(12) UK Patent Application (19) GB (11) 2 187 131 (13) A

(43) Application published 3 Sep 1987

(21) Application No 8702125

(22) Date of filing 30 Jan 1987

(30) Priority data

(31) 61/023594

(32) 5 Feb 1986

(33) JP

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(51) INT CL⁴ B29C 33/00 // 45/26

(52) Domestic classification (Edition I) **B5A** 1R314C6 1R400 1R418 20T14 2A2 2E10 2E12C N1 **U1S** 2108 B5A

(56) Documents cited GB 1087400

EP A2 0121929

(58) Field of search

DOM

Selected US specifications from IPC sub-class B29C

(54) Injection moulds

(57) A mold for molding an optical disc includes a stationary mold member 12 having a recess 16, and a movable mold member having a plate-like sintered ceramic member 22 secured to its body, member 22 having a flat seat surface 32. The recess 16 and the flat seat surface 32 jointly provides a mold cavity when the first and second mold members are mated together. A thin disc-shaped stamper 34 is detachably secured to the flat seat surface. The ceramic member 22 is made of a ceramic material, e.g. silicon carbide, having Rockwell harness (A-Scale) of not less than 90, so that the flat seat surface 32 is not easily damaged.

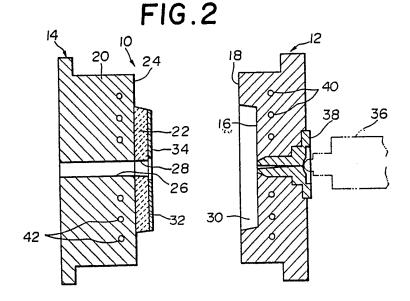
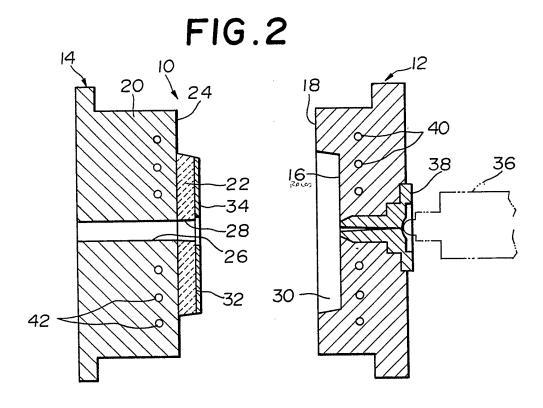


FIG. (PRIOR ART)
14a 10a 24a 30a 40a
16a 38 36
34a 32a
42a 22a



SPECIFICATION

Mold for molding optical disc

5 BACKGROUND OF THE INVENTION

Field of the invention

This invention relates to a mold for molding an optical disc such as a compact disc and a laser disc.

10 Prior art

In recent years, there have been increasingly used compact discs which store digital audio data and reproduce the recorded sound with high accuracy. As is well known in the art, a large number of fine pits 15 are formed in a selected pattern in a surface of the compact disc so as to produce digital audio signals when they are detected, thereby reproducing the recorded music or other sounds. Generally, such an optical disc is injection molded using a disc-shaped 20 thin stamper secured at one face to a mold and having a large number of fine projections corresponding in shape and size to the pits of the resultant optical disc. One such a conventional mold 10a as shown in Figure 1 comprises a stationary mold member 12a 25 having a recess 16a, and a movable mold member 14a movable toward and away from the stationary mold member 12a. The movable mold member 14a has a projection 22a formed on one face 24a thereof and adapted to be fitted in the recess 16a of the stati-30 onary mold member 12a when the two mold members 12a and 14a are mated together. The projection 22a has a flat seat surface 32a machined to a mirror surface. With this construction, when the stationary and movable mold members 12a and 14a are mated 35 together, a mold cavity 30a is defined by the surface

- of the recess 16a of the stationary mold member 12a and the flat seat surface 32a as shown in Figure 1. A disc-shaped stamper 34a having a thickness of about 0.3 mm is detachably secured to the seat surface 32a 40 of the projection 22a by a bolt (not shown) received in a central hole 26a of the movable mold member 14a. A molding material is injected from a injection
- molding machine 36 into the mold cavity 30a via a nozzle 38a mounted on the stationary mold member 45 12a so as to mold a compact disc. The stationary and movable mold members 12a and 14a are made of steel such as one manufactured and sold by Uddeholm under the tradename of Stavax. Holes 40a
- and 42a are formed in the stationary and movable 50 mold members 12a and 14a, respectively, for passing cooling water therethrough.

Usually, various kinds of stampers are provided for being exchangeably mounted on the flat seat surface 32a of the movable mold member 14a so as to 55 produce various kinds of compact discs. With this conventional mold 10a, however, if a jig or other tool inadvertently hits against the flat seat surface 32a of the movable mold member 14a at the time of exchanging the stampers 34a and at other occasions,

- 60 the seat surface 32a is damaged. As a result, the thin stamper 34a seated on the damaged seat surface 32a is deformed at the damaged portion of the seat surface 32a, so that such deformation is transferred to the molded optical discs. Thus, there is a possibility
- 65 that the optical discs of an inferior quality are prod-

uced in a large quantity. And, when the flat seat surface 32a of the movable mold member 14a is damaged, the damage seat surface 32a must be polished, which leads to low productivity.

In addition, when the molding resin is injected into the mold cavity 30a, the stamper 34a is subjected to vibration by the molding resin under pressure, so that the marginal portion of the flat seat surface 32a tends to undergo damage. This is undesirable since 75 the stamper 34a is not held in proper position with respect to the flat seat surface 32a.

Summary of the invention

It is thereof an object of this invention to provide a 80 mold for molding an optical disc in which a flat seat surface for holding a stamper thereon is less liable to damage.

According to the present invention, there is provided a mold for molding an optical disc comprising a 85 first mold member having a first cavity surface and a second mold member movable relative to said first movable member and having a second cavity surface, the first and second cavity surfaces jointly providing a mold cavity when the first and second mold 90 members are mated together, the second cavity surface having a flat seat surface for detachably holding a disc-shaped thin stamper thereon, the flat seat surface being made of a sintered ceramic material having Rockwell hardness (A-Scale) of not less than 90.

The flat seat surface is sufficiently hard that it is not 95 subjected to undue damage even if the flat seat surface is inadvertently hit by a jig for exchanging the stamper so as to prevent the stamper from being deformed when it is mounted on the flat seat surface, 100 thereby ensuring the molding of optical disc of a good quality for a prolonged period of time. In addition, the flat seat surface is not subjected damage even if the stamper seated thereon is subjected to vibration when the molding material is injected to 105 the mold cavity. Therefore, the mold requires much less maintenance and can be easily handled, so that the mold can be used quite efficiently, thereby improving the productivity of the molded compact discs.

110

Brief description of the drawings

Figure 1 is a cross-sectional view of a mold provided in accordance with the prior art; and Figure 2 is a mold provided in accordance with the

115 present invention.

Description of the preferred embodiments of the in-

A mold 10 shown in Figure 2 comprises a statio-120 nary mold member 12 and a movable mold member 14 movable toward and away from the stationary mold member 12 along associated guide rods (not shown). The stationary mold member 12 is made of steel and has a disc-shaped recess 16 formed in one 125 flat face 18 thereof. The movable mold member 14 comprises a body 20 made of steel and a sintered ceramic member 22 of a disc-shape fixedly secured at one face by an adhesive to one flat face 24 of the body 20 facing the recess 16 of the stationary mold 130 member 12. The ceramic member 22 may be fixedly secured to bolts to the body 20. The body 20 has an axial hole 26 formed therethrough, and the ceramic member 22 also has a central aperture 28 formed therethrough and disposed in alignment with the 5 hole 26 of the body 20. When the movable mold member 14 is moved into engagement with the stationary mold member 12, the ceramic member 22 is fitted in the recess 16 with the faces 18 and 24 of the tow mold members mated together, so that a mold cavity 30 of a disc-shape is defined by the other flat face 32 of the ceramic member 22 and the surface defining the recess 16 of the stationary mold member 12. Thus, the surface defining the recess 16 defines a cavity surface, and the flat face 32 of the ceramic member 22 also defines a cavity surface.

The flat face 32 of the sintered ceramic member 22 facing the recess 16 of the stationary mold member 12 serves as a seat surface on which a thin disc-shaped stamper 34 with a central aperture is seated 20 at one face thereof. The stamper 34 is detachably secured to the seat surface 32 of the ceramic member 22 by a bolt (not shown) passing through the aperture 28 and the hole 26 and a nut (not shown) threaded onto a distal end of the bolt. In this condition, a molten molding resin is injected into the mold cavity 30 from a molding injection machine 36 via a nozzle 38 mounted on the stationary mold member

12. A plurality of elongated holes 40 are formed in the stationary mold member 12, and a plurality of el30 ongated holes 42 are formed in the body 20 of the movable mold member 14. Cooling water is passed through these holes 40 and 42 during the molding operation to maintain the temperature of the mold 10 at predetermined temperatures.

35 The sintered ceramic member 22 is made of a ceramic material having Rockwell hardness (A-Scale) of not less than 90. If Rockwell hardness of the ceramic material is less than 90, the flat seat surface 32 of the ceramic member 22 may be subjected to damage 40 when a stamper-exchanging jig or the like hits on the seat surface 32 and when it is subjected to abrasion by a cleaning means.

Preferably, the sintered density of said ceramic material should be not less than 85% of the theoreti-45 cal density. In this case, if the ceramic member 22 is made, for example, of silicon carbide, it has a sintered density of not less than 2.74 g/cm³. More preferably, the sintered density of the ceramic material should be not less than 93% of the theoretical density, in which case the ceramic member 22 made of silicon carbide has a sintered density of not less than 3.03 g/cm³. As the sintered density becomes lower, the pores of the ceramic material becomes larger, so that a surface of the ceramic member 22 can not be 55 finished to a satisfactory smoothness.

The ceramic member 22 can be made of a silicon carbide, silicon nitride, alumina, aluminum nitride, zirconia, spinel, titanium carbide, boron carbide or the like. Among these ceramics materials, silicon carbide is most preferred since it has a high coefficient of thermal conductivity, so that the mold 10 can be cooled smoothly during the molding, thereby shortening the molding time to improve the shot cycle.

Either of α type and β type silicon carbide can be 65 used for the ceramic member 22. There are several

methods of sintering silicon carbide. One method is to sinter silicon carbide under pressure, and another method is to sinter silicon carbide under atmospheric pressure. A further method is to react silicon with carbon during the sintering. Any one of these three methods can be used to produce the sintered silicon carbide for the ceramic member 22. Such sintered silicon carbide is produced by adding a small amount of an assistant, such as carbon (C) and boron (B), to silicon carbide (SiC) in the form of fine powder and then sintering the powder. In addition, boron carbide (B₄C) or the like may be added as an assistant to the powder of silicon carbide to carry out the sintering of the ceramic material smoothly.

For producing the ceramic member 22 of silicon carbide, a binder and an assistant are added to powder of silicon carbide to form a mixture, and water is added to the mixture. Then, the mixture is adequately blended by a ball mill or the like to form a slurry.
 Then, the slurry is treated by a spray dryer or the like to form granular material. Then, the granular material is compacted by a press into a solidified solid body. Then, the solidified solid body is processed into a predetermined size and shape by a lathe or a mill and then is sintered to form a ceramic member 22. Finally, the ceramic member 22 is polished by diamond-lapping into a final form.

Preferably, the flat seat surface 32 of the ceramic member 22 thus produced should have a surface 95 roughness of about 0.05 S to about 1.2 S. If the surface roughness is more than 1.2 S, there is a possibility that such a coarse roughness may be transferred to the molded disc via the thin stamper 34. On the other hand, if the surface roughness of the flat 100 seat surface 32 becomes unduly smaller, the contact between the stamper 34 and the flat seat surface 32 of the ceramic member 22 becomes excessively firm or tight. Due to a difference in thermal expansion coefficient between the stamper 34 and the ceramic 105 member 22, fine wrinkles are liable to be produced on the stamper 34. The surface roughness of the flat seat surface 32a of the conventional mold 10a of Stavax must be not more than 0.01 S. Since the flat seat surface 32 for detachably hol-

ding the stamper 34 thereon is made of the ceramic material, the flat seat surface 32, even when being stricken by a jig or the like, is not damaged or deformed to such an extent that this deformation is transferred to the surface of the molded optical disc.
It is considered that the reason for this is that the flat seat surface 32 is so hard that it will not be vitally damaged, and that even if an indentation develops on the flat seat surface 32 upon the striking of the jig against it, the indentation is quite shallow and hence
negligible, so that no deformation is transferred to the surface of the molded optical disc.

In addition, the ceramic member 22 is relatively brittle as compared with metals, and therefore even if the flat seat surface 32 of the ceramic member 22 is hit by a jig and is indented slightly, the flat seat surface 32 will not be bulged around such an indentation, as is the case with a steel surface, because the seat surface 32 can not be plastically deformed. In such a case, with the conventional mold 10a shown in Figure 1, a molding pressure is concentrated on

that portion of the stamper 34 held in contact with such a bulged portion on the steel seat surface 32a during the molding operation, so that the molded optical disc is correspondingly deformed. On the 5 other hand, with the mold 10 according to the present invention, no such a bulged portion will develop on the flat seat surface 32 of the ceramic member 22 even if it is damaged, and therefore no undue molding pressure is concentrated on that portion of the stamper 34 held in contact with the damaged portion on the flat seat surface 32, so that the stamper 34 will not be deformed, thereby ensuring the molding of optical discs of a required quality.

Another advantage that the flat seat surface 32 is
15 made of the hard ceramic material is that the seat
surface 32 will not be subjected to damage even if the
stamper 34 is subjected to vibration when the molding resin is injected into the mold cavity 30.

The invention will now be illustrated by way of the 20 following Example:

Example

A mold similar to the mold 10 shown in Figure 2 was prepared. For the purpose of simplicity, like re-25 ference numerals are used in this Example to denote corresponding parts. First, a stationary mold member 12 and a body 20 of a movable mold member 14 were made of steel (Stavax). A discshaped ceramic member 22 made of silicon carbide 30 was prepared, the ceramic member 22 having a central aperture 28 therethrough and having an outer diameter of 140 mm, an inner diameter of 34 mm and a thickness of 12.7 mm. Then, the ceramic member 22 was fixedly secured in place to a face 24 of the 35 body 20 by an epoxy adhesive. Then, a seat surface 32 of the ceramic member 22 was ground and subsequently polished by diamond-lapping into a highly flat surface having a surface roughness of 0.2 S, a parallelism of 0.002 and a flatness of 0.003.

The mold 10 thus prepared was mounted on an injection molding machine 36. Then, a stamper 34 having a thickness of 0.3 mm was mated with and secured to the flat seat surface 32 of the ceramic member 22, and a thousand of laser discs having an outer diameter of 120 mm, an inner diameter of 15 mm and a thickness of 1.2 mm were successively molded. During the molding operation, water of 80°C was passed through the holes 40 and 42 of the stationary and movable mold members 12 and 14, and a molten molding material of polycarbonate resin of 300°C was injected into the mold cavity 30.

After the molding operation, the lazer discs were inspected, and no undesirable effects such as wrinkles were found. Thus, the mold 10 proved to be satisfactory.

Then, molding operations were carried out, exchanging stampers as was the case with the practical molding operation. It was found that the frequency of damage to the flat seat surface 32 was lower than that of damage to the flat seat surface 32a of the conventional mold 10a shown in Figure 1. In addition, conventionally, 10 to 15 shots were necessary before the injection molding becomes stable, after one stamper is replaced by another. With the mold 10 in-

or so were necessary before the injection molding becomes stable. Thus, it takes much shorter time before the molding operation becomes stable.

While the mold according to the present invention
70 has been specifically shown and described herein,
the invention itself is not to be restricted to the exact
showing of the drawings or the description thereof.
For example, in the illustrated embodiment,
although only the cavity surface defined by the flat
75 seat surface 32 is made of the ceramic material, all
the cavity surfaces may be made of the ceramic material. Also, although the cooling holes 42 are prov-

the cavity surfaces may be made of the ceramic material, all the cavity surfaces may be made of the ceramic material. Also, although the cooling holes 42 are provided in the body 20 of the movable mold member 14, these holes may be formed in the ceramic member

22, in which case it is desirable to provide the body 20 and the ceramic member 22 with recesses and projections, respectively, so that the projections are fitted in the recesses for holding the ceramic member 22 with respect to the body 20. With this
 arrangement, since the flat seat surface 32 is cooled more efficiently, the ceramic member 22 can be made of a ceramic material having a lower coeffic-

90 CLAIMS

ient of thermal conductivity.

- A mold for molding an optical disc comprising a first mold member having a first cavity surface and a second mold member movable relative to said first mold member and having a second cavity surface, said first and second cavity surfaces jointly providing a mold cavity when said first and second mold members are mated together, said second cavity surface having a flat seat surface for detachably holding a
 disc-shaped thin stamper thereon, said flat seat surface being made of a sintered ceramic material having Rockwell hardness (A-Scale) of not less than 90.
- A mold according to claim 1, in which said second mold member comprises a body and a sep-105 arate ceramic member fixedly secured to said body, said separate ceramic member having said flat seat surface.
- A mold according to claim 1, in which a sintered density of said ceramic material is not less than
 85% of a theoretical density.
 - 4. A mold according to claim 1, in which said ceramic material is made of silicon carbide.
- A mold according to claim 1, in which said flat seat surface has a surface roughness of about 0.05 S
 to 1.2 S.
 - 6. A mold for moulding an optical disc, substantially as hereinbefore described with reference to Figure 2 of the accompanying drawings.

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