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(57) Abrégé/Abstract:

An improved acoustical damping wall (ceiling or floor) or door material comprises a laminar structure having as an integral part thereof one or more layers of viscoelastic material which also functions as a glue and one or more constraining layers, such as metal, cellulose, wood, or petroleum-based products such as plastic, vinyl, plastic or rubber. In one embodiment, standard wallboard, typically gypsum, comprises the external surfaces of the laminar structure; and one or more constraining layers are fabricated between the gypsum exterior. The resulting structure improves the attenuation of sound transmitted through the structure.





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(54) Title: ACCOUSTICAL SOUND PROOFING MATERIAL AND METHODS FOR MANUFACTURING SAME

(57) Abstract: An improved acoustical damping wall (ceiling or floor) or door material comprises a laminar structure having as an integral part thereof one or more layers of viscoelastic material which also functions as a glue and one or more constraining layers, such as metal, cellulose, wood, or petroleum-based products such as plastic, vinyl, plastic or rubber. In one embodiment, standard wallboard, typically gypsum, comprises the external surfaces of the laminar structure; and one or more constraining layers are fabricated between the gypsum exterior. The resulting structure improves the attenuation of sound transmitted through the structure.

ACCOUSTICAL SOUND PROOFING MATERIAL AND METHODS FOR MANUFACTURING SAME

FIELD OF THE INVENTION

This invention relates to acoustical damping materials and, in particular, to soundproofing materials of a novel laminar construction which significantly improves the soundproofing ability of walls, ceilings, floors, and doors, thereby to prevent the transmission of sounds from one area to another.

BACKGROUND OF THE INVENTION

Noise is emerging as both an economic and public policy issue. Soundproof rooms are required for a variety of purposes. For example, apartments, hotels and schools all require rooms with walls, ceilings and floors that minimize the transmission of sound thereby to avoid annoying people in adjacent rooms. Soundproofing is particularly important in buildings adjacent to public transportation, such as highways, airports and railroad lines, as well as theaters, home theaters, music practice rooms, recording studios and others. One measure of the severity of the problem is the widespread emergence of city building ordinances that specify minimum Sound Transmission Class ("STC") rating. Another measure is the broad emergence of litigation between homeowners and builders over the issue of unacceptable noise. To the detriment of the U.S. economy, both problems have resulted in major builders refusing to build homes, condos and apartments in certain municipalities; and in widespread cancellation of liability insurance for builders.

In the past, walls typically were made up of studs with drywall on both exterior surfaces of the studs and baffles or plates commonly placed between the studs in an attempt to reduce the transmission of sound from one room to the next.

Unfortunately, even the best of such walls using standard

drywall are capable of only reducing sound transmission by approximately 30db, and much of that is focused on mid-range and high frequencies rather than lower frequencies which cause most of the complaints and litigation.

Various techniques and products have emerged to abate this problem,

such as: replacement of wooden studs by steel studs; resilient channels to offset and
isolate drywall panels from studs; mass-loaded vinyl barriers; cellulose sound-board;
cellulose and fiberglass batt insulation; and techniques such as staggered-beam and
double-beam construction. All help reduce the transmission of noise, but, again, not
to such an extent that certain sounds (e.g., lower frequencies, high decibel) in a given
room are prevented from being transmitted to an adjacent room, including rooms
above or below. A brief review of commercially available products shows that there
has been little innovation in these techniques and technologies for many years.

Accordingly, what is needed is a new material and a new method of construction to reduce the transmission of sound from a given room to an adjacent room.

SUMMARY OF THE INVENTION

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In accordance with some embodiments of this invention, a new laminar and associated manufacturing process is provided which may significantly improve the ability of a wall, ceiling, floor or door to reduce the transmission of sound from one room to an adjacent room, or from the exterior to the interior of a room, or from the interior to the exterior of a room.

Some embodiments disclosed herein relate to a laminar structure used for constructing walls, floors, or ceilings or doors comprising: two external layers of a material, at least one internal constraining layer, and two or more internal layers of a viscoelastic glue separated by said at least one internal constraining layer; wherein the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

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Some embodiments disclosed herein relate to a laminar structure comprising: at least one internal layer of a selected material; two internal layers of a viscoelastic glue, one such layer on each side of said internal layer; and at least one additional layer on the other side of each of the at least one of the internal layers of viscoelastic glue; wherein the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

Some embodiments disclosed herein relate to the method of forming a laminar structure which comprises: providing a layer of first material having two surfaces; placing a layer of viscoelastic glue onto one surface of said layer of first material; placing a layer of a second material over said viscoelastic glue; pressing said layer of second material against said layer of viscoelastic glue and said layer of first material for a selected time; and drying said layer of second material, said layer of first material and said viscoelastic glue; wherein the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

Some embodiments disclosed herein relate to the method of forming a laminar structure which comprises: providing a layer of first material having two surfaces; placing a layer of viscoelastic glue onto one surface of said layer of first material; placing a layer of a second material, which is 1/10th to 1/2 the thickness of the first material over said viscoelastic glue; pressing said layer of second material against said layer of viscoelastic glue and said first material for a selected time; and drying said layer of second material, said layer of first material and said viscoelastic glue; wherein the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

Some embodiments disclosed herein relate to the method of forming a laminar structure which comprises: providing a layer of first material having two surfaces; placing a layer of viscoelastic glue onto one surface of said layer of first material; placing a layer of a second material over said viscoelastic glue; pressing said layer of second material against said layer of viscoelastic glue and said first material for a selected time; and drying said layer of second material, said layer of

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first material and said viscoelastic glue; wherein the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

Some embodiments disclosed herein relate to a laminar, soundabsorbing structure which comprises: a layer of first material having two surfaces; a layer of viscoelastic glue on one surface of said layer of first material; and a layer of a second material over said viscoelastic glue; wherein the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

The material comprises a lamination of several different materials. In accordance with one embodiment, a laminar substitute for drywall comprises a sandwich of two outer layers of selected thickness gypsum board which are glued each to an interior constraining layer, such as a metal, cellulose (e.g., wood) or petroleum-based product such as vinyl, composite plastic or rubber, using a sound absorbent adhesive. In one embodiment, the constraining layer comprises a selected

thickness galvanized steel and the glue layer is a specially formulated QuietGlue of a specific thickness which is a viscoelastic material. Formed on the interior surfaces of the two gypsum boards, the glue layers are each about 1/16 inch thick and the galvanized steel between .005 and .5 inch thick. In one instance, a 4 foot x 8 foot panel constructed using a 1/16" layer of glue and 30 gauge galvanized steel weighs approximately 108 pounds versus the weight of a typical drywall of the same thickness of about 75 pounds, has a total thickness of approximately 5/8 inches and has an STC of approximately 38. The double-sided standard construction using this particular material will give an STC of approximately 58. The result is a reduction in noise transmitted through the wall of approximately 60 db compared to a 30 db reduction of transmitted noise using standard commercially available drywall.

In one embodiment, the galvanized steel metal layer is preferably not oiled and of regular spackle. The resulting product, even though it contains the galvanized steel center sheet, can be cut with a standard hand saw using wood blades, but cannot be scribed and broken like ordinary drywall.

Another embodiment of this invention uses additional layers of material and is non-symmetric. Two external gypsum board layers have directly adjacent their faces layers of quiet glue, followed by two metal layers, followed by two additional layers of glue, and then a central piece of laminated wood (in one embodiment a layer of laminated wood of the type used in plywood). The total finished thickness of this structure can vary, but the additional two layers of metal result in a significant increase in the attenuation of sound passing through the material.

The laminated sheets of this invention use unique glues capable of substantially absorbing sound and vibration together with one or more constraining layers which reduce the transmissibility of the sound from one layer to the adjacent layers of material. The constraining layers can be metal,

cellulose, wood, plastic composites, vinyl or other porous or semi-porous materials. The resulting attenuation of sound is significantly improved compared to the attenuation of sound obtained using standard drywall.

DETAILED DESCRIPTION OF THE DRAWINGS

This invention will be more fully understood in light of the following drawings taken together with the following detailed description.

- FIG. 1 shows a laminar structure fabricated in accordance with this invention for reducing the transmission of sound through the material.
- FIG. 2 shows a second embodiment of a laminated structure containing nine (9) layers of material capable of significantly reducing the transmission of sound through the material.
- FIGS. 3 and 4 show alternative embodiments of this invention capable of reducing the transmission of sound through the material.
- Figs. 5-10 show sound attenuation test results on several embodiments of this invention.

DETAILED DESCRIPTION

The following detailed description is meant to be exemplary only and not limiting. Other embodiments of this invention — such as the number, type, thickness and placement order of both external and internal layer materials — will be obvious to those skilled in the art in view of this description.

The process for creating such laminar panels takes into account many factors: exact chemical composition of the glue; various symmetric and non-symmetric thicknesses of glue and layered material; pressing process; drying and dehumidification process.

FIG. 1 shows the laminar structure of one embodiment of this invention. In FIG. 1, the layers in the structure will be described from top to bottom with the structure oriented horizontally as shown. It should be understood, however, that the laminar structure of this invention will be oriented vertically when placed on vertical walls and doors, as well as horizontally or even at an angle when placed on ceilings and floors. Therefore, the reference to top and bottom layers is to be understood to refer only to these layers as oriented in FIG. 1 and not in the context of the vertical use of this structure. In FIG. 1, the top layer 11 is made up of a standard gypsum material and in one embodiment is 1/4 inch thick. Of course, many other combinations and thicknesses can be used for any of the layers as desired. The thicknesses are limited only by the acoustical attenuation (i.e., STC rating) desired for the resulting laminar structure and by the weight of the resulting structure which will limit the ability of workers to install the laminar layer on walls, ceilings, floors and doors for its intended use.

The gypsum board in top layer 11 typically is fabricated using standard well-known techniques and thus the method for fabricating the gypsum board will not be described. Next, on the bottom of the gypsum board 11 is a layer of glue 12 called "QGquiet glue". Glue 12, made of a unique viscoelastic polymer, has the property that the energy in the sound which strikes the glue, when constrained by surrounding layers, will be significantly absorbed by the glue thereby reducing the sound's amplitude across a broad frequency spectrum, and thus the energy of sound which will transmit through the resulting laminar structure. Typically, this glue is made of the materials as set forth in TABLE 1, although other glues having the characteristics set forth directly below Table 1 can also be used in this invention.

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TABLE 1

Quiet Glue™ Chemical Makeup

	WEIGI	HT 8
Components		
	Min	Max
acetaldehyde	0.00001%	0.00010읭
acrylate polymer	33.00000%	65.00000위
acrylonitrile	0.00001원	0.00100왕
ammonia ,	0.00100%	0.01000읭
bis(1-hydroxy-2-pyridinethionato) Zinc	0.01000%	0.10000%
butyl acrylate	0.00100%	0.100008
butyl acrylate, methyl methacrylate, styrene, methacrylic acid 2-		
hydroxyethyl acrylate polymer	5.00000%	15.000008
CI Pigment Yellow 14	0.01000읭	0.02000응
ethyl acrylate	0.0001%	0.00010%
ethyl acrylate, methacrylic acid, polymer with ethyl-2-propenoate	1.00000응	5.00000%
formaldehyde	0.00100%	0.01000%
hydrophobic silica	0.00100왕	0.01000%
paraffin oil	0.10000%	1.000008
polymeric dispersant	0.00100%	0.01000%
potassium tripolyphosphate	0.00000%	0.00200%
silicon dioxide	0.00100%	0.10000%
sodium carbonate	0.01000%	0.10000%
stearic acid, aluminum salt	0.00100%	0.10000%
surfactant	0.00100%	0.10000%
vinyl acetate	0.10000%	1.000008
water	25.00000%	40.000008
zinc compound	0.00100%	0.10000%

The physical solid-state characteristics of QuietGlue include:

- 1) a broad glass transition temperature below room temperature;
 - 2) mechanical response typical of a rubber (i.e., high

elongation at break, low elastic modulus);

- 3) strong peel strength at room temperature;
- 4) weak shear strength at room temperature;
- 5) swell in organic solvents (e.g., Tetrahydrofuran, Methanol);
 - 6) does not dissolve in water (swells poorly);
- 7) peels off the substrate easily at temperature of dry ice.

Following glue layer 12 is a metal layer 13. Metal layer 13 is, in one embodiment, 30 gauge galvanized steel of .013 inch thickness. Of course, other gauge galvanized steel and even other metals can be used if desired. For example, aluminum can also be used if desired, as can specialty metals such as sheets of ultra-light weight titanium and laminated layers of metal including laminates of aluminum and titanium. Of importance is that galvanized steel, if used, be non-oiled and of regular spackle. Non-oil is required to insure that the QuietGlue layer 12 will adhere to the top surface of metal layer 13 and the adjacent QuietGlue layer 14 on the bottom of metal layer 13 will also adhere to the surfaced metal 13. Regular spackle insures that the metal has uniform properties over its whole area.

Next, glue layer 14 is placed in a carefully controlled manner with respect to coverage and thickness on the bottom of metal layer 13. Glue layer 14 is again a viscoelastic material which absorbs sound and is typically the same material as glue layer 12. Finally, gypsum board layer 15 is placed on the bottom of the structure and carefully pressed in a controlled manner with respect to uniform pressure (pound per square inch), temperature and time

Finally, the assembly is subjected to dehumidification and drying to allow the panels to dry, typically for forty-eight (48) hours.

Typically, but not always, gypsum board layers 11 and 15 will contain fiber to reduce shrinkage so that the resulting laminar structure will meet fire codes. Typical fire codes

require a wall structure capable of withstanding flames for up to one hour. The metal core, together with the external gypsum board layers are intended to give to the resulting laminar structure a minimum of one hour resistance to fire, and possibly as high as four (4) hours in certain configurations, and thereby allows the resulting structure to meet typical fire codes.

Metal layer 13, typically 30-gauge steel (but may be other metals, ranging from 10 gauge to 40 gauge, depending on weight, thickness, and STC desired), is about the thickness of a business card. Of importance, before assembling, this metal should not be creased because creasing will ruin the ability of this metal to assist in reducing the transmission of sound. Only completely flat, undamaged pieces of metal can be used in the laminar structure.

In an alternative embodiment, steel 13 is replaced by mass-loaded vinyl or similar product. However, the steel has much less forgiveness than vinyl and thus can outperform vinyl as a constraining layer. However, for other ease-of-cutting reasons, vinyl can be used in the laminar structure in place of steel, if desired. Cellulose, wood, gypsum, plastic or other constraining materials may also be used in place of vinyl or metal. The alternative material can be any type and any appropriate thickness.

The resulting structure is capable of being cut using standard wood saws with wood blades.

FIG. 2 shows a second embodiment of this invention. Two external layers 21 and 29 of gypsum board have coated on each of their interior faces a layer of QuietGlue 22 and 28, respectively, preferably made of a viscoelastic polymer, such as glue 12 in Fig. 1. Such a viscoelastic polymer has the ability to absorb sound energy through deformation of the viscoelastic material in response to the acoustic energy of the sound. On the interior faces of the QuietGlue are two sheet metal layers 23 and 27. Typically, these sheet metal layers 23 and 27 are each galvanized steel. In one embodiment, the galvanized steel

is 30 gauge, .013 inches thick, but other thicknesses of steel, as well as other metals, can also be used as desired. The interior faces of the steel layers 23 and 27 are coated with additional layers 24 and 26, respectively, of quiet glue, again a viscoelastic material of the same type as glue layers 22 and 28. Then the core of the structure is made up of a pine laminar sheet 25 which is of a type commonly used in plywood. In one embodiment, the pine laminar sheet is $1/10^{th}$ of an inch thick, but may also be MDF or other wood types.

Again, the galvanized steel is non-oiled and regular spackle for the reasons discussed above in conjunction with the embodiment of Fig. 1. The layers of glue are all viscoelastic material capable of absorbing sound. The resulting product has a thickness of approximately 7/8th of an inch and weighs approximately 148 pounds per 4 x 8 section. The stand-alone STC for the resulting material is 42 which yields a double-sided standard construction STC of 62. The steel layers should not be creased before assembly. Creasing of the steel may ruin the steel for its intended purpose. Using completely flat pieces undamaged is required to achieve optimal results. The resulting structure again is cutable with a standard power saw using wood blades. The interior layer 25 of wood is in one embodiment Sierra pine 1/10th inch thick MDF acquired in Rocklin, California (http://www.sierrapine.com).

In fabricating the structures of Figs. 1 and 2, the glue is first rolled in a prescribed manner, typically to 1/16 inch thickness, although other thicknesses can be used if desired, onto the gypsum and then steel is laid on the glue. Depending on the drying and dehumidification techniques deployed, anywhere from 10 to 30 hours are required to dry totally the glue in the case that the glue is water-based. A solvent-based viscoelastic glue can be substituted. The resulting structure is dried in a prescribed manner under a pressure of approximately 2 to 5 pounds per square inch, depending on the exact requirements of each assembly, although other pressures can be used as desired.

To make the embodiment of Fig. 2, each of the gypsum board-glue-metal layer structures has an additional layer of glue rolled onto the exposed surface of the metal to approximately $1/16^{\rm th}$ inch thickness and then the thin pine wood layer is placed between the two layers of glue on the already fabricated gypsum-glue-metal sheets. The resulting structure is placed in a press and 1 to 5 pounds per square inch of pressure is applied to the structure and up to 48 hours is allowed for drying.

Fig. 3 shows another embodiment of the acoustical soundproofing material of this invention. In Fig. 3, two external layers of gypsum board 30 and 34 have on their interior faces glue layers 31 and 33, respectively. Between the two glue layers 31 and 33 is a constraining material 32 made up of vinyl. This vinyl is mass loaded and, in one embodiment, is 1 pound per square foot or greater, and is available from a number of manufacturers, including Technifoam, Minneapolis, Minnesota. The total weight of this structure when the external layers 30 and 34 of gypsum board are each 5/8 inch thick, the layers of viscoelastic QuietGlue 31 and 33 are each approximately 1/16 of an inch thick and the mass loaded vinyl is approximately 1/32 of an inch thick, is about 190 pounds per 4 x 8 foot section. The total finished thickness of the material is 1.3 to 1.5 inches depending on the thickness of the vinyl and the actual thicknesses of the viscoelastic QuietGlue layers 31 and 33.

The embodiment of Fig. 3 cannot be scored like regular drywall, but rather must be cut using a wood saw. A typical wood saw blade is adequate to actually cut the soundproofing material of Fig. 3.

Fig. 4 shows an additional embodiment of the soundproofing material of this invention. In this embodiment, two external layers 35 and 39 are 5/8 inch plywood and have on their interior faces layers 36 and 38 of quiet glue, respectively. Between the QuietGlue is a layer of mass loaded vinyl 37. The structure shown in Fig. 4 is meant to be used on floors or in other construction areas where wood would normally be used. The

plywood sheets 35 and 39 are each typically 5/8 inch thick in one embodiment. In this embodiment, the layers of QuietGlue 36 and 38 are each approximately 1/16 inch thick (although other thicknesses can be used if desired) and the mass loaded vinyl 37 is typically 1/16 to 1/4 inch thick. When the mass loaded vinyl is 1/8 inch thick, then the total thickness of the structure of Fig. 4 is approximately 1.5 inches thick. If the vinyl is 1/16 inch thick, then the total thickness is approximately 1.4 inches.

The structure of Fig. 3 standing alone has an STC of 38, while the structure of Fig. 4 has an STC of 36. The structures of Figs. 1 and 2 have STCs of 37 and 38, respectively.

It is noted that uneven application of QuietGlue or leaving an air gap at the ends of the sheets of soundproofing material described above may hurt the STC ratings by several db.

Moreover, to improve the soundproofing qualities of walls, floors, ceilings or doors made with these materials, glue must be evenly applied all the way to the ends and corners of the sheets. None of the panels described above can be scored like regular drywall. Rather, these panels must be cut using a saw blade, typically a wood saw blade.

The sound transmission class numbers given above basically are numbers which are used in the architectural field to rate partitions, doors and windows for their effectiveness in blocking sound. The number assigned to a particular partition design as a result of STC testing represents a best fit type of approach to a set of curves that define the sound transmission class. The test is conducted in such a way to make it independent of the test environment and gives a number for the partition only. The STC measurement method is defined by ASTM E90 laboratory test for sound measurements obtained in 1/3 octave bands, and ASTM E413 for calculating "STC" (Sound Transmission Class) numbers from the sound transmission loss in each partition, and these standards are available on the internet at http://www.astm.org.

Data showing the transmission loss in decibels as a function of frequency for the soundproofing material of this invention is set forth in Figs. 5, 6, 7, 8, 9 and 10. Fig. 5 shows a standard 2 x 4 construction with Quiet Rock Ultra, as shown in Fig. 3, on both sides of studs with no insulation. The transmission loss in decibels varies from 25 db at 63 Hz to approximately 58 db at 4,000 Hz.

The center frequency of octave bands is set forth in the two rows of the table. The top line of each row represents the 1/3 octave band center frequency. The second row of numbers in each horizontal category represents the total in db, and the third set of numbers represents a 95% confidence level in db deficiencies. The EWR and OITC stand for External Wall Rating and Outdoor-Indoor Transmission Class, respectively, and represent other methods of measuring transmission loss. The final sound transmission class number is set forth under the notation STC in the lower right corner. For the use of two panels of the type shown in Fig. 3, on both sides of standard 2" x 4" wood stud construction, the STC is 54.

It is known to those practicing in this field that a similar configuration with standard 5/8 inch drywall on both sides of standard 2 x 4 construction yields an STC of 34. Accordingly, this invention yields a 20 STC point improvement over standard drywall in this particular construction.

The National Research Council of Canada (NRC) has documented the STC rating of many other configurations (e.g., using wood and steel studs in standard, staggered beam or double beam construction with various isolators such as resilient channels and with various acoustic insulation fillers such as sound board, cellulose and fiberglass batt). This invention has been subjected to the same types of tests.

The use of a single panel, alone, of the type shown in Fig. 3 yields an STC of 38, as shown in the bottom right corner of Fig. 6. Thus, the use of the single panel of the type shown in Fig. 1 to reduce sound transmission is less effective than the

use of two panels on both sides of 2×4 studes as shown in Fig. 5.

The use of the structure shown in Fig. 4 on both sides of standard 2 x 4 construction results in an STC of 49, as shown in Fig. 7. This indicates that the wood structure shown in Fig. 4 is less effective in reducing sound transmission than the structure shown in Fig. 3, which contains gypsum board on the external surfaces together with an internal layer of vinyl, though both are significant improvements over standard materials.

Fig. 8 shows that the use of the wood structure in Fig. 4 on 2 x 4 studs alone, with no insulation, has an STC of 49, which is lower than the STC rating given to the structure of Fig. 3 in a similar configuration. It is known to those practicing in this field that a similar wall with standard plywood on both sides yields an STC rating of 29. Thus, this represents a significant improvement over standard wood.

The use of the structure of Fig. 4 on one side with no insulation with standard 2 x 4 construction results in an STC of 43, as shown in the graph of Fig. 9. This is a substantial improvement in sound attenuation over standard plywood, but not as good as use of standard 2 x 4 construction with the structure of Fig. 4 on both sides of the studs, as shown in Fig. 85. Finally, the use of the structure of Fig. 4 alone results in an STC of 36 as shown in Fig. 10, which is below the STC of 38 (Fig. 6) for the structure of Fig. 3 in a similar configuration.

Accordingly, the laminar structure of this invention provides a significant improvement in the sound transmission class number associated with the structures and thus reduces significantly the sound transmitted from one room to adjacent rooms.

An alternative embodiment of this invention is asymmetric, being made up of a relatively thick layer of material on one surface of which is placed viscoelastic glue. Over the viscoelastic glue is placed a thin layer of material relative to

the first layer of material. This thin layer of material can be a constraining layer, such as metal or vinyl or rubber or any other appropriate thin material. This structure has sound reducing qualities, but is lighter and easier to handle than the structures described in Figs. 1 through 4. Such a structure, for example, could be made up of layers 11, 12 and 13 of the structure shown in Fig. 1.

The dimensions given for each material in the laminar structures of this invention can be varied as desired to control cost, overall thickness, weight and STC results. The described embodiments and their dimensions are illustrative only and not limiting.

Other embodiments of this invention will be obvious in view of the above description.

CLAIMS:

1. A laminar structure used for constructing walls, floors, or ceilings or doors comprising:

two external layers of a material,

5 at least one internal constraining layer, and

two or more internal layers of a viscoelastic glue separated by said at least one internal constraining layer; wherein

the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

- 10 2. The laminar structure as in claim 1, wherein the constraining layer comprises metal.
 - The laminar structure as in claim 1, wherein said two external layers comprise each a selected thickness gypsum board layer.
- 4. The laminar structure as in claim 3, wherein said glue comprises a viscoelastic material capable of absorbing sound.
 - 5. The laminar structure as in claim 4, wherein said at least one internal constraining layer comprises a sheet metal layer of selected thickness.
 - The laminar structure as in claim 5, wherein said sheet metal layer of selected thickness comprises galvanized steel.
- 20 7. A laminar structure comprising:

at least one internal layer of a selected material;

two internal layers of a viscoelastic glue, one such

layer on each side of said internal layer; and

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at least one additional layer on the other side of each of the at least one of the internal layers of viscoelastic glue; wherein

the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

- 5 8. The laminar structure as in claim 7 wherein said at least one additional layer comprises an external layer of a first sound
 - 9. The laminar structure as in claim 8 wherein said external layer of a first sound absorbing material comprises gypsum.
- 10. The laminar structure as in claim 8 wherein said at least one external layer comprises a plurality of layers of selected materials.
 - The laminar structure as in claim 10 wherein said plurality of layers of selected materials comprise:
 - a first layer of metal;
 - a second layer of viscoelastic glue; and
- a third layer of selected material.
 - The laminar structure as in claim 11 wherein said third layer of selected material comprises gypsum.
 - 13. The laminar structure as in claim 7 wherein said at least one internal layer comprises a metal layer.
- 20 14. The laminar structure as in claim 7 wherein said at least one internal layer comprises a layer of a cellulose material.
 - The laminar structure as in claim 7 wherein said at least one internal layer comprises a layer of a solid petroleum-based synthetic material selected from a group consisting of a vinyl, plastic composite, or rubber.

16. The method of forming a laminar structure which comprises:

providing a layer of first material having two surfaces;

placing a layer of viscoelastic glue onto one surface of said layer of first material;

placing a layer of a second material over said viscoelastic glue;

pressing said layer of second material against said layer of viscoelastic glue and said layer of first material for a selected time; and

drying said layer of second material, said layer of first material and said viscoelastic glue; wherein

the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

17. The method of claim 16, including:

providing an internal layer of material or multiple layers of selected materials;

forming a layer of viscoelastic glue on each of what are to be internal surfaces of two or more laminar structures formed using the steps of claim 16;

placing two or more such laminar structures with the two or more to-be internal surfaces adjacent said internal layer or said multiple layers;

pressing the composite structure formed in the preceding step at a selected pressure for a selected time; and

drying the composite structure being pressed.

The method of claim 16 wherein said first material comprises a metal layer, and said second material comprises a gypsum layer.

- 19. The method of claim 17 wherein said internal layer comprises a cellulose-based layer.
- 20. The method of claim 17 wherein said cellulose-based layer is wood.
- The method of claim 17 wherein said internal layer comprises a layer selected from the group consisting of vinyl, plastic composite, and rubber.
 - The method of claim 17 wherein said internal layer comprises a metal layer selected from the group consisting of galvanized steel, stainless steel, aluminum, titanium, and a composite of two or more metals.
- The method of claim 22 wherein said metal layer comprises galvanized steel.
 - The laminar structure as in claim 1 wherein the internal constraining layer is a cellulose product.
 - The laminar structure as in claim 24 wherein said cellulose product is wood.
- The laminar structure as in claim 1 wherein said at least one internal constraining layer is selected from the group consisting of cellulose, wood, metal, plastic, vinyl, plastic composite and rubber.
 - The method of forming a laminar structure which comprises: providing a layer of first material having two surfaces;
- placing a layer of viscoelastic glue onto one surface of said layer of first material;
 - placing a layer of a second material, which is 1/10th to 1/2 the thickness of the first material over said viscoelastic glue;

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pressing said layer of second material against said layer of viscoelastic glue and said first material for a selected time; and

drying said layer of second material, said layer of first material and said viscoelastic glue; wherein

- the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.
 - The method of claim 27 wherein said first material comprises a gypsum layer, and said second material comprises a metal layer.
- The method of claim 27 wherein said first material comprises a gypsum layer, and said second material comprises a layer selected from the group consisting of plastic and a plastic composite layer.
 - The method of claim 27 wherein said first material comprises a gypsum layer, and said second material comprises a layer selected from the group consisting of vinyl and rubber.
- 15 31. The method of claim 27 wherein said first material comprises a gypsum layer, and said second material comprises a layer selected from the group consisting of cellulose-based material and wood.
- 32. The method of claim 27 wherein said first material comprises a layer selected from the group consisting of a cellulose-based material and wood, and said second material comprises a metal.
 - 33. The method of claim 27 wherein said first material comprises a material selected from the group consisting of a cellulose-based material and a wood layer, and said second material comprises a material selected from the group of materials consisting of a petroleum-based plastic composite and a petroleum-based rubber layer.

- The method of claim 27 wherein said first material comprises a layer selected from the group consisting of a cellulose-based material and wood, and said second material comprises a layer selected from the group consisting of a petroleum-based plastic composite, vinyl and rubber.
- The method of forming a laminar structure which comprises:

 providing a layer of first material having two surfaces;

placing a layer of viscoelastic glue onto one surface of said layer of first material;

placing a layer of a second material over said viscoelastic glue;

pressing said layer of second material against said layer of viscoelastic glue and said first material for a selected time; and

drying said layer of second material, said layer of first material and said viscoelastic glue; wherein

the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

- The method of claim 35 wherein the two exterior layers are symmetric, made of the exact same type of material, and having the exact same density and thickness.
- 37. The method of claim 35 wherein the two exterior layers are nonsymmetric, made of other than the exact same type of material, and having other than the exact same density and thickness.
 - The method of claim 35 wherein the two or more interior layers are symmetric, made of the same type of material, and having the same density and thickness.

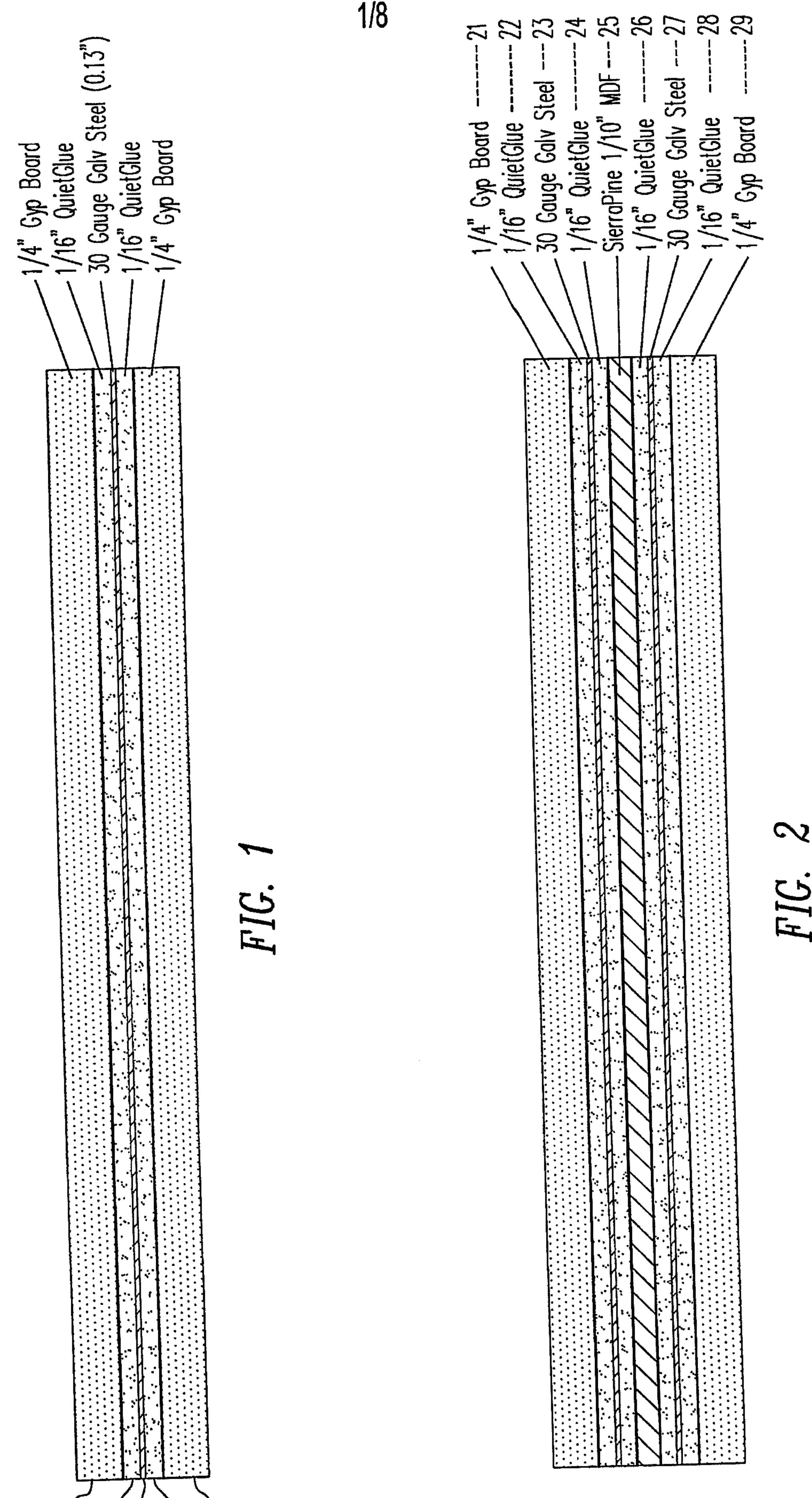
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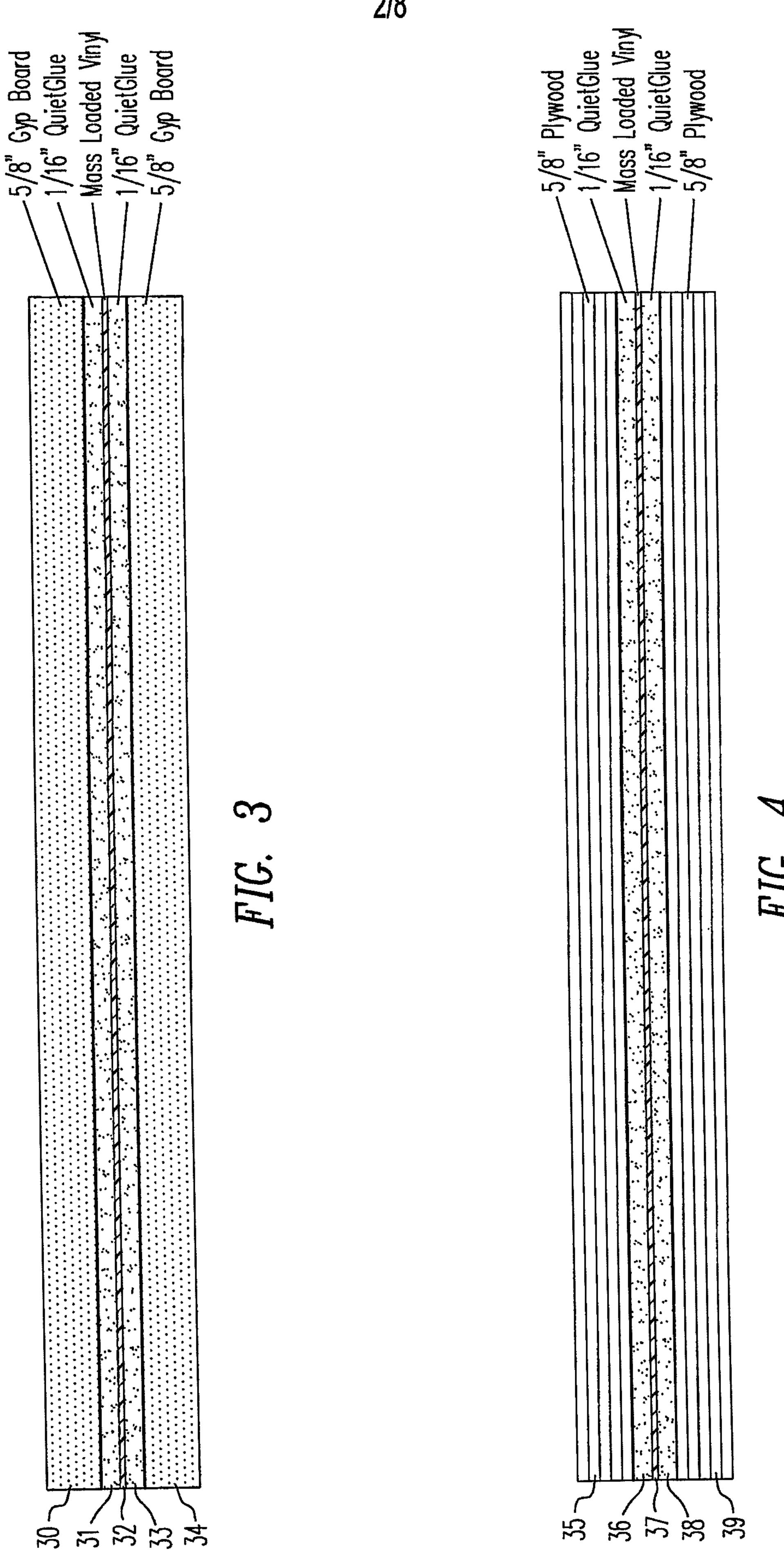
- The method of claim 35 wherein the two or more interior layers are non-symmetric, made of other than the exact same type of material, and having other than the same density and thickness.
- 40. A laminar, sound-absorbing structure which comprises:
- a layer of first material having two surfaces;

a layer of viscoelastic glue on one surface of said layer of first material; and

a layer of a second material over said viscoelastic glue; wherein the viscoelastic glue comprises an amount between 33% to 65% by weight of acrylate polymer.

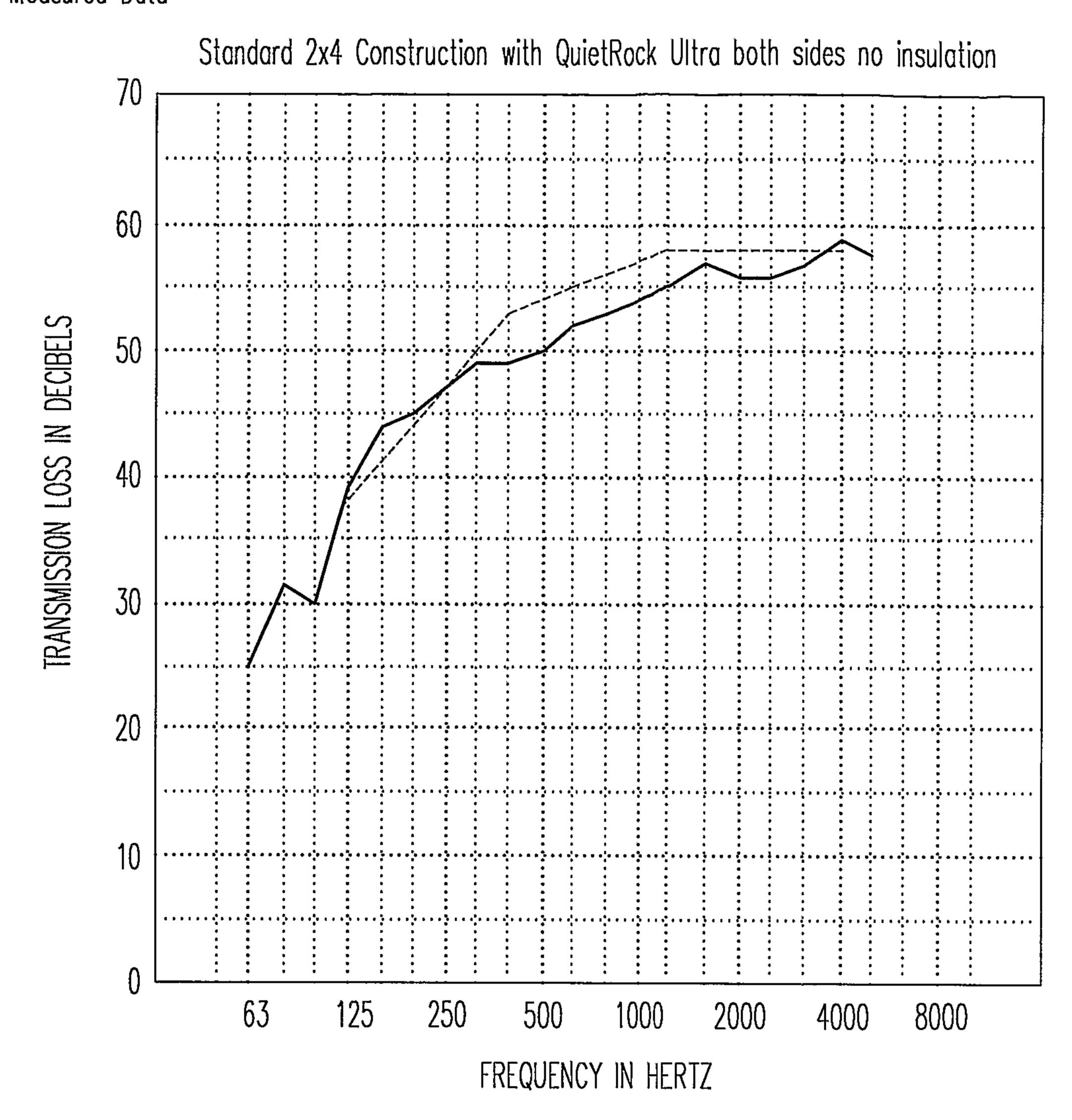
A laminar, sound-absorbing structure as in claim 40 wherein said layer of second materials is 1/10th to 1/2 the thickness of the first material.





----- Limiting STC Contour

Measured Data

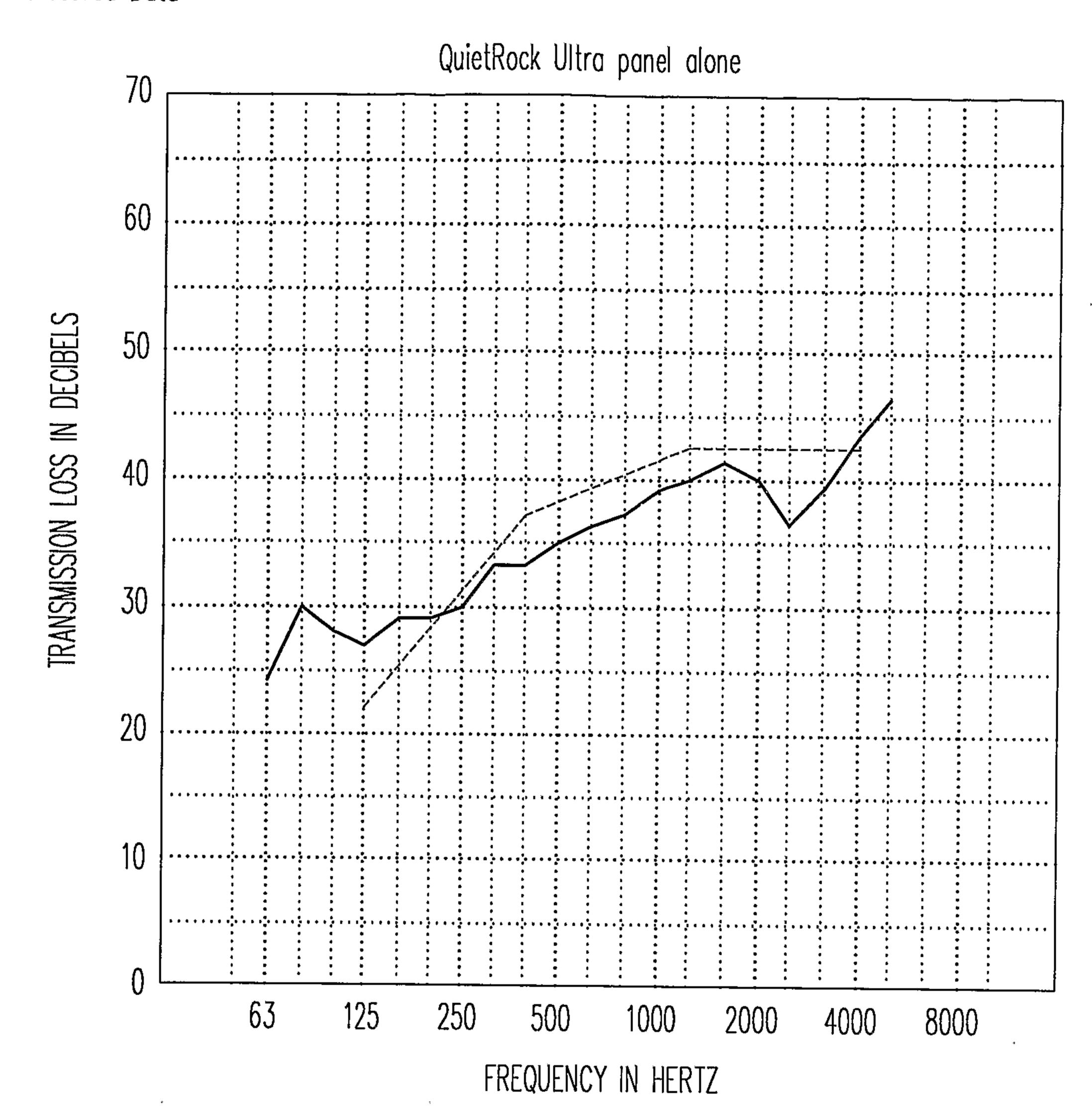


1/3 OCT BND	CNTR FREQ	63	80	100	125	160	200	250	315	400	500
TL in dB 95% Confidence	25 1.42	31 1.92	30 2.07	39 1.47	44 0.89	45 0.76	47 0.80	49 0.52	49 0.36	50 0.38	
deficiencies						0., 0	(0)	(1)	(4)	(4)	
1/3 OCT BND	1/3 OCT BND CNTR FREQ			1000	1250	1600	2000	2500	3150	4000	5000
TL in dB		52	53	54	55	57	56	56	57	59	58
95% Confidence	e in dB	0.29	0.44	0.38	0.39	0.36	0.56	0.55	0.31	0.32	0.50
deficiencies		(3)	(3)	(3)	(3)	(1)	(2)	(2)	(1)		
EWR OITC			Sp	ecimen	Area:	16 sq.	ft.				STC
55 44	Temperature: 73 deg. F									54	
Relative Humidity: 58%										(27)	
			Te	est Date	e: 05 Ji	une 200	3			•	

FIG. 5

----- Limiting STC Contour

Measured Data



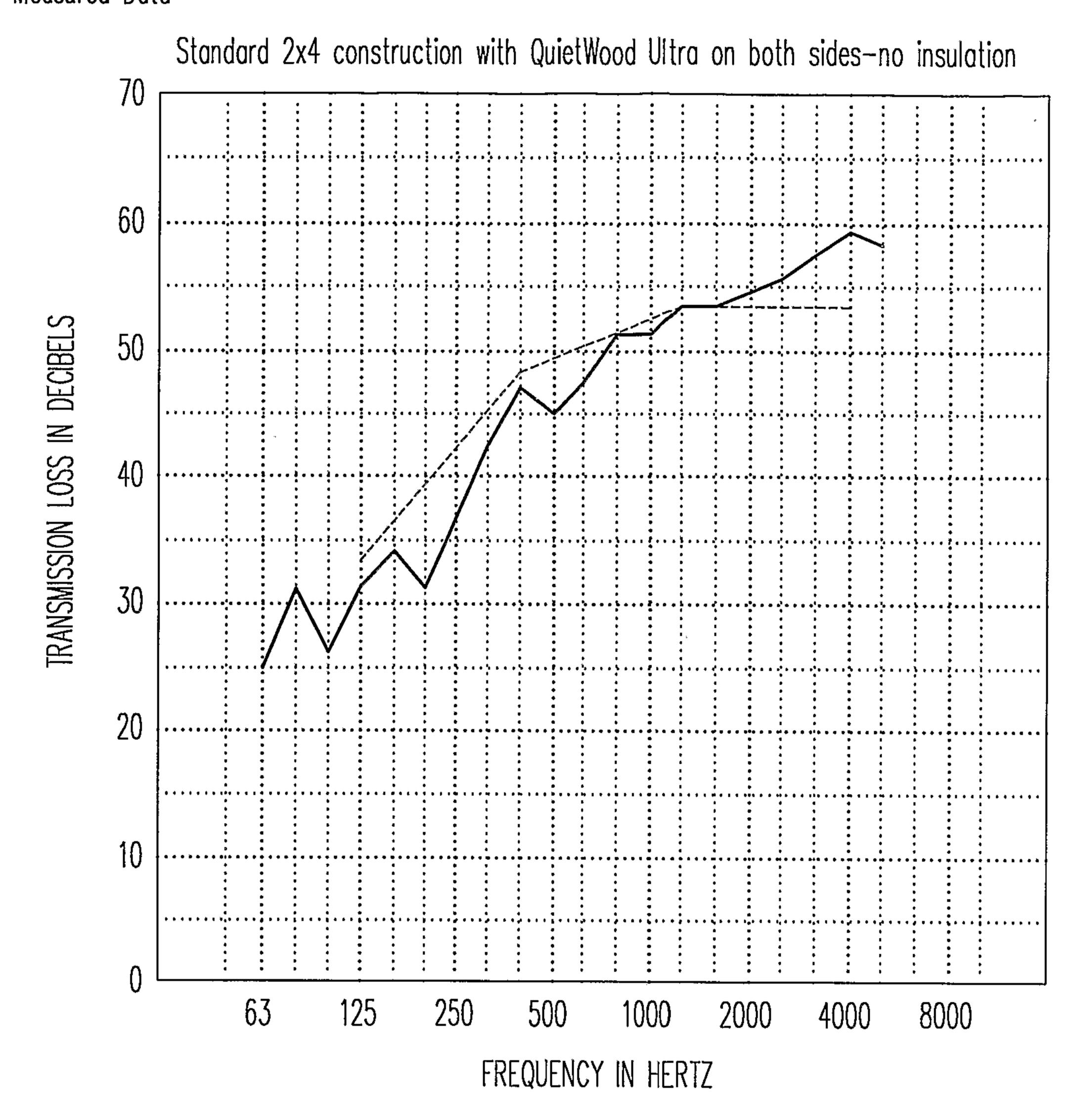
· · · · · · · · · · · · · · · · · · ·												
1/3 OCT BND CNTR FREQ			63	80	100	125	160	200	250	315	400	500
TL in	dB		24	30	28	27	29	29	30	33	33	35
95% C	onfidence	e in dB	1.42	1.92	2.07	1.47	0.89	0.76	0.80	0.52	0.36	0.38
deficie	ncies	<u> </u>	j	_					(1)	(1)	(4)	(3)
1/3 00	1/3 OCT BND CNTR FREQ			800	1000	1250	1600	2000	2500	3150	4000	5000
TL in	TL in dB			37	39	40	41	40	36	39	43	46
95% C	onfidence	e in dB	0.29	0.44	0.38	0.39	0.36	0.56	0.55	0.31	0.32	0.50
deficier	ncies	<u></u>	(3)	(3)	(2)	(2)	(1)	(2)	(6)	(3)		
EWR	OITC		Specimen Area: 16 sq. ft.									STC
40	34	Temperature: 73 deg. F								38		
Relative Humidity: 57%										(31)		
Test Date: 05 June 2003												

Test Date: Up June 2005

----- Limiting STC Contour

Measured Data

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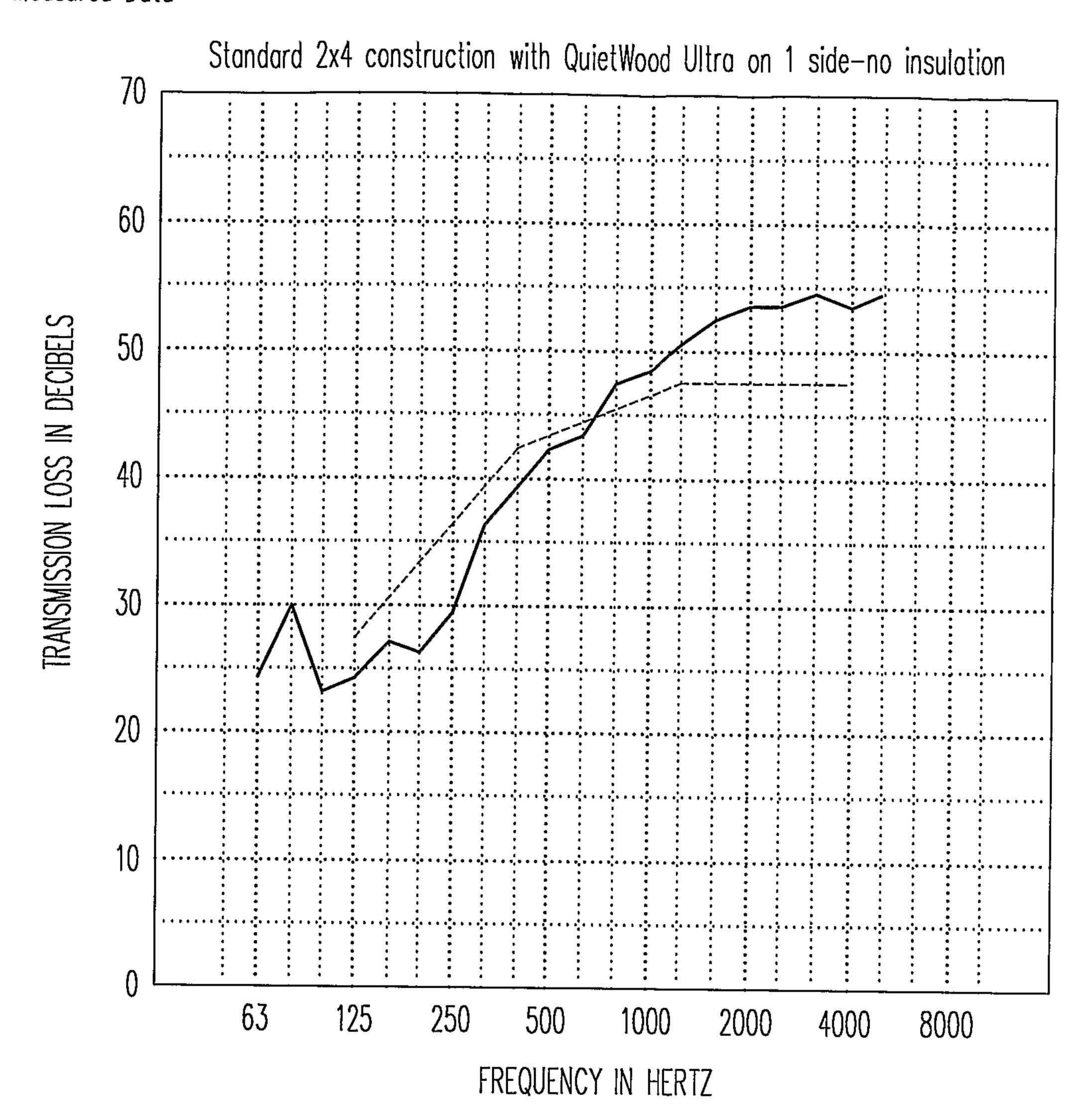


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1/3 OCT BND	CNTR FREQ	63	80	100	125	160	200	250	315	400	500
TL in dB		25	31	26	31	34	31	36	42	47	45
95% Confidence	e in dB	1.42	1.92	2.07	1.47	0.89	0.76	0.80	0.52	0.36	0.38
deficiencies					(2)	(2)	(8)	(6)	(3)	(1)	(4)
1/3 OCT BND	1/3 OCT BND CNTR FREQ			1000	1250	1600	2000	2500	3150	4000	5000
TL in dB				51	53	53	54	55	57	59	58
95% Confidence	e in dB	0.29	0.44	0.38	0.39	0.36	0.56	0.55	0.31	0.32	0.50
deficiencies		(3)	(0)	(1)	(0)	(0)					
EWR OITC			Sc	ecimen	Area:	16 sq.	ft.				STC
48 39		Specimen Area: 16 sq. ft. Temperature: 73 deg. F									49
Relative Humidity: 56%											(30)
						ine 200				ļ	

FIG. 7

----- Limiting STC Contour

Measured Data

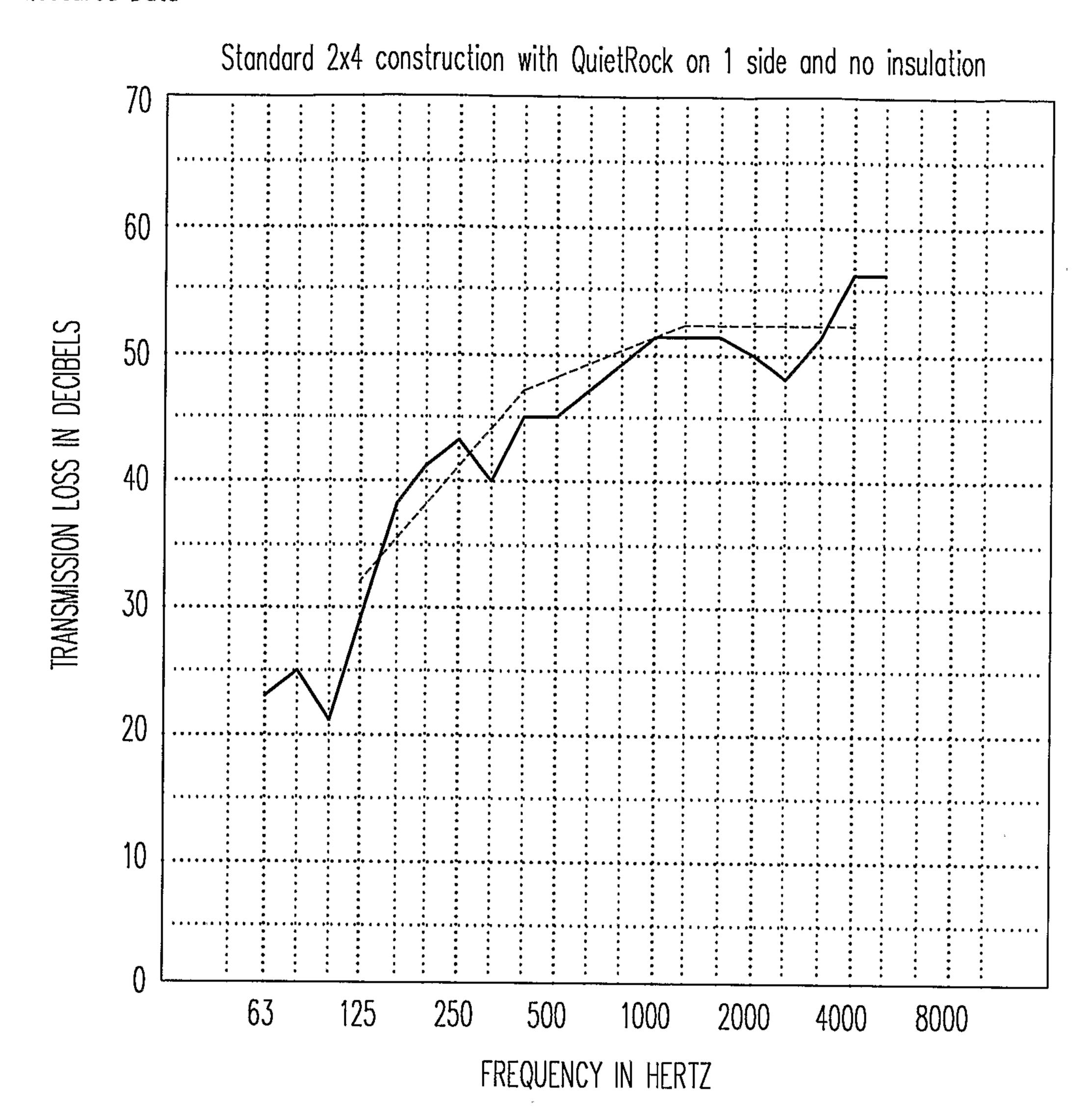


1/3 OCT BND CNTR FREQ TL in dB 95% Confidence in dB deficiencies			63 24 1.42	80 30 1.92	100 23 2.07	125 24 1.47 (3)	160 27 0.89 (3)	200 26 0.76 (7)	250 29 0.80 (7)	315 36 0.52 (3)	400 39 0.36 (3)	500 42 0.38 /1\
1/3 00 TL in d	1/3 OCT BND CNTR FREQ		630 43 0.29 (1)	800 47 0.44	1000 48 0.38	1250 50 0.39	1600	2000 53 0.56	2500 53 0.55	3150 54	4000 53 0.32	5000 54 0.50
EWR OITC 42 33 Specimen Area: 16 sq. ft. Temperature: 73 deg. F Relative Humidity: 57% Test Date: 05 June 2003									STC 43 (28)			

FIG. 8

----- Limiting STC Contour

Measured Data

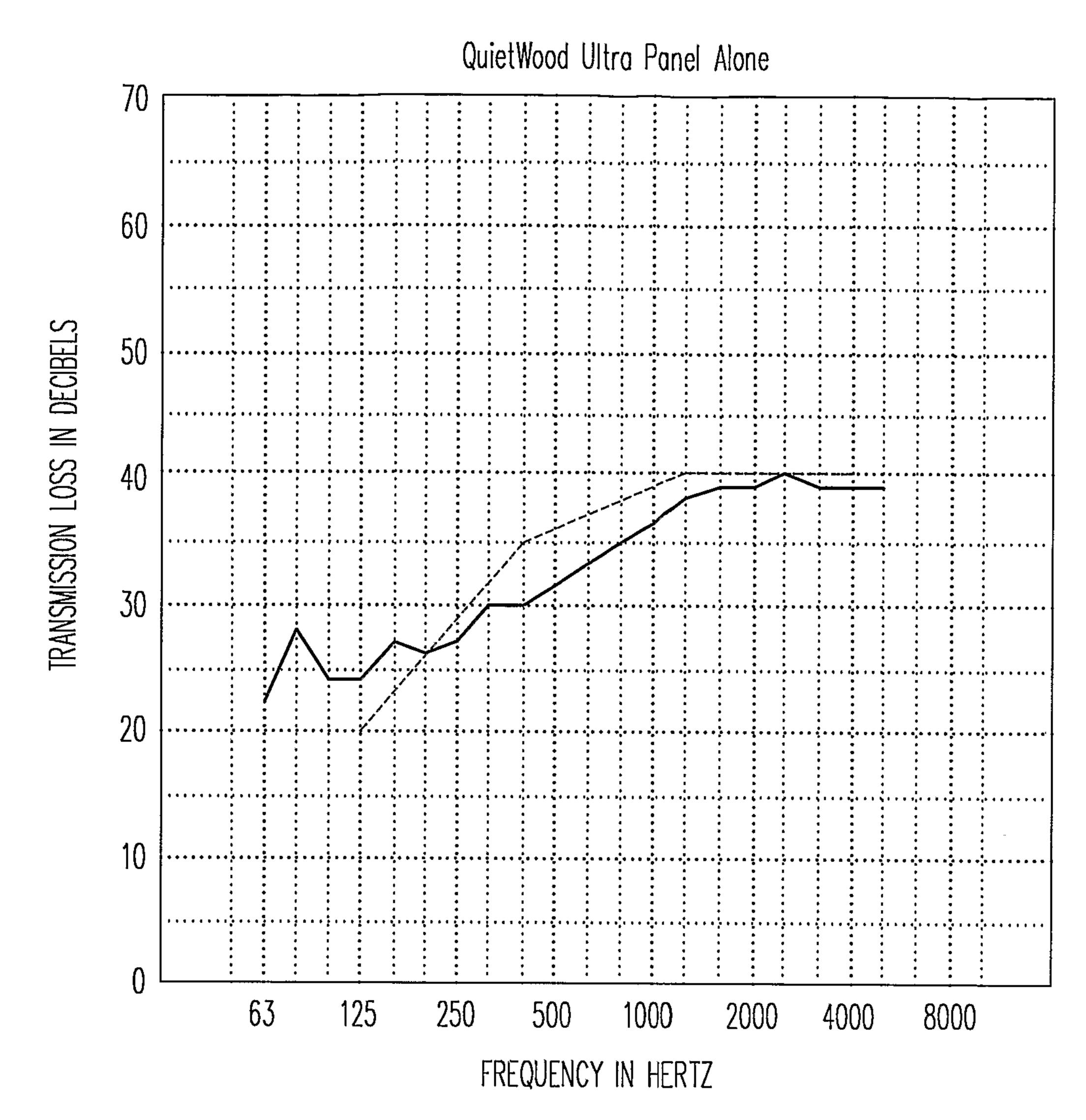


TL in	onfidence	63 23 1.42	80 25 1.92	100 21 2.07	125 29 1.47 (3)	160 38 0.89	200 41 0.76	250 43 0.80	315 40 0.52	400 45 0.36	500 45 0.38	
		ANITO COCO	C70	000	1000		4000		0500	(4)	(2)	(3)
TL in 6	1/3 OCT BND CNTR FREQ TL in dB 95% Confidence in dB deficiencies		630 47 0.29 (2)	800 49 0.44 (1)	1000 51 0.38 (0)	1250 51 0.39 (1)	1600 51 0.36 (1)	2000 50 0.56 (2)	2500 48 0.55 (4)	3150 51 0.31 (1)	4000 56 0.32	5000 56 0.50
EWR 50	OITC 36	Specimen Area: 16 sq. ft. Temperature: 73 deg. F Relative Humidity: 57% Test Date: 05 June 2003									STC 48 (24)	

FIG. 9

----- Limiting STC Contour

Measured Data



1/3 OCT BND CNTR FREQ			63	80	100	125	160	200	250	315	400	500
TL in dB	}		22	28	24	24	27	26	27	30	30	31
95% Con	nfidence	in dB	1.42	1.92	2.07	1.47	0.89	0.76	0.80	0.52	0.36	0.38
deficienc	ies							(0)	(2)	(2)	(5)	(5)
1/3 OCT BND CNTR FREQ			630	800	1000	1250	1600	2000	2500	3150	4000	5000
TL in dB	TL in dB			35	36	38	39	39	40	39	39	39
95% Con	nfidence	in dB	0.29	0.44	0.38	0.39	0.36	0.56	0.55	0.31	0.32	0.50
deficienc	ies		(4)	(3)	(3)	(2)	(1)	(1)	(0)	(1)	(1)	
EWR	OITC			Sp	ecimen	Area:	16 sq.	ft.			- · · ·	STC
37	31	Temperature: 73 deg. F									36	
Relative Humidity: 58%										(30)		
				Te	est Date	: 05 Ji	une 200	3			1	

FIG. 10