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(71) Applicant (for all designated States except US): **FUJI PHOTO FILM B.V.** [NL/NL]; Oudenstaart 1, NL-5047 TK Tilburg (NL).

(72) Inventors; and

(75) Inventors/Applicants (for US only): **OLIJVE, Joseph Hubertus** [NL/NL]; Lek 46, NL-5172 BR Kaatsheuvel (NL). **KASE, Akira** [JP/NL]; Nistelroedestraat 43, NL-5045 MD Tilburg (NL).

(74) Agent: **VAN LOON, C.J.J.**; C/o Vereenigde, Johan De Wittlaan 7, NL-2517 JR The Hague (NL).

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(54) Title: POROUS MEMBRANE AND RECORDING MEDIUM COMPRISING SAME

(57) Abstract: The present invention relates to a porous membrane wherein said porous membrane comprises an isotropic bulk matrix in the form of an open polymer network and at least one surface layer, which surface layer is a perforated continuous layer of which the average surface pore diameter is between 0.02 and 1.2 μm , and the thickness of said surface layer is smaller than the thickness of said bulk matrix. The invention further relates to image recording materials, in which these porous membranes are used.

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Title: Porous membrane and recording medium comprising same

Field of the invention

The present invention relates to porous membranes obtained by curing compounds through radiation. The invention further relates to image recording materials in which these porous membranes are used, in particular
5 as an ink-receiving layer. The invention also relates to processes for preparing said membranes and said recording media, as well as to the use of said membranes and said recording media.

Background of the invention

10 Several examples can be found in which curable mixtures are used to produce inkjet recording media. EP-A-1 289 767, EP-A-1 418 058 and EP-A-1 477 318 disclose layers, cured by UV or other radiation in which the porous character is provided by organic or inorganic particles in order to obtain sufficient solvent uptake. However, application of inorganic particles can cause
15 physical weakness of the layer, resulting in cracking or breaking of the layer.

EP-A-0 738 608 describes curing compositions containing a water soluble high-molecular weight compound, but these compositions yield solid layers and therefore do not dry quickly.

WO-A-99/21723 discloses a substrate coated with a binder dissolved
20 in an aqueous solvent mixture, which layer is then cured, and teaches that any amount of solvent is suitable, and there is no limit to the degree in which the binder is diluted before curing.

WO-A-01/91999 and GB-A-2 182 046 disclose a curable inkjet coating that is cured after drying the coating.

25 US-A-6 210 808 describes an inkjet recording sheet wherein a colloidal suspension of water-insoluble particles and water-insoluble monomers/prepolymers is cured.

US-A-6 734 514 discloses a radiation curable coating for ink jet printing comprising water insoluble latexes.

Another method is the application of foamed layers as in for example EP-A-0 888 903.

In the above mentioned prior art the receiving layer is not isolated, but formed directly on the substrate after drying and/or further manipulation of the coated substrate. It would be advantageous, to be able to isolate such a layer as a membrane which can be used as such or which can be applied to a substrate in a separate process to give advantageous properties, for instance as an inkjet receiving medium. Membranes are produced by various methods such as dry and wet phase inversion of polymeric solutions, stretching of homogeneous, partially crystalline polymer films, sintering of particulate materials, thermal gelation of homogeneous polymer solutions and by radical polymerization with simultaneous phase separation by irradiation or thermal initiation. Of these methods the wet phase inversion method – in which a polymer solution is contacted with a precipitating agent or non-solvent causing separation into a solid polymer-rich phase and a liquid solvent-rich phase – is by far the most widely used technique for obtaining porous structures. Examples in which this technique is applied can be found in WO-A-98/32541, WO-A-2005/016655, US-A-4 707 265, US-A-5 079 272, EP-A-0 803 533, EP-A-0 812 697, EP-A-0 824 959, EP-A-0 889 080 and EP-A-1 149 624.

The main disadvantages of wet phase inversion are the limited production speed obtainable and the high amounts of organic solvents required.

Dry phase inversion processes are described *e.g.* in EP-A-1 176 030. An alternative method is disclosed in US-A-4 466 931, EP-A-0 216 622 and EP-A-0 481 517 describing a membrane which is produced by irradiating curable monomers in non-volatile organic solvents which are to be removed by washing with a washing liquid of low boiling point.

As many curable compounds are hydrophobic in nature both dry and wet phase inversion techniques require organic apolar solvents to obtain a clear solution.

Membranes can also be made by other methods such as thermal polymerization as described in *e.g.* EP-A-0 251 511, JP-A-5 177 120 and US-A-4 942 204 or grafting acrylic acid to PVC films as described in GB-A-1 549 352 but these membranes or films are not porous and are not
5 formed by phase separation from a solvent.

Membranes made from amphiphilic copolymers as free standing films are described in WO-A-01/88025 which are also not porous and of relatively small size (up to 1 mm²).

Although under certain conditions acceptable results can be
10 obtained with the above-mentioned prior art materials, there is still a need for improvement. The present invention seeks to fulfill, at least in part, this need.

For recording media improvement is required in particular with respect to smearing properties, which may be associated with absorption properties of the porous film, in particular absorption speed. At the same time
15 a porous film must be provided that has a good gloss.

There is a need for a membrane that can be produced at high speeds without requiring costly measures to guarantee safety and to prevent pollution of the environment. This invention aims at solving these problems, at least in
20 part.

Detailed description

An object of the present invention is to provide a porous membrane, preferably as part of a recording medium, which membrane has a combination of high gloss and suitable liquid absorption properties at the same time. Thus
25 the present invention seeks to find a solution for the a priori conflicting demands of high absorption capacity, which is typically obtained by providing a high porosity, and high gloss.

Yet another object of the invention is to provide a porous membrane preferably for use in a recording medium, which recording medium has good
30 smear behaviour, which is associated with a high absorption speed.

It is another object of this invention to provide a porous membrane that can be produced at low cost and at high coating speeds. It is a further object of this invention to provide a recording medium having excellent drying characteristics and also a good gloss.

5 Thus, in a first aspect, the present invention is directed to a porous membrane which comprises a porous receiving layer, which porous receiving layer comprises an isotropic bulk matrix in the form of an open polymer network and at least one surface layer, which surface layer is a perforated continuous layer of which the average surface pore diameter is between 0.02
10 and 1.2 μm , preferably between 0.05 and 0.7 μm .

In another aspect, the invention is directed to a porous receiving layer, which porous receiving layer comprises an isotropic bulk matrix comprising an isotropic polymeric network and containing matrix pores, on which matrix is present at least one perforated continuous surface layer
15 having surface pores, wherein the thickness of said surface layer is smaller than the thickness of said bulk matrix, and wherein the average density of said bulk matrix is smaller than the average density of said surface layer.

The term "surface pore" refers to the pores visible on the surface of the receiving layer. The "surface pore diameter" refers to the diameter of these
20 pores. For noncircular pores the pore diameter may be taken as the diameter of a circle having the same surface area as the noncircular pore.

The surface structure (average pore diameter and relative total surface pore area) can be determined from scanning electron microscopy (SEM) images, optionally using image analysis software. Examples of SEM images
25 showing different surface structures of cured porous membranes are given in Figures 1-4.

The term "matrix pore" refers to pores inside the polymer structure (as opposed to surface pores). These pores are generally interconnected according to the invention. If reference is made to the diameter of a matrix
30 pore, this can be taken as the diameter for spherical pores. For non-spherical

pores the diameter may be taken as the diameter of a sphere having the same volume as the matrix pore. An example of a SEM image of a cross-section showing the matrix structure and the surface layer is given in Figure 5.

In the invention the structure of the membrane is preferably isotropic (invariant with respect to direction) except for the surface layer. An isotropic structure is assumed to give a more homogeneous solvent flux and when applied as receiving layer a quicker solvent absorption. The matrix pores are preferably interconnecting, so both the polymer phase as well as the open space is preferably continuous. Alternatively the structure can be described as an open polymer network.

The porous membrane or the recording medium comprising the porous membrane of the present invention has a unique structure and is e.g. obtainable by the steps of:

- providing a mixture of at least one type of curable monomer and a solvent, wherein the concentration of said curable monomer is effective to obtain a porous membrane having a surface layer, which surface layer is a perforated continuous layer of which the average surface pore diameter is between 0.02 and 1.2 μm ;
- applying said mixture to a support;
- curing said curable monomer mixture, thereby causing phase separation between the crosslinked monomer and the solvent;
- subjecting the resulting porous membrane to a drying step to remove said solvent; and
- optionally separating the support and the porous membrane.

The thickness of the surface layer of the porous membrane of the present invention is preferably less than 4.0 μm , more preferably between 0.04 and 3.0 μm , most preferably between 0.05 and 1.0 μm .

By coating on a substrate a curable composition comprising at least one curable compound and a solvent, curing the coated composition thereby causing phase separation between the crosslinked compounds and the solvent

a substrate provided with a porous layer is formed. The membrane may be subjected to a washing and/or drying step. By this method a porous membrane can be obtained which can be used in various applications and which is characterized by its high solvent flux and/or uptake capability. If separated the porous membrane of the present invention can be fixed afterwards to all kinds of supports. Separation from the substrate can be easily achieved by proper treatment of the substrate *e.g.* by applying a 'release' layer comprising for instance a siloxane based polymer before coating the curable compound mixture on the substrate. The isolated porous membrane of this invention can be separately attached to a substrate via an adhesive layer. This adhesive layer can also impart certain properties to the resulting medium. Throughout the present text the terms curable compound and (curable) monomer are used interchangeably.

In another embodiment substrate and porous layer are not separated to give an isolated porous membrane, but are used as formed *e.g.* a membrane coated on a nonwoven support or on a glossy support in which the porous membrane can function as a colorant receiving layer when used in recording media. This can be for example an inkjet recording medium in which case the colorant is an ink-solution.

In another embodiment a substrate is coated with two or more layers of a curable compound mixture. By this method porous membranes can be designed and prepared with varying properties throughout the porous membrane. So an outer layer can be designed and prepared having colorant fixing properties, *e.g.* by introducing mordants in the outer layer, and an inner porous layer can be constructed having an optimised water uptake capability. Alternatively to introduce the so-called backview option in backlit material, the outer layer is optimized for scratch resistance and the colorant fixing property is located in the layer closest to a transparent support. Or for separation membrane applications the porosity of the outer layer is controlled

to determine the separation characteristics while the inner layer(s) are optimized to give both strength to the membrane and allow high solvent fluxes.

In general the dry thickness of the porous membrane of this invention in isolated form may typically be between 10 μm and 500 μm , more preferably between 30 and 300 μm . When adhered to a substrate the membrane need not give internal strength and the optimal thickness is based on properties such as solvent uptake capacity. In the latter case the dry thickness is typically between 5 and 50 μm . When the substrate is impermeable to aqueous solvents the dry thickness is preferably between 20 and 50 μm , while when the substrate is able to absorb part of the solvent as is the case for *e.g.* (coated) base paper the preferred dry thickness is between 5 and 30 μm . When the porous layer is a multilayer the thickness of the various layers can be selected freely depending on the properties one likes to achieve.

Many curable compounds are hydrophobic in nature and require high concentrations of organic apolar solvents to obtain a clear solution. Large amounts of volatile organic solvents are not preferred since these may result in hazardous conditions in the production area during the drying phase of the membrane while non-volatile solvents are difficult to remove and are thus not preferred either. For reasons of safety, health and the environment, as well as from economic viewpoint, water is the most preferred solvent. It was found that suitable curable compounds are water reducible to form an aqueous solution. A compound is regarded as water reducible when at 25 °C at least 2 wt% of water is compatible with the curable compound. Preferably at least 4 wt%, more preferably at least 10wt% of water is miscible with the curable compounds of the invention. Preferably environmental friendly solvents, such as water, are used. A solvent comprising water is generally referred to as an aqueous solvent. The aqueous solvent preferably comprises at least 30 wt.% water, more preferably at least 50 wt%, and may further comprise other polar or apolar co-solvents. In case the miscibility with water is not sufficient to dissolve the curable compound completely admixing of a co-solvent is

desirable. Preferably the solvent contains at least 60 wt.%, preferably at least 70 wt.% and more preferably at least 80 or even 90 wt.% of water. In a specific embodiment the solvent is water and does not contain organic co-solvents. For example, 10% CN132, 27.5% CN435 and 62.5% water, or 21.5% CN132, 21.5%
5 CN435 and 57% water, or 60% CN132 and 40% water, or 49.75% CN132, 49.75% water and 0.5% dodecyltrimethylammonium chloride can give a favourable porous matrix. CN132 and CN435 are curable monomers available from Cray Valley, France. CN132 is a low viscosity aliphatic epoxy acrylate. CN435 (available in the US as SR9035) is an ethoxylated trimethylolpropane
10 triacrylate.

As co-solvents, polar volatile solvents that can be sufficiently removed by drying are preferred. Preferred co-solvents are lower alkyl alcohols, alkanones, alkanals, esters, or alkoxy-alkanes. The term "lower alkyl" means that the alkyl chain contains less than 7, preferably less than 6 and
15 more preferably less than 5 carbon-atoms, preferably 1-4 carbon atoms. In one embodiment the solvent is a mixture of isopropanol and water. Other preferred co-solvents are *e.g.* methanol, ethanol, 1-propanol, acetone, ethylacetate, dioxane, methoxy ethanol and dimethylformamide. Most preferred are co-solvents having a boiling point lower than that of water.

20 The solubility of the curable compound in the solvent is another parameter of importance. Preferably the curable composition is a clear solution. The solvent can be chosen such that the selected curable compound or compound mixture is completely dissolved. A clear solution is more stable and is generally preferred. However a slight turbidity usually does not cause
25 instability and is in most cases acceptable. On the other hand for phase separation to occur the growing polymer should be insoluble in the solvent. This puts certain restrictions to the curable compounds that can be selected in combination with a certain solvent. Possible methods that can facilitate the selection of suitable combinations are described in *e.g.* EP-A-216622 (cloud
30 point) and US-A-3823027 (Hansen system).

To obtain a large difference in solubility between the initial compounds and the resulting polymer and thus a fast phase separation preferably the molecular weight (MW) of the initial compounds is not too large, although also with high-MW polymers porous membranes can be realized by careful selection of the solvent. Preferably the MW of the curable monomers or oligomers is less than 10000 Dalton, more preferably less than 5000 Dalton. Good results are obtained with compounds having a MW of less than 1000 Dalton.

In addition to the curable compound having a water reducibility of between 2 wt% and 50 wt% other types of curable monomers may be present in the curable composition. Curable compounds according the invention are described for example in "Development of ultraviolet and electron beam curable materials" (edited by Y. Tabata, CMC publishing, 2003, ISBN 4882317915) and may be selected from, but are not limited to epoxy compounds, oxetane derivatives, lactone derivatives, oxazoline derivatives, cyclic siloxanes, or ethenically unsaturated compound such as acrylates, methacrylates, polyene-polythiols, vinyl ethers, vinylamides, vinylamines, allyl ethers, allylesters, allylamines, maleic acid derivatives, itaconic acid derivatives, polybutadienes and styrenes. Preferably as the main component (meth)acrylates are used, such as alkyl-(meth)acrylates, polyester-(meth)acrylates, urethane-(meth)acrylates, polyether-(meth)acrylates, epoxy-(meth)acrylates, polybutadiene-(meth)acrylates, silicone-(meth)acrylates, melamine-(meth)acrylates, phosphazene-(meth)acrylates, (meth)acrylamides and combinations thereof because of their high reactivity. Other types of curable compounds may be combined with the main component in order to modify certain characteristics of the resulting membrane. These compounds can be used in the form of a monomer solution, monomer suspension, monomer dispersion, oligomer solution, oligomer suspension, oligomer dispersion, polymer solution, polymer suspension and polymer dispersion.

In order to prepare the porous membrane of the invention the curable composition and the processing conditions have to be selected with care. Upon irradiation the monomers (or oligomers or prepolymers) crosslink to gradually form polymers. During this process the solubility of the growing
5 polymer in the solvent decreases resulting in phase separation and by result the polymer separates from the solution. Finally the polymer forms a network with a porous structure wherein the solvent fills the pores. Upon drying the solvent is removed and a porous membrane remains. In certain embodiments the membrane is not dried but optionally washed and kept in a wet condition
10 to prevent collapsing of the pores. To obtain an optimal structure of the porous membrane it is important to carefully select the concentration of the curable compound or mixture of curable compounds. When the concentration is too low, it is assumed that upon curing no network structure is formed and when the concentration is too high experiments indicate that a more or less
15 homogenous gelled layer may be formed that yields a non-porous, transparent layer after drying. Also when the monomers are too soluble in the solvent no phase separation occurs and then usually a gel structure is formed after polymerization. A porous structure is essential for a high solvent flux. In view of this, the concentration of the curable compound or compounds in the solvent
20 is preferably between 10 and 80 wt.%, more preferably between 20 and 70 wt.%, most preferably between 30 and 60 wt%.

When the porous membrane is used as a colorant receiving medium, *e.g.* an inkjet recording medium, where aqueous inks are used to form images the membrane should have a hydrophilic character in order to rapidly absorb
25 the aqueous solvents involved. In the case that the curable composition contains water as main solvent the polymer formed generally must have hydrophobic character because incompatibility with the solvent is important for phase separation to occur. This implies that for this application the membrane of the invention must have both hydrophilic character and
30 hydrophobic character. These seemingly contradictory demands can be

realized for instance by selecting a curable compound that has an amphiphilic structure: a part of the molecule is hydrophilic and another part has a hydrophobic character. An amphiphilic monomer may have both hydrophilic and hydrophobic groups or may have amphiphilic groups (*e.g.* a (1,2- or 1,3-) propylene oxide chain or a (1,2-, 1,3- or 1,4-) butylene oxide chain). Examples of hydrophobic groups are aliphatic or aromatic groups, alkyl chains longer than C3 and the like. An alternative approach is to include in the curable composition curable compounds that are hydrophilic and those that are hydrophobic. The latter method allows the properties of the membrane to be controlled by varying the ratio of both types of curable compounds. Hydrophilic monomers are for example water soluble monomers and monomers having hydrophilic groups such as hydroxy, carboxylate, sulfate, amine, amide, ammonium, ethylene oxide chain and the like. Amphiphilicity can be obtained in several ways. Amphiphilic monomers can for instance be made by introducing a polar group (such as hydroxy, ether, carboxylate, sulfate, amine, amide, ammonium, *etc.*) into the structure of a hydrophobic monomer. On the other hand starting from a hydrophilic structure an amphiphilic monomer can be made by increasing the hydrophobic character by introducing *e.g.* alkyl or aromatic groups.

Good results are obtained when at least one of the curable compounds has a restricted water reducibility. Preferably water is miscible with the curable monomer at 25 °C in a weight ratio of between 2/98 and 50/50, more preferably between 4/96 and 50/50, even more preferably between 10/90 and 50/50. Many suitable curable compounds are amphiphilic in nature. A suitable concentration of the monomer can be achieved by addition of a co-solvent, a surfactant, by adjusting the pH of the composition or by mixing in monomers that maintain a good solubility at higher water loads. The miscibility ratios of water with the latter monomers are typically larger than 50 wt.% at 25 °C.

Another possible method of achieving the porous membrane of the invention is applying a mixture of a monomer having a poor miscibility with water, typically miscibility ratios of water with monomer at 25 °C lower than 2 wt.%, with a monomer having a good miscibility, *i.e.* a miscibility of water in the monomer at 25 °C larger than 50 wt.%. Many different types of monomers can be successfully applied in the invention by carefully selecting combinations of two, three or more types of monomers and optimising their respective concentrations and solvent composition.

Suitable monomers exhibiting a miscibility with water at 25 °C in a weight ratio water/monomer between 2/98 and 50/50 are: poly(ethylene glycol) diacrylate (preferably MW<500, e.g. triethylene glycol diacrylate, tetraethylene glycol diacrylate, *etc.*), ethylene glycol epoxyate dimethacrylate, glycerol diglycerolate diacrylate, propylene glycol glycerolate diacrylate, tripropylene glycol glycerolate diacrylate, oligo(propylene glycol) diacrylate, poly(propylene glycol) diacrylate, oligo(propylene glycol) glycerolate diacrylate, poly(propylene glycol) glycerolate diacrylate, oligo(butylene oxide) diacrylate, poly(butylene oxide) diacrylate, oligo(butylene oxide) glycerolate diacrylate, poly(butylene oxide) glycerolate diacrylate, ethoxylated trimethylolpropane triacrylate (ethoxylation 3-10 mol), ethoxylated bisphenol-A diacrylate (ethoxylation 3-10 mol), 2-hydroxyethyl acrylate, 2-hydroxypropylacrylate, 2-hydroxy-3-phenoxy propyl acrylate, 2-(ethoxyethoxy)ethylacrylate, N,N'-(m)ethylene-bis(acrylamide). Also suitable are commercially available compounds such as CN129 (an epoxy acrylate), CN131B (a monofunctional aliphatic epoxy acrylate), CN133 (a trifunctional aliphatic epoxy acrylate), CN9245 (a trifunctional urethane acrylate), CN3755 (an amino diacrylate), CN371 (an amino diacrylate), all from Cray Valley, France.

Suitable (hydrophilic) monomers having a good miscibility with water (weight ratio water/monomer larger than 50/50 at 25 °C) are: poly(ethylene glycol) (meth)acrylates (preferably MW>500), poly(ethylene glycol) di(meth)acrylates (preferably MW>500), ethoxylated

trimethylolpropane triacrylates (ethoxylation more than 10 mol), (meth)acrylic acid, (meth)acrylamide, 2-(dimethylamino)ethyl (meth)acrylate, 3-(dimethylamino)propyl (meth)acrylate, 2-(diethylamino)ethyl (meth)acrylate, 2-(dimethylamino)ethyl (meth)acrylamide, 3-(dimethylamino)propyl (meth)acrylamide, 2-(dimethylamino)ethyl (meth)acrylate quaternary ammonium salt (chloride or sulfate), 2-(diethylamino)ethyl (meth)acrylate quaternary ammonium salt (chloride or sulfate), 2-(dimethylamino)ethyl (meth)acrylamide quaternary ammonium salt (chloride or sulfate), 3-(dimethylamino)propyl (meth)acrylamide quaternary ammonium salt (chloride or sulfate).

Suitable (hydrophobic) monomers having a poor miscibility with water (weight ratio water/monomer smaller than 2/98 at 25 °C) are: alkyl (meth)acrylates (e.g. ethyl acrylate, n-butyl acrylate, n-hexylacrylate, octylacrylate, laurylacrylate), aromatic acrylates (phenol acrylate, alkyl phenol acrylate, *etc.*), aliphatic diol (di)(meth)acrylates (e.g. 1,4-butanediol diacrylate, 1,6-hexanediol diacrylate, Hydroxypivalic acid neopentylglycol diacrylate, neopentylglycol diacrylate, tricyclodecanedimethanol diacrylate), trimethylolpropane triacrylate, glyceryl triacrylate, pentaerythritol triacrylate, pentaerythritol tetraacrylate, dipentaerythritol pentaacrylate, dipentaerythritol hexaacrylate, ditrimethylolpropane tetraacrylate, styrene derivatives, divinylbenzene, vinyl acetate, vinyl alkyl ethers, alkene, butadiene, norbornene, isoprene, polyester acrylates having alkyl chain longer than C₄, polyurethane acrylates having alkyl chain longer than C₄, polyamide acrylates having alkyl chain longer than C₄.

Preferably the curable composition comprises between 1-100wt% of monomers that are miscible with water in a ratio water/monomer of between 2/98 and 50/50 at 25 °C, more preferably between 10-80wt%, most preferably between 40-70wt% based on the total amount of curable monomers. The curable composition may additionally comprise up to 99wt%, preferably between 30-60wt% of monomers that are miscible with water in a ratio

water/monomer larger than 50/50 at 25°C, based on the total amount of curable monomers. Also monomers having a poor miscibility may be present in the mixture up to 99 wt%. Another way of obtaining a membrane according the invention is to combine between 1 and 99 wt%, preferably between 30 and 80 wt% of monomers having a good miscibility with water and between 1-99wt%, preferably between 10-80wt%, more preferably between 20-70wt% of monomers that have a poor miscibility with water in a ratio water/monomer less than 2/98 at 25 °C.

The curable compound mixture is preferably subjected to radiation to obtain the porous membrane. In principle (electromagnetic) radiation of any suitable wavelength can be used, such as for example ultraviolet, visible or infrared radiation. Polymerization initiators or free radical initiators may be applied to initiate the polymerization reaction upon irradiation of the curable composition. Advantages of free radical polymerization are the high reaction rate and the flexibility; chemical polymerization requires thorough mixing of the cross-linking agent and is usually much slower. Initiators may be used in accordance with the present invention and can be mixed into the mixture of the curable compound(s), preferably prior to applying the mixture to the support. Photo-initiators are usually required when the coated mixture is cured by UV or visible light radiation. Suitable photo-initiators are those known in the art such as radical type, cation type or anion type photo-initiators.

Examples of radical type I photo-initiators are α -hydroxyalkylketones, such as 2-hydroxy-1-[4-(2-hydroxyethoxy)phenyl]-2-methyl-1-propanone (Irgacure™ 2959: Ciba), 1-hydroxy-cyclohexyl-phenylketone (Irgacure™ 184: Ciba), 2-hydroxy-2-methyl-1-phenyl-1-propanone (Sarcure™ SR1173: Sartomer), oligo[2-hydroxy-2-methyl-1-{4-(1-methylvinyl)phenyl}propanone] (Sarcure™ SR1130: Sartomer), 2-hydroxy-2-methyl-1-(4-tert-butyl-)phenylpropan-1-one, 2-hydroxy-[4'-(2-hydroxypropoxy)phenyl]-2-methylpropan-1-one, 1-(4-Isopropylphenyl)-2-

hydroxy-2-methyl-propanone (Darcure™ 1116: Ciba); α -aminoalkylphenones such as 2-benzyl-2-(dimethylamino)-4'-morpholinobutyrophenone (Irgacure™ 369: Ciba), 2-methyl-4'-(methylthio)-2-morpholinopropiophenone (Irgacure™ 907: Ciba); α,α -dialkoxyacetophenones such as α,α -dimethoxy- α -phenylacetophenone (Irgacure™ 651: Ciba), 2,2-diethoxy-1,2-diphenylethanone (Uvatone™ 8302: Upjohn), α,α -diethoxyacetophenone (DEAP: Rahn), α,α -di-(n-butoxy)acetophenone (Uvatone™ 8301: Upjohn); phenylglyoxalates such as methylbenzoylformate (Darocure™ MBF: Ciba); benzoin derivatives such as benzoin (Esacure™ BO: Lamberti), benzoin alkyl ethers (ethyl, isopropyl, n-butyl, iso-butyl, etc.), benzylbenzoin benzyl ethers, Anisoil; mono- and bis-Acylphosphine oxides, such as 2,4,6-trimethylbenzoyl-diphenylphosphine oxide (Lucirin™ TPO: BASF), ethyl-2,4,6-trimethylbenzoylphenylphosphinate (Lucirin™ TPO-L: BASF), bis(2,4,6-trimethylbenzoyl)-phenylphosphine oxide (Irgacure™ 819: Ciba), bis(2,6-dimethoxybenzoyl)-2,4,4-trimethyl-pentylphosphineoxide (Irgacure 1800 or 1870). Other commercially available photo-initiators are 1-[4-(phenylthio)-2-(O-benzoyloxime)]-1,2-octanedione (Irgacure OXE01), 1-[9-ethyl-6-(2-methylbenzoyl)-9H-carbazol-3-yl]-1-(O-acetyloxime)ethanone (Irgacure OXE02), 2-hydroxy-1-{4-[4-(2-hydroxy-2-methyl-propionyl)-benzyl]-phenyl}-2-methyl-propan-1-one (Irgacure127), oxy-phenyl-acetic acid 2-[2 oxo-2-phenyl-acetoxy-ethoxy]-ethyl ester (Irgacure754), oxy-phenyl-acetic-2-[2-hydroxy-ethoxy]-ethyl ester (Irgacure754), 2-(dimethylamino)-2-(4-methylbenzyl)-1-[4-(4-morpholinyl) phenyl]-1-butanone (Irgacure 379), 1-[4-[4-benzoylphenyl]thio]phenyl]-2-methyl-2-[(4-methylphenyl)sulfonyl]-1-propanone (Esacure 1001M from Lamberti), 2,2'-bis(2-chlorophenyl)-4,4',5,5'-tetraphenyl-1,2'-bisimidazole (Omnirad BCIM from IGM).

Examples of type II photo-initiators are benzophenone derivatives such as benzophenone (Additol™ BP: UCB), 4-hydroxybenzophenone, 3-hydroxybenzophenone, 4,4'-dihydroxybenzophenone, 2,4,6-trimethylbenzophenone, 2-methylbenzophenone, 3-methylbenzophenone, 4-

methylbenzophenone, 2,5-dimethylbenzophenone, 3,4-dimethylbenzophenone, 4-(dimethylamino)benzophenone, [4-(4-methylphenylthio)phenyl]phenylmethanone, 3,3'-dimethyl-4-methoxy benzophenone, methyl-2-benzoylbenzoate, 4-phenylbenzophenone, 4,4-bis(dimethylamino)benzophenone, 4,4-bis(diethylamino)benzophenone, 4,4-bis(ethylmethylamino)benzophenone, 4-benzoyl-N,N,N-trimethylbenzenemethanaminium chloride, 2-hydroxy-3-(4-benzoylphenoxy)-N,N,N-trimethyl-1-propanaminium chloride, 4-(13-Acryloyl-1,4,7,10,13-pentaoxatridecyl)benzophenone (Uvecryl™ P36: UCB), 4-benzoyl-N,N-dimethyl-N-[2-(1-oxo-2-propenyl)oy]ethylbenzenemethanaminium chloride, 4-benzoyl-4'-methyldiphenyl sulphide, anthraquinone, ethylanthraquinone, anthraquinone-2-sulfonic acid sodium salt, dibenzosuberone; acetophenone derivatives such as acetophenone, 4'-phenoxyacetophenone, 4'-hydroxyacetophenone, 3'-hydroxyacetophenone, 3'-ethoxyacetophenone; thioxanthenone derivatives such as thioxanthenone, 2-chlorothioxanthenone, 4-chlorothioxanthenone, 2-isopropylthioxanthenone, 4-isopropylthioxanthenone, 2,4-dimethylthioxanthenone, 2,4-diethylthioxanthenone, 2-hydroxy-3-(3,4-dimethyl-9-oxo-9H-thioxanthonyloxy)-N,N,N-trimethyl-1-propanaminium chloride (Kayacure™ QTX: Nippon Kayaku); diones such as benzyl, camphorquinone, 4,4'-dimethylbenzyl, phenanthrenequinone, phenylpropanedione; dimethylanilines such as 4,4',4''-methylidyne-tris(N,N-dimethylaniline) (Omnirad™ LCV from IGM); imidazole derivatives such as 2,2'-bis(2-chlorophenyl)-4,4',5,5'-tetraphenyl-1,2'-bisimidazole; titanocenes such as bis(eta-5-2,4-cyclopentadiene-1-yl)-bis-[2,6-difluoro-3-1H-pyrrol-1-yl]phenyl]titanium (Irgacure™784: Ciba); iodonium salt such as iodonium, (4-methylphenyl)-[4-(2-methylpropyl-phenyl)-hexafluorophosphate (1-)]. If desired combinations of photo-initiators may also be used.

For acrylates, diacrylates, triacrylates or multifunctional acrylates, type I photo-initiators are preferred. Especially alpha-hydroxyalkylphenones, such as 2-hydroxy-2-methyl-1-phenyl propan-1-one, 2-hydroxy-2-methyl-1-(4-

tert-butyl-) phenylpropan-1-one, 2-hydroxy-[4'-(2-hydroxypropoxy)phenyl]-2-methylpropan-1-one, 2-hydroxy-1-[4-(2-hydroxyethoxy)phenyl]-2-methylpropan-1-one, 1-hydroxycyclohexylphenylketone and oligo[2-hydroxy-2-methyl-1-{4-(1-methylvinyl)phenyl}propanone], alpha-aminoalkylphenones, alpha-
5 sulfonalkylphenones and acylphosphine oxides such as 2,4,6-trimethylbenzoyl-diphenylphosphine oxide, ethyl-2,4,6-trimethylbenzoyl-phenylphosphinate and bis(2,4,6-trimethylbenzoyl)-phenylphosphine oxide, are preferred. Preferably the ratio of photo-initiator and curable compound(s) is between 0.001 and 0.1, more preferably between 0.005 and 0.05, based on
10 weight. It is preferred to minimize the amount of photo-initiator used, in other words preferably all photo-initiator has reacted after the curing step (or curing steps). Remaining photo-initiator may have adverse effects such as yellowing or degradation of dyes in case the membrane is used as a recording medium. When applied as a separation membrane excessive washing may be required to
15 wash out remaining photo-initiator.

When more than one layer is applied in each layer the type and concentration of photo-initiator can be chosen independently. For example, in a multilayer structure the photo-initiator in the toplayer may be different from the photo-initiator in lower layer(s) which can give more efficient curing with
20 low initiator concentrations than when a single initiator is applied throughout all layers. Some types of photo-initiator are most effective in curing the surface while other types cure much deeper into the layer when irradiated with radiation. For the lower layers a good through cure is important and for a high efficiency of curing it is preferred to select a photo-initiator that has an
25 absorption spectrum not fully overlapping with the spectrum of the photo-initiator applied in the toplayer. Preferably the difference in absorption maximum between photo-initiators in the top layer and in the bottom layer is at least 20 nm. In the case UV radiation is used a light source can be selected having emissions at several wavelengths. The combination of UV light source
30 and photo-initiators can be optimized so that sufficient radiation penetrates to

the lower layers to activate the photo-initiators. A typical example is an H-bulb with an output of 600 Watts/inch as supplied by Fusion UV Systems which has emission maxima around 220 nm, 255 nm, 300 nm, 310 nm, 365 nm, 405 nm, 435 nm, 550 nm and 580 nm. Alternatives are the V-bulb and the D-bulb
5 which have a different emission spectrum. It is obvious that there need to be sufficient overlap between the spectrum of the UV light source and that of the photo-initiators. From a choice of light sources and photo-initiators optimal combinations can be made. The method of multiple types of photo-initiator allows for thicker layers to be cured efficiently with the same intensity of
10 irradiation. Additionally by applying different types of photo-initiator characteristics such as gloss and porosity can be optimised to levels not possible with a single type of photo-initiator.

Curing rates may be increased by adding amine synergists to the curable compound. Amine synergists are known to enhance reactivity and
15 retard oxygen inhibition. Suitable amine synergists are *e.g.* free alkyl amines such as triethylamine, methyldiethanol amine, triethanol amine; aromatic amine such as 2-ethylhexyl-4-dimethylaminobenzoate, ethyl-4-dimethylaminobenzoate and also polymeric amines as polyallylamine and its derivatives. Curable amine synergists such as ethylenically unsaturated
20 amines (*e.g.* (meth)acrylated amines) are preferable since their use will give less odor, lower volatility and less yellowing due to its ability to be incorporated into the polymeric matrix by curing.

The amount of amine synergists is preferably from 0.1-10wt% based on the amount of curable compounds in the curable composition, more
25 preferably from 0.3-3 wt% based on the amount of curable compounds.

Curing by infrared radiation is also known as thermal curing. Thus curing polymerization may be effectuated by combining the ethylenically unsaturated monomers with a free radical initiator and heating the mixture. Exemplary free radical initiators are organic peroxides such as ethyl peroxide
30 and benzyl peroxide; hydroperoxides such as methyl hydroperoxide, acyloins

such as benzoin; certain azo compounds such as α,α' -azobisisobutyronitrile and γ,γ' -azobis(γ -cyanovaleric acid); persulfates; peracetates such as methyl peracetate and tert-butyl peracetate; peroxalates such as dimethyl peroxalate and di(tert-butyl) peroxalate; disulfides such as dimethyl thiuram disulfide and ketone peroxides such as methyl ethyl ketone peroxide. Temperatures in the range of from about 23 °C to about 150 °C are generally employed. More often, temperatures in the range of from about 37 °C to about 110 °C are used.

Irradiation by ultraviolet light is preferred. Suitable wavelengths are for instance UV-A (400-320 nm), UV-B (320-280 nm), UV-C (280-200 nm), provided the wavelength matches with the absorbing wavelength of the photoinitiator, if present.

Suitable sources of ultraviolet light are mercury arc lamps, carbon arc lamps, low pressure mercury lamps, medium pressure mercury lamps, high pressure mercury lamps, swirlflow plasma arc lamps, metal halide lamps, xenon lamps, tungsten lamps, halogen lamps, lasers and ultraviolet light emitting diodes. Particularly preferred are ultraviolet light emitting lamps of the medium or high pressure mercury vapor type. In addition, additives such as metal halides may be present to modify the emission spectrum of the lamp. In most cases lamps with emission maxima between 200 and 450 nm are most suitable.

The energy output of the exposing device may be between 20 and 240 W/cm, preferably between 40 and 150 W/cm but may be higher as long as the desired exposure dose can be realised. The exposure intensity is one of the parameters that can be used to control the extent of curing which influences the final structure of the membrane. Preferably the exposure dose is at least 40 mJ/cm², more preferably between 40 and 600 mJ/cm², most preferably between 70 and 220 mJ/cm² as measured by an High Energy UV Radiometer (UV Power Puck™ from EIT – Instrument Markets) in the UV-B range indicated by the apparatus. Exposure times can be chosen freely but need not be long and are typically less than 1 second.

In case no photo-initiator is added, the curable compound can be advantageously cured by electron-beam exposure as is known in the art. Preferably the output is between 50 and 300 keV. Curing can also be achieved by plasma or corona exposure.

5 The pH of the curable compositions is preferably chosen between a value of 2 and 11, more preferably between 3 and 8. The optimum pH depends on the used monomers and can be determined experimentally. The curing rate appeared to be pH dependent: at high pH the curing rate is clearly reduced resulting in a less porous membrane. At low pH values (2 and lower) yellowing
10 of the membrane occurs upon aging which is not desired when a good whiteness is preferred.

Where desired, a surfactant or combination of surfactants may be added to the aqueous composition as a wetting agent, to adjust surface tension, or for other purposes such as a good gloss. It is within the ability of one skilled
15 in the art to employ a proper surfactant depending upon desired use and the substrate to be coated. Commercially available surfactants may be utilized, including radiation-curable surfactants. Surfactants suitable for use in the curable composition include nonionic surfactants, ionic surfactants, amphoteric surfactants and combinations thereof. Preferred nonionic
20 surfactants include ethoxylated alkylphenols, ethoxylated fatty alcohols, ethylene oxide/propylene oxide block copolymers, fluoroalkyl ethers, and the like. Preferred ionic surfactants include, but are not limited to, the following: alkyltrimethylammonium salts wherein the alkyl group contains from 8 to 22 (preferably 12 to 18) carbon atoms; alkylbenzyltrimethylammonium salts
25 wherein the alkyl group contains from 8 to 22 (preferably 12 to 18) carbon atoms, and ethylsulfate; and alkylpyridinium salts wherein the alkyl group contains from 8 to 22 (preferably 12 to 18) carbon atoms. Surfactants may be fluorine based or silicon based. Examples of suitable fluorosurfactants are: fluoro C₂-C₂₀ alkylcarboxylic acids and salts thereof, disodium N-
30 perfluorooctanesulfonyl glutamate, sodium 3-(fluoro-C₆-C₁₁ alkyloxy)-1-C₃-C₄

alkyl sulfonates, sodium 3-(omega -fluoro-C₆-C₈ alkanoyl-N-ethylamino)-1-propane sulfonates, N-[3-(perfluorooctanesulfonamide)-propyl]-N,N-dimethyl-N-carboxymethylene ammonium betaine, perfluoro alkyl carboxylic acids (e.g. C₇-C₁₃-alkyl carboxylic acids) and salts thereof, perfluorooctane sulfonic acid
5 diethanolamide, Li, K and Na perfluoro C₄-C₁₂ alkyl sulfonates, Li, K and Na N-perfluoro C₄-C₁₃ alkane sulfonyl-N-alkyl glycine, fluorosurfactants commercially available under the name Zonyl® (produced by E.I. Du Pont) that have the chemical structure of RfCH₂CH₂SCH₂CH₂CO₂Li or RfCH₂CH₂O(CH₂CH₂O)_x H wherein Rf = F(CF₂CF₂)₃₋₈ and x = 0 to 25, N-
10 propyl-N-(2-hydroxyethyl)perfluorooctane sulfonamide, 2-sulfo-1,4-bis(fluoroalkyl)butanedioate, 1,4-bis (fluoroalkyl)-2-[2-N,N,N-trialkylammonium) alkyl amino] butanedioate, perfluoro C₆-C₁₀ alkylsulfonamide propyl sulfonyl glycinates, bis-(N-perfluorooctylsulfonyl-N-ethanolaminoethyl)phosphonate, mono-perfluoro C₆-C₁₆ alkyl-ethyl
15 phosphonates, and perfluoroalkylbetaine. Also useful are the fluorocarbon surfactants described e.g. in US-A-4 781 985 and in US-A-5 084 340.

Silicon based surfactants are preferably polysiloxanes such as polysiloxane-polyoxyalkylene copolymers. Such copolymers may be for example dimethylsiloxane-methyl (polyoxyethylene) copolymer, dimethylsiloxane-
20 methyl (polyoxyethylene-polyoxypropylene) siloxane copolymer, trisiloxane alkoxyate as a copolymer of trisiloxane and polyether, and siloxane propoxyate as a copolymer of siloxane and polypropylene oxide. The siloxane copolymer surfactants may be prepared by any method known to those having skill in the art and can be prepared as random, alternate, block, or graft
25 copolymers. The polyether siloxane copolymer preferably has a weight-average molecular weight in a range of 100 to 10,000. Examples of polyether siloxane copolymers commercially available in the market include SILWET DA series, such as SILWET 408, 560 or 806, SILWET L series such as SILWET-7602 or COATSIL series such as COATSIL 1211, manufactured by CK WITCO;
30 KF351A, KF353A, KF354A, KF618, KF945A, KF352A, KF615A, KF6008,

KF6001, KF6013, KF6015, KF6016, KF6017, manufactured by SHIN-ETSU; BYK-019, BYK-300, BYK-301, BYK-302, BYK-306, BYK-307, BYK-310, BYK-315, BYK-320, BYK-325, BYK-330, BYK-333, BYK-331, BYK-335, BYK-341, BYK-344, BYK-345, BYK-346, BYK-348, manufactured by BYK-CHEMIE; and
5 GLIDE series such as GLIDE 450, FLOW series such as FLOW 425, WET series such as WET 265, manufactured by TEGO.

Surfactants may be added in the curable composition and/or may be introduced by impregnation of the membrane for the purpose of improving printer transportability, blocking resistance and waterproofness. The
10 surfactant, when used, preferably is present in an amount between 0.01 and 2% based on the dry weight of the membrane, more preferably between 0.02 and 0.5%. Preferably the surfactants are soluble in the composition in the concentration used. When an aqueous solvent is used preferably the solubility of the surfactant in water at 25 °C is at least 0.5%.

15 For a fast uptake of especially aqueous inks the surface needs to be hydrophilic. The hydrophilicity of the surface is suitably expressed by measuring the contact angle of water drops. Values below 80° are indicative for hydrophilic surfaces and are preferred for applications as ink receiving layer.

In accordance with the present invention, a membrane is referred to
20 as "porous, nanoporous or microporous" if it contains a substantial amount of pores preferably having a diameter of between 0.0001 and 2.0 µm. More preferably the majority of the pores of the porous membrane of the invention have a size of between 0.001 and 1.0 µm, even more preferably between 0.003 and 0.7 µm. For selected embodiments the average pore diameter preferably is
25 between 0.01 and 1.0 µm, more preferably between 0.03 and 0.4 µm. There is no limitation as to the pore shape. The pores can for instance be spherical or irregular or a combination of both. Preferably the pores are inter-connected, since this will contribute to a high flux or quick solvent absorption.

The porosity of the membrane is preferably between 5 and 90 percent as determined by analysing SEM cross-section images. The porosity is determined by the following formula:

$$5 \quad \frac{\text{Dry thickness [m]}}{\text{Coated amount of solids [kg/ m}^2\text{]}} * 100 \% - 100 \%$$

10 wherein the density of the coated solids (matrix) is assumed to be 1 kg/dm³. More preferably the porosity is between 10 and 70 percent, even more preferably between 20 and 50%.

For membranes applied as ink receiving layer it is important to exhibit a high gloss for which the surface layer need to be smooth and the size and total area of the pores on the surface of the membrane must be controlled
 15 within certain limits. Good gloss can be additionally expressed in a surface roughness (Ra) value. Ra values are influenced by pore diameter/pore area. Preferred Ra values for membranes having a good gloss are below 0.8 μm, more preferably below 0.5 μm, even more preferably below 0.3 μm and most preferably below 0.2 μm. A glossy appearance is thought to be determined
 20 mainly by the smoothness of the surface area between the pores. In ISO 13565-1 (1998) and JIS B0671-1 (2002) a method is described by which it is possible to determine the Ra value of the surface eliminating the contribution of the pores to the calculation. In a special embodiment the membrane is composed of distinct structures: an isotropic bulk matrix in the form of an open polymer
 25 network and a thin surface layer of a completely different structure. This surface layer or skin layer is a continuous layer having pores that are not connected and can be described as a perforated continuous layer. By varying the process and recipe conditions the number and size of surface pores can be controlled according to desired specifications. This surface layer is thought to
 30 contribute to the gloss of the membrane. For applications such as reversed

osmosis it may be preferred that there are no pores at all at the surface or only pores of a very small diameter, which means that the skin layer can be regarded as a closed continuous layer. For the application as ink receiving layer the surface layer is assumed to prevent the dyes present in the ink from
5 being absorbed deep into the membrane which would lead to a low optical density of the printed image. So the surface layer contributes to a high optical density. On the other hand a skin layer reduces the flow rate through the membrane which may result in worse drying properties. Therefore preferably this skin layer is thin, having a thickness less than 4 μm , more preferably the
10 thickness of the skin layer is between 0.04 and 3.0 μm or even thinner e.g. between 0.05 and 1.0 μm . Except for the thin skin layer the membrane is preferably symmetric, although an asymmetric structure to some extent is allowable.

An important characteristic of the membrane is the swellability of
15 the porous layer. In addition to the porosity the swellability contributes to the speed and capacity of solvent uptake. Depending on the desired properties, a certain balance can be selected between the porosity and the swellability. To attain a certain level of solvent uptake a high porosity can be combined with a low swelling behaviour or *vice versa*. This enables a large variation in
20 membrane structures all with a good solvent uptake speed. For membranes applied as ink receiving layer the swelling preferably is between 1 and 50 μm , more preferably between 2 μm and 30 μm , most preferably between 3 and 20 μm . Because the dry thickness of the porous layer may vary depending on the desired application the swelling is more appropriately expressed in a relative
25 way as a percentage of the dry thickness. Preferably the swelling is at least 5%, more preferably between 6 and 150% of the dry thickness of the porous membrane, even more preferably between 10 and 80%. The swelling in this invention is determined by subtracting the dry thickness of the layer before swelling from the swollen thickness of the layer after swelling, wherein the
30 swollen thickness represents the thickness of the layer after immersion in

20 °C distilled water for 3 minutes, and dry thickness represents the thickness of the layer being allowed to stand at 23 °C and 60%RH for more than 24 hours. The thickness of the layer can be determined by various methods. For example, there is a method in which after a sample is immersed in distilled water at a given temperature for a given time to swell the layer, while the swelling process is observed by touching the swollen layer continuously with a needle positioning sensor to measure the thickness of the layer before and after swelling. There is also a method to measure the height of the swollen layer by optical sensor without touching the surface, and subtracting the height of the dry layer to know the swelling amount of the layer. The degree of swelling can be controlled by the types and ratio of monomers, the extent of curing/cross-linking (exposure dose, photo-initiator type and amount) and by other ingredients (e.g. chain transfer agents, synergists).

Surprisingly the membrane due to its swelling character showed higher image densities when used as an ink receiving layer and an improved ozone fastness. Without wishing to be bound by theory, the researchers assume that due to swelling the colorants are incorporated in the polymer network structure and after drying are protected against the influences of ozone and other gasses. In a porous network without swelling capability the colorants can penetrate deep into the layer while by swelling the colorants are thought mainly to be trapped in the surface region of the layer explaining the increased density observed.

A disadvantage of a strongly swelling porous layer is a rather weak scratch resistance. A large swellability is achieved by a low degree of crosslinking which makes the structure of the membrane sensitive to physical disturbance. Surprisingly it was found that a second curing treatment of the dry membrane after drying is completed is more effective for enhancing the robustness than intensifying the curing of the wet coated layer. Again, without wishing to be bound by theory, the inventors suggest that by drying the unreacted curable double bonds are moving closer to each other, thereby

increasing the probability of crosslinking upon curing. This second curing step may be done by UV-curing, but also other methods are suitable such as EB-curing or other sources of radiation, *e.g.* those mentioned hereinabove. In case UV curing is applied for the second curing at least part of the photo-initiator
5 need to remain in reactive form after the first curing step. On the other hand it is important that finally essentially all photo-initiator has reacted because remaining photo-initiator may lead to yellowing of the membrane due to aging which is undesirable for certain applications. This can be easily achieved by tuning the initial concentration of the photo-initiator in the recipe.

10 Alternatively the photo-initiator for the second curing is added separately *e.g.* by impregnation.

Instead of a second curing of the membrane in the dry state the membrane may be cured while being wet. One way of execution is to perform the second curing shortly after the first curing without intermediate drying
15 step. Another way is to prewet the dried membrane by a liquid that may contain one or more ingredients such as surfactants. An advantage of this procedure is that in the wet state the membrane structure changes upon curing when the membrane is swellable in the liquid applied. So properties as porosity can be modified by performing a second curing step when the
20 membrane is in the swollen state. By this method a wider range of materials and process conditions become suitable since tuning of the structure remains possible after the initial curing step. In between both curing steps an impregnation can be carried out. By impregnation compounds can be brought into the membrane that are not very well compatible with the curable
25 composition of the first curing step. When the structure of the membrane after the first curing is already good, a second curing is superfluous and just drying after impregnation is sufficient. But when it is desired to fix the compounds brought in by impregnation to the matrix a second curing step is the preferred method of crosslinking. Preferably the membrane is partly dried before an
30 impregnation step is executed. By partial drying the compounds introduced by

impregnation e.g. by coating, spraying or dipping, can deeper penetrate into the membrane. By partial drying part of the solvent is removed, e.g. 25% or 50% and in some cases up to 80% of the solvent is removed prior to impregnation. With a good process design more than 2 curing steps will in general not result in improved properties, however certain circumstances such as limited UV intensity may make multiple curing beneficial.

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Preferably the exposure dose in the second curing step is between 80 and 300 mJ/m², more preferably between 100 and 200 mJ/m² as measured by an High Energy UV Radiometer (UV Power Puck™ from EIT – Instrument Markets) in the UV-B range indicated by the apparatus.

The porous membrane may also comprise one or more non-curable water soluble polymers and/or one or more hydrophilic polymers that are not crosslinked by exposure to radiation. The non-curable water soluble polymer may be added to the curable compound mixture before curing or applied to the cured membrane after curing.

In addition to a non-curable water soluble polymer, up to 20 wt.% crosslinking agent may be added, preferably between 0.5 and 5 wt.%, based on the amount of non-curable water soluble polymer in the layer. Suitable crosslinking agents are described in EP-A-1 437 229. The crosslinking agents can be used alone or in combination.

In one embodiment at least two mixtures are coated on a substrate of which at least one is a curable compound mixture, which after curing and drying results in a membrane comprising at least one top layer and at least one bottom layer that is closer to the substrate than the top layer. At least the top layer, and preferably also the bottom layer comprises the porous membrane of this invention. For a two-layer membrane structure the bottom layer preferably has a dry thickness of between 3 and 50 μm, preferably between 7 and 40 μm, most preferably between 10 and 30 μm and the toplayer preferably between 1 and 30 μm, preferably between 2 and 20 μm, most preferably between 4 and 15 μm.

In another embodiment a substrate is coated with at least three layers of which at least one layer, preferably the top (outer) layer comprises a curable compound mixture. After applying the curable compositions to the substrate, curing and drying, a membrane comprising at least three layers is formed, which three layers then comprise at least one bottom layer with a dry thickness of between 3 and 50 μm , preferably between 5 and 40 μm , most preferably between 7 and 30 μm , at least one middle layer with a dry thickness of between 1 and 30 μm , preferably between 2 and 20 μm , most preferably between 3 and 15 μm , and at least one toplayer above the middle layer. The top layer preferably has a dry thickness of less than 10 μm , preferably of between 0.1 and 8 μm , most preferably between 0.4 and 4 μm .

In a preferred embodiment, the substrate is coated with two, three or more curable compound mixtures, which after curing and drying results in a recording medium in which all layers are layers comprising a porous membrane of the invention. Said mixtures may have the same or different compositions depending on the results one likes to achieve. Furthermore the curable compound mixtures might be coated simultaneously and then cured or might be coated consecutively and cured. Consecutively means, that a first mixture is coated, then cured; then a second mixture is coated, cured and so on. In the latter situation it is likely that at least a part of the second mixture is impregnating the first layer so care has to be taken that the pores of the resulting membrane do not become blocked.

Preferably the top layer and the middle layer comprising the porous membrane of the present invention are essentially free from (porous) organic or inorganic particles that are capable of absorbing aqueous solvents. More preferably the porous membrane is essentially free from particles. Essentially free means here that the amount or location of particles is such that there is no significant decrease in gloss or colour density. A quantity of less than 0.1 g/m^2 is regarded as essentially free. Preferably all porous layers are essentially free from particles. An exception are matting agents, that are added to prevent

handling problems such as blocking, caused by a too smooth surface and which preferably are added in the top layer of the medium in a low amount. Usually less than 0.5% of the total solid content of the porous layer(s) is formed by matting agents.

5 It may be desirable to add in the toplayer a matting agent (also known as anti-blocking agents) to reduce friction and to prevent image transfer when several printed inkjet media are stacked. Very suitable matting agents have a particle size from 1 to 20 μm , preferably between 2 and 10 μm . The amount of matting agent is from 0.005 to 1 g/m^2 , preferably from 0.01 to 10 0.4 g/m^2 . In most cases an amount of less than 0.1 g/m^2 is sufficient. The matting agent can be defined as particles of inorganic or organic materials capable of being dispersed in an aqueous composition. The inorganic matting agents include oxides such as silicon oxide, titanium oxide, magnesium oxide and aluminium oxide, alkali earth metal salts such as barium sulphate, 15 calcium carbonate, and magnesium sulphate, and glass particles. The organic matting agents include starch, cellulose esters such as cellulose acetate propionate, cellulose ethers such as ethyl cellulose, and synthetic resins. The synthetic resins are water insoluble or sparingly soluble polymers which include a polymer of an alkyl(meth)acrylate, an alkoxyalkyl(meth)acrylate, a 20 glycidyl(meth)acrylate, a (meth)acrylamide, a vinyl ester such as vinyl acetate, acrylonitrile, an olefin such as ethylene, or styrene and a copolymer of the above described monomer with other monomers such as acrylic acid, methacrylic acid, alpha, beta -unsaturated dicarboxylic acid, hydroxyalkyl(meth)acrylate, sulfoalkyl(meth)acrylate and styrene sulfonic 25 acid. Further, a benzoguanamin-formaldehyde resin, an epoxy resin, polyamide, polycarbonates, phenol resins, polyvinyl carbazol or polyvinylidene chloride can be used. These matting agents may be used alone or in combination.

Usually the porous membrane has an opaque appearance due to the 30 porous structure of the matrix. Investigations revealed that a higher image

density can be obtained when the outer layer or layers are somewhat transparent. This can be achieved by modifying the structure of the outer layer in such a way that the porosity is less. An additional advantage of a less porous toplayer is a better gloss. Because solvent absorption speed is among
5 others dependent on porosity it is preferred that this more transparent toplayer is rather thin. Because the thickness of the more transparent layer usually does not correspond with the thickness of the toplayer as coated it may be more correct to refer to this layer as top region. Most effect of the transparency of the top region on image density is obtained when the colorants
10 are fixed in the upper layers of the membrane, preventing diffusion of the colorant to lower layers. Fixing can be achieved by incorporating into the membrane mordant functionality. For instance a curable mordant can be added to the curable composition or mordants that are non-curable can be added. Mordants are preferably added in the outer layer or layers *e.g.* in the
15 top layer and/or in the layer just below the toplayer. Preferably the mordants are cationic making them suitable to form complexes with anionic colorants and may be organic or inorganic. The organic and inorganic mordants may be employed alone independently or in combination with each other. A very suitable method to fix the mordants in the outer layer is to introduce negative
20 charges in the outer layer, for instance by applying anionic curable compounds in the curable composition.

A cationic mordant described above is preferably a polymeric mordant having a primary to tertiary amino group or a quaternary ammonium salt as a cationic group; a cationic non-polymeric mordant may also be
25 employed. Such a polymeric mordant is preferably a homopolymer of a monomer (mordant monomer) having a primary to tertiary amino group or a salt thereof, or a quaternary ammonium base, as well as a copolymer or a condensation polymer of such a mordant monomer with other monomers (hereinafter referred to as a non-mordant monomers). Such a polymeric
30 mordant may be in the form either of a water-soluble polymer or a water-

dispersible latex particle, *e.g.* a dispersion of a polyurethane. Suitable mordant monomers are for example alkyl- or benzyl ammonium salts comprising one or more curable groups such as vinyl, (di)allyl, (meth)acrylate, (meth)acrylamide and (meth)acryloyl groups.

5 A non-mordant monomer as described above is a monomer which does not contain a basic or cationic moiety such as a primary to tertiary amino group or its salt, or quaternary ammonium salt and which exhibits no or substantially slight interaction with a dye contained in the ink jet printing ink. Such a non-mordant monomer may for example be alkyl (meth)acrylates;
10 cycloalkyl (meth)acrylates; aryl (meth)acrylates; aralkyl esters; aromatic vinyls; vinyl esters; allyl esters. Any of the non-mordant monomers listed above may be employed alone or in combination with each other.

 An organic mordant is preferably a polyamine or a polyallylamine and its derivatives whose weight mean molecular weight is 100 000 or less. A
15 polyamine or its derivative may be any known amine polymer and its derivative. Such a derivative may for example be a salt of a polyamine with an acid (acid may for example be an inorganic acid such as hydrochloric acid, sulfuric acid, phosphoric acid and nitric acid, an organic acid such as
20 methanesulfonic acid, toluenesulfonic acid, acetic acid, propionic acid, cinnamic acid, (meth)acrylic acid and the like, a combination thereof, or those in which a part of the amine is converted into a salt), a derivative of a
polyamine obtained by a polymeric reaction, a copolymer of a polyamine with other copolymerizable monomers (such monomers may for example be
25 (meth)acrylates, styrenes, (meth)acrylamides, acrylonitrile, vinyl esters and the like).

 It is also possible to employ an inorganic mordant as a mordant, including a polyvalent water-soluble metal salt or a hydrophobic metal salt compound. An inorganic mordant of the invention is preferably an aluminium-containing compound, titanium-containing compound, zirconium-containing
30 compound, a compound of a metal in the series of Group IIIB in the periodic

table (salt or complex). Certain multivalent metal ions are known to be flocculating agents; well known example are aluminum and iron(III) salts such as poly(aluminum chloride) and the sulfates of both ions. These compounds may also be applied as mordants. At high concentrations these compounds may flocculate in the presence of other compounds in aqueous solution but at lower concentrations application as a clear solution is possible.

The amount of mordant is preferably from 0.01 to 5 g/m², more preferably from 0.1 to 3 g/m².

If the mordant is a relatively small molecule the mordant or the mordant-colorant complex may diffuse within the layer or to other layers causing reduced sharpness. This problem is also referred to as long term bleeding. A very good method to prevent diffusion of the mordant molecule is to incorporate negative charges into the polymer matrix of the porous membrane. Preferably curable compounds bearing a negative charge are added to the curable composition. Examples of these negatively charged curable compounds are ethenically unsaturated compounds having sulfonic or carboxylic or phosphoric acid group, or their metal (or ammonium) salts. Sulfonic acid derivatives are more preferred due to stronger binding with mordants. For example, (meth)acrylic acid-(sulfoalkyl)esters such as sulfopropyl acrylic acid and sulfopropyl methacrylic acid, (meth)acryl-(sulfoalkyl)amides such as 2-acryloylamido-2-methylpropane-1-sulfonic acid, styrenesulfonic acid, itaconic acid-(alkylsulfonic acid)ester, itaconic acid-bis-(alkylsulfonic acid)ester, maleic acid-(alkylsulfonic acid)ester, maleic acid-bis-(alkylsulfonic acid)ester, alkylsulfonic acid allyl ether, mercapto compounds such as mercaptoalkylsulfonic acid, and their metal/ammonium salts. When applied these negatively charged curable compounds are preferably added up to an amount of 30 wt.%, more preferably in an amount between 0.5 and 10 wt.% based on the weight of the curable compounds in the curable composition, most preferably between 1 and 5 wt.%. Better than by wt.% the introduced negative charges are expressed by equivalentents since a monomer molecule may

contain more than one negatively charged group and the MW of monomers may vary significantly. Preferably the porous membrane of the invention comprises up to 10 milli equivalents (meq) per m² with a minimum of 0.1 meq/m², more preferably between 0.3 and 5 meq/m², most preferably between 5 0.5 and 3 meq/m². The negatively charged compounds may be added to one composition or to the compositions for more than one layer.

Especially preferred are anionic curable compounds that comprise one or more functional thiol groups. These compounds then act as chain transfer agents which are known to be less sensitive to oxygen inhibition and 10 have a remarkable effect on the structure of the membrane: the porosity is less and the surface becomes smoother. Surprisingly the image density increases when chain transfer agents are applied, even in relatively low amounts. An additional advantage of the use of chain transfer agents is that the tackiness of the surface of the membrane after curing becomes less and the structure 15 becomes more rigid. Examples include mercaptoacetic acid, mercaptopropionic acid, alkyl mercaptopropionate, mercapto-propylsulfonate, ethyldithiocarbonato-S-sulfopropylester, dimercaptopropane sulfonate and mercaptobenzimidazole sulfonate.

Alternatively chain transfer agents that are non-ionic are added in 20 addition to or in stead of the negatively charged curable compounds to obtain similar effects on structure and surface properties. Classes of compounds that comprise suitable substances are mercaptans, polymethacrylates, polyhalo alkanes, benzoquinones, oximes, anthracenes, disulfides, sulfonyl chlorides, sulfoxides, phosphines, alkyl anilines, alkyl amines and metal compounds 25 (such as aluminum, iron, cobalt, copper salts or complexes). Preferred compounds are mercaptoethanol, mercaptoethylether, mercaptobenzimidazole, ethyldithioacetate, butanethiol, dimethyldisulfide, tetrabromomethane, dimethylaniline, ethylenedioxydiethanethiol and triethylamine.

A special class of chain transfer agents are so-called RAFT agents 30 (RAFT = Reversible Addition-Fragmentation chain Transfer). This RAFT

reaction is a controlled radical polymerization and generally leads to very narrow molecular weight distributions. Suitable RAFT agents comprise a dithioester group of the formula $R_1-C(=S)-S-R_2$, a xanthate group of the formula $R_1-O-C(=S)-S-R_2$ or a thioxanthate (trithiocarbonate) group of the formula $R_1-S-C(=S)-S-R_2$, a dithiocarbamate group of the formula $R_1-NR-C(=S)-S-R_2$ where R, R_1 and R_2 are selected from an alkyl group, a cycloalkyl group, an aryl group, a heterocyclic group or an arenyl group. Examples are ethyldithioacetate, benzyl dithiobenzoate, cumyl dithiobenzoate, benzyl 1-pyrrolicarbodithioate, cumyl 1-pyrrolicarbodithioate, o-ethyldithiocarbonato-S-(3-sulfopropyl) ester, N,N-dimethyl-S-thiobenzoylthiopropionamide, N,N-dimethyl-S-thiobenzoylthioacetamide, trithiocarbonates and dithiocarbamates.

Chain transfer agents can be characterized by a so-called chain transfer constant which preferably is larger than 0.1, more preferably larger than 1.0. For transfer constants lower than 0.1 no or only very limited effects are achieved. Optimum quantities depend very much on the composition of the curable composition, on the type of the chain transfer agent (reactivity) and on the irradiation dose so the optimum concentration has to be determined case by case. At high levels of chain transfer agents it was found that adhesion problems may occur if the compound is in the layer adjacent to the support. When a multilayer membrane is made the chain transfer agent is preferably in the toplayer where the effect on image density is expected to be the highest. Very high levels may retard the crosslinking reaction too much resulting in a dense non-porous layer or even a layer that is still uncured. Preferably the chain transfer agent is present in an amount between 0.001 and 1.0 mmol/g curable compound. For most compounds the preferred range will be between 0.005 and 0.1 mmol/g curable compound. If the membrane consists of more than one layer the mentioned range apply to the layer or layers comprising the chain transfer agent.

For adequate colorant fixing properties it is important to have a surplus of positive charges that can bind the negatively charged colorant

molecules. Preferably the ratio of negative charges present in the anionic curable compounds and positive charges present in the cationic compounds (e.g. mordants) is at least 1:1 and more preferably between 1:2 and 1:10.

Cationic mordants may coagulate with the negatively charged curable compounds if added to the curable composition. Therefore it is generally desirable not to add the mordants to the composition but to apply the mordants to the porous membrane after curing. This may be done by impregnation after partial drying or after complete drying. Impregnation can be performed e.g. by coating or by spraying a solution onto the membrane or by dipping the membrane into a solution. Metering coating such as slide or slot coating is preferred. After drying a porous membrane remains wherein the mordant molecules are trapped at the site where the negative charges are build in into the matrix.

In a preferred embodiment (part of the) cationic mordants are not introduced after curing but are combined with anionic curable compounds in the curable composition. These anionic and cationic compounds form complexes in solution which surprisingly do not precipitate but remain in solution. Those complexes appear to have a better solubility in monomer mixtures that have a limited compatibility with water. This limited compatibility with water makes these monomer mixtures very suitable to initiate phase separation. The single ionic compounds are thought to be more hydrophilic due to their charge than the complexes in which the charges are shielded. Also a combination of both methods (introduction in the curable composition and by impregnation) can be used. When after the membrane is made there is no surplus of positive charges or the surplus is insufficient to fix the dyes at high printing densities additional cationic compounds may be added in a subsequent step, e.g. by impregnation, after the membrane has been formed. So initially in the curable composition the ratio of negative charges present in the anionic curable compounds and positive charges present in the cationic compounds may be larger than 1, e.g. 2:1. Preferably this ratio

is reduced in a subsequent step as described above by introducing more cationic charges.

In general mordants are applied to fix the colorants (dyes) from ink. Since at least three colours are used in a colour printer and there exist many brands of ink usually a combination of mordants is required to fix all colorants. Ideally such a mix of mordants is capable of fixing all existing dyes.

Alternatively a medium is developed that is dedicated to certain types of ink by which a higher quality may be realized than with a medium suitable for all types of ink.

By impregnation all kinds of additives may be brought into the porous membrane. Preferably these additives are water soluble or may be dispersed or added as an emulsion. To maintain the porous character the total quantity of additives added should be lower than the total pore volume of the membrane, in other words the pores should not be completely filled with additives. The pH of the impregnation solution preferably is comparable to the pH of the porous membrane or if necessary may be adjusted to obtain a clear solution. The impregnation solution may be applied in a wide range of concentrations depending on the type of additives. A suitable concentration is between 1 and 20 wt.%, between 5 and 15 wt.% is more preferred. The impregnation coating may be a single layer, but may also be a multilayer. A multilayer is very suitable to direct one or more compounds to a desired region in the membrane. Compounds such as mordants and optical brighteners are preferably present in the top region of the membrane; by impregnating the membrane by a multilayer wherein these compounds are present in the toplayer these compounds will be located near the surface of the membrane. The toplayer of the impregnation solution is preferably an aqueous solution and may comprise mordants, optical brighteners, surfactants, curable monomers, amine synergists, water soluble polymers, transportability improving/ friction reducing agents, UV-absorbers, dye fading prevention agents (radical scavengers, light stabilisers, anti-oxidants), cross-linking

agents and conventional additives such as pH regulators, viscosity regulators, biocides, organic solvents. The subsequent second curing fixates the membrane structure through which the final state is obtained.

Also the non-curable water soluble polymer mentioned above can be brought into the porous membrane by impregnation.

Other additives that may be added to one or more of the curable compositions or may be included by impregnation are UV absorbing agents, brightening agents, anti-oxidants, light stabilising agents, radical scavengers, anti-blurring agents, antistatic agents and/or anionic, cationic, non-ionic, and/or amphoteric surfactants.

Suitable optical brighteners are disclosed in *e.g.* RD11125, RD9310, RD8727, RD8407, RD36544 and Ullmann's Encyclopedia of industrial chemistry (Vol. A18 p153-167), and comprise thiophenes, stilbenes, triazines, imidazolones, pyrazolines, triazoles, bis(benzoxazoles), coumarins and acetylenes. Preferred optical brightening agents to be used in the invention are water-soluble and comprise compounds selected from the classes distyrylbenzenes, distyrylbiphenyls, divinylstilbenes, diaminostilbenes, stilbenyl-2H-triazoles, diphenylpyrazolines, benzimidazoles and benzofurans. In a preferred embodiment the optical brightening agents are cationic and are trapped by negative sites present in the matrix. An effective method of applying these agents is by impregnation as described above. The positively charged optical brightening agents are preferentially trapped in the top region of the porous membrane where they have the most effect. Then lower amounts are sufficient compared with anionic agents that tend to diffuse through the complete layer of the membrane (or all layers in case of a multilayer membrane). Commercially available examples of suitable cationic optical brightening agents are Blankophor™ ACR (Bayer) and Leucophor™ FTS (Clariant).

Whiteness is suitably expressed by the b-value of the CIELAB color model. CIE L*a*b (CIELAB) is a color model used conventionally to describe

all the colors visible to the human eye. It was developed for this specific purpose by the International Commission on Illumination (*Commission Internationale d'Eclairage*, hence the *CIE* acronym in its name). The three parameters in the model represent the luminance of the color (**L**, the smallest L represents black), its position between red and green (**a**, the smallest a represents green) and its position between yellow and blue (**b**, the smallest b represents blue). For very white membranes low b-values are preferred, values between -5 and -8 indicate a very bright white appearance. Relatively high values (-4 and higher) indicate a more yellowish colour and are less preferred. Membranes with lower values (-8 and lower) tend to be bluish and are generally less preferred. The amount of optical brightening agent is preferably lower than 1 g/m²; more preferably between 0.004 and 0.2 g/m²; most preferably between 0.01 and 0.1 g/m².

Further the porous membrane may comprise one of more light stabilising agents such as sterically hindered phenols, sterically hindered amines, and compounds as disclosed in GB2088777, RD 30805, RD 30362 and RD 31980. Especially suitable are water-soluble substituted piperidinium compounds as disclosed in WO-A-02/55618 and compounds such as CGP-520 (Ciba Specialty Chemicals, Switzerland) and Chisorb 582-L (Double Bond Chemical, Taiwan). Other additives may be one or more plasticizers, such as (poly)alkylene glycol, glycerol ethers and polymer lattices with low Tg-value such as polyethylacrylate, polymethylacrylate and the like and one or more conventional additives, such as described for example in EP-A-1 437 229 and EP-A-1 419 984, and in international patent applications WO-A-2005/032832, WO-A-2005/032834 and WO-A-2006/011800 such as acids, biocides, pH controllers, preservatives, viscosity modifiers c.q. stabilisers, dispersing agents, inhibitors, anti-blurring agents, antifoam agents, anti-curling agents, water resistance-imparting agents and the like in accordance with the objects to be achieved.

The above-mentioned additives (UV absorbers, antioxidants, anti-blurring agents, plasticizers, conventional additives) may be selected from those known to a person skilled in the art and may be added in a range of preferably from 0.01 to 10 g/m². Any of the components mentioned above may
5 be employed alone or in combination with each other. They may be added after being solubilized in water, dispersed, polymer-dispersed, emulsified, converted into oil droplets, or may be encapsulated in microcapsules.

The porous membrane of the invention may be produced by the following steps:

- 10 - providing a mixture of at least one type of curable monomer and a solvent;
- applying said mixture to a support;
- curing said curable monomer mixture, thereby causing phase separation between the crosslinked monomer and the solvent;
- 15 - subjecting the formed porous membrane to a drying step to remove said solvent resulting in a membrane having a total surface pore area of between 0.3 and 18 % with respect to the surface area of said porous membrane and an average surface pore diameter of between 0.02 and 1.0 μm; and
- 20 - optionally separating the support and the porous membrane.

When high intensity UV light is applied for cross-linking the curable composition heat is generated by the UV lamp(s). In many systems cooling by air is applied to prevent the lamps from becoming overheated. Still a significant dose of IR light is irradiated together with the UV-beam. In one
25 embodiment the heating-up of the coated support is reduced by placing an IR reflecting quartz plate in between the UV lamp(s) and the coated layer that is guided underneath the lamp(s).

With this technique coating speeds up to 200 m/min or even higher, such as 300 m/min or more, can be reached. To reach the desired dose more
30 than one UV lamp in sequence may be required, so that the coated layer is

successively exposed to more than one lamp. When two or more lamps are applied all lamps may give an equal dose or each lamp may have an individual setting. For instance the first lamp may give a higher dose than the second and following lamps or the exposure intensity of the first lamp may be lower.

5 Surprisingly at constant dose the relative intensities appeared to have subtle effects on the photopolymerisation reaction which influences the porosity and the structure. By varying the exposure conditions a person skilled in the art can determine optimum settings for the process depending on the properties one wishes to achieve.

10 Whereas it is possible to practice the invention on a batch basis with a stationary support surface, to gain full advantage of the invention, it is much preferred to practice it on a continuous basis using a moving support surface such as a roll-driven continuous web or belt. Using such apparatus the curable composition can be made on a continuous basis or it can be made on a large
15 batch basis, and the composition poured or otherwise applied continuously onto the upstream end of the driven continuous belt support surface, the irradiation source being located above the belt downstream of the composition application station and the membrane removal station being further downstream of the belt, the membrane being removed in the form of a
20 continuous sheet thereof. Removal of the solvent from the membrane can be accomplished either before or after the membrane is taken from the belt. For this embodiment and all others where it is desired to remove the porous membrane from the support surface, it is, of course, preferable that the support surface be such as to facilitate as much as possible the removal of the
25 membrane therefrom. Typical of the support surfaces useful for the practice of such embodiments are smooth, stainless steel sheet or, better yet, teflon or teflon-coated metal sheet. Rather than using a continuous belt, the support surface can be of an expendable material, such as release paper or the like (but not soluble in the solvent), in the form of a roll thereof such that it can be
30 continuously unrolled from the roll, upstream of the solution application

station, as a continuous driven length and then rerolled, with the porous membrane thereon, downstream of the radiation station.

It is also within the purview of the invention to form the thin layer of solution as a coating on or intermingled and supported by a porous sheet or fibrous web to which the resulting membrane remains bounded and which can function, for example, as a strengthening reinforcement or backing for the porous membrane. Such porous support surface of which the porous membrane is formed should, of course, be of a material which is insoluble in the solvent used. Typical of the porous support surfaces which can be used for the practice of such embodiments are paper, woven and nonwoven fabric, and the like.

Embodiments are also recognized in which the porous material is not to be separated from a solid support, but in which the two bonded together are the desired final product. Examples of such embodiments are polyester film supported porous membranes which are utilized in electrophoretic separations, membranes attached to a transparent or opaque sheet to be used as recording media for images and the like.

As the support, any of a transparent support composed of a transparent material such as a plastic, and an opaque support composed of an opaque material such as a paper can be used. For most membrane applications the support – if present – must be porous to allow the passing of fluids or gasses. These porous supports can be paper, woven and nonwoven fabric. Examples of nonwoven fabric are materials based on cellulose, polyamide, polyester, polypropylene and the like.

As a material which can be used in the transparent support for recording media, materials which are transparent and have the nature of enduring the radiated heat upon use in Overhead Projection (OHP) and back light display are preferred. Examples of these materials include polyesters such as polyethylene terephthalate (PET), polyethylene naphthalate (PEN), triacetate cellulose (TAC), polysulfone, polyphenylene oxide, polyethylene, polypropylene, polyvinylchloride, polyimide, polycarbonate, polyamide and the

like. Other materials that may be used as support are glass, polyacrylate and the like. Inter alia, polyesters are preferable, and polyethylene terephthalate is particularly preferable.

The thickness of the transparent support is not particularly limited, however 50 to 200 μm is preferable from the viewpoint of the handling property.

As an opaque support having high gloss, a support with the surface on which a colorant receiving layer is provided, having a gloss of at least 5%, preferably 15% or larger, is preferable. The gloss is a value obtained according to the method of testing the specular surface gloss of the support at 75° (TAPPI T480).

Embodiments include paper supports having high gloss such as resin coated (RC) paper, baryta paper which are used in art paper, coated paper, cast coated paper, supports as used for silver salt photographic paper and the like; films having high gloss by making opaque plastic films such as polyesters, such as polyethylene terephthalate (PET), cellulose esters such as nitrocellulose, cellulose acetate, cellulose acetate butyrate, polysulfone, polyphenylene oxide, polyimide, polycarbonate, polyamide and the like (which may have the surface subjected to calender treatment) by containing of a white pigment or the like; or supports in which a covering layer of polyolefin containing or not containing a white pigment is provided on the surface of the aforementioned various paper supports, the aforementioned transparent support or films containing a white pigment or the like. An example of a suitable embodiment includes a white pigment-containing expanded polyester film (e.g. expanded PET which contains polyolefin fine particles and in which a void is formed by stretching).

The thickness of the opaque support is not particularly limited, however 50 to 300 μm is preferable from the viewpoint of the handling property.

As already mentioned an important characteristic of a recording medium is the gloss. The gloss is preferably larger than 20% at 20°, more preferably larger than 30% as measured by a Dr. Lange Refo 3-D reflectometer. It has been found that the gloss of the medium can be improved by selecting the appropriate surface roughness of the used support. It was found, that providing a support having a surface roughness characterised by the value Ra being less than 1.0 µm, preferably below 0.8 µm a very glossy medium can be obtained. A low value of the Ra indicates a smooth surface. The Ra is measured according to DIN 4776 using a UBM equipment, software package version 1.62, with the following settings:

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(1) Point density 500 P/mm, (2) Area 5.6 × 4.0 mm², (3) Cut-off wavelength 0.80 mm, (4) Speed 0.5 mm/sec.

In case paper is used as the support for the present invention the paper is selected from materials conventionally used in high quality printing paper. Generally it is based on natural wood pulp and if desired, a filler such as talc, calcium carbonate, TiO₂, BaSO₄, and the like can be added. Generally the paper also contains internal sizing agents, such as alkyl ketene dimer, higher fatty acids, paraffin wax, alkenylsuccinic acid, such as kymene, epichlorhydrin fatty acid amid and the like. Further the paper may contain wet and dry strength agents such as a polyamine, a poly-amide, polyacrylamide, poly-epichlorohydrin or starch and the like. Further additives in the paper can be fixing agents, such as aluminium sulphate, starch, cationic polymers and the like. The Ra value for a normal grade base paper is usually below 2.0 µm and may typically have values between 1.0 and 1.5 µm. The porous layer of the present invention or layers of which at least one comprises the porous layer of this invention can be directly applied to this base paper.

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In order to obtain a base paper with a Ra value below 1.0 µm such a normal grade base paper can be coated with a pigment. Any pigment can be used. Examples of pigments are calcium-carbonate, TiO₂, BaSO₄, clay, such as kaolin, styrene-acrylic copolymer, Mg-Al-silicate, and the like or combinations

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thereof. The amount being between 0.5 and 35.0 g/m² more preferably between 2.0 and 25.0 g/m². The paper can be coated on one side or on both sides. The amount mentioned before is the amount coated on one side. If both sides are coated the total amount preferably is between 4.0 and 50 g/m². This pigmented
5 coating can be applied as a pigment slurry in water together with suitable binders like styrene-butadiene latex, styrene-acrylate latex, methyl methacrylate-butadiene latex, polyvinyl alcohol, modified starch, polyacrylate latex or combinations thereof, by any technique known in the art, like dip coating, roll coating, blade coating, bar coating, size press or film press. The
10 pigment coated base paper may optionally be calendered. The surface roughness can be influenced by the kind of pigment used and by a combination of pigment and calendering. The base pigment coated paper substrate has preferably a surface roughness between 0.4 and 0.8 µm. If the surface roughness is further reduced by super calendering to values below 0.4 µm the
15 thickness and stiffness values will in general become rather low.

The porous layer or layers of which at least one comprises the porous layer of this invention, can be directly applied to the pigment coated base paper.

In another embodiment, the pigment coated base paper having a
20 pigmented top side and a back-side is provided on at least the topside with a polymer resin through high temperature co-extrusion giving a laminated pigment coated base paper. Typically temperatures in this (co-) extrusion method are above 280 °C but below 350 °C. The preferred polymers used are poly olefins, particularly polyethylene. In a preferred embodiment the polymer
25 resin of the top side comprises compounds such as an opacifying white pigment *e.g.* TiO₂ (anatase or rutile), ZnO or ZnS, dyes, colored pigments, including blueing agents, *e.g.* ultramarine or cobalt blue, adhesion promoters, optical brighteners, antioxidant and the like to improve the whiteness of the laminated pigment coated base paper. By using other than white pigments a
30 variety of colors of the laminated pigment coated base paper can be obtained.

The total weight of the laminated pigment coated base paper is preferably between 80 and 350 g/m². The laminated pigment coated base paper shows a very good smoothness, which after applying the porous layer or layers comprising the porous layer or layers of the present invention results in a recording medium with excellent gloss.

On the other hand, depending on the product one wants to make a polyethylene-coated paper can be used with a matt surface or silky surface such as is well known in the art. Such a surface is obtained by conducting an embossing treatment upon extruding a polyethylene on a paper substrate.

As is evident from the description given above, the recording media comprising the porous layer of this invention can be a single layer or a multi-layer applied onto a support. It can also comprise layers, which are non porous and are located below the porous layer.

The media including the inventive porous layer or layers, can be coated in one single step or in successive steps as long as the preferred pore sizes, and porosity is obtained.

As a coating method, any method can be used. For example, curtain coating, extrusion coating, air-knife coating, slide coating, roll coating method, reverse roll coating, dip coating, rod bar coating. This coating can be done simultaneously or consecutively, depending on the embodiments used. In order to produce a sufficiently flowable composition for use in a high speed coating machine, it is preferred that the viscosity does not exceed 4000 mPa.s at 25 °C, more preferably that it should not exceed 1,000 mPa.s at 25 °C.

Before applying the coating to the surface of the support material described above this support may be subjected to a corona discharge treatment, glow discharge treatment, flame treatment, ultraviolet light irradiation treatment and the like, for the purpose of improving the wettability and the adhesiveness.

When used as recording media the membranes of the present invention can be used for a multitude of recording applications so it is within

the scope of the present invention to provide recording media that are suitable for creating high quality images by using techniques as for example Giclée printing, color copying, screen printing, gravure, dye-sublimation, flexography, ink jet and the like.

5 Except for application in (inkjet) recording media, the porous membranes find use in a variety of other applications, such as in membranes for water treatment, in the chemical and petrochemical industry, for ultra filtration processes in the electrocoating of paint, in the food industry such as in the production process of cheese, clarification of fruit juice and in the beer
10 production, in the pharmaceutical industry where a high resistivity membrane for organic solvents is required, and in the biotechnology industry especially where flux reduction due to fouling by protein needs to be avoided. The membrane can be made suitable for nanofiltration or reversed osmosis by selecting appropriate ingredients and process conditions. The hydrophilic
15 character of the porous membrane according to this invention may result in a significant reduction of the fouling rate of the membrane and makes it suitable for all kind of other application where conventional micro- and ultra filtration is applied.

20 The present invention will be illustrated in more detail by the following non-limiting examples. Unless stated otherwise, all given ratios and amounts are based on weight.

Examples

25 The following coating solutions were prepared at room temperature with constant stirring.

 A three layer concept was used, wherein a bottom, middle and toplayer were applied to a support.

For the bottom (BL) layer the following solution was used:

Material	BL Recipe A	Units
CN-132	217.3	gram
Water	465.0	gram
Isopropanol	108.7	gram
CN-435	144.9	gram
AAMPSA	9.7	gram
1 N NaOH	45.7	gram
Irgacure™ 2959	8.7	gram

For the middle layer (ML) the following solution was used:

Material	ML Recipe A	Units
CN-132	217.3	gram
Water	467.9	gram
Isopropanol	108.7	gram
CN-435	144.9	gram
AAMPSA	9.7	gram
1 N NaOH	45.7	gram
Irgacure™ 2959	5.8	gram

For the top layer (TL) the following solution was used:

Material	TL Recipe A	Units
CN-132	217.3	gram
Water	363.8	gram
Isopropanol	81.5	gram
CN-435	144.9	gram
GMA-gelatin	41.9	gram
AAMPSA	9.7	gram
Zonyl™ FSN 3%	70.7	gram
PA10 – GMA-gelatin	24.6	gram
1 N NaOH	36.9	gram
Irgacure™ 2959	2.9	gram

CN-132 is an acrylate monomer supplied by Cray Valley.

CN-435 is an acrylate monomer supplied by Cray Valley.

5 GMA-gelatin is a 22% aqueous solution of GMA-modified gelatin in a weight ratio of 1:10. GMA is glycidylmethacrylate supplied by Sigma Aldrich. The gelatin used was a hydrolysed acid pigskin gelatin (7-8 kDa) (HAPG). AAMPSA is 2-acryloylamido-2-methyl-propanesulfonic acid monomer supplied by Sigma Aldrich.

10 Irgacure™ 2959 is a photo-initiator supplied by Ciba Specialty Chemicals.

Zonyl™ FSN is a fluoro-surfactant supplied by DuPont.

PA10 is a 10% dispersion of Orgasol™ 2001 polyamide beads with an average size of 10 µm, supplied by Arkema, in a 13 wt% solution of GMA modified gelatin (GMA:gelatin weight ratio is 1:10).

15

A photographic grade paper having polyethylene laminated at both sides was used as a support.

The solutions given above were coated simultaneously via a slide coating machine with a coating speed of 30 m/min. For the bottom, middle and toplayer an amount of 40, 15 and 5 cc/m² was applied respectively.

UV curing was applied using a Light Hammer 10 lamp of Fusion UV Systems Inc., placed in-focus, with varying intensity. After this curing process, the cured samples were dried for 3 minutes at 40°C, 8%RH.

To obtain differences in surface characteristics the process conditions were varied as mentioned in Table 1. The time interval between coating and curing was varied by changing the position of the lamp relative to the coating machine. Curing intensity is varied by changing the power supply to the lamp.

After drying and storage, several samples were additionally cured by Light Hammer™ 6 fitted in a bench-top conveyer LC6E (both supplied by Fusion UV) using 100% lamp intensity at a coating speed of 30 m/min.

15

Evaluation

Gloss

Gloss is determined by the Dr. Lange Refo 3-D reflectometer. After calibration the reflectometer is placed on the sample and the gloss value is recorded at an angle of 20°. The value in the table is an average of at least two independent measurements.

20

Surface structure

The surface structure (average pore diameter and relative total surface pore area) is determined from scanning electron microscopy (SEM) images. Of each sample 5 pictures were evaluated by image analysis software. Average values are given in Table 1.

25

Smearing test (drying speed)

	Equipment	: HP325 printer (paper: HP photo Paper, print quality: best)
	Ink	: HP344 (HP Vivera ink, black)
5	Image	: Line pattern, 6 x 0.8 mm line, 20 cc/m ²
	Friction by	: Eraser rubber (from a pencil supplied by Conté, France)
	Weight	: 30 gram
	Sample size	: 10 × 15 cm

10

A print image of high density black lines was made on the sample. These lines were printed with an interval of 4 seconds; after the last line was printed, the sheet was fed out of the printer immediately. On the outside of the printer a rubber eraser was positioned so that it touched the sheet during the transportation out of the interior of the printer. To the pencil a weight was attached to bring the weight of the eraser to 30 g. The lines were printed after 0, 4, 8, 12, 16, and 20 seconds respectively. Between the time the last line is printed and the moment the eraser touches the printed lines about 0.5 seconds passes. This method ensured that after printing the lines pass the fixed eraser after 0.5 – 4.5 – 8.5 – 12.5 – 16.5 – 20.5 seconds. If these lines are still wet, smearing of the black line will occur which can easily be judged by visual inspection.

20

SEM images

25

Figures 1, 2, 3 and 4 show the SEM images obtained for Samples 1, 2, 3 and 4, respectively. Each Sample was photographed at two different magnifications. The scale bar in the figures on the left-hand side represents 10 μm. The scale bare in the figures on the right-hand side represents 1 μm. Figure 5 shows a cross-section of sample 3 which is representative for the matrix structure of all samples.

30

Samples:*Table 1: process conditions and resulting surface parameters.*

sample	time interval coating – curing (sec)	curing intensity	gloss (20°)	average surface pore diameter (µm)	relative total surface pore area	average thickness of the surface layer (µm)	smearing (sec)
#1	14	70%	28	0.67	16	0.24	< 4
#2	4	70%	44	0.64	2	0.17	< 12
#3	7	70%	33	0.55	12	0.27	< 12
#4	7	100%	8	1.07	28	0.17	< 4

5 The curing intensity has a clear influence on the diameter of the pores and thus on the area covered by pores which influences the gloss. The time interval between coating and curing apparently has more effect on the number of pores. By changing process parameters pore size as well as number of pores can be controlled. With a low surface pore area a high gloss can be
10 obtained as shown by example 2. A large surface pore area and/or a large average size gives a relatively low gloss as is demonstrated by example 4.

 A person skilled in the art will understand that not only by process conditions but also by recipe changes of the curable composition the surface characteristics may be adjusted. This unique structure makes it possible to
15 combine the good absorbing properties of porous membranes with the glossy appearance of a continuous layer or less glossy membranes with a high flux or high speed of liquid uptake.

Claims

1. Porous membrane comprising an isotropic bulk matrix in the form of an open polymer network and at least one surface layer, which surface layer is a perforated continuous layer of which the average surface pore diameter is
5 between 0.02 and 1.2 μm , and wherein the thickness of said surface layer is smaller than the thickness of said bulk matrix.
2. Membrane according to claim 1, wherein the thickness of the surface layer is less than 4.0 μm , preferably between 0.04 and 3.0 μm , more preferably between 0.05 and 1.0 μm .
- 10 3. Membrane according to any of the previous claims, wherein the total pore area on the surface of said membrane is between 0.1 and 30%.
4. Membrane according to any of the previous claims wherein the average surface pore diameter is between 0.05 and 0.7 μm .
5. Membrane according to any of the previous claims wherein the total
15 pore area on the surface of said membrane is between 0.3 and 18%.
6. Membrane according to any of the previous claims wherein said membrane is essentially free from inorganic or organic particles that are capable of absorbing aqueous solvents.
7. Membrane according to any of the previous claims wherein said
20 membrane comprises at least three layers.
8. Membrane according to any of the previous claims wherein said membrane is formed by curing a curable composition comprising at least one type of curable compound and a photo-initiator by irradiation by UV-light.
9. Membrane according to claim 8, wherein said photo-initiator is an
25 alpha-hydroxyalkylphenone, an alpha-aminoalkylphenone, an alpha-sulfonylalkylphenone, an acylphosphine oxide or a combination thereof.

10. Process for obtaining a porous membrane according to any of the previous claims comprising the steps of:

- providing a mixture of at least one type of curable monomer and a solvent, wherein the concentration of said curable monomer is between 10wt% and 80wt%;
- applying said mixture to a support;
- curing said curable monomer mixture, thereby causing phase separation between the crosslinked monomer and the solvent;
- subjecting the resulting porous membrane of which the surface layer is a perforated continuous layer having average surface pore diameters between 0.02 and 1.2 μm and a thickness that is smaller than the thickness of said bulk matrix (preferably between 0.04 and 3 μm), to a drying step to remove said solvent; and
- optionally separating the support and the porous membrane.

11. Recording medium comprising a support and the porous membrane according to any of the claims 1-9 adhered to said support.

12. Medium according to claim 11 wherein said support is a transparent support suitable for back-lit applications and is selected from the group consisting of polyethylene terephthalate (PET), polyethylene naphthalate (PEN), polysulfone, polyphenylene oxide, polyimide, polycarbonate and polyamide.

13. Medium according to claim 11, wherein said support is a reflective support and is selected from the group consisting of a paper support, a plastic film and a support in which a covering layer of polyolefin optionally containing a white pigment is provided.

14. Use of a medium according to any of the claims 10-13 for printing images or characters thereon, using Giclée printing, colour copying, screen printing, gravure, dye-sublimation, flexography, and/or ink jet printing.

1/3

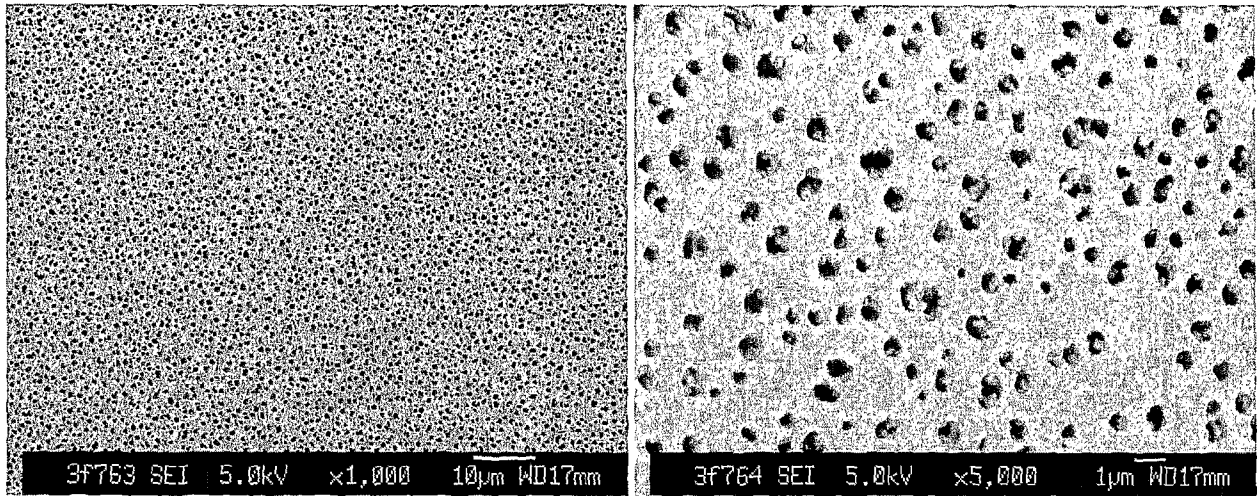


Fig. 1

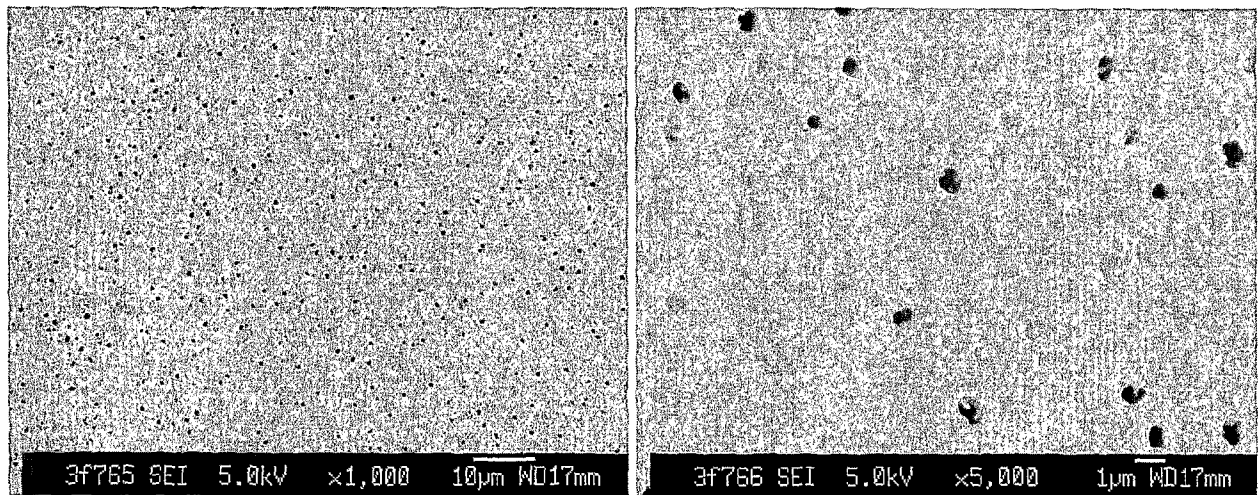


Fig. 2

2/3

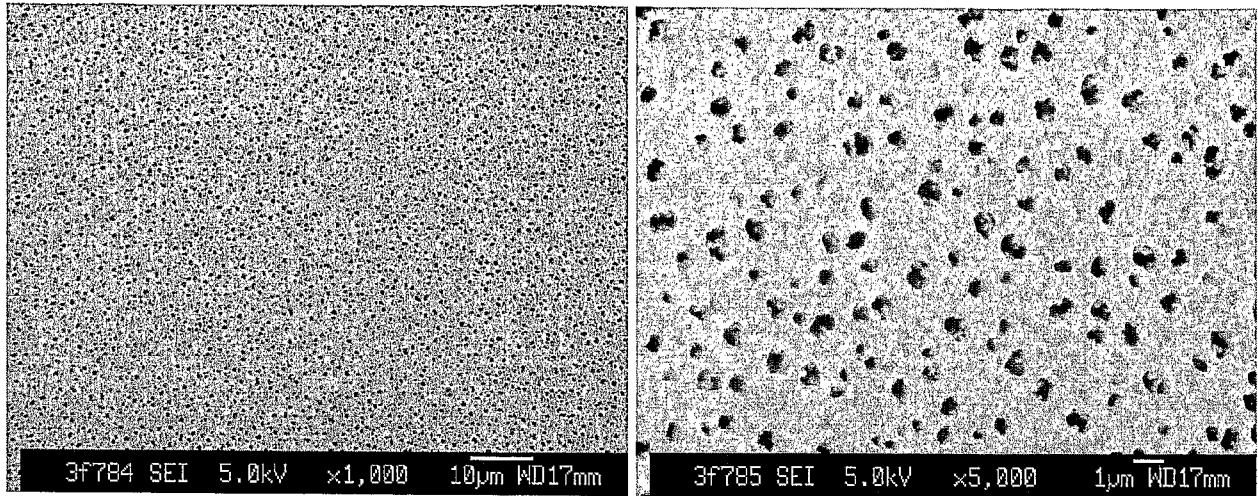


Fig. 3

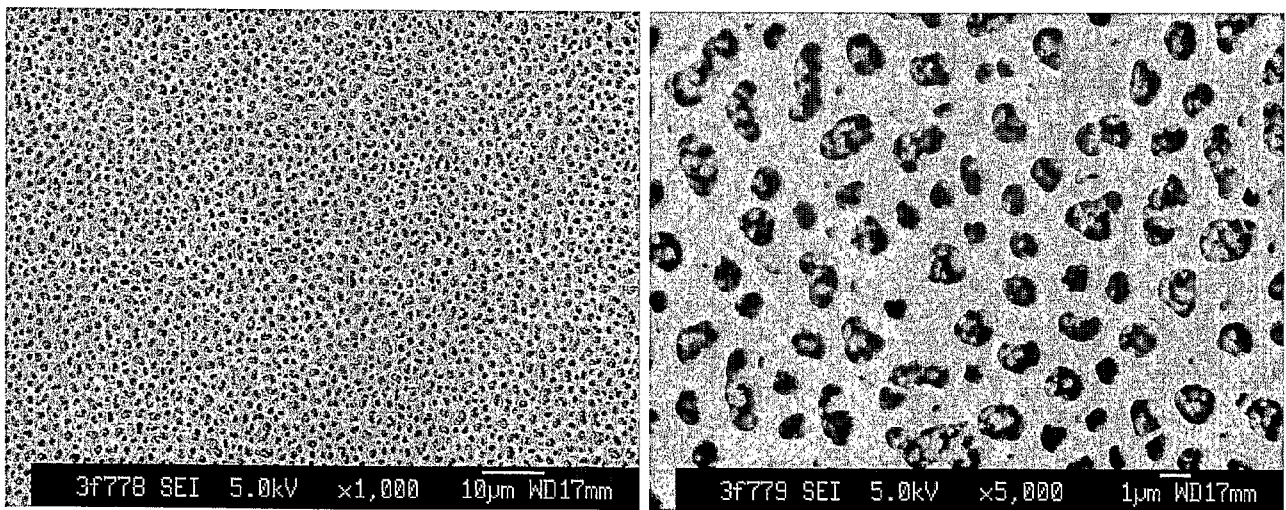


Fig. 4

3/3

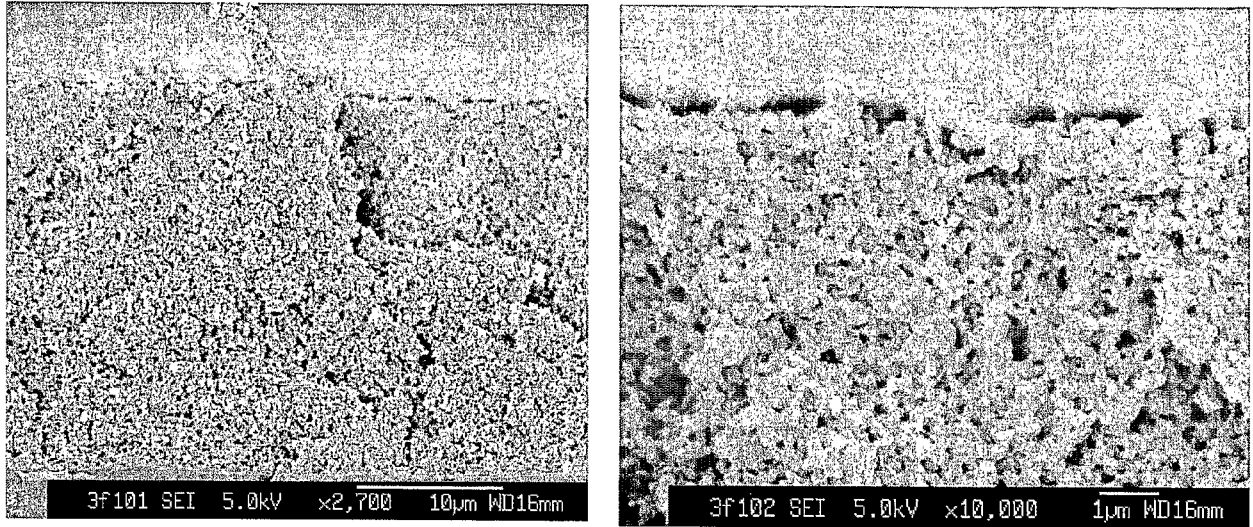


Fig. 5

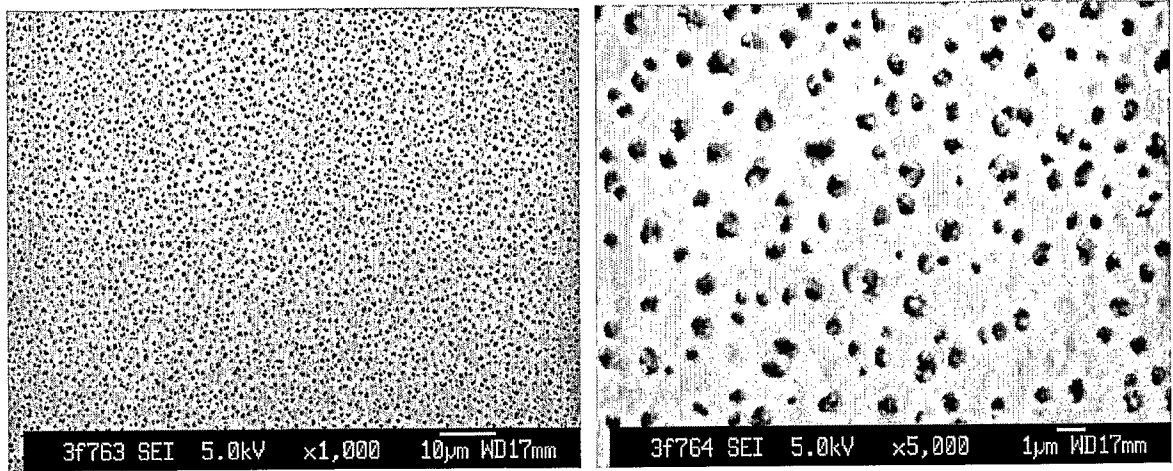


Fig. 1

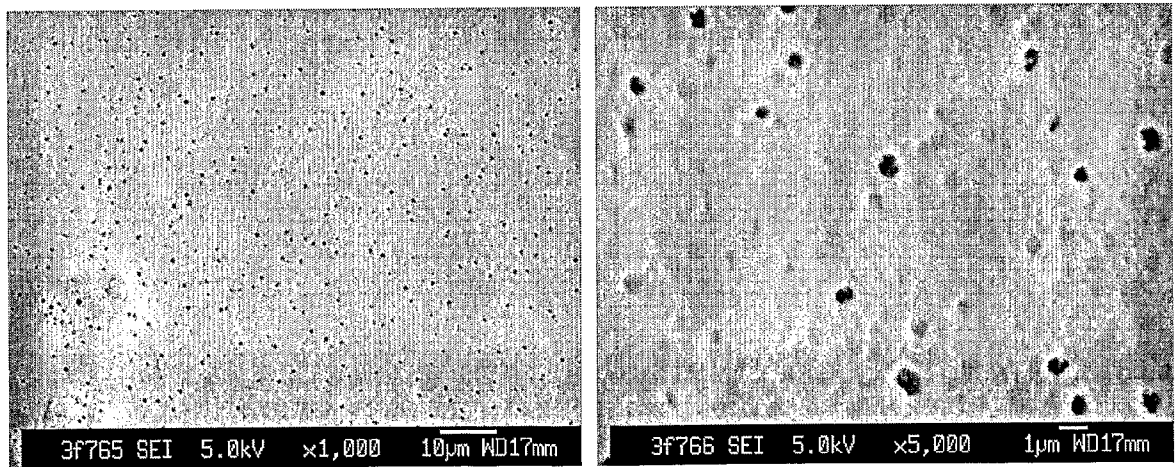


Fig. 2

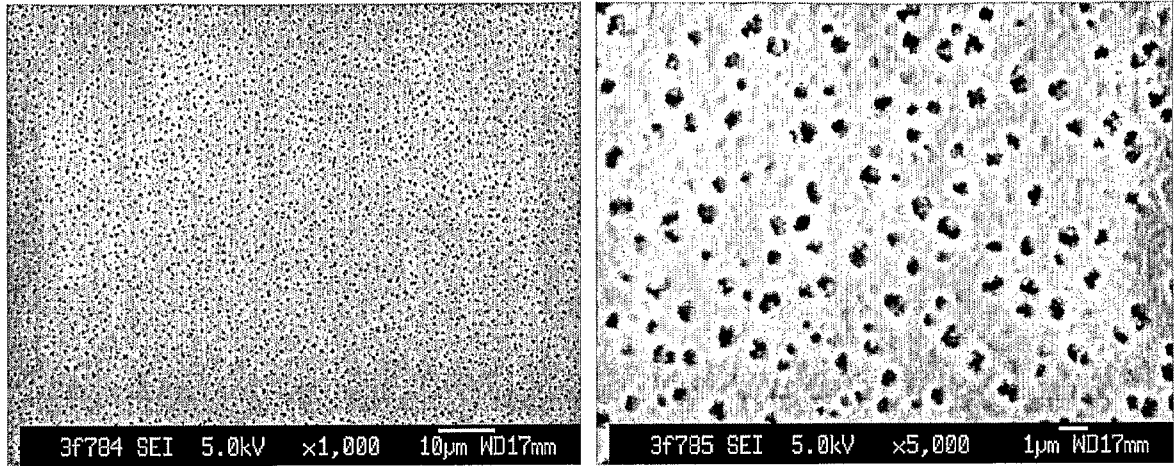


Fig. 3

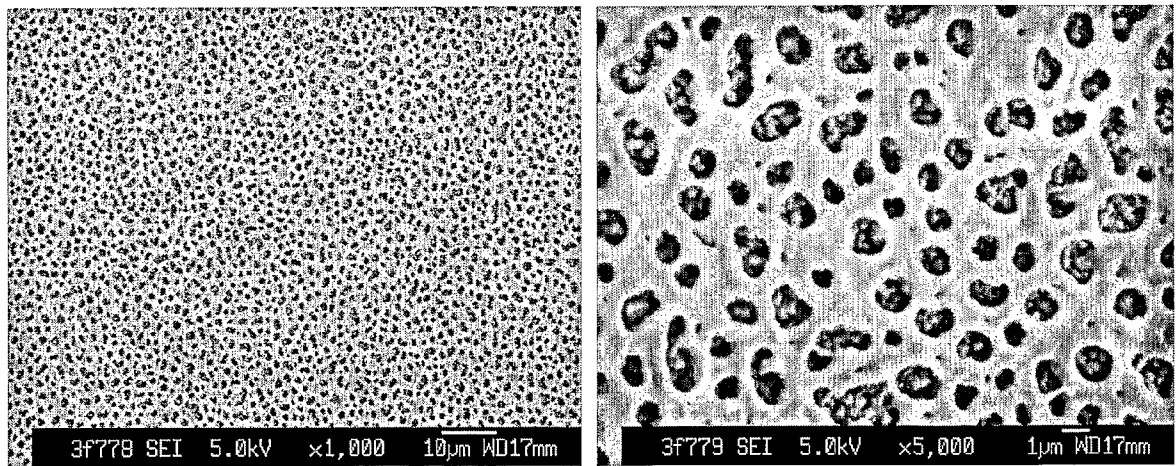


Fig. 4

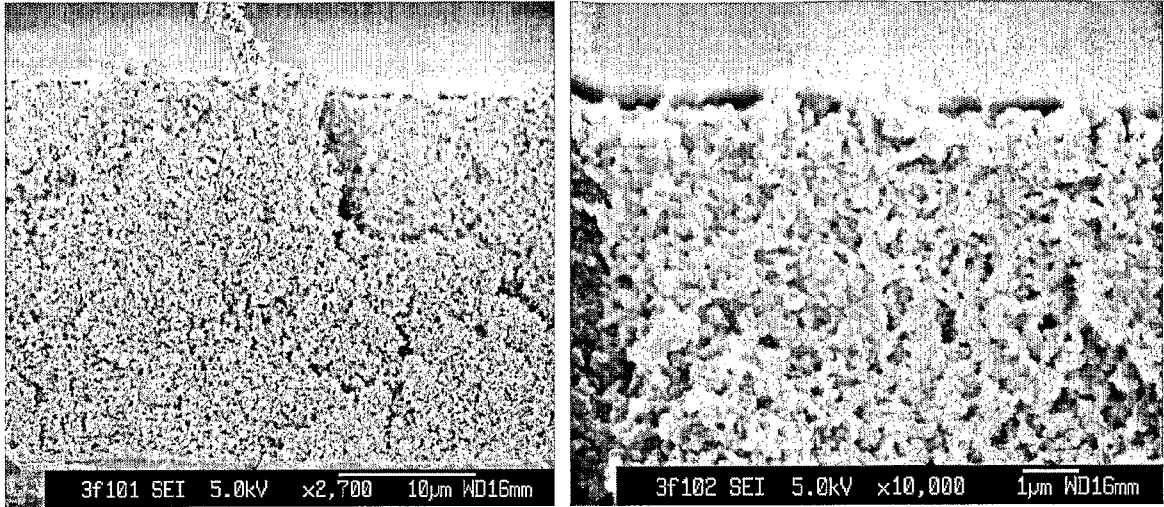


Fig. 5

INTERNATIONAL SEARCH REPORT

International application No
PCT/NL2006/000407

A. CLASSIFICATION OF SUBJECT MATTER
 INV. B01D67/00 B01D69/12 C08J5/22 B41M5/52 B01D69/02
 B01D69/10 B41M5/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
 B01D C08J B41M

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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X	WO 2005/016655 A (FUJI PHOTO FILM B.V; GANDASASMITA, ISKANDAR; VAN ES, ANDRIES, JOHANNES) 24 February 2005 (2005-02-24) cited in the application abstract page 4, line 26 - page 5, line 25 page 8, line 25 - line 29 page 15, line 24 - page 16, line 22 claims 1,9	1-14

Further documents are listed in the continuation of Box C.

See patent family annex.

* Special categories of cited documents :

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- * & * document member of the same patent family

Date of the actual completion of the international search

16 November 2006

Date of mailing of the international search report

08/12/2006

Name and mailing address of the ISA/

European Patent Office, P.B. 5618 Patentlaan 2
 NL - 2280 HV Rijswijk
 Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
 Fax: (+31-70) 340-3016

Authorized officer

Vogel, Thomas

INTERNATIONAL SEARCH REPORT

International application No
PCT/NL2006/000407

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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International application No

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