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(54) Title: TETRAFLUOROPROPENE BASED BLOWING AGENT COMPOSITIONS

(57) Abstract: The present invention relates to blowing agent compositions comprising tetrafluoropropene (HFO) and at least one co-blowing agent selected from carbon dioxide, water, alkanes and an alcohol used in the preparation of foamable thermoplastic compositions having low density. The HFOs include, but are not limited too, cis- and/or trans- 1,3,3,3-tetrafluoropropene (HFO-1234ze), 2,3,3,3-tetrafluoropropene (HFO 1234yf), or mixtures thereof. The blowing agent compositions are useful in the production of low density insulating foams with improved R value.

#### **Tetrafluoropropene Based Blowing Agent Compositions**

#### Summary of Invention

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The present invention relates to blowing agent compositions comprising tetrafluoropropene (HFO) and at least one co-blowing agent selected from carbon dioxide, water, alkanes and an alcohol used in the preparation of foamable thermoplastic compositions having low density. The tetrafluoropropene component is selected from cis- and/or trans- 1,3,3,3-tetrafluoropropene (HFO-1234ze), 2,3,3,3-tetrafluoropropene (HFO 1234yf) or mixtures thereof. The co-blowing agent is selected from carbon dioxide, water, alkanes, an alcohol such as ethanol or mixtures thereof. The blowing agent compositions are useful in the production of low density insulating foams with improved R-value properties.

### Background of Invention

With the continued concern over global climate change there is an increasing need to develop technologies to replace those with high ozone depletion potential (ODP) and high global warming potential (GWP). Though hydrofluorocarbons (HFC), being non-ozone depleting compounds, have been identified as alternative blowing agents to chlorofluorocarbons (CFCs) and hydrochlorofluorocarbons (HCFCs) in the production of thermoplastic foams, they still tend to have significant GWP.

Hydrofloroolefins, such as HFO-1243zf, (cis/trans)-HFO-1234ze, HFO-1234yf, and (E/Z)-HFO-1225ye, have been identified as potential low GWP blowing agents for the production of thermoplastic foams, including extruded polystyrene foams for thermal insulation.

It was discovered that blowing agent compositions comprising a tetrafluoropropene and at least one co-blowing agent selected from carbon dioxide, water, alkanes and an alcohol can permit the production of lower density, closed-cell foam with good long term R value which will be particularly

useful for thermal insulating foams. This invention may also permit the production of low density, closed-cell foams with enlarged, controlled cell size.

WO 2004/037913, WO 2007/002703, and US Pat. Publication 2004119047 disclose blowing agents comprising halogenated alkenes of generic formula that would include numerous HFOs and HCFOs, among many other materials including brominated and iodinated compounds. Specific examples are shown for blowing agent compositions for foaming polystyrene comprising HFOs, specifically HFO-1234ze and HFO-1234yf, either alone or in combination with an HFC, and blowing agent compositions for PUR foaming comprising HCFO-1233zd.

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GB 950,876 discloses a process for the production of polyurethane foams. It discloses that any suitable halogenated saturated or unsaturated hydrocarbon having a boiling point below 150°C, preferably below 50°C, can be used as the blowing agent. Trichlorofluoroethene, chlorotrifluoroethene, and 1,1-dichloro-2,2-difluoroethene are disclosed in a list of suitable blowing agents along with 3,3,3-trifluoropropene.

CA 2016328 discloses a process for preparing closed-cell, polyisocyanate foam. Disclosed are organic compound blowing agents including halogenated alkanes and alkenes, where the alkene is propylene, and the halogenated hydrocarbons can be chlorofluorocarbons. Among the many exemplary compounds listed are specific chlorofluoroethylenes containing 1 chlorine and from 1 to 3 fluorines along with specific pentafluoropropene, tetrafluoropropene, and difluoropropene.

US 2008/135800 discloses the use of HFO-1234ze as blowing agent for polystyrene foaming. Blowing agent compositions shown in examples include: 100% trans-HFO-1234ze, 50wt% trans-HFO-1234ze and 50wt% HFC-245fa, and 80wt% HFO-1234ze and 20wt% HFC-245fa. Of the polystyrene foam examples shown using 1234ze in the blowing agent formulation, the lowest density produced was about 5 pcf. The patent application discloses that water, CO<sub>2</sub>, and alcohols can be used as coblowing agents and claims various composition ranges that these coblowing agents could be used (eg. 10% to 20% water, etc).

In the production of insulating foam it is desired to have low density foamed products that maintain a high, long term R-value (insulating value). Though HFC-134a can provide long term R-value it is not soluble enough in polystyrene to produce foam product to the same low density as with using HCFC-142b or CFC-12. HFC-134a also has a very high nucleation density such that foams produced with it tend to have a very fine cell structure, which is not desired in all applications. HFC-152a and HFC-32 can be used to produce lower density foams with larger cell sizes than with HFC-134a but their high diffusivities in polystyrene will result in foams that age faster and don't possess the same long term R-value.

### <u>Detailed Description of Invention</u>

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The present invention relates to the use of blowing agents with negligible ozone-depletion and low GWP comprising tetrafluoropropene and at least one coblowing agent selected from carbon dioxide, water, alkanes and an alcohol and mixtures thereof. The present invention discloses blowing agent and foamable resin compositions useful for the production of foams with decreased density and improved long term R value that can be used as insulating foams. In a preferred embodiment of this invention the tetrafluoropropene is selected from cis- and/or trans- 1,3,3,3-tetrafluoropropene (HFO-1234ze), 2,3,3,3-tetrafluoropropene (HFO 1234yf) or mixtures thereof. The co-blowing agent of component is selected from carbon dioxide, water, 1,1-difluoroethane, alkanes and an alcohol, such as ethanol, and mixtures thereof. The blowing agent combination of the present invention provides for thermoplastic foams having a density of less than 5 pounds per cubic foot (pcf), desirably 4.5pcf and less, preferrably less than 3pcf, even more preferrably less than 2pcf, and even more preferrably from about 1.5pcf to about 2pcf.

It was discovered that it is possible to produce low density foams, particularly of polystyrene, where the blowing agent is a combination of HFO-1234ze and at least one co-blowing agent selected from carbon dioxide, water, alkanes and an alcohol and mixtures thereof, where the foam density can be less 5pcf (80 kg/m³) and even about 4pcf (64 kg/m³) or less. It was also discovered that this can be done using less total blowing agent then previously demonstrated. It was found that foamable resin compositions containing less than 10wt% blowing agent could still achieve a foam density of less 5pcf. Previous work using HFO-1234ze disclosed using 10wt% to

14wt% total blowing agent to achieve foams of no less than 5pcf in density when using HFO-1234ze. The inclusion of co-blowing agents was found to provide for further reductions in foam density and improvements in foam properties and/or processibility

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The composition of the present invention can comprise about 50wt% or more tetrafluoropropene, preferably 60wt% or more tetrafluoropropene. The tetrafluoropropene is preferably 1,3,3,3-tetrafluoropropene, and even more preferably predominantly the trans-isomer of 1,3,3,3-tetrafluoropropene. The compositions would be useful in the production of thermal insulating foams, particularly thick-sectioned foams of greater than or equal to about ½ inch thick.

Preferred compositions of the present invention comprise from greater than about 5wt% CO<sub>2</sub> to about 90wt% CO<sub>2</sub>, preferably greater than 50wt%CO<sub>2</sub>, and more preferably greater than about 70wt% CO<sub>2</sub>, and the majority of the remaining blowing agent comprising 1234ze. Compositions may optionally contain an alcohol, preferably ethanol, from about 5wt% to less than about 40wt%, and/or less than from about 2wt% to about 15wt%, preferably less than 5wt% water. These compositions would be particularly useful in the production of thin sectioned insulating foams.

The open cell content of the foam of the present invention can be varied dependant on the specific combination and ratios of components of the blowing agent. Open cell contents of greater than 50% are achievable as well as open cell contents of from about 0% to less than about 30%. For applications such as thermal insulating foams and marine floatation, open cell contents of less than about 10% and most preferably less than about 5% are desired. The average cell size of the foam of the present invention can range from about 0.02mm to about 5mm, preferably form about 0.05 to about 1 m and most preferably from about 0.1 to about 0.5 mm.

Additional preferred blowing agent compositions for production of polymer foam comprise 5 to 50wt% CO<sub>2</sub>, preferably 5 to 25wt% CO<sub>2</sub>, and greater than 50wt%1234ze. Compositions may optionally contain an alcohol, preferably ethanol, from 5 to less than about 40wt% and/or less than 15wt% water, preferably less than 5wt% water. In one embodiment of the present invention, the blowing agent

compositions optionally contain between 1wt% and 15wt% water. These foams would be particularly useful in the production of thick-sectioned insulating foams.

Water can be used as an additional blowing agent for blends of 1234ze/CO2/water and 1234ze/CO2/ethanol/water. Water can be used from about 10wt% or less in the blends.

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The present invention will show that for CO<sub>2</sub>-rich formulations, 1234ze will improve the dimensional stability of the foam. Ethanol can further help to reduce density and provide enlargement in cell size and improve cell size uniformity.

For 1234ze-rich formulations, CO<sub>2</sub> will permit production of lower density

foam than 1234ze alone. Ethanol added to 1234ze and CO<sub>2</sub> combination will permit

production of even lower density foam but may increase the permeability of 1234ze

from the foam, so there will be an optimal quantity permissible and the level of CO<sub>2</sub>

or ethanol will likely depend on the level of the other.

Blends of 1234ze and HFC-152a (1,1-difluoroethane) are also particularly useful. Blends from around 25wt% to around 75wt% 1234ze will be preferred, particularly those around 50wt% 1234ze. Blowing agent blends of 1234ze and 152a at ratios of between 1:3 and 3:1, preferably of between 1:2 and 2:1, optionally with CO<sub>2</sub> at around 1 to 3wt% in the total formulation, and optionally with ethanol at around 10wt%, 20wt%, and 30wt% in the blowing agent formulation are be effective in accordance with the present invention.

Blends of 1234ze with alkanes are useful, particularly those with pentanes, including cyclopentane, normal pentane, isopentane, and mixtures thereof. Blends at around 50wt% 1234ze with various pentanes and from 0 to 3wt% CO<sub>2</sub> in the total formulation are effective in accordance with the present invention. In another embodiment of the present invention are blowing agent compositions comprising tetrafluoropropene and from about 5wt% to about 50wt% of an alkane.

In another embodiment of the present invention, the tetrafluoropropene in the blends described above is HFO-1234yf.

Foams described in the present invention can have a good skin quality, essentially free of defects, and can uniform cell size variations. Foam defects include, among others, blowholes and large voids, such as caused by undissolved blowing agent in the resin, and bubbles on the foam skin.

Another embodiment of this invention are foamable resin compositions containing greater than about 1 parts per hundred (pph) and less than about 100pph of the blowing agent composition with respect to resin, preferably greater than about 2pph and less than about 40pph, more preferably greater than about 3pph and less than about 25pph, and even more preferably greater than about 4 pph and less than about 15 pph of the blowing agent composition with respect to resin.

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The process for preparing a foamed thermoplastic product is as follows: Prepare a foamable polymer composition by blending together components comprising foamable polymer composition in any order. Typically, prepare a foamable polymer composition by plasticizing a polymer resin and then blending in components of a blowing agent composition at an initial pressure. A common process of plasticizing a polymer resin is heat plasticization, which involves heating a polymer resin enough to soften it sufficiently to blend in a blowing agent composition. Generally, heat plasticization involves heating a thermoplastic polymer resin near or above its glass transition temperature (Tg), or melt temperature (Tm) for crystalline polymers.

In one embodiment of the present invention the thermoplastic polymer composition comprises polymers containing styrene, ethylene, propylene, and mixtures thereof. In a preferred embodiment of the present invention, the thermoplastic polymer composition comprises polymers containing styrene, including, but not limited to, polystyrene, styrene-acrylonitrile copolymers, and mixtures thereof. In another embodiment of the present invention, the styrenic thermoplastic polymer composition comprises less than about 35wt% copolymerized acrylonitrile.

A foamable polymer composition can contain additional additives such as nucleating agents, cell-controlling agents, dyes, pigments, fillers,

antioxidants, extrusion aids, stabilizing agents, antistatic agents, fire retardants, IR attenuating agents and thermally insulating additives. Nucleating agents include, among others, materials such as talc, calcium carbonate, sodium benzoate, and chemical blowing agents such azodicarbonamide or sodium bicarbonate and citric acid. IR attenuating agents and thermally insulating additives can include carbon black, graphite, silicon dioxide, metal flake or powder, among others. Flame retardants can include, among others, brominated materials such as hexabromocyclodecane and polybrominated biphenyl ether.

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Foam preparation processes of the present invention include batch, semibatch, and continuous processes. Batch processes involve preparation of at least one portion of the foamable polymer composition in a storable state and then using that portion of foamable polymer composition at some future point in time to prepare a foam.

A semi-batch process involves preparing at least a portion of a foamable polymer composition and intermittently expanding that foamable polymer 15 composition into a foam all in a single process. For example, U.S. Pat. No. 4,323,528, herein incorporated by reference, discloses a process for making polyolefin foams via an accumulating extrusion process. The process comprises: 1) mixing a thermoplastic material and a blowing agent composition to form a 20 foamable polymer composition; 2) extruding the foamable polymer composition into a holding zone maintained at a temperature and pressure which does not allow the foamable polymer composition to foam; the holding zone has a die defining an orifice opening into a zone of lower pressure at which the foamable polymer composition foams and an openable gate closing the die orifice; 3) 25 periodically opening the gate while substantially concurrently applying mechanical pressure by means of a movable ram on the foamable polymer composition to eject it from the holding zone through the die orifice into the zone of lower pressure, and 4) allowing the ejected foamable polymer composition to expand to form the foam.

A continuous process involves forming a foamable polymer composition and then expanding that foamable polymer composition in a non-stop manner.

For example, prepare a foamable polymer composition in an extruder by heating

a polymer resin to form a molten resin, blending into the molten resin a blowing agent composition at an initial pressure to form a foamable polymer composition, and then extruding that foamable polymer composition through a die into a zone at a foaming pressure and allowing the foamable polymer composition to expand into a foam. Desirably, cool the foamable polymer composition after addition of the blowing agent and prior to extruding through the die in order to optimize foam properties. Cool the foamable polymer composition, for example, with heat exchangers.

Foams of the present invention can be of any form imaginable including sheet, plank, rod, tube, beads, or any combination thereof. Included in the present invention are laminate foams that comprise multiple distinguishable longitudinal foam members that are bound to one another.

The advantageous properties of the present invention can be referenced to the following examples, which illustrate but do no limit the present invention.

#### 15 EXAMPLES

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Extruded polystyrene foam was produced using a counter-rotating twin screw extruder with an internal barrel diameter of 27mm and a barrel length of 40 diameters. The screw design was suitable for foaming applications. The pressure in the extruder barrel was controlled with the gear pump and was set high enough such that the blowing agent dissolved in the extruder. The extruder die was an adjustable-lip slot die with a gap width of 6.35mm. A general purpose polystyrene resin (Total Petrochemicals PS-523W, MFI = 11) was used for the extrusion trials and fed to the extruder at controlled rates of about either 3.64 kg/hr (8 lb/hr) or 4.54 kg/hr (10 lb/hr). Blowing agents were pumped into the polystyrene resin melt at controlled rates using high-pressure delivery pumps. In the extruder, the blowing agent was mixed and dissolved in the resin melt to produce an expandable resin composition. The expandable resin composition was cooled to an appropriate foaming temperature and then extruded from the die where the drop in pressure initiates foaming. In some examples, talc was used as a nucleating agent and was pre-blended with polystyrene to make a masterbatch of 50wt% talc in polystyrene. Beads of this masterbatch were mixed with polystyrene pellets to achieve the desired wt% talc in each experiment.

A portable halocarbon detector was used to verify that there were no significant leaks of blowing agent from the extruder, such as out of the resin feed port, around the injector or pressure transducer ports, at adapter flanges, etc. Significant leaks of blowing agent from the extruder will result in uncertainty in the formulation or overestimation of the amount of blowing agent added. In all the examples no leak of blowing agent was detected.

Typical foam properties measured include density, open cell content, and cell size. Density was measured according to ASTM D792 or using a simple water displacement method, open cell content was measured using gas pychnometry according to ASTM D285-C, and cell size was measured by averaging the cell diameters from scanning electron microscope (SEM) micrographs of foam sample fracture surfaces. SEM images are also used to observe the cell structure and qualitatively check for open cell content.

#### COMPARATIVE EXAMPLES 1 - 3: E-HFO-1234ze Blown Foam

15 Comparative examples 1 through 3 were produced using E-HFO-1234ze (trans-1,3,3,3-tetrafluoropropene) as the blowing agent at loadings of 5.9wt%, 7.0wt%, and 7.9wt% respectively at a resin feed rate of 4.54 kg/m³. The density and average cell size of the resulting foams is shown in Table 1. Increasing the quantity of blowing agent above 5.9wt% did not result in a decrease in foam density when using essentially E-HFO-1234ze as the blowing agent. There were also increasing foam defects as the wt% of E-HFO-1234ze used as the blowing agent increased from 5.9wt% to 7.0wt% to 7.9wt%; at 7.9wt% there were noticeably more blowholes.

Table 1: E-HFO-1234ze Blown Foam

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Example	wt% 1234ze	Density (kg/m³)	Open Cell %	Avg. Cell Size (micron)
1	5.9	66.1	< 10%	~ 250
2	7.0	68.8	< 10%	~ 150
3	7.9	69.3	< 10%	~ 200
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### COMPARATIVE EXAMPLE 4: HFO-1234yf Blown Foam

Comparative example 4 was produced using HFO-1234yf (2,3,3,3-tetrafluoropropene) as the blowing agent at a loading of 5.7wt% at a resin feed rate of 4.54 kg/m<sup>3</sup>. The resulting foam had a density of 71.6 kg/m<sup>3</sup> (4.5pcf) and an open cell content of <15%.

#### COMPARATIVE EXAMPLE 5: HFC-134a / CO<sub>2</sub> Blown Foam

Comparative example 5 was produced using HFC-134a (1,1,1,2-tetrafluoroethane) as the blowing agent and carbon dioxide (CO<sub>2</sub>) as the coblowing agent at a resin feed rate of 3.64 kg/m<sup>3</sup>. HFC-134a was used at a loading of 5wt% and CO<sub>2</sub> was used at a loading of 1wt%. The foam had a density of 52.3 kg/m<sup>3</sup> (3.26pcf), average cell size of < 100 micron, but had numerous defects and blowholes. SEM images showed the foam to be highly open celled.

#### EXAMPLE 6: HFO-1234ze / CO<sub>2</sub> Blown Foam

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processing conditions, as Comparative Example 5 except that E-HFO-1234ze was used as the blowing agent in place of HFC-134a (1,1,1,2-tetrafluoroethane); carbon dioxide (CO<sub>2</sub>) was used as the coblowing agent. E-HFO-1234ze was used at a loading of 5.2wt% and CO<sub>2</sub> was used at a loading of 1wt%. The foam had a density of 55.6 kg/m<sup>3</sup> (3.47pcf), average cell size of < 100 micron, and had very few defects.

This is in contrast to Comparative Example 5, where at almost identical processing conditions and blowing agent loadings there were significant foam defects. SEM images showed the foam had relatively high open cell content but more uniform cell structure than Comparative Example 5.

#### EXAMPLE 7: HFO-1234ze / CO<sub>2</sub> Blown Foam

Example 6 was produced in the same manner as Example 6 except that E-HFO-1234ze was used at a loading of 4.5wt% and CO<sub>2</sub> was used at a loading of 1wt%. The foam had a density of 55.5 kg/m<sup>3</sup> (3.46pcf), an average cell size of < 100 micron, and had no obvious defects. SEM images showed the foam to be predominantly closed cell, having lower open cell content than Example 6.

#### EXAMPLE 8: HFO-1234ze / HFC-152a Blown Foam

Example 8 was produced in the same manner as Example 6 except that E-HFO-1234ze and HFC-152a (1,1-difluoroethane) were used as the blowing agents. E-HFO-1234ze was used at a loading of 5.0wt% and HFC-152a was used at a loading of 4.0wt%. The foam had a density of 50.6 kg/m<sup>3</sup> (3.16pcf) and had some blowholes.

#### EXAMPLE 9: HFO-1234ze / HFC-152a / CO<sub>2</sub> Blown Foam

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Example 9 was produced in the same manner as Example 8 except that CO<sub>2</sub> was used as a co-blowing agent. E-HFO-1234ze was used at a loading of 5.0wt%, HFC-152a was used at a loading of 4.0wt%, and CO<sub>2</sub> was used at a loading of 0.6wt%. The foam had a density of 50.5 kg/m<sup>3</sup> (3.15pcf) and had some blowholes.

#### EXAMPLE 10: HFO-1234ze / HFC-152a Blown Foam

Example 10 was produced in the same manner as Example 6 except that E-HFO-1234ze was used at a loading of 4.5wt% and HFC-152a was used at a loading of 1.8wt%. The foam had a density of 52.9 kg/m<sup>3</sup> (3.30pcf) and had no obvious defects.

#### 15 EXAMPLE 11: HFO-1234ze / Ethanol / CO<sub>2</sub> Blown Foam

Example 11 was produced in the same manner as Example 6 except that the blowing agent combination included E-HFO-1234ze, CO<sub>2</sub>, and dry ethanol (EtOH). E-HFO-1234ze was used at a loading of 7.0wt%, CO<sub>2</sub> was used at a loading of 0.6wt%, and ethanol was used at a loading of 2.0wt%. The foam had a density of 49.8 kg/m<sup>3</sup> (3.11pcf), an average cell size of < 50 micron, and had very few defects.

#### EXAMPLE 12: HFO-1234ze / Ethanol Blown Foam

Example 12 was produced in the same manner as Example 11 except that the blowing agent combination included only E-HFO-1234ze and dry ethanol (EtOH). E-HFO-1234ze was used at a loading of 7.1wt% and ethanol was used at a loading of 1.8wt%. The foam had a density of 50.7 kg/m<sup>3</sup> (3.16pcf), an average cell size of < 50 micron, and had no obvious defects.

## EXAMPLE 13: HFO-1234ze / Cyclopentane Blown Foam

Example 13 was produced in the same manner as Example 6 except that E-HFO-1234ze and cyclopentane (cC5) were used as the blowing agents. E-HFO-1234ze was used at a loading of 5.0wt% and cyclopentane was used at a loading of 4.0wt%. The foam had a density of  $40.2 \text{ kg/m}^3$  (2.51pcf) and had no obvious defects, had a large cross-section, and had enlarged cell size (> 250  $\mu$ m). SEM images showed the cell structure to be almost completely closed-cell. The backpressure at the extruder die was noticeably lower than with examples 1 through 12, at ~970 psig, indicating increased processibility.

The results of Examples 6 through 13 and Comparative Examples 1, 2, 3, and 5 are shown in Table 2. The examples show that the blowing agent combinations of the present invention permit the production of polystyrene foam of lower density and/or larger cell size than when using tetrafluoropropene as the only blowing agent.

Table 2:

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	Blowing Agent Loading						Foam Properties	
Example	134a (wt%)	1234ze (wt%)	CO2 (wt%)	152a (wt%)	EtOH (wt%)	cC5 (wt%)	Density (kg/m³)	Comments
Comp. 1	-	5.9	-	-	-	-	66.1	Very few defects
Comp. 2	-	7.0	-	-	-	-	68.8	Few defects
Comp. 3	-	7.9	-	-	-	- }	69.3	Some blowholes
Comp. 5	5.0	-	1.0	-	-	-	52.3	Defects, blowholes
6	-	5.2	1.0	-	-	-	55.6	Very few defects
7	-	4.5	1.0	-	-	-	55.5	No defects
8	-	5.0	-	4.0	-	-	50.6	Some blowholes
9	-	5.0	0.6	4.0	-	-	50.5	Some blowholes
10	•	4.5	-	1.8	-	-	52.9	No defects
11	-	7.0	0.6		2.0	-	49.8	Very few defects
12	-	7.1	-	-	1.8	-	50.7	No defects
13	-	5.0	-	-	-	4.0	40.2	No defects

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Although the invention is illustrated and described herein with reference to specific embodiments, it is not intended that the appended claims be limited to the details shown. Rather, it is expected that various modifications may be

made in these details by those skilled in the art, which modifications may still be within the spirit and scope of the claimed subject matter and it is intended that these claims be construed accordingly.

#### Claims

1. A blowing agent composition for thermoplastic foaming comprising tetrafluoropropene and at least one co-blowing agent selected from carbon dioxide, water, alkanes, 1,1-difluoroethane, an alcohol or mixtures thereof.

- 2. The blowing agent composition of claim 1 where the alcohol is ethanol.
- 3. The blowing agent composition of claim 1 where the alkane is selected from pentanes, butanes or mixtures thereof.
- 4. The blowing agent composition of claim 1 wherein said tetrafluoropropene is HFO-1234ze.
- 5. The blowing agent composition of claim 4 where the HFO-1234ze is essentially the trans isomer.
- 6. The blowing agent composition of claim 1 wherein said tetrafluoropropene is HFO-1234yf.
- 7. The blowing agent composition of claim 1 comprising about 50wt% or more tetrafluoropropene.
- 8. The blowing agent composition of claim 1 comprising between about 5wt% and about 90wt% carbon dioxide.
- 9. The blowing agent composition of claim 2 comprising between about 5wt% or about 40wt% or less ethanol.
- 10. The blowing agent composition of claim 1 comprising between about 1wt% and about 15wt% water.
- 11. The blowing agent composition of claim 1 comprising tetrafluoropropene and 1,1-difluoroethane at a ratio of between about 1:3 and about 3:1 respectively.
- 12. The blowing agent composition of claim 1 comprising tetrafluoropropene and 1,1-difluoroethane at a ratio of between about 1:2 and about 2:1 respectively.

13. The blowing agent composition of claim 1 comprising about 5wt% to about 50wt% of an alkane.

- 14. The blowing agent composition of claim 1 wherein said alkane is a pentane, a butane, or mixtures thereof.
- 15. The blowing agent composition of claim 1 further comprising nucleating agents, cell-controlling agents, dyes, pigments, fillers, antioxidants, extrusion aids, stabilizing agents, antistatic agents, fire retardants, IR attenuating agents, thermally insulating additives, and mixtures thereof.
- 16. A foamable resin composition comprising a thermoplastic resin and a blowing agent comprising tetrafluoropropene and at least one co-blowing agent selected from carbon dioxide, water, alkanes, an alcohol or mixtures thereof.
- 17. The foamable resin composition of claim 16 containing less than about 10wt% of the tetrafluoropropene.
- 18. The foamable resin composition of claim 16 wherein said thermoplastic resin is selected from polystyrene, polyethylene, polypropylene, styrene-acrylonitrile copolymer or mixtures thereof.
- 19. An alkenyl aromatic polymer foam comprising a foamable resin and a blowing agent composition comprising tetrafluoropropene and at least one co-blowing agent selected from carbon dioxide, water, alkanes, an alcohol or mixtures thereof
- 20. The polymer foam of claim 19 having a density of between about 1.5 pounds per cubic foot and about 5 pounds per cubic foot.
- 21. The polymer foam of claim 19 having an open cell content of less than about 50%.
- 22. The polymer foam of claim 19 having an average cell size of from about 0.02mm to about 5mm

## INTERNATIONAL SEARCH REPORT

International application No. PCT/US 10/22306

A. CLASSIFICATION OF SUBJECT MATTER IPC(8) - C09K 5/00 (2010.01) USPC - 252/71 According to International Patent Classification (IPC) or to both national classification and IPC						
	Minimum documentation searched (classification system followed by classification symbols)					
	USPC-252/71,67,68,2,364					
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched						
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) Data bases: Pubwest (PGPB, USPT, EPAB, JPAB); Google Patents, Google Scholar Terms: ethanol, blowing agent, foaming agent, resin, tetrafluoropropene, HFO 1234ze, HFO 1234yf, butane, alkane, CO2, carbon dioxide, water, H2O, weight percent, 1,1-difluoroethane, polystyrene, density, cell size, alkenyl aromatic, thermoplastic						
C. DOCUI	MENTS CONSIDERED TO BE RELEVANT					
Category*	Citation of document, with indication, where ap	Relevant to claim No.				
X	US 2008/0125505 A1 (BOWMAN et al.) 29 May 2008 ( 0047, 0051, 0064-0066, 0071-0072, 0097-0099, 0103]	1-22				
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Furthe	er documents are listed in the continuation of Box C.					
"A" docume	categories of cited documents: ent defining the general state of the art which is not considered particular relevance	"T" later document published after the intendate and not in conflict with the applic the principle or theory underlying the i	ation but cited to understand			
"E" earlier a	pplication or patent but published on or after the international ate	"X" document of particular relevance; the considered novel or cannot be considered step when the document is taken alone	claimed invention cannot be ered to involve an inventive			
cited to special	ent which may throw doubts on priority claim(s) or which is o establish the publication date of another citation or other reason (as specified)	"Y" document of particular relevance; the considered to involve an inventive s	claimed invention cannot be step when the document is			
means "P" docume	ent referring to an oral disclosure, use, exhibition or other	combined with one or more other such obeing obvious to a person skilled in the "&" document member of the same patent	e art			
	ority date claimed	Date of mailing of the international search	ch report			
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Mail Stop PC	nailing address of the ISA/US T, Attn: ISA/US, Commissioner for Patents	Authorized officer:  Lee W. Young				
P.O. Box 1450, Alexandria, Virginia 22313-1450 Facsimile No. 571-273-3201		PCT Helpdesk: 571-272-4300 PCT OSP: 571-272-7774				