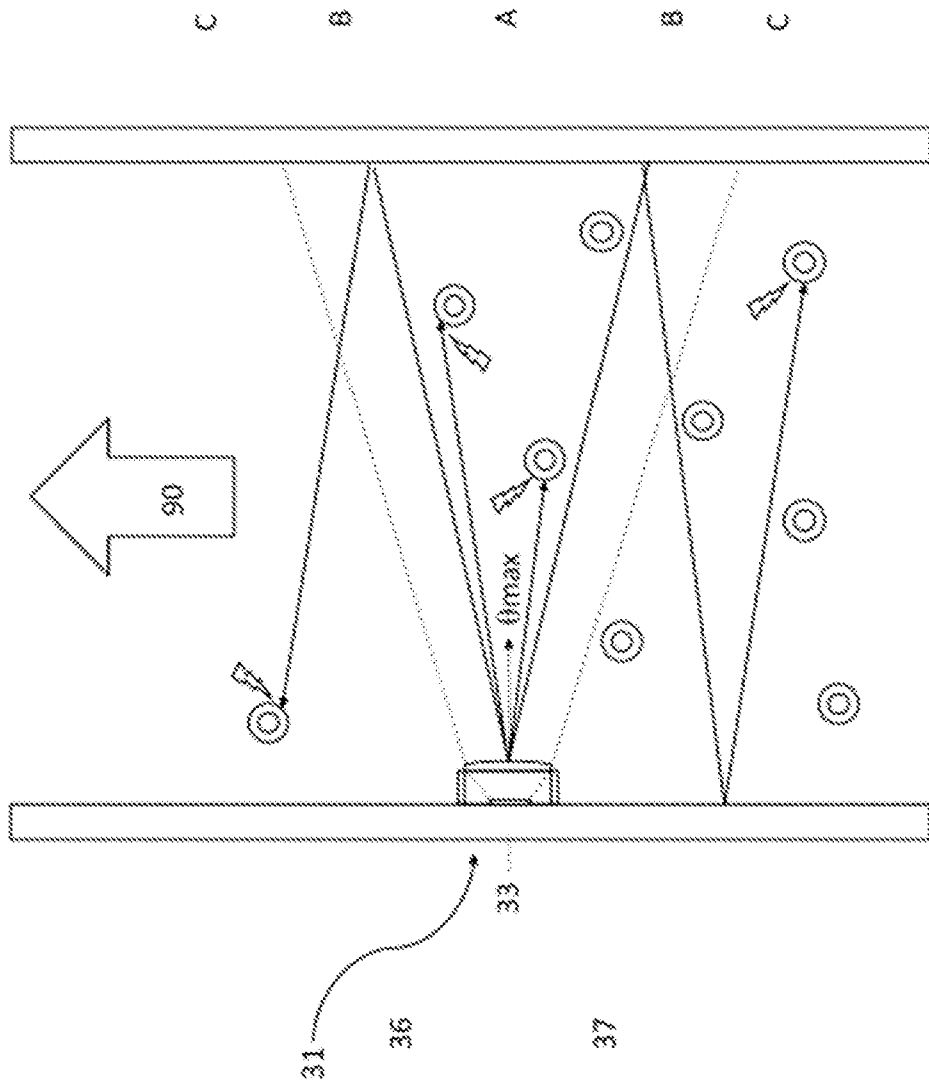


Figure 11

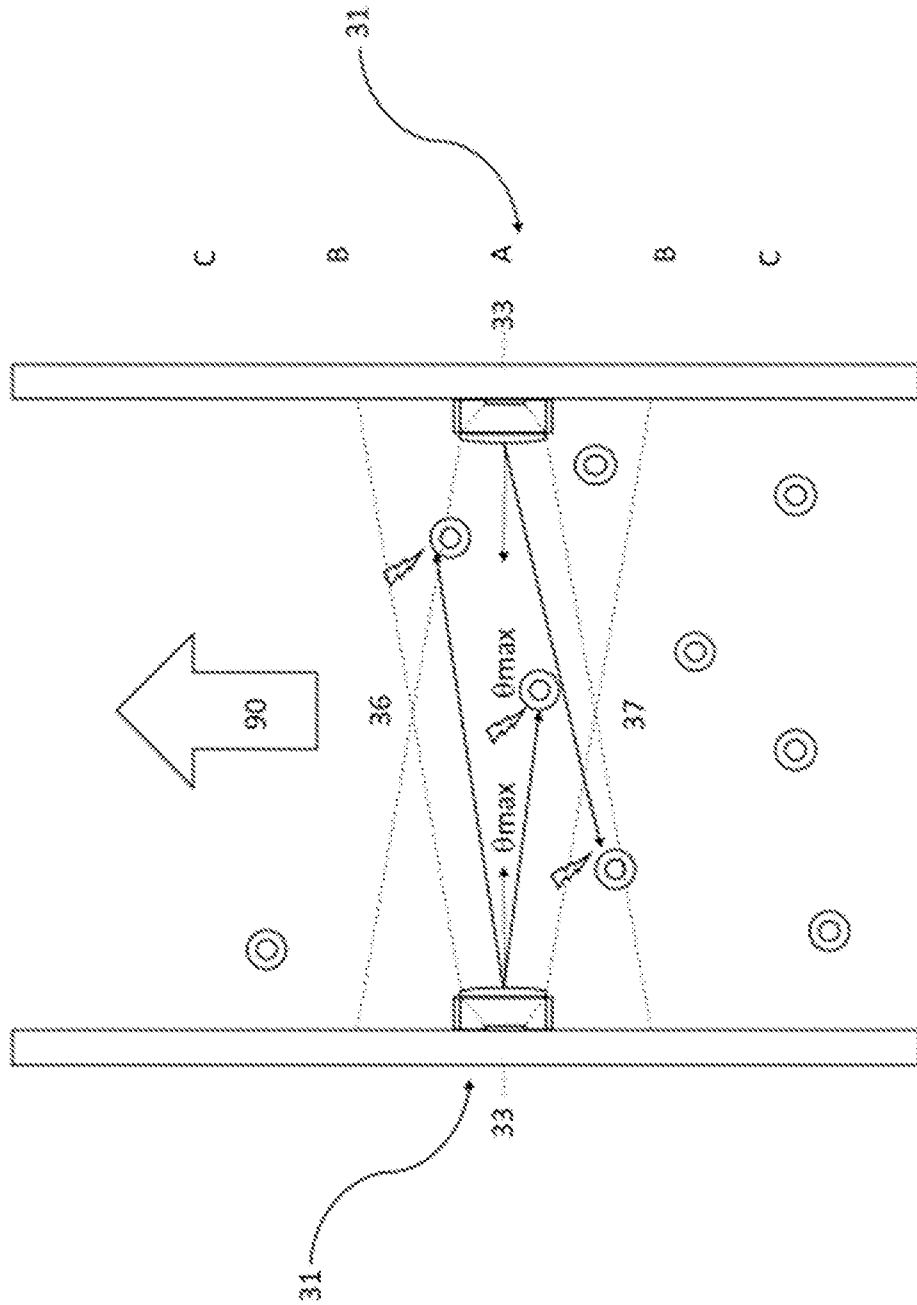


Figure 12

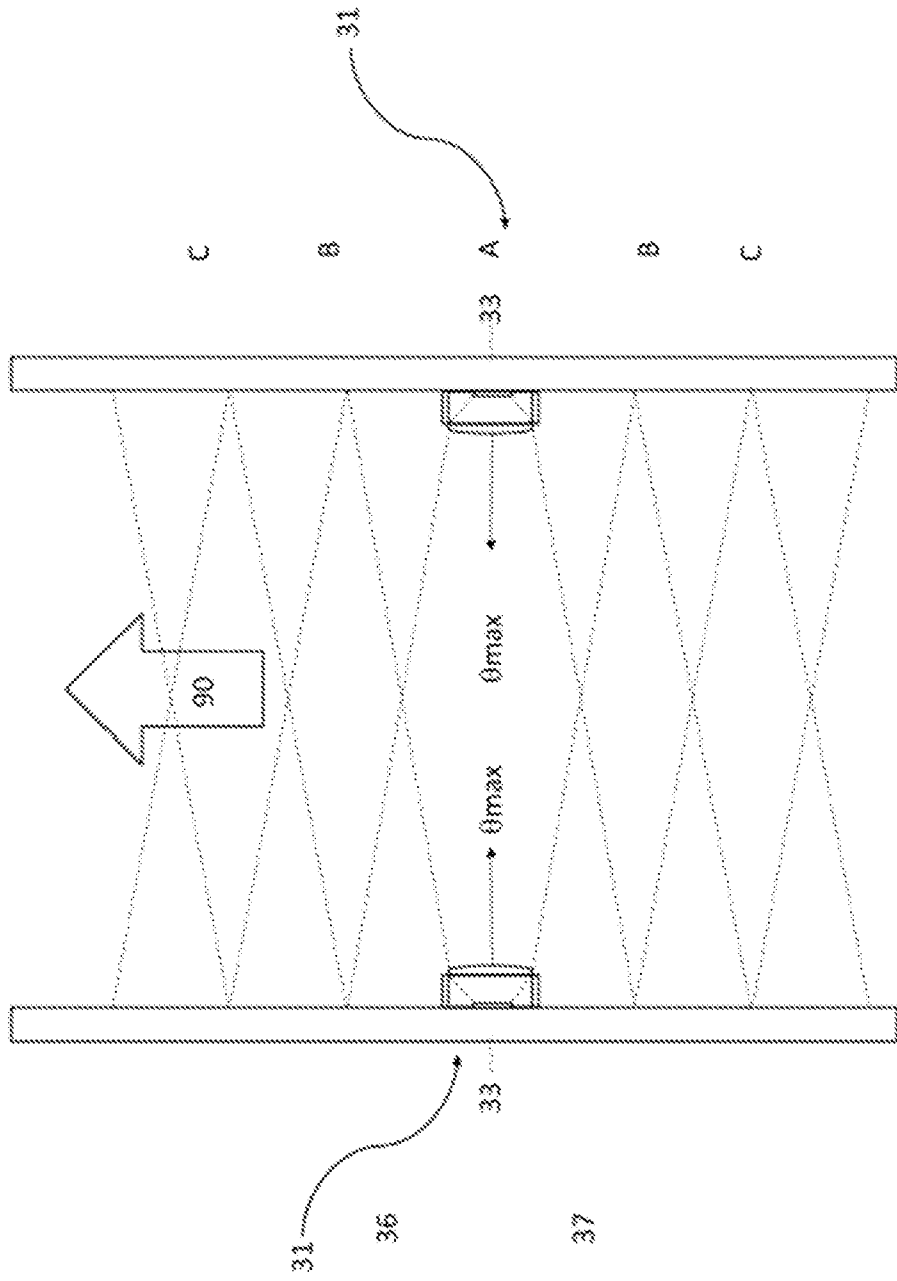


Figure 13

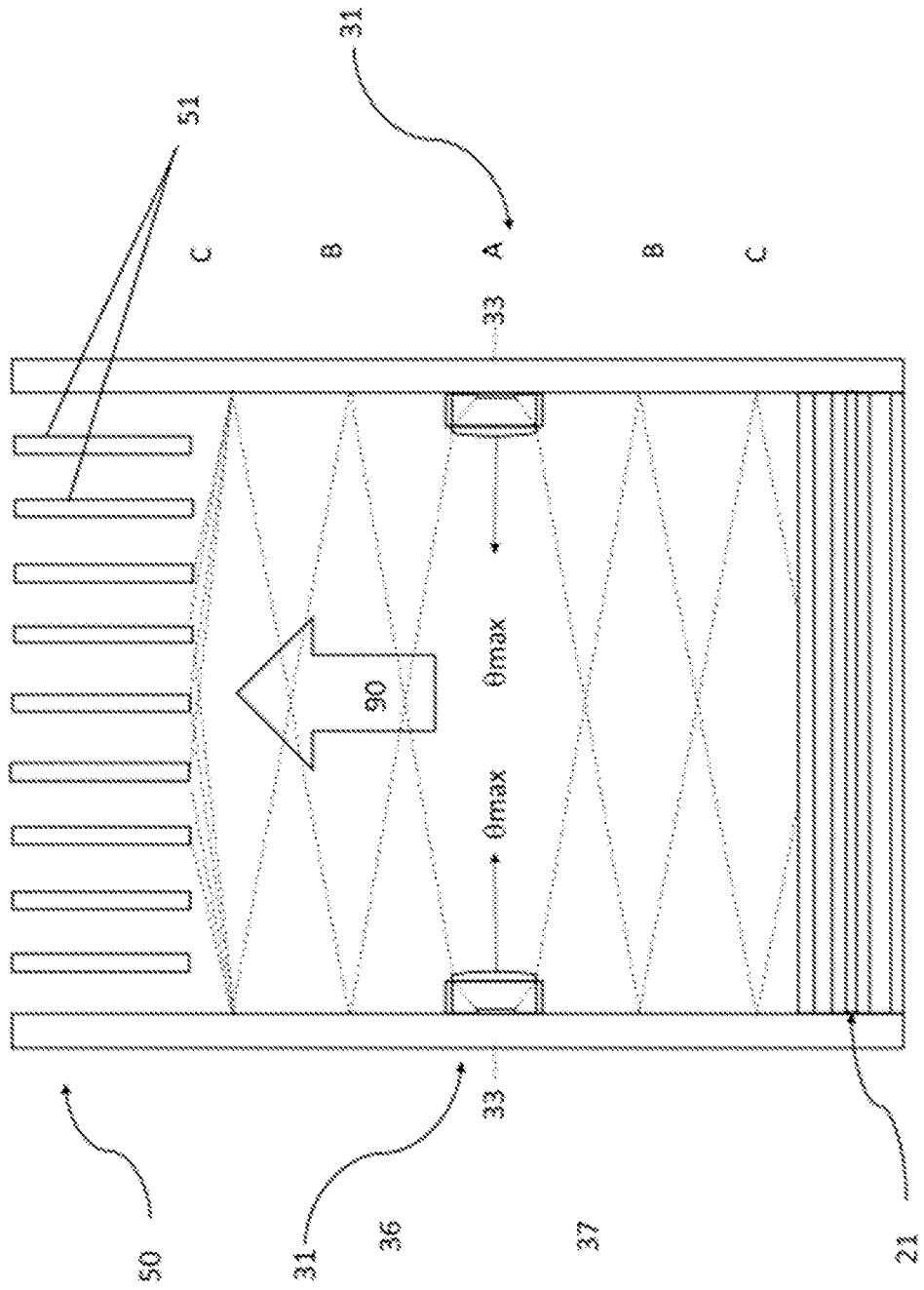


Figure 14

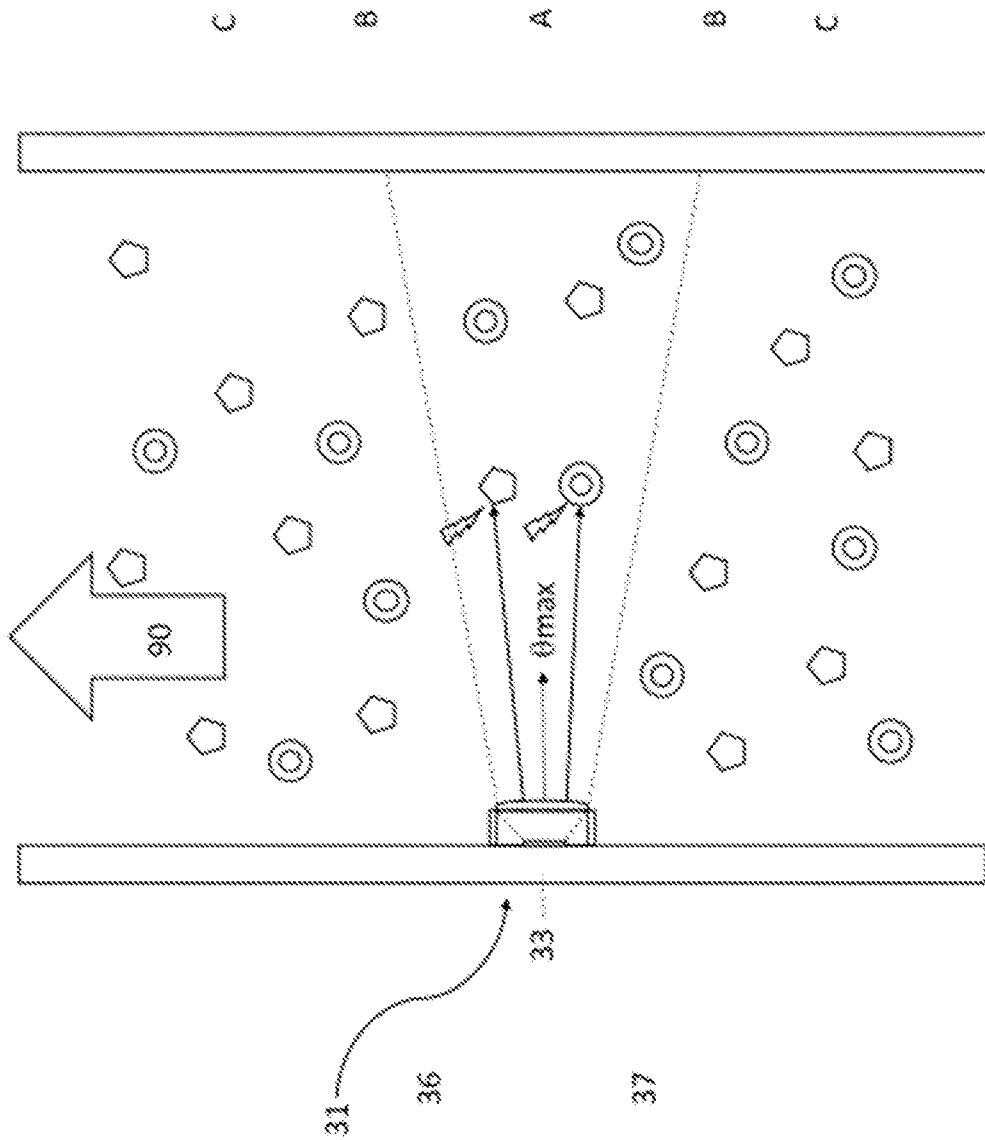


Figure 15

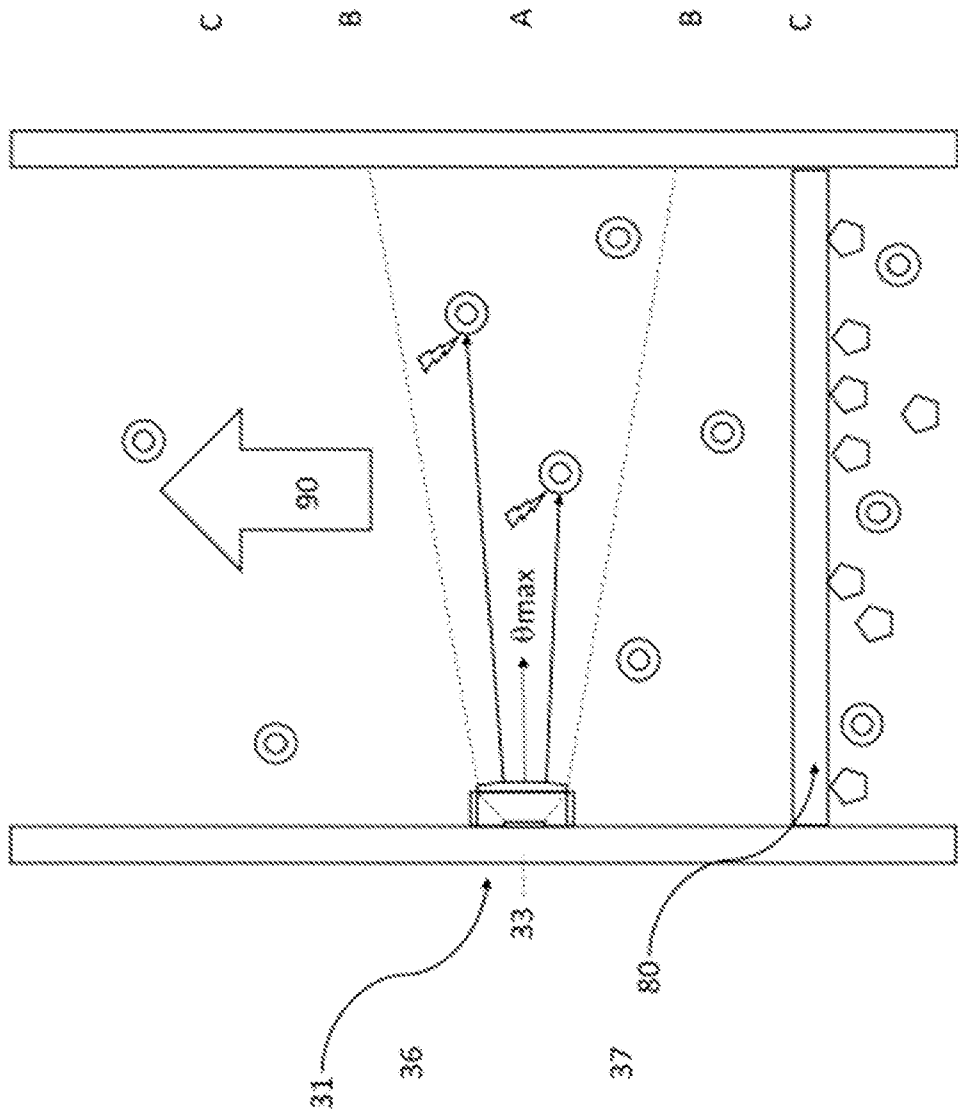


Figure 16

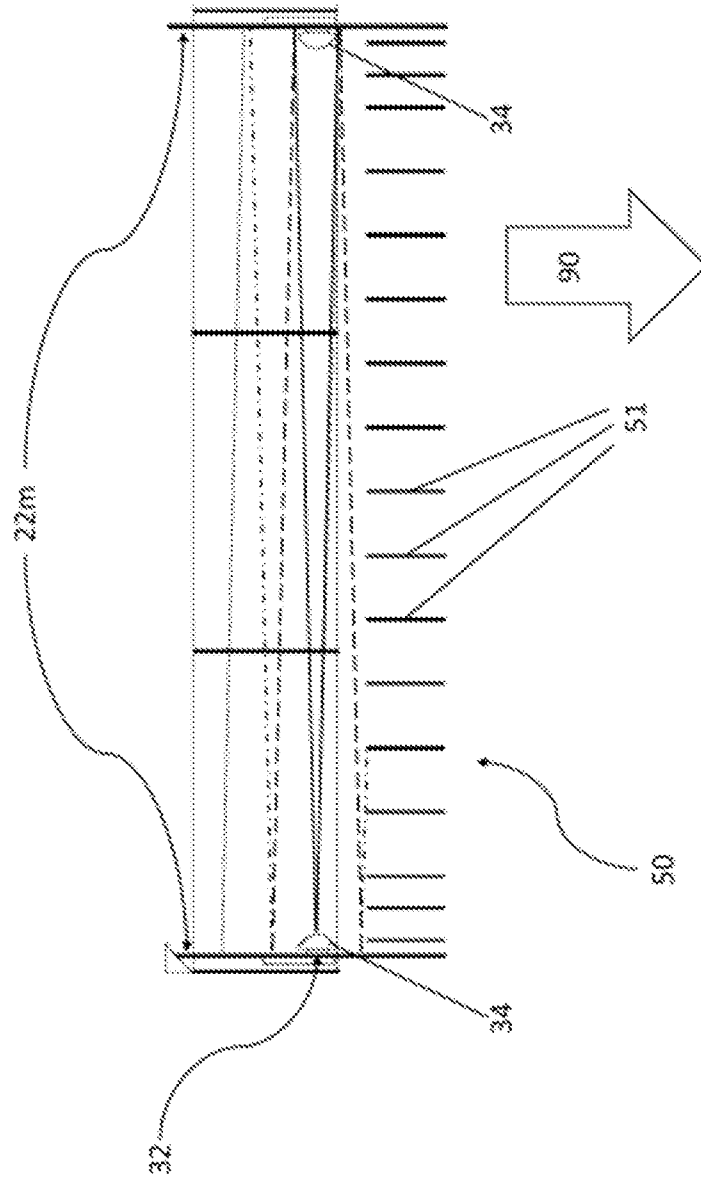
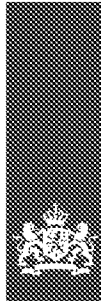


Figure 17



RAPPORT BETREFFENDE HET ONDERZOEK NAAR DE STAND VAN DE TECHNIEK

Octrooiaanvraag 2034255

Classificatie van het onderwerp ¹ : A61L9/20	Onderzochte gebieden van de techniek ¹ : A61L, F24F
Computerbestanden: KIME	Omvang van het onderzoek: Volledig
Datum van de onderzochte conclusies: 2 maart 2023	Niet onderzochte conclusies: -

Van belang zijnde literatuur

Categorie ²	Vermelding van literatuur met aanduiding, voor zover nodig, van speciaal van belang zijnde tekstgedeelten of figuren	Van belang voor conclusie(s)
X	US 2022/0290892 A (AIR PURIX INC) 15 september 2022 * figuur 2; alinea's [0017], [0024], [0029]; conclusie 1 * - - -	1-19
X	WO 2021/210034 A (BEGHELLI SPA) 21 oktober 2021 * figuur 2; conclusies 1, 3, 17 * - - -	1-19
X	CN 213441994 U (DONGGUAN SANHE MECHANICAL&ELECTRICAL CO LTD) 15 juni 2021 & machinevertaling van CN 213441994 U (KIME) * figuur 3; conclusies 1, 2, 9 * - - - - -	1-19
Datum waarop het onderzoek werd voltooid: 23 augustus 2023		De bevoegde ambtenaar: dr. R. Boers Octrooiencentrum Nederland onderdeel van Rijksdienst voor Ondernemend Nederland

1, 2 Zie toelichting volgend blad.

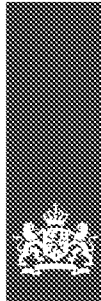
Toelichting:

¹ Classificatie gebieden van de techniek:
gedefinieerd volgens International Patent Classification (IPC).

² Categorie van de vermelde literatuur:

X: op zichzelf van bijzonder belang zijnde stand van de techniek
Y: in samenhang met andere geciteerde literatuur van bijzonder belang zijnde stand van de techniek
A: niet tot de categorie X of Y behorende van belang zijnde stand van de techniek
O: verwijzend naar niet op schrift gestelde stand van de techniek
P: literatuur gepubliceerd tussen voorrangs- en indieningsdatum

T: niet tijdig gepubliceerde literatuur over theorie of principe ten grondslag liggend aan de uitvinding
E: octrooliteratuur gepubliceerd op of na de indieningsdatum van de onderhavige aanvraag en waarvan de indieningsdatum of de voorrangsdatum ligt voor de indieningsdatum van de onderhavige aanvraag
D: in de aanvraag genoemd
L: om andere redenen vermelde literatuur
&: lid van dezelfde octroofamilie; corresponderende literatuur



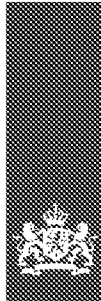
AANHANGSEL

Behorende bij het Rapport betreffende het Onderzoek naar de Stand van de Techniek

Octrooiaanvraag 2034255

Het aanhangsel bevat een opgave van elders gepubliceerde octrooiaanvragen of octrooien (zogenaamde leden van dezelfde octrooifamilie), die overeenkomen met octrooigeschriften genoemd in het rapport. De opgave is samengesteld aan de hand van gegevens uit het computerbestand van het Europees Octroobureau per 23 augustus 2023. De juistheid en volledigheid van deze opgave wordt noch door het Europees Octroobureau, noch door Octrooicentrum Nederland gegarandeerd; de gegevens worden verstrekt voor informatiedoeleinden.

In het rapport genoemd octrooigeschrift		Datum van publicatie	Overeenkomende octrooigeschriften		Datum van publicatie
US 2022290892	A1	15-09-2022	US 2022288267	A1	15-09-2022
WO 2021210034	A1	21-10-2021	CN 115461092	A	09-12-2022
			EP 4135783	A1	22-02-2023
			IT 202000008248	A1	17-10-2021
			US 2023158199	A1	25-05-2023
CN 213441994	U	15-06-2021	(geen)		



SCHRIFTELIJKE OPINIE

Octrooiaanvraag 2034255

Indieningsdatum: 2 maart 2023	Voorrangsdatum:
Classificatie van het onderwerp ¹ : A61L9/20	Aanvrager: Ubed B.V.
Deze schriftelijke opinie bevat een toelichting op de volgende onderdelen:	
<input checked="" type="checkbox"/> Onderdeel I	Basis van de schriftelijke opinie
<input type="checkbox"/> Onderdeel II	Voorrang
<input type="checkbox"/> Onderdeel III	Vaststelling nieuwheid, inventiviteit en industriële toepasbaarheid niet mogelijk
<input type="checkbox"/> Onderdeel IV	De aanvraag heeft betrekking op meer dan één uitvinding
<input checked="" type="checkbox"/> Onderdeel V	Gemotiveerde verklaring ten aanzien van nieuwheid, inventiviteit en industriële toepasbaarheid
<input type="checkbox"/> Onderdeel VI	Andere geciteerde documenten
<input type="checkbox"/> Onderdeel VII	Overige gebreken
<input checked="" type="checkbox"/> Onderdeel VIII	Overige opmerkingen
	De bevoegde ambtenaar: dr. R. Boers Octroioentrum Nederland onderdeel van Rijksdienst voor Ondernemend Nederland

¹ Gedefinieerd volgens International Patent Classification (IPC).

Schriftelijke Opinie

Octrooiaanvraag 2034255

Onderdeel I Basis van de schriftelijke opinie

Deze schriftelijke opinie is opgesteld op basis van de op 2 maart 2023 ingediende conclusies.

Onderdeel V Gemotiveerde verklaring ten aanzien van nieuwheid, inventiviteit en industriële toepasbaarheid

1. Verklaring

Nieuwheid	Ja: conclusie(s)	
	Nee: conclusie(s)	1-3, 5, 7, 8, 12-17
Inventiviteit	Ja: conclusie(s)	-
	Nee: conclusie(s)	4, 6, 9-11, 18, 19
Industriële toepasbaarheid	Ja: conclusie(s)	1-19
	Nee: conclusie(s)	-

2. Literatuur en toelichting

In het rapport betreffende het onderzoek naar de stand van de techniek worden de volgende publicaties genoemd:

- D1: US 2022/0290892 A (AIR PURIX INC) 15 september 2022
- D2: WO 2021/210034 A (BEGHELLI SPA) 21 oktober 2021
- D3: CN 213441994 U (DONGGUAN SANHE MECHANICAL&ELECTRICAL CO LTD) 15 juni 2021

Opgemerkt wordt dat UVC-licht gedefinieerd wordt door licht met een golflengte van 100-280 nm.

D1 openbaart een antimicrobiële luchtventilatie-eenheid ("air purification system") voor het behandelen van lucht met UVC-licht (zie figuur 2; conclusie 1), omvattende:

- ten minste een centrifugale ventilatoreenheid die een waaier en een gekanaliseerde ventilatorbehuizing omvat ("tangential fan", 108) met een holle cilindrische waaier ("cylindrical impeller", zie paragraaf [0024]); en
- ten minste een LED UVC-stralingseenheid (115, zie paragraaf [0029]) omvat,
- waarbij de UVC-stralingseenheid of -eenheden geconfigureerd is of zijn om een bestraling mogelijk te maken van lucht die door de antimicrobiële luchtventilatie-eenheid stroomt, waarbij de ten minste ene UVC-stralingseenheid geconfigureerd is om ten minste een deel van het inwendige van de gekanaliseerde ventilatorbehuizing te belichten met UVC-licht.

Daarnaast is er een licht-afsluitend schotgeheel ("exhaust louvers", 122, zie paragraaf [0017]) en een gespiegeld inwendig oppervlak (110, "reflector") aanwezig.

Conclusies 1-3, 5, 7, 8, 12, 14 en 15 zijn daardoor niet nieuw ten opzichte van D1, evenals de bijbehorende werkwijze en toepassing volgens conclusies 16 en 17.

Conclusies 4, 6, 13 en 18 zijn gericht op algemeen gebruikelijke uitvoeringsvormen en gebruikelijke

Schriftelijke Opinie

Octrooiaanvraag 2034255

alternatieve centrifugale ventilatoren, die een deskundige kan kiezen afhankelijk van hoe hij zijn inrichting vorm wil geven. De conclusies 4, 6, 13 en 18 worden daardoor niet inventief bevonden na het bekende uit D1.

D2 openbaart een antimicrobiële luchtventilatie-eenheid ("system for sanitazion") voor het behandelen van lucht met UVC-licht (zie figuur 2; conclusie 1), omvattende:

- ten minste een centrifugale ventilatoreenheid die een waaier en een gekanaliseerde ventilatorbehuizing omvat ("tangential fan", 22); en
- ten minste een LED UVC-stralingseenheid (250, zie conclusie 3) omvat,
- waarbij de UVC-stralingseenheid of -eenheden geconfigureerd is of zijn om een bestraling mogelijk te maken van lucht die door de antimicrobiële luchtventilatie-eenheid stroomt, waarbij de ten minste ene UVC-stralingseenheid geconfigureerd is om ten minste een deel van het inwendige van de gekanaliseerde ventilatorbehuizing te belichten met UVC-licht.

Daarnaast is er een licht-afsluitend schotgeheel ("staggered metal grids", 21, conclusie 17) en een gespiegeld inwendig oppervlak ("reflecting walls") aanwezig.

Conclusies 1, 2, 7, 8, 12-15 zijn daardoor niet nieuw ten opzichte van D2, evenals de bijbehorende werkwijze en toepassing volgens conclusies 16 en 17.

Conclusies 3-6 en 18 zijn gericht op algemeen gebruikelijke uitvoeringsvormen en gebruikelijke alternatieve centrifugale ventilatoren, die een deskundige kan kiezen afhankelijk van hoe hij zijn inrichting vorm wil geven. De conclusies 3-6 en 18 worden daardoor niet inventief bevonden na het bekende uit D2.

D3 openbaart een antimicrobiële luchtventilatie-eenheid ("ultraviolet disinfection device") voor het behandelen van lucht met UVC-licht (zie figuur 3; conclusie 1), omvattende:

- ten minste een centrifugale ventilatoreenheid die een waaier en een gekanaliseerde ventilatorbehuizing omvat ("cross-flow fan", 410; conclusie 9); en
- ten minste een UVC-stralingseenheid (300) omvat,
- waarbij de UVC-stralingseenheid of -eenheden geconfigureerd is of zijn om een bestraling mogelijk te maken van lucht die door de antimicrobiële luchtventilatie-eenheid stroomt, waarbij de ten minste ene UVC-stralingseenheid geconfigureerd is om ten minste een deel van het inwendige van de gekanaliseerde ventilatorbehuizing te belichten met UVC-licht.

Daarnaast is er een licht-afsluitend schotgeheel aanwezig ("light blocking plate", 500, zie conclusie 2).

De onderhavige aanvraag onderscheidt zich ten opzichte van D3 in het gebruik van een UVC-LED.

D3 is daardoor niet nieuwheidschadelijk voor conclusies 1-19.

Het wordt echter niet inventief bevonden om een UVC-LED toe te passen in de antimicrobiële luchtventilatie-eenheid van D3, omdat de deskundige weet dat deze minder stroom gebruiken en klein zijn, en daarmee uitermate geschikt voor het gebruik in toepassingen waar het formaat van de inrichting klein gehouden moet worden en de inrichting zuinig met energie moet omspringen, zoals in voertuigen.

Schriftelijke Opinie

Octrooiaanvraag 2034255

Conclusies 1-3, 5, 7, 8, 12-14 zijn daardoor niet inventief ten opzichte van D3, evenals de bijbehorende werkwijzeconclusie 16 en toepassingen volgens conclusies 17 en 18.

Conclusies 4, 6 en 15 zijn gericht op algemeen bekende centrifugale ventilatoren, die een deskundige als alternatief kan kiezen voor de ventilator gebruikt in D3 afhankelijk van hoe hij zijn inrichting vorm wil geven, en gebruikelijke uitvoeringsvormen. De conclusies 4, 6 en 15 worden daardoor niet inventief bevonden ten opzichte van D3.

De waarden genoemd in conclusies 9-11 zijn gebruikelijke waarden voor UVC-LED's. Een deskundige zal dus bij het toepassen van UVC-LED's veelal automatisch uitkomen op deze waarden. De conclusies 9-11 worden daardoor evenmin inventief bevonden na het bekende uit een van D1-D3.

Matrassen omvattende een antimicrobiële luchtventilatie-eenheid zijn algemeen bekend. Het wordt dan ook niet inventief bevonden om de niet-inventief bevonden antimicrobiële luchtventilatie-eenheid van onderhavige conclusie 1 toe te passen in matrassen.

Conclusie 19 wordt hierdoor na het bekende uit een van D1-D3 niet inventief bevonden in combinatie met algemene kennis van de deskundige.

Onderdeel VIII Overige opmerkingen

De volgende opmerkingen met betrekking tot de duidelijkheid van de conclusies, beschrijving en figuren, of met betrekking tot de vraag of de conclusies naverkbaar zijn, worden gemaakt:

De in de beschrijving gebruikte referentie US5925230 met titel "Deionization apparatus having non-sacrificial electrodes of different types" lijkt niet de bedoelde referentie te zijn.

Zinsneden die beginnen met de uitdrukking "optioneel", "bij voorkeur", "beter", "bijvoorbeeld", "zoals" of "in het bijzonder" hebben geen beperkende invloed op de beschermingsomvang van de conclusie waarin deze zijn opgenomen. Zulke zinsneden worden daarom bij de beoordeling van nieuwheid en inventiviteit van de betreffende conclusies buiten beschouwing gelaten.

Conclusie 5, een antimicrobiële luchtventilatie-eenheid volgens een der voorgaande conclusies, kan niet afhankelijk zijn van conclusie 4 aangezien een holle cilindrische waaier niet hetzelfde is als een ventilatorwielwaaier.