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(57) Claim

1. ^A system for landing an aircraft alonq ^a preferred landing guidance path defined by ^a predetermined glideslope and a centerline, comprising:
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(a) explosive ground installations, each* including a transmitter, operated in response to a trigger signal, for radiating a sequence of transmissions, to the aircraft which transmissions include precision guidance signals radiated through directional guidance antennas directed along the guidance path;

(b) an airborne installation including radio means for receiving said transmissions and processor means for processing said transmissions in response to an actuating signal, to provide guidance indications for guiding the landing of the aircraft;

(c) at each ground installation and airborne

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installation, ^a GPS receiver for producing ^a GPS siqnal representative of GPS system time;

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(d) at each ground installation, synchronizing means, operating in response to said GPS signal, for generating a trigger signal to actuate said transmitter; and

(e) in each airborne installation, synchronizing means, operating in response to said GPS signal, for
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whereby received transmissions, synchronized with respect to GPS time will also be synchronized with respect to the operation of said processor means.

15. Apparatus for landing an aircraft, comprising:

a) ^a ground based transmitter, operating in response to GPS system time, for radiating ^a sequence of direction guidance signals on the same frequency;

b) an airborne radio receiver adapted to receive said signals from said ground transmitter and to process, as ^a function of GPS system time, said signals to provide indications for guiding the landing of the aircraft, and c) ^a GPS receiver at each of the ground based transmitter and the airborne radio receiver, which receivers produce ^a trigger signal representative of GPS system time.

21. In ^a system for landing an aircraft along ^a preferred landing guidance path defined by a predetermined glideslope and a centerline, said system having:

one or more ground installations each including ^a transmitter, operated in response to ^a trigger signal, for radiating ^a sequence of transmissions on the same frequency to the aircraft which transmissions include precision guidance signals radiated through directional guidance antennas directed along the guidance path; and

an airborne installation including ^a radio for receiving the sequence of transmissions and ^a processor for processing said transmissions in response to an actuating signal, to provide indications for guiding the landing of the aircraft, apparatus comprising:

a) for each ground installation and airborne installation, ^a GPS system

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receiver for producing the trigger signal representative of GPS system time; and

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b) for each airborne installation, synchronizing means, operating in response to said trigger signal, for producing ^a signal to actuate the processor

whereby received transmissions, synchronized with respect to GPS system time, will also be synchronized with the operation of the processor.

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A system for landing an aircraft, using a ground installation and an airborne installation which are synchronized together using GPS system time. Specifically, the ground installation includes a ground transmitter (32) which radiates the sequence of signals (A, B, C, D) which provide precision guidance information to the aircraft, an aircraft installation which includes a radio receiver (8) and a processor (15) to receive a process the transmitted guidance signals and to provide indications (18, 20) to aid the pilot in landing the aircraft, a GPS receiver in the air (68) and on the ground (60) for producing signals representative of GPS system time, and a channel selector (72) in the aircraft for actuating the processor to synchronize its operation with the ground installation transmitter. Range information is provided by measuring the time interval between the transmission of a reference at the ground and its receipt in the air.

" ADVANCED INSTRUMENT LANDING SYSTEM "

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Technical Field

This invention relates to an advanced instrument landing system, and more particularly relates to ⁰⁵ improvements in ^a type of landinq system in which all ground installations seauentially radiate guidance pulses on the same frequency, the improvement permitting the ground installation of such ^a same-frequency landinq system to radiate at uniquely assigned times in an ¹⁰ established clock system and to be uniquely identified by an approaching aircraft that has both knowledqe of such uniquely assigned times and access to the established clock system time. The improvement also provides, to the aircraft, ^a precision ranqe to the qround station.

15 Background of the Invention

In cases where ^a ground installation of ^a single frequency landing system is remotely located from other similar installations, there is no need for the ground station to radiate at an assigned time, and the ²⁰ approaching aircraft has no difficulty in identifying the ground installation. However, in impacted geoqraphic locations, where there are multiple similar landinq installations located relatively closely together, it is

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necessary to provide means for uniquely identifying at least one such same-frequency installation to the exclusion of others in the vicinity.

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05 10 15 20 25 In conventional landing systems, such as the conventional Instrument Landing System (ILS) and the FAA Microwave Landing System (MLS), uniaue identification and signal exchanges between approaching aircraft and ^a particular qround installation are established by uniquely assigning different frequencies out of ^a band of frequencies to each of the various installations, and tuning the airborne units to the frequency of the selected installation. The FAA MLS system has ²⁰⁰ separate frequency channels assigned for its use in the band of 5000 to 5250 MHz. The ILS system has some ⁴⁰ channels in paired bands allocated to its use in the vicinity of ¹⁰⁰ and 300 MHz. Therefore, an adequate number of separately indentifiable channels for ^a sinqle frequency landing system can be inferred as being between ⁴⁰ and 200 channels. In my patent 4,429,312 entitled "Independent Landing Monitoring System", ^a different type of identification of ^a same-frequency landing installation is discussed in which some of the signals transmitted to the aircraft are pulse encoded to identify that installation. That system is generally satisfactory when the aircraft is in ^a remote area isolated from other ground stations and when the aircraft has a weather radar to interrogate the ground installation, ^a decoding circuit added to the radar together, and an appropriate code selector switch for station selection in the cockpit.

³⁰ However, not all aircraft have weather radars to interrogate the ground installation. In addition, where there are several airfields in close geographic proximity, or where there are several landing installations of this type at the same airport, the same-frequency signals

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from all such landing systems can arrive at the aircraft simultaneously and hence they cannot be adequately separated for unique range tracking identification and guidance generation purposes. This is basically the same problem that plagues the conventional Air Traffic Control Radar Beacon System (ATCRBS) used by the FAA for air traffic control purposes; it is called "garbling". The weather radar technique of my U.S. patent 4,429,312, with associated identifying codes, is thus very suitable for use at isolated remote sites, such as offshore oil rigs, but not suitable for areas with many same-frequency landing systems in close proximity. The problem comes basically from the fact that these systems, and the airborne radars all use ^a common frequency Thus, there is no way to trigqer one particular installation uniquely for positive identification purposes. There is, therefore, always the risk of undesirably triggering a nearby installation, with the result that confusing responses to the aircraft from both locations will be ²⁰ synchronously received in that aircraft.

In addition to ^a method of uniquely identifying ^a particular same frequency ground station, ^a very desirable characteristic for ^a landing system is the capability of providing range information. Range data has at least 25 three major uses:

> 1. ^a means for alerting the pilot of his proximity to touchdown;

^a means for automatically reducing the gain of the landing installation as the aircraft range to touchdown diminishes in order to maintain loop stability (often referred to as "course softening"); and

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3. ^a means for using the elevational angular data provided by the landing system to determine altitude above the runway during the approach.

In the conventional ILS system, range to ⁰⁵ touchdown is generally provided by marker beacons on the ground at established distances from touchdown. These beacons radiate vertical fan shapped-beams through which the approaching aircraft passes. The range information thus acquired in the aircraft is used for pilot alerting ¹⁰ and for "course softening" purposes.

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In FAA MLS and conventional ILS practice, an alternative and more accurate measurement of range is provided by conventional TACAN/DME interrogators which are carried by almost all aircraft. The airborne TACAN/DME 15 equipment interrogates ^a DME beacon that is co-located with the MLS or ILS ground installation and receives therefrom ^a direct measurement of range using usual DME techniques.

For some landing applications, a very precise ²⁰ measurement of range is required, and for this purpose, ^a Precision DME (usually referred to as PDME) is employed. The PDME is similar to the conventional DME, but uses faster rise time pulses to obtain higher precision. This PDME syr.tem imposes on aircraft, which have to use it in ²⁵ order to obtain ^a required very precise measurement of range, the additional burden of having installeld on board appropriate PDME airborne equipment. Another technique for obtaining precision range in ^a landing system is provided by the teaching of my U.S. patent 4,429,312. ³⁰ Range is measured in this disclosure by having the weather radar interrogate the landing system ground installation and trigger the transmission of pulsed angular guidance signals. These pulsed replies are synchronous with the

weather radar interrogations and are ranqe tracked in ^a conventional manner to provide precision range in the aircraft. Ranqe measurements of higher precision can be obtained by the use of fast rise time pulses.

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Both of the above described methods for identifying ground station installations (i.e., frequency selection or pulse group encodinq) require additional equipment and adjustable cockpit controls for either tuning to the frequency of the ground installation, or for selectinq the decodement of the signals radiated from that ground station. In addition, measurement of range, by means of marker beacons or DME equipment, requires the installation of appropriate marker beacons or DME beacons at the landing system ground installation. The measurement of very precise range requires the addition of specialized PDME equipment, both air and ground. While the use of the weather radar to provide precision range (as taught in my U.S. patent 4,429,312) eliminates the need for added PDME equipment, not all aircraft carry ^a weather radar. Thus, all conventional landing systems have tended to require added airborne equipment, or cockpit controls, or both, in order to achieve unique communication with and range to a selected ground installation.

In addition to the two techniques discussed above for obtaining range (i.e., the aircraft passing over marker beacons and the measurement of the time elapsed between an aircraft's transmission of an interrogation and the aircraft's reception of ^a reply from a transponder located at the landing system), there is the clocked station technique, That technique may be practiced using hiqh precision clocks and low precision clocks. For example, equipment in one participating unit, such as ^a ground or airborne station, transmits ^a signal at ^a known time in an established very precise clock system

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Equipment in ^a second unit, such as an aircraft, measures the time of reception of that transmitted siqnal in the same established clock system; by knowing the time at which the siqnal was transmitted, the propagation time between the two stations and thus the distance can be computed. One known use of this clocked ranqing method is the United States Air Force ΆΝ/ΆΡΝ-169, Station Keepinq Equipment (SKE).

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Another means for establishinq ^a common clock time, is for each participant to carry low-cost clocks of nominal stability and to periodically synchronize those clocks to ^a common time reference. Such synchronization of low-cost clocks may be established by an initial conventional two-way ranging process that determines the ranges between participants and thereafter uses measured range data, by an exchange between participants of relative clock times. Thus, the low-cost clocks of each participant are synchronized to ^a clock in one selected aircraft out of all participating aircraft. This synchronization process is then repeated at periodic intervals, which intervals occur frequently enouqh to maintain the common time base to adequate accuracy. ^A variation of this method of synchronizing all clocks to ^a clock in ^a selected unitjis to synchronize all clocks to an "average value" of all the clock times that exist when the clock synchronization process is initiated.

Therefore, this "local" synchronization process requires ^a precision ranging and ^a data exchange or communications system, including transmitters and receivers in each participating unit. ^A requirement for clock synchronization equipment, in all aircraft, is undesirable in many applications, (i.e., cost, weiqht and complexity.

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One advantage of using ^a common clock system is that identity may be established by the use of "time slotting". In this time slotting concept, each of the participants is assigned ^a specific clock time at which to radiate, which time repeats at specified intervals. For example, ^a specific participant, such as No. 3, miqht radiate on the third second of every minute. Associated with this radiation at ^a specific time is ^a subsequent time interval or time slot, during which no other participant can radiate. This use of an established clock time and an associated time slot, by the participant to which it is assiqned, permits reception of that transmission by other participants to be used to establish the identity of the sender of that transmission (i.e., any transmission received during that time interval must be from the participant assigned to transmit in that time slot). This use of an assiqned time slot or time period to provide ^a protected identity system can be viewed as being similar to the use of ^a distinctive frequency for identity, which frequency cannot be used by another station in ^a specific geographic area.

While the use of established and precise clock time, with precision of the order of ^a fraction of ^a microsecond, can provide both precision ranginq and unique identity, current use of such ^a common and precise clock time is limited by the attendant cost and complexity of very stable clocks, such as atomic clocks, or by the cost and complexity of the synchronizing equipment (i.e., communications system, etc.) required for lower cost clocks.

Considered broadly, ^a landing system does not inherently require the use of multiple different frequencies since operation at all installation sites is usually performed on ^a single frequency. Single-frequency

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operation is an advantage because, if the actual landing guidance system can always operate on the same frequency for different sites, great simplification in terms of airborne equipment complexity and cost is possible. For example, the airborne receiver can be ^a fixed-frequency ⁵ device.

Therefore, it should be appreciated that ^a landing system is needed which would provide both station selection and ranging data in ^a fixed frequency landing system, while using only airborne equipment which is installed in an IFR (Instrument Flight Rules) aircraft. Moreover, such ^a ¹⁰ system should be simple and low in cost. With the eventual addition of NAVSTAR or Global Positioning System (GPS) Navigation Sets on all but the smallest aircraft, it also would be very desirable to find ^a means to use GPS to provide channelization (i.e. identity) and range data for single frequency landing systems. This is especially true since such fixed frequency landing systems are, inherently, lower cost and are found in more locations throughout the world. Thus, there is ^a need for an advanced instrument landing system.

Summary of the Invention

In accordance with one embodiment of the present invention, there is provided ^a system for landing an aircraft along ^a preferred landing guidance path defined by ^a predetermined glideslope and ^a centerline, comprising:

a) one or more ground installations, each including ^a transmitter, operated in response to ^a trigger signal, for radiating ^a sequence of transmissions on the same frequency to the aircraft which transmissions include precision guidance signals radiated through directional guidance antennas directed along the guidance path;

b) an airborne installation including radio means for receiving said transmissions and processor means for processing said transmissions in response to an actuating signal, to provide guidance indications for guiding the landing of the aircraft;

c) for produci ng ^a GPS signal representative of GPS system time; at each ground installation and airborne installation, ^a GPS receiver

d) response to said GPS signal, for generating the trigger signal to actuate said transmitter; and at each ground Installation, synchronizing means, operating in 35

e) in each airborne installation, synchronizing means, operating in

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response to said GPS signal, for producing the actuating signal to actuate said processor means,

whereby received transmissions, synchronized with respect to GPS time will also be synchronized with respect to the operation of said processor 5 means.

In one specific embodiment of the invention, the sequence of signals radiated from the ground installation includes ^a ranging reference signal. These ranging reference signals, and associated guidance pulses, will be synchronously repetitive as received in the aircraft, with respect to the GPS clock time trigger signals generated in the aircraft. The time at which the ranging reference signal is received in the aircraft can thus be measured by conventional synchronous range tracking circuits, and the distance between the aircraft and the ground installation can thus be precisely calculated. Thus, GPS clock time provides precision range data to ^a selected low-cost single freqency ground station.

With the advent of GPS, precisely synchronized airborne clocks will become commonplace in airborne vehicles. Thus, availability of such universal time makes

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the consideration of applying such clock techniques on ^a wider scale very appropriate. Other advantages and features of the present invention will be come readily apparent from the detailed description of the invention, 05 · the embodiments presented, the accompanying drawings, and the claims.

Brief Description of the Drawing

FIG. ¹ is ^a block diagram of the advanced landing system that is the subject of the present invention.

10 Detailed Desciption

While this invention is susceptible of embodiment in many different forms, there is shown in the drawing and will herein be described in detail, one specific embodiment, with the understanding that the present ¹⁵ disclosure is to be considered as an exemplification of the principles of the invention and is not intended to limit the invention to the specific embodiment illustrated.

^A preferred embodiment of the present advanced landing system will be illustrated and described with 20 reference to the landing system of my U.S. patent 4,429,312. It should be understood, however, that this invention provides techniques which are applicable to many different landing systems, and therefore it is not limited to improvements to the precision landing system of the ²⁵ type shown and described in that patent.

As shown in that patent, and described in Columns ⁸ and ⁹ thereof, the patented system provides ^a ground based precision landinq guidance installation which radiates localizer and glideslope guidance beams from separate 30 antennas which are directed along the approach path toward

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^a landing aircraft, and which are received in the aircraft and processed to recover signals which provide landing indications to the pilot. In the system shown in that patent, the ground based system can either be triggered to generate replies in synchronization to some reference signal, as for example in synchronization to signals received from ^a weather radar, or can be free running and simply received and used by an approaching aircraft. The former type of system is the system to which the present improvements are directed and therefore the free running mode of operation of the landing system will not be further discussed.

Turning to FIG. 1, the landing system there illustrated includes ^a ground installation and an airborne installation. The ground installation includes, for lateral aircraft guidance, two directive antennas ²¹ and ²² having precision quidance localizer antenna beam patterns ²³ and 24, with cross-sections marked ^B and C. The ground installation also includes ^a non-directive antenna ⁵ delivering an omni-pattern 25. These antennas 5, 21 and 22 are connected by ^a switch 26 and cable 27 to ^a radar transmitter 32. Timing and switching circuitry ²⁹ controls the switch ²⁶ and initiates the outputs of the transmitter 32.

The directive antenna patterns of two paired glideslope antennas ³³ and ³⁴ are aligned and partially overlapped respectively above and below ^a predetermined glideslope (usually ³ degrees), so that for aircraft approaching precisely along the glideslope, the signal intensities received in the aircraft from these paired antennas ³³ and ³⁴ will be equal.

For vertical glidelsope guidance, the ground installation further includes two directive antennas ³³

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and ³⁴ for radiating paired precision glideslope guidance beams 33a and 34a, with cross-sections marked ^D and E. These two antennas ³³ and ³⁴ are likewise connected to the transmitter ³² through the antenna switch 26. The paired ⁰⁵ beam patterns of the antennas ²³ and ²⁴ for lateral guidance overlap so that they provide equal intensity signals along the extended centerline CL of the runway. Thus, if the signal intensities of both antennas are equal, as received in the airborne vehicle, it must be ¹⁰ laterally located over the centerline of the runway.

For an on-course approach, all four guidance signal intensities received in the aircraft will be equal. However, deviation above or below, or to the riqht or left of the desired approach course, wiill cause an unbalance 15 in the paired signals received at the receiver, indicating to the pilot the direction in which the aircraft has deviated from the desired course. This operation is thoroughly described in my U.S. patent 4,429,312.

The airborne installation of the system according to ²⁰ that patent is shown in the right in FIG. 1, and includes ^a radar receiver ⁸ and an antenna 3. The radar receiver ⁸ is connected to ^a range gate and navigation processor ¹⁵ which provides range data to a range readout 18 and to a course deviation indicator 20 connected thereto.

25 A transmission from the ground installation is initiated by sending a trigger signal T2 to the timing and switching circuitry 29. This transmission includes ^a sequence of multiple successively delivered signals. First, the timing and switching circuitry ²⁹ delivers, 30 through the omni antenna 5, ^a coded pulse group reference signal ^A from the transmitter 32. The strength of the reference signal is used to set the gain of the aircraft receiver ⁸ so as to keep, the airborne receiver operating

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within a linear portion of its response characteristic. After ^a fixed delay, determined by the timing and switching circuitry 29, the switch ²⁶ then steps sequentially to connect the transmitter ³² in turn to each ⁰⁵ of the four directive antennas 21, 22, ³³ and ³⁴ to deliver transmissions, including right and left paired localizer pulses, and up and down paired glideslope pulses. These pulses are delivered one at ^a time with suitable delays between them. Adjustable attenuators ⁴⁴ 10 serve to balance the antenna drives so that the guidance signals are all of equal amplitude when the aircraft is exactly on course for landing, as explained in my U.S. patent 4,429,312. The sequence of these four guidance signals is predetermined and fixed so that the aircraft ¹⁵ can identify the signals by their order in the sequence.

The pulses radiated in these precision guidance beams B, C, ^D and ^E in FIG. 1, plus the reference signal group ^A from the omni antenna, are received at the airborne antenna 3, and delivered by the receiver ⁸ to ^a ²⁰ processor ¹⁵ in the aircraft. The processor ¹⁵ is programmed to use the reference signal ^A to determine range and to display it at the range readout 18, and to use the precision landing signals B, C, ^D and ^E to create and deliver to the course deviation indicator ²⁰ output ²⁵ signals which show the position of the aircraft with respect to the desired approach path.

The equipment used to uniquely identify the ground installation of FIG. ¹ will now be described. The ground installation of FIG. ¹ is provided with ^a GPS 30 receiver/computer 60, ^a GPS antenna 62 connected to the receiver, and ^a Time Slot Selector 64. The GPS receiver/computer ⁶⁰ provides precision geographic position using the GPS or NAVSTAR Satellite system 66. The ground installation need only be provided with ^a

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receiver suitable for providing an output signal T1 representative of GPS system time. The availability of such receivers is becominq all the more commonplace. ^A relatively current description of available equipment is provided in the November 4, 19&5 edition of Aviation Week & Space Technology, "Global Positioning Develops As Civil Navigation System", page 58. The Time Slot Selector ⁶⁴ uses the GPS system time output signal T1 to develop ^a trigger signal T2 for the timing and switching means 29. Each ground installation would have ^a uniaue time slot or channel assigned so that it's transmissions are differentiated from those of surrounding or nearby ground stations. This trigger signal T2 is delivered by the Time Slot Selector ⁶⁴ at specific GPS clock times assigned to that specific qround station for purposes of uniquely identifying that ground station. The number of times per second that the trigger signal T2 must be generated depends on the rate at which guidance signals are required by the aircraft in order to have adequate guidance loop stability. ^A nominal value is twenty times ^a second. The timing and switching circuitry ²⁹ sets the switch ²⁶ to the correct position, provides delays, and drives the transmitter ³² to deliver the omni encoded reference signal ^A followed by the two sets of paired directive signals ^B and C, and ^D and E.

Turning now to the aircraft installation, just as in the case of the ground installation, an aircraft need only be provided with ^a simple GPS receiver/computer which provides an output signal T1 representative of GPS system time. This receiver ⁶⁸ is also provided with ^a suitable antenna ⁷⁰ and the output of the receiver is connected to ^a time slot selector 72. Preferably, the Time Slot Selector ⁷² is tunable to whatever channel the pilot desires in order to receive a selected ground installation 35 which, in accordance with the drawing, is the channel

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corresponding to the ground installation of FIG. 1. Once the Time Slot Selector ⁶⁴ is tuned to the ground station of interest, the synchronous guidance signals returned from the ground installation through the aircraft antenna ³ and aircraft receiver ⁸ become isolated by the time slot gating process and thus become identifiable as returns of interest to that aircraft, as distinguished from same-freauency synchronous landinq guidance signals from other ground installations in the vicinity transmitting at the same frequency.

Since the time at which the selected ground installation transmitter ³² is triggered into operation is known, and since the time that it takes for the synchronous transmitted signals to be received in the aircraft can be measured, the ranqe gate and navigation processor 15 can easily calculate the ranqe between the aircraft and the ground installation. This ranqe may be displayed on ^a diqital readout ¹⁸ in the cockpit of the aircraft. If the GPS receiver/computer installed in the aircraft is ^a "full computer", an output signal PA can be obtained which is representative of the aircraft's geographic position relative to the surface of the earth. Since the ground installation of interest is fixed on the earth, the position of the ground installation PG can be used, together with the aircraft position signal PA, to obtain ^a direct readout of the range 18' between the aircraft and the ground installation. This readout may also be used as a cross reference or check on the range readout 18 obtained by measuring the time between the transmission and the receipt of signals at the aircraft. It may also be used with altitude information to determine glideslope position and, hence, as an instrument cross reference check. Furthermore, it may be used with glideslope information to cross-check the aircraft's altimeter.

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The timing accuracy of the GPS clock time trigger signal T1 is limited by the GPS circular error probability (CEP). Conventional P~Code and C/A code CEP's are expected to be ¹⁰ to ⁵⁰ meters. Differential P-Code and differential C/A CEP accuracy is typically from ² to ⁶ meters. Since the GPS CEP and hence GPS clock errors due to unknown propagation delays at both the ground and airborne installations should be the same, assuming the use of similar GPS constellations, the range obtained by measuring the difference or interval between the GPS clock time at which landing guidance signals are transmitted from the ground and the GPS clock time at which they are received in the air (i.e., clocked range measurement) would have these unknown errors eliminated. Therefore, the clocked range measurement accuracy should coincide with differential GPS position accuracy (i.e., better than conventional). In other words, we have the surprising result that the use of clocked GPS time for channelization results in ^a range-to-touehdown measurement approaching that of differential GPS, while using only ^a conventional GPS receiver.

Those skilled in the art will appreciate the fact that excellent range measurement accuracy is of importance for the landing operation, particularly for those applications where centerline guidance is desired for an offset ground beacon installation. This would be especially useful in military applications. Centerline guidance may be achieved by the use of the range readout 18 and course deviation indicator ²⁰ signals.

The number of stations that can be uniquely and usefully identified by this use of GPS clock time and associated time slotting technique may be determined by considering the following:

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(1) No two ground stations should radiate close enough together in time such that signals from one qround station can possibly arrive at an aircraft and be detectable and, hence, potentially generate siqnals falsely usable to generate landing quidance in the time slot assigned to another ground station. To preclude this occurrance, it is necessary to first establish the distance from ^a ground station at which an aircraft can usably detect signals from that ground station. Assuming this distance is ⁸⁰ miles, then no two ground stations in such proximity can, in qeneral, radiate quidance signals closer together in time than the noted ⁸⁰ miles, multiplied by the ⁶ microseconds per mile speed of radio frequency propagation, or approximately ⁵⁰⁰ microseconds. If this precaution is not taken, then signals from both qround stations could possibly arrive at one aircraft in the **pjat od—il5⁰ mJ ff**e*e»»aad time slot G2 during which the processor is activated to qenerate landinq quidance, and hence, either cause garbling or provide guidance data directing the aircraft to the wronq qround station.

(2) ^A further consideration in this regard is that each ground station should, preferably, radiate ²⁰ quidance pulse groups per second to maintain quidance loop stability. This then means that each ground station must have allocated to it, each second, ²⁰ ^x ⁵⁰⁰ microseconds, or 10,000 microseconds, durinq which no other ground station in the noted ⁸⁰ mile proximity can radiata. This 10,000 microseconds, or 0.01 seconds total time interval, must therefore be allocated to each ground station per second for this typical illustration. This means that only ¹⁰⁰ uniquely identifiable ground stations can be located in the noted ⁸⁰ mile proximity. As ^a practical matter, therefore, one can note that at least some 100 unique sets of identifying radiating times can be assigned for uniquely identifying any one of 100 same frequency ground stations within an ⁸⁰ mile radius area. This

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number is more than adequate since, as noted previously, the conventional ILS system has only ⁴⁰ frequency channels assigned for uniaue identity purposes.

Finally, the airborne navigation processor ¹⁵ may be provided with ^a relatively narrow range gate for trackinq all ground installation response signals, including the omni signals ^A and the paired directive signals ^B and C, and ^D and ^E from the ground installation. The directive signals would be processed to give precision guidance to the pilot, using the visual course deviation indicator display 20. Infrequently, bowsver, other same-frequency signals from the selected landing installation or other landing installations in the vicinity (such as generated by ^a system covered by my Patent 4,429,312), may fall within the range gate. The effect of these same-frequency signals will be minor, if averaged with the desired signals from the selected ground installation, since they occur relatively infrequently and are not synchronous to GPS time. This minor effect may be further minimized by storing the values of all received signals that fall within the range gate in ^a computer memory, and by usinq, for guidance purposes only, those stored signals that fall within prescribed limits of ^a running average of all siqnals. This is termed "wild-point" editing.

This invention is not to be limited to the embodiments shown and described, because changes may be made within the scope of the following claims. For example, the technique of my U.S. Patent 4,429,312 may be used simultaneously with the technique described in this patent application. This simultaneous use may be of particular advantage in making ^a transition to GPS (i.e., the ground installation could radiate both on ^a clock basis and in response to weather radar interrogations or free run. Thus, it should be understood that no

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limitation with respect to the specific apparatus illustrated herein is intended or should be inferred. It is, of course, intended to cover by the appended claims, all such modifications as fall within the scope of the 05 claims.

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1. ^A system for landing an aircraft along ^a preferred landing guidance path defined by ^a predetermined **c.** glideslope and ^a centerline, comprising:

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 Similar ground installations, each including a transmitter, operated in response to a trigger

on the same frequency signal, for radiating a sequence of transmissions to the -2 aircraft which transmissions include precision guidance signals radiated through directional quidance antennas (a) directed along the quidance path;

¹⁰ (b) an airborne installation including radio means for receiving said transmissions and processor means for processinq said transmissions in response to an actuating signal, to provide quidance indications for guiding the landing of the aircraft;

¹⁵ (c) at each ground installation and airborne installation, ^a GPS receiver for producing ^a GPS siqnal representative of GPS system time;

(d) at each ground installation, synchronizing means, operating in response to said GPS signal, 20 for generating $\frac{t\lambda_c}{t}$ trigger signal to actuate said transmitter; and

> (e) in each airborne installation, synchronizing means, operating in response to said GPS signal, for
the actuating producing a trigger signal to actuate said processor means,

25 whereby received transmissions, synchronized with respect to GPS time will also be synchronized with respect to the operation of said processor means.

2. The system of Claim 1, wherein said ground installation synchronizing means includes time slot selection means for selecting the times at which said transmitter actuating signal is produced, as ^a 05 function of GPS system time, whereby each ground installation radiates at assigned times.

3. The system of Claim 2, wherein said airborne installation synchronizing means includes time slot selection means for selecting time intervals, with respect to GPS time, during which selected time 05 interval said processor means is actuated to process said sequence of transmissions.

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4. The system of Claim 3, wherein said time interval starts with the radiation of said transmissions from ^a selected ground station, and

wherein said time interval lasts for ^a length 05 of time sufficiently long to permit reception of said transmissions from said selected ground station out to a predetermined operating range.

5. The system of Claim 4, wherein said ground station assigned times defined by said time slot selector means adjusted relative to other ground installation transmissions such that no other ground ⁰⁵ station is permitted to radiate, with respect to radiation of said selected ground station, for ^a length of time adequate to preclude radiations from such other ground stations interferring with the proper processing of transmissions from said ¹⁰ selected ground station.

6. The system of Claim 1, wherein the sequence of transmissions radiated from ^a ground intallation to the aircraft includes ^a reference signal transmitted by the ground installation upon reception thereat of said 05 **actuating** trigger signal; and

wherein said airborne processor means includes means for determining range from the aircraft to said ground installation based upon the time interval between the reception of ^a GPS system time signal and said reference 10 signal.

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7. The system of Claim 3, wherein said airborne processor means includes range gate tracking means, responsive to said time slot selection means and to the times of arrivals in the aircraft of said reference signals and said precision guidance signals, for rejecting signals which are received bysaid radio means, which fall within said selected time intervals and which, if processed, would produce extraneous guidance indications.

8. The system of Claim 6, wherein each ground installation includes an omni-directional antenna , and said reference signal is radiated by said ground installation through its omni-directional antenna .

9. The system of Claim 6, wherein said reference signals radiated by each ground installation are encoded to identify the respective ground installation.

10. The system of Claim 1, wherein said guidance antennas at each ground intallation include plural directional radiatinq means arranged in pairs and operative to radiate guidance signal beams paired about the guidance path, said directional radiating means including overlapping paired localizer radiating means directed on horizontally opposite sides of the centerline and further including overlapping paired glideslope radiating means directed above and below said predetermined glideslope; and

wherein each ground installation includes signal timing and switching means, utilizing said transmitter actuating signal, for coupling ^a different radiating means to the transmitter to radiate each successive guidance signal beam from the respective localizer and glideslope radiating means.

11. The system of Claim 10, wherein each airborne installation includes indicator means for indicating the WO 87/07030

deviation of the aircraft from the landing path; and wherein said processor means:

⁰⁵ (a) is responsive to said quidance signals received by said radio means, and to the time positions in each sequence;

> (b) pairs the received quidance signal beams and compares the intensities of the signals of each pair; and

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[|] 10 (c) generates and delivers to said indicator means output signals for indicating deviations from said landing ' guidance path.

12. The system of Claim 1, wherein the GPS receiver in said airborne installation includes means for determining » the geographic position of said aircraft, whereby for ^a known ground installation geographic position, the range ⁰⁵ between the aircraft and the ground installation can be determined.

> 13. The system of Claim 1, wherein said GPS receiver in said airborne installation includes:

means for determining the distance from said ⁱ aircraft to ^a ground installation in response to the time 05 difference between the production of said trigger signal and the receipt of said precision guidance signals at said aircraft. i.l · I : :

> 14. The system of Claim 1, wherein said GPS receiver in said ground installation is located at a known position and includes:

(a) means for determining the position of said ⁰⁵ ground installation in response to the signals received from ^a constellation of satellites;

> (b) means for measuring the difference between said determined position and said known positon; and

(c) means for storing and transmitting to said ¹⁰ airborne installation correction signals characterized bv said position difference.

15. Apparatus for landing an aircraft, comprising:

a) ^a ground based transmitter, operating in response to GPS system time, for radiating ^a sequence of direction guidance signals on the same frequency;

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b) an airborne radio receiver adapted to receive said signals from said ground transmitter and to process, as ^a function of GPS system time, said signals to provide indications for guiding the landing of the aircraft, and c) ^a GPS receiver at each of the ground based transmitter and the airborne radio receiver, which receivers produce ^a trigger signal representative of GPS system time.

16. The system of claim 15, wherein said ground based transmitter includes means for selecting the time at which said transmissions take place relative to GPS system time, whereby ^a pre-assigned time slot is assigned to the ground based transmitter.

17. The system of claim 16, wherein said airborne receiver includes time slot selection means for selectively receiving signals from said ground based transmitter in accordance with said pre-assigned time slot.

18. The system of claim 15, further including in said aircraft, means for computing the range between said aircraft and said ground based transmitter utilizing the time interval between the transmission of said signal by said ground installation and the receipt of said signal in said aircraft.

19. The system of claim 18, wherein said sequence of directional guidance signals includes ^a reference signal which is transmitted after ^a fixed time delay after the receipt of ^a GPS trigger signal.

20. The system of claim 15, wherein said transmitted signals are transmitted at ^a single frequency and include precision guidance signals radiated along directional guidance antennas defining ^a pre-determined glideslope and centerline.

21. In ^a system for landing an aircraft along ^a preferred landing guidance path defined by ^a predetermined glideslope and ^a centerline, said system having:

one or more ground installations each including ^a transmitter, operated in response to ^a trigger signal, for radiating ^a sequence of transmissions on the same frequency to the aircraft which transmissions include precision guidance signals radiated through directional guidance antennas directed along the guidance path; and

an airborne installation including ^a radio for receiving the sequence

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of transmissions and ^a processor for processing said transmissions in response to an actuating signal, to provide indications for guiding the landing of the aircraft, apparatus comprising:

a) for each ground installation and airborne installation, a GPS system ⁵ receiver for producing the trigger signal representative of GPS system time; and

b) for each airborne installation, synchronizing means, operating in response to said trigger signal, for producing ^a signal to actuate the processor

10 whereby received transmissions, synchronized with respect to GPS system time, will also be synchronized with the operation of the processor. 22. ^A system for landing an aircraft substantially as hereinbefore described with reference to the drawing.

23. Apparatus for landing an aircraft substantially as hereinbefore .T5 described with reference to the drawing.

DATED this TWENTY SECOND day of NOVEMBER 1989 SUNDSTRAND DATA CONTROL, INC

Patent Attorneys for the Applicants SPRUSON & FERGUSON

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