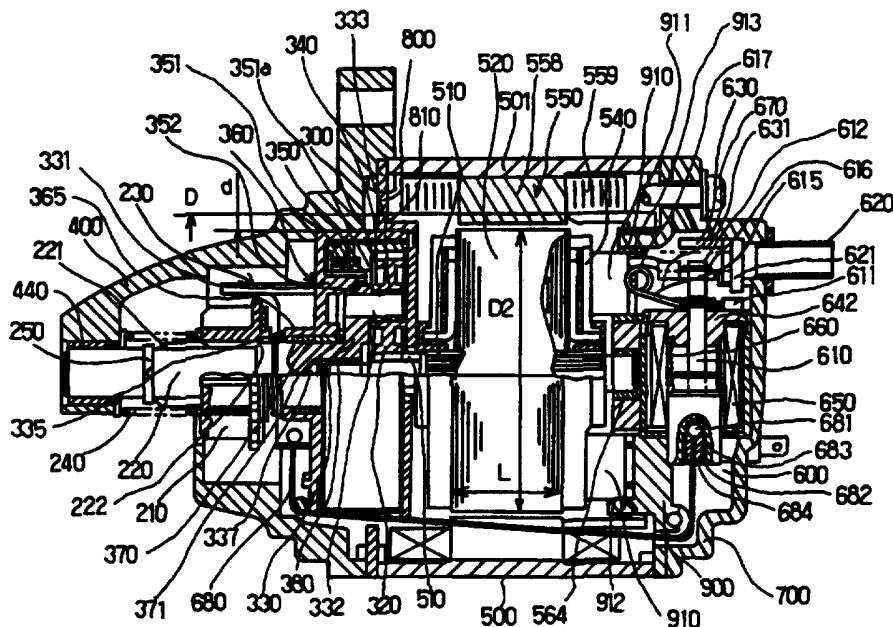




INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁶ : F02N 15/04, 11/00	A1	(11) International Publication Number: WO 96/16268 (43) International Publication Date: 30 May 1996 (30.05.96)
<p>(21) International Application Number: PCT/JP94/01987</p> <p>(22) International Filing Date: 24 November 1994 (24.11.94)</p> <p>(71) Applicant (for all designated States except US): NIPPON-DENSO CO., LTD. [JP/JP]; 1-1, Showa-cho, Kariya-city, Aichi-Pref. 448 (JP).</p> <p>(72) Inventors; and (75) Inventors/Applicants (for US only): SHIGA, Tsutomu [JP/JP]; Nippondenso Co., Ltd., 1-1, Showa-cho, Kariya-city, Aichi-Pref. 448 (JP). HAYASHI, Nobuyuki [JP/JP]; Nippondenso Co., Ltd., 1-1, Showa-cho, Kariya-city, Aichi-Pref. 448 (JP). OHMI, Masanori [JP/JP]; Nippondenso Co., Ltd., 1-1, Showa-cho, Kariya-city, Aichi-Pref. 448 (JP). KAJINO, Sadayoshi [JP/JP]; Nippondenso Co., Ltd., 1-1, Showa-cho, Kariya-city, Aichi-Pref. 448 (JP).</p> <p>(74) Agent: USUI, Hirohiko; Nippondenso Co., Ltd., 1-1, Showa-cho, Kariya-city, Aichi-Pref. 448 (JP).</p>	<p>(81) Designated States: AU, BR, CN, JP, KR, US, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).</p> <p>Published With international search report.</p>	

(54) Title: STARTER WITH PLANETARY REDUCTION GEAR MECHANISM



(57) Abstract

On the outer circumference of an armature core (520), there are arranged a stator core (558) forming a field pole and a stator coil (559) wound on the stator core (558). The stator coil (559) has its one end portion arranged in the space at the outer circumference of a planetary reduction gear mechanism (300), i.e., at the outer circumference of a center bracket (360). A motor partition (800) is formed with a stepped portion (810) so as to accommodate the aforementioned one end portion. On the other hand, the other end of the stator coil (559) is arranged in the space at the outer circumference of a brush (910). In short, the planetary reduction gear mechanism (300) has its external diameter (d) made smaller than the inner circumferential diameter (D) of the stator coil (559).

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgystan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Larvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

DESCRIPTION**TITLE OF THE INVENTION**

Starter with Planetary Reduction Gear Mechanism

TECHNICAL FIELD

5 The present invention relates to a starter with a planetary reduction gear mechanism for starting an engine.

BACKGROUND ART

10 In the starter with the planetary reduction gear mechanism of the prior art, there is disclosed in Japanese Patent Laid-Open No. 110931/1988 a face type commutator for a starter motor, which is formed generally perpendicularly to the axial direction of an armature shaft.

 However, the construction of the prior art specified above has the following problems.

15 Since this construction has an overlapping structure of the planetary reduction gear mechanism, a field pole of the starter motor, a brush device and a magnet switch on a common axis, the axial structure is further increased if the starter motor is enlarged to improve the output, so that the starter
20 has its engine mountability seriously deteriorated. At the time of mounting the starter on the engine, still the worse, the length from mounting face to the motor and the magnet switch is increased to deteriorate the impact-resistance.

 The present invention has been conceived in view of the

background described above and has a first object to provide a starter with a planetary reduction gear mechanism, which has its axial length suppressed and its mountability and impact-resistance improved.

5

DISCLOSURE OF THE INVENTION

In order to achieve the above-specified object, according to the present invention, there is provided a starter with a planetary reduction gear mechanism, comprising: a starter motor including an armature shaft for rotatably holding
10 an armature core wound with an armature coil, a commutator connected with the armature coil and arranged generally in parallel with the end portion of the armature core, a brush slidably held by the commutator, and a field pole arranged on the outer circumference of the armature core; and a planetary
15 reduction gear mechanism including a sun gear formed on the outer circumference of the armature shaft of the starter motor, a planetary gear borne on one end of a drive shaft arranged coaxially with the armature shaft and meshing with the sun gear, and an internal gear meshing with the planetary gear,
20 wherein the field pole of the starter motor has its end portion overlapping at least one of the planetary reduction gear mechanism and the brush.

25

According to this construction, the field pole of the starter motor has its end portion overlapping either the outer
circumference of the planetary reduction gear mechanism or the
outer circumference of the brush so that the axial length of

the field pole required in the prior art can be absorbed by the space at the outer circumference thereby to reduce the axial length. As a result, the starter can have its mountability and impact-resistance improved. Since, moreover, the armature core
5 can have its external diameter enlarged, the torque can be set to a high value to improve the starter.

In addition, the armature coil has its end portion arranged generally in parallel with the end face of the armature core, and wherein the coil has its end portion formed
10 as a commutator.

According to this construction, the armature coil has its end portion arranged generally in parallel with the end face of the armature core and used as the commutator. As a result, the axial length of the armature itself can be remarkably
15 reduced without requiring the commutator of the prior art, and the field pole can have its end portion arranged in the space of the outer circumference of the brush so that the axial length of the starter can be totally reduced.

In addition, there is further comprised a magnet switch
20 for supplying an electric power to the starter motor, said magnet switch being arranged at the brush side of the starter motor and generally perpendicularly to the axial direction of the armature shaft.

According to this construction, the magnet switch is
25 arranged at the brush side of the starter motor and generally perpendicularly to the axial direction of the armature shaft, so that the axial length to the end portion of the magnet

switch can be further reduced.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a sectional side elevation showing an embodiment of a starter of the present invention. Figs. 2A and 2B are a front elevation and a partially sectional side elevation when a pinion rotation regulating member is assembled with a pinion portion. Fig. 3 is a partially sectional side elevation of an armature. Fig. 4 is a top plan view of a core plate. Fig. 5 is a side elevation of an upper coil bar. Fig. 6 is a front elevation showing the upper coil bar. Fig. 7 is a schematic perspective view showing the arranged state of the upper coil bar and a lower coil bar. Fig. 8 is a section of an upper coil member and a lower coil member to be fitted in slots. Fig. 9 is a front elevation of an upper coil end assembled with the core of an armature. Fig. 10 is a front elevation of an insulating spacer. Fig. 11 is a sectional side elevation of a fixing member. Fig. 12 is a sectional side elevation of an insulating cap. Fig. 13 is a perspective view showing the plunger of the magnet switch. Fig. 14 is a section of an end frame. Fig. 15 is a section of a brush holder. Fig. 16 is a sectional side elevation of the brush holder. Figs. 17A, 17B and 17C are electric circuit diagrams showing the working states of the pinion.

BEST MODE FOR CARRYING OUT THE INVENTION

Next, a starter of the present invention will be

described in connection with its one embodiment with reference to Figs. 1 to 17C.

The starter is coarsely divided into: a housing 400 enclosing a pinion 200 meshing with a ring gear 100 arranged at an engine and a planetary gear mechanism 300; a motor 500; and an end frame 700 enclosing a magnet switch 600. In the starter, moreover, the housing 400 and the motor 500 are partitioned by a motor partition 800, and the motor 500 and the end frame 700 are partitioned by a brush holding member 900.

[Pinion 200]

As shown in Fig. 1, 2A or 2B, the pinion 200 is formed with a pinion gear 210 meshing with the ring gear 100 of the engine.

The pinion gear 210 is formed in its circumference with a pinion helical spline 211 to be fitted in a helical spline 221 formed in an output shaft 220. The pinion gear 210 is formed, at the side opposed to the ring gear, with an annular flange 213 having a larger diameter than the external diameter of the pinion gear 210. This flange 213 is formed all over its outer circumference with teeth 214 having a larger number than that of the external teeth of the pinion gear 210. These teeth 214 are provided for fitting a regulating pawl 231 of a later-described pinion rotation regulating member 230. A washer 215 is made rotatable at the rear face of the flange 213 but prevented from axially coming out by bending an annular portion 216, which is formed at the rear end of the pinion gear 210, toward the outer circumference.

On the other hand, the pinion gear 210 is always urged backwards of the output shaft 220 by a return spring 240 made of a compression coil spring.

[Pinion Rotation Regulating Member 230]

5 Here will be described the operations of the pinion rotation regulating member 230. A string member 680 is transmission means for transmitting the operation of the magnet switch 600 to the regulating pawl 231. The string member 680 is caused by the operation of the magnet switch 600 to pull the
10 rotation regulating portion 232 downwards thereby to establish the engagement between the regulating pawl 231 and the teeth 214 of the flange 213 of the pinion gear 210. Since the regulating pawl 231 engages with the teeth 214 of the pinion gear 210, the pinion gear 210 is moved forwards, when turned
15 through an armature shaft 510 of the motor 500 and the planetary reduction mechanism 300, along the helical spline 221 of the output shaft 220. When the pinion gear 210 comes into abutment against the ring gear 100 so that its forward movement is blocked, the pinion rotation regulating member 230 itself is
20 bent by the further rotating force of the output shaft 210 so that the pinion gear 210 is slightly rotated to mesh with the ring gear 100. As the pinion gear 210 moves forwards, the regulating pawl 231 goes out of engagement with the teeth 214 so that the regulating pawl 231 drops at the back of the flange
25 213 of the pinion gear 210 to have its front end abutting against the rear face of the washer 215 thereby to prevent the pinion gear 210 from being retracted by the rotation of the

ring gear 100 of the engine.

[Planetary Gear Mechanism 300]

The planetary gear mechanism 300 is reduction means for reducing the rotational speed of the later-described motor 500 to augment the output torque of the motor 500, as shown in Fig. 1. This planetary gear mechanism 300 is composed of: a sun gear 310 formed on the outer circumference of the front side of the armature shaft 510 (as will be described later) of the motor 500; three pairs of planetary gears 320 made rotatable around the sun gear 310; a planet carrier 330 made integral with the output shaft 220 for supporting the planetary gears 320 rotatably around the sun gear 310; and an internal gear 340 made of a resin into a cylindrical shape meshing with the outer circumferences of the planetary gears 320.

[Overrunning Clutch 350]

The overrunning clutch 350 is so supported as to rotate the internal gear 340 only in one direction (to rotate in response to the revolution of the engine). This overrunning clutch 350 is composed of a clutch outer 351 made integral with the front side of the internal gear 340 to form a first cylindrical portion, an annular clutch inner 352 formed at the rear face of a center bracket 360 to form the stationary side covering the front of the planetary gear mechanism 300 and a second cylindrical portion arranged to confront the inner circumference of the clutch outer 351, and rollers (not shown) fitted in a roller path 351a formed at an inclination in the inner circumference of the clutch outer 351.

[Center Bracket 360]

The center bracket 360 is arranged in the rear side of the housing 400. The housing 400 and the center bracket 360 are connected by a ring spring (not shown), which has its one
5 end retained by the housing 400 and its other end retained by the center bracket 360, so that the rotational reaction to be received by the clutch inner 352 forming part of the overrunning clutch 350 may be absorbed by the ring spring and prevented from being transmitted directly to the housing 400.

10 [Planet Carrier 330]

The planet carrier 330 is equipped at its rear end with a flanged projection 331 radially extending for supporting the planetary gear 320. In this flanged projection 331, there is
15 fixed a pin 332 extending backwards for supporting the planetary gear 320 rotatably through a metal bearing 333.

Moreover, the planet carrier 330 is rotatably supported by a housing bearing 440 having its front end portion fixed in the front end of the housing 400, and a center bracket bearing 370
20 fixed in an inner cylindrical portion 365 of the inner circumference of the center bracket 360.

This planet carrier 330 is formed at its front end with an annular groove, in which is fitted a stop ring 335. Between this stop ring 335 and the front end of the inner cylindrical
25 portion 365, there is interposed a washer which is made rotatable with respect to the planet carrier 330. When the stop ring 335 comes into abutment against the front end of the inner cylindrical portion 365 through the washer, the planet

carrier 330 is regulated from moving backwards. Moreover, the center bracket bearing 370 supporting the rear side of the planet carrier 330 is formed at its rear end with a flanged portion 371 which is interposed between the rear end of the inner cylindrical portion 365 and the flanged projection 331. When this flanged projection 331 comes into abutment against the rear end of the inner cylindrical portion 365, the planet carrier 330 is regulated from moving forwards.

Incidentally, an axially extending recess 337 is formed in a rear face of the output shaft 220. A shaft 510 has its front end rotatably supported through a planet carrier bearing 380 which is arranged in that recess 337.

[Motor 500]

The motor 500 is enclosed by the yoke 501, the motor partition 800 and the later-described brush holding member 900. Incidentally, the motor partition 800 accommodates the planetary gear mechanism 300 together with the center bracket 360 and acts to prevent the lubricating oil in the planetary gear mechanism 300 from invading the motor 500.

The motor 500 is constructed of, as shown in Fig. 1: the armature 540 composed of the armature shaft 510, and the armature core 520 and an armature coil 530 fixed on the armature shaft 510 and made rotatable together; and stationary magnetic poles 550 for rotating the armature 540. These stationary magnetic poles 550 are fixed on the inner circumference of the yoke 501.

[Armature Shaft 510]

The armature shaft 510 is rotatably borne by the planet carrier bearing 380 in the rear portion of the planet carrier 330 and a brush holding member bearing 564 fixed in the inner circumference of the brush holding member 900. The armature shaft 510 has its front end inserted in the planetary gear mechanism 300 and formed on its outer circumference with the sun gear 310 of the planetary gear mechanism 300.

[Armature Core 520]

The armature core 520 is prepared by laminating a number of core plates 521, as shown in Fig. 4, and by press-fitting the armature shaft 510 in the hole 522 which is formed in the center of the laminate. The core plate laminate 521 is formed by pressing thin steel sheets and by insulating its surfaces. The core plate laminate 521 is formed in the radially internal side (or around the hole 522) with a plurality of punched holes 523 for lightening the core plate laminate 521 itself. This core plate laminate 521 is formed in its outer circumference with a plurality of (e.g., twenty five) slots 524 for receiving the armature coil 530. Moreover, the outer circumferential end of the core plate laminate 521 is formed between the individual slots 524 with fixing pawls 525 for fixing the armature coil 530 in the slots 524. The fixing pawls 525 will be described in the description of means for fixing the following armature coil 530.

[Armature Coil 530]

The armature coil 530 adopted in the present embodiment is a double-layer coil which is prepared by radially laminating

a plurality of (e.g., twenty five) upper-layer coil bars 531 and lower-layer coil bars 532 of the same number as that of the upper-layer coil bars 531. Moreover, these individual upper-layer coil bars 531 and lower-layer coil bars 532 are
5 combined to have their end portions electrically connected to constitute an annular coil.

[Upper-Layer Coil]

The upper-layer coil bar 531 is made of a material having an excellent conductivity (e.g., copper) and is formed
10 with: an upper-layer coil member 533 extending in parallel with the stationary magnetic poles 550 and held on the outer circumferential side of the slots 524; and two upper-layer coil ends 534 bent inwards from the two ends of the upper-layer coil member 533 and extending perpendicularly to the axial direction
15 of the armature shaft 510. Incidentally, the upper-layer coil member 533 and the two upper-layer coil ends 534 may be formed: integrally by the cold-casting; by the pressing into the C-bent shape; or by the seaming technique of welding the upper-layer coil member 533 and the two upper-layer coil ends 534 made
20 separate.

The upper-layer coil member 533 is a straight bar having a square section, as shown in Figs. 5 to 8, and is so forced together with a later-described lower-layer coil member 536 into the slots 524 that it is covered with an upper-layer
25 insulating film (e.g., a thin film of a resin such as nylon or paper), as shown in Fig. 8.

Of the two upper-layer coil ends 534, as shown in Fig.

7, one upper-layer coil end 534 is inclined at the forward side with respect to the rotating direction whereas the other upper-layer coil end 534 is inclined at the backward side with respect to the rotating direction. These two upper-layer coil ends 534 are radially inclined at an equal angle with respect to the upper-layer coil member 533 and are formed into an identical shape. As a result, the upper-layer coil bar 531 takes its identical shape even after it is turned by 180 degrees on the upper-layer coil bar 531. In short, the two upper-layer coil ends 534 are made identical to provide an excellent workability when the upper-layer coil bar 531 is assembled with the armature core 520.

Of the two upper-layer coil ends 534, the upper-layer coil end 534, as located at the side of the magnet switch 600, comes into direct abutment against later-described brushes 910 to feed an armature coil 530 with the electric power. For this, at least the surface of the upper-layer coil ends 534, against which the brushes 910 are to abut, is smoothed. The starter of the present embodiment need not be equipped with any independent commutator for energizing the armature coil 530. In short, the independent commutator can be eliminated to reduce the number of parts and steps of manufacturing the starter thereby to suppress the production cost. Since, moreover, the starter need not be arranged therein with the independent commutator, another effect is that the starter can be axially small-sized.

Furthermore, the upper-layer coil ends 534 come into

direct abutment against the brushes 910 so that the heat to be generated by the sliding contact between the upper-layer coil ends 534 and the brushes 910 propagates from the upper-layer coil ends 534 to the upper-layer coil member 533, the armature core 520 and the armature shaft 510. Since, however, the armature coil 530, the armature core 520 and the armature shaft 510 have larger heat capacities than those of the independent commutator of the prior art, the sliding contact portions between the upper-layer coil ends 534 and the brushes 910 can be kept at a low temperature.

[Lower-Layer Coil Bar 532]

The lower-layer coil bar 532 is made, like the upper-layer coil bar 531, of a material having an excellent conductivity (e.g., copper) and is formed with: the lower-layer coil member 536 extending in parallel with the stationary magnetic poles 550 and held on the inner side of the slots 524; and two lower-layer coil ends 537 bent inwards from the two ends of the lower-layer coil member 536 and extending perpendicularly of the axial direction of the shaft 510. Incidentally, the lower-layer coil member 536 and the two lower-layer coil ends 537 may be formed, as in the upper-layer coil bar 531: integrally by the cold-casting; by the pressing into the C-bent shape; or by the seaming technique of welding the lower-layer coil member 536 and the two lower-layer coil ends 537 made separate.

Incidentally, the insulations between the individual upper-layer coil ends 534 and the individual lower-layer coil

ends 537 are retained by the insulating spacer 560, and the insulations between the individual lower-layer coil ends 537 and the armature core 520 are retained by an insulating ring 590 made of a resin (e.g., nylon or phenolic resin).

5 The lower-layer coil member 536 is a straight bar having a square section, as shown in Figs. 7 and 8, and is forced together with the upper-layer coil member 533 into the slots 524, as shown in Fig. 3. Incidentally, the lower-layer coil member 536 is so fitted in the slots 524 together with the
10 upper-layer coil member 533 covered with the upper-layer insulating film 125, while being covered with a lower-layer insulating film 105 (made of nylon or paper).

 Of the two lower-layer coil ends 537, one lower-layer coil end 537, as located at the front side of the starter, is
15 inclined in the direction opposed to that of the upper-layer coil end 534 whereas the other lower-layer coil end 537 at the rear side is also inclined in the direction opposed to that of the upper-layer coil end 534. These two lower-layer coil ends 537 are radially inclined at an equal angle with respect to the
20 lower-layer coil member 537 and are formed into an identical shape. As a result, like the upper-layer coil bar 531, the lower-layer coil bar 531 takes its identical shape even after it is turned by 180 degrees on the lower-layer coil bar 532. In short, the two lower-layer coil ends 537 are made identical
25 to provide an excellent workability when the lower-layer coil bar 532 is assembled with the armature core 520.

 The two lower-layer coil ends 537 are formed at their

inner circumferential end portions with lower-layer inner extensions 539 extending in the axial direction. The lower-layer inner extensions 539 have their outer circumferences fitted in the recesses 562, which are formed in the inner circumferences of the insulating spacer 560, and overlapped on and electrically and mechanically sealed by the welding to the inner circumferences of upper-layer inner extensions 538 at the end portions of the upper-layer coil ends 534. Incidentally, the lower-layer inner extensions 539 have their inner circumferences insulated and arranged from the armature shaft 510.

On the other hand, the two upper-layer coil ends 534 are formed at their inner circumferential end portions with the upper-layer inner extensions 538 extending in the axial direction. These upper-layer inner extensions 538 have their inner circumferences overlapped on and electrically and mechanically sealed by the welding to the outer circumference of the lower-layer inner extensions 539 which are formed at the inner ends of the later-described lower-layer coil bar 532. Moreover, the upper-layer inner extensions 538 have their outer circumferences abutting through insulating caps 580 on the inner faces of the outer circumferential annular portions 571 of stationary members 570 press-fitted in the armature shaft 510.

[Insulating Spacer 560]

The insulating spacer 560 is a thin sheet ring made of a resin (e.g., an epoxy resin, a phenolic resin or nylon) and formed in its outer circumferential side, as shown in Fig. 10,

with the plurality of holes 561, in which are fitted the projections 534a of the individual upper-layer coil ends 534. On the other hand, the insulating spacer 560 is formed in its inner circumference with recesses 562, in which are fitted the lower-layer inner extensions 539 of the lower-layer coil ends 537. These holes 561 and recesses 562 of the insulating spacer 560 are used to position and fix the armature coil 530, as will be described hereinafter.

[Fixing Member 570]

10 The fixing member 570 is a resin annular member which is composed, as shown in Fig. 11, of: an inner circumferential annular portion 572 to be press-fitted on the armature shaft 510; a regulating ring 573 extending perpendicularly to the axial direction for blocking the upper-layer coil ends 534 and the lower-layer coil ends 537 from axially extending; and the outer circumferential portion 571 enclosing the upper-layer inner extensions 538 of the upper-layer coil ends 534 for preventing the internal diameter of the armature coil 530 from being extended by the centrifugal force. Incidentally, this fixing member 570 has the disc-shaped insulating cap 580 made of resin (e.g., nylon) and sandwiched between the upper-layer coil ends 534 and the lower-layer coil ends 537, as shown in Fig. 12, so as to ensure the insulations between the upper-layer coil ends 534 and the lower-layer coil ends 537.

25 In this armature 540, the upper-layer coil ends 534 at the two ends of the upper-layer coil bar 531 and the lower-layer coil ends 537 at the two ends of the lower-layer

coil bar 532 forming the armature coil 530 are individually formed perpendicularly to the axial direction of the armature shaft 510. As a result, the armature 540 can have its axial size reduced to shorten the axial size of the motor 500 so that the starter can be made smaller than that of the prior art.

In the present embodiment, moreover, the magnet switch 600 is arranged in the axially shortened space of the motor 500 and the shortened space which is established by eliminating the independent commutator. Although the axial size of the starter is not changed from that of the prior art, the space for the magnet switch 600 mounted above the motor 500 in the prior art can be eliminated to reduce the volume to be occupied by the starter to a far smaller value than that of the prior art.

[Stationary Magnetic Pole 550]

The stationary magnetic pole 550 is composed of a stator core 558 arranged in the yoke 501 and a stator coil 559 wound on the stator core 558. The stator coil 559 has its one end portion arranged (to intersect L1) in the space at the outer circumference of the planetary reduction gear mechanism 300, i.e., at the outer circumference of the center bracket 360. Incidentally, the motor partition 800 is formed with a stepped portion 810 (to intersect L2) so as to accommodate the aforementioned one end portion. On the other hand, the other end of the stator coil 559 is arranged in the space at the outer circumference of the later-described brush 910. In short, the planetary reduction gear mechanism 300 has its external diameter d made smaller than the inner circumferential

diameter D of the stator coil 559.

As a result, the end portion of the stator coil 559 can be arranged in the space at the outer circumference so that the gap between the armature core 520 of the starter motor and the planetary reduction gear mechanism 300 can be reduced to reduce the axial structure.

Thus, the armature core 530 can have its external diameter D_2 made larger than the thickness L to set the torque of $D^2 EL$ thereby to improve the output of the starter.

Moreover, the area of the armature coil 534 to abut against the brush 910 can be enlarged, and the brush width can be increased in proportion to the increase in the external diameter of the armature so that the brush resistance is lowered to improve the output effectively.

[Magnet Switch 600]

As shown in Figs. 1 and 13, the magnet switch 600 is held by the later-described brush holding member 900 and arranged in the later-described end frame 700 such that it is fixed generally perpendicularly to the armature shaft 510. Moreover, the magnet switch 600 is arranged perpendicularly to the axial direction of the armature shaft 510.

The magnet switch 600 moves a plunger 610 upwards, when energized, to bring two contacts (i.e., a lower movable contact 611 and an upper movable contact 612) into sequentially contact with the head 621 of a terminal bolt 620 and the abutting portion 631 of a stationary contact 630. Incidentally, the terminal bolt 620 is connected with the not-shown battery

cable.

On the upper side of the plunger 610, there is fixed a plunger shaft 615 extending upwards from the plunger 610. The plunger shaft 615 protrudes upward from the through hole which is formed at the center of the stationary core 642. The upper movable contact 612 is carried on the plunger shaft 615 above the stationary core 642 to slide vertically along the plunger shaft 615. This upper movable contact 612 is regulated, as shown in Fig. 31, from moving upwards from the upper end of the plunger shaft 615 by a snap ring 616 attached to the upper end of the plunger shaft 615. As a result, the upper movable contact 612 is made vertically slidable along the plunger shaft 615 between the snap ring 616 and the stationary core 642. Incidentally, the upper movable contact 612 is biased upwards at all times by a contact pressure spring 670 which is made of a leaf spring attached to the plunger shaft 615.

The upper movable contact 612 is made of a metal having an excellent conductivity such as copper and has its two ends brought, when moved upward, into abutment against the two abutting portions 631 of the stationary contact 630. On the upper movable contact 612, moreover, the individual lead wires 910a of the paired brushes 910 are fixed electrically and mechanically by the caulking or welding. In the groove of the upper movable contact 612, moreover, there is inserted and fixed electrically and mechanically the end portion of a resistor 617 for providing a plurality of (e.g., two in the present embodiment) restricting means.

Incidentally, the individual lead wires 910a of the brushes 910 are fixed electrically and mechanically in the upper movable contact 612 by the caulking or welding. However, the upper movable contact 612 and the individual lead wires 910a of the brushes 910 may be integrally formed.

The resistor 617 is constructed of a plurality of turns of metal wire having a high resistance for allowing the motor 500 to rotate at a low speed at the initial stage of the starter. On the other end of the resistor 617, there is fixed by the caulking or the like the power movable contact 611 which is positioned below the head 621 of the terminal bolt 620.

The lower movable contact 611 is made of a metal having an excellent conductivity such as copper and is brought into abutment against the upper face of the stationary core 642, when the magnet switch 600 is OFF so that the plunger 610 takes its lower position, and into abutment against the head 621 of the terminal bolt 620 before the upper movable contact 612 comes into the abutment against the abutting portion 631 of the stationary contact 630 when the resistor 617 is carried upwards by the plunger shaft 615.

The plunger 610 is formed in its lower face with a recess 682 for receiving a ball member 681 attached to the rear end of the string member 680 (e.g., wire). The recess 682 has its inner circumferential wall internally threaded, as at 683. Into this internal thread 683, there is fastened a fixing screw 684 for fixing the ball member 681 in the recess 682. The string member 680 has its length adjusted by adjusting the

insertion of the fixing screw 684 into the internal thread 683. Incidentally, the length of the string member 680 is adjusted such that the regulating pawl 231 of the pinion rotation regulating member 230 is fitted in the teeth 214 of the outer circumference of the pinion gear 210 when the lower movable contact 611 comes into abutment against the terminal bolt 620. Incidentally, the internal thread 683 and the fixing screw 684 constitute an adjusting mechanism.

Since, moreover, the armature shaft 510 is arranged perpendicularly of its axial direction, the magnet switch 600 has its only radial length added to the total axial length of the starter so that it will not enlarge the entire structure of the starter.

[End Frame 700]

The end frame 700 is a magnet switch cover made of a resin (e.g., a phenolic resin) having the magnet switch 600 accommodated therein, as shown in Fig. 14.

The end frame 700 is formed on its back face with spring holding pillars 710 which are protruded forwards according to the positions of the brushes 910 for holding compression coil springs 914 to bias the brushes 910 forwards.

[Brush Holding Member 900]

The brush holding member 900 performs not only the role to partition the inside of the yoke 501 and the inside of the end frame 700 while supporting the rear end of the armature shaft 510 rotatably through the brush holding member bearing 564 but also the roles to act as the brush holder, to hold the

magnet switch 600 and to act as a pulley 690 for guiding the string member 680. Incidentally, the brush holder 900 is formed with the not-shown hole for guiding the string member 680 therethrough.

5 The brush holder 900 is a partition shaped by casting a metal such as aluminum and is formed, as shown in Figs. 1, 15 and 16, with a plurality of (not shown) brush holding holes 911 and 912 for holding the brushes 910 axially. The upper brush holding holes 911 are the holes for holding the brush 910 to receive the plus voltage and hold the brush 910 through
10 insulating cylinders 913 made of a resin (e.g., nylon or a phenolic resin). On the other hand, the lower brush holding holes 912 are the holes for holding the brush 910 to be grounded to the earth and hold the brush 910 directly therein.

15 Since the brushes 910 are thus held by the brush holder 900, it is unnecessary to provide the starter with any independent brush holder. As a result, it is possible to reduce the number of parts and assembling steps of the starter.

20 Moreover, the brushes 910 are urged by the compression coils 914 to bring their front end faces onto the rear faces of the upper-layer coil ends 534 at the rear side of the armature coil 530.

25 Incidentally, the upper brush 910 has its lead wires 910a connected electrically and mechanically by the seaming technique such as the welding or caulking to the upper movable contacts 612 to be moved by the magnet switch 600. On the other hand, the lower brush 910 has its lead wires 910a

connected electrically and mechanically by the caulking to a recess 920 formed in the rear face of the brush holding member 900. Incidentally, the present embodiment is equipped with a pair of lower brushes 910 which are connected to one lead wire 910a, which has its center caulked in the recess 920 of the rear face of the brush holding member 900. The brush holding member 900 is formed on its back face with two pedestals 930 for holding the front face of the magnet switch 600, and two stationary pillars 940 for embracing the magnet switch 600. The two stationary pillars 940 hold the magnet switch 600 by caulking their individual rear ends while the magnet switch 600 abutting against the pedestals 930.

The brush holding member 900 is formed on the lower side of its rear face with a pulley holding portion 950 for holding the pulley 690 for changing the moving direction of the string member 680 from the vertical direction to the axial direction of the magnet switch 600.

[Operations of Embodiment]

Next, the operations of the aforementioned starter will be described with reference to Figs. 17A to 17C.

When a key switch 10 is set to the start position by the driver, the electric power is fed from a battery 20 to the attraction coil 650 of the magnet switch 600. When the attraction coil 650 is energized, the plunger 610 is attracted by the magnetic force generated by the attraction coil 650 so that it is lifted from its lower position.

As the plunger 610 starts its rise, the upper movable

contact 612 and the lower movable contact 611 are lifted by the plunger shaft 615, and the string member 680 also has its rear end lifted. When the rear end of the string member 680 rises, the front end of the same is pulled downwards so that the pinion rotation regulating member 230 is moved downwards. The lower movable contact 611 is brought into abutment against the head 621 of the terminal bolt 620 (as shown in Fig. 17A) by the downward movement of the pinion rotation regulating member 230, when the regulating pawl 231 is fitted in the teeth 214 on the outer circumference of the pinion gear 210. The terminal bolt 620 is supplied with the voltage of the battery 20 so that its voltage is applied to the upper brush 910 in the course of the lower movable contact 611, the resistor 617, the upper movable contact 612 and the lead wire 910a. Then, the armature coil 530 generates a relatively weak magnetic force, which acts upon (i.e., attracts or repulses) the magnetic force of the stationary magnetic pole 550 so that the armature 540 is rotated at a low speed.

As the armature shaft 510 rotates, the planetary gear 320 of the planetary gear mechanism 300 is rotationally driven by the sun gear 310 at the front end of the armature shaft 510. In case the rotating torque of the planetary gear 320 to drive the ring gear 100 rotationally through the planet carrier 330 is to be imparted to the internal gear 340, this internal gear 340 has its rotation regulated by the action of the overrunning clutch 350. In short, the internal gear 340 does not rotate, the planet carrier 330 is decelerated by the rotation of the

planetary gear 320. When the planet carrier 330 rotates, the pinion gear 210 will rotate but has its rotation regulated by the pinion rotation regulating member 230 so that it moves forwards along the helical spline 221 of the output shaft 220.

5 As a result of the forward movement of the pinion gear 210, the pinion gear 210 comes into complete meshing engagement with the ring gear 100 of the engine until it comes into abutment against the pinion retaining ring 250. As the pinion gears 210 advances, moreover, the regulating pawl 231 comes out
10 of engagement with the teeth 214 of the pinion gear 210 until its front end drops at the rear side of the washer 215 which is disposed on the rear face of the pinion gear 210.

 With the pinion gear 210 being in the forward position, on the other hand, the upper movable contact 612 comes into
15 abutment against the abutting portion 631 of the stationary contact 630. Then, the battery voltage of the terminal bolt 620 is applied directly to the brushes 910 in the course of the upper movable contact 612 and the lead wire 910a. In short, the armature coil 530 composed of the individual upper-layer
20 coil bars 531 and the individual lower-layer coil bars 532 is fed with the high current to generate an intense magnetic force thereby to rotate the armature 540 at a high speed.

 The rotation of the armature shaft 510 is reduced by the planetary gear mechanism 300 so that the planet carrier 330
25 is rotationally driven by the increased rotating torque. At this time, the pinion gear 210 has its front end brought into abutment against the pinion retaining ring 250 so that it

rotates together with the planet carrier 330. Since, moreover, the pinion gear 210 is in meshing engagement with the ring gear 100 of the engine, it drives the ring gear 100, i.e., the output shaft of the engine rotationally.

5 Next, when the engine is started to rotate its ring gear 100 faster than the pinion gear 210, a retracting force is generated in the pinion gear 210 by the action of the helical spline. Since, however, the pinion gear 210 is blocked from its backward movement by the rotation regulating pawl 231
10 having dropped at the back of the pinion gear 210, the engine can be started without fail while preventing the premature disengagement of the pinion gear 210 (as shown in Fig. 17B).

 When the started engine has its ring gear 100 rotated faster than the pinion gear 210, this pinion gear 210 is
15 rotationally driven by the ring gear 100. Then, the rotating torque having been transmitted from the ring gear 100 to the pinion gear 210 is further transmitted through the planet carrier 330 to the pin 332 supporting the planetary gear 320. In other words, the planetary gear 320 is driven by the planet
20 carrier 330. Then, a torque reversed from that for the engine starting time is applied to the internal gear 340 so that the overrunning clutch 350 allows the ring gear 100 to rotate. More specifically, if the torque reversed from that for the
25 engine starting time is applied to the internal gear 340, the roller of the overrunning clutch 350 comes out of the recess of the clutch inner 352 to allow the rotation of the internal gear 340.

In short, the relative rotation of the ring gear 100 of the started engine to drive the pinion gear 210 rotationally is absorbed by the overrunning clutch 350 so that the armature 540 is not rotationally driven by the engine.

5 After the engine has been started, the key switch 10 is moved out of the start position by the driver to stop the power supply to the attraction coil 650 of the magnet switch 600. When the power supply to the attraction coil 650 is stopped, the plunger 610 is returned back downward by the action of the
10 compression coil spring 660.

 Then, the upper movable contact 612 leaves the abutting portion 631 of the stationary contact 630, and the lower movable contact 611 then leaves the heat 621 of the terminal bolt 620 to interrupt the power supply to the upper brush 910.

15 When the plunger 610 is returned downwards, the pinion rotation regulating member 230 is returned upwards by the action of its return spring portion 236 so that the regulating pawl 231 leaves the back of the pinion gear 210. Then, the pinion gear 210 is returned backwards by the action of the
20 return spring 240 to come out of meshing engagement with the ring gear 100 of the engine and to bring its rear end into abutment against the flange-shaped protrusion 222 of the output shaft 220. In short, the pinion gear 210 is returned to the stage before the start of the starter (as shown in Fig. 17C).

25 As a result that the plunger 610 is returned downwards, moreover, the lower movable contact 611 comes into abutment against the upper face of the stationary core 642 of the magnet

switch 600 so that the lead wire 910a of the upper brush 910 is turned conductive in the course of the upper movable contact 612, the resistor 617, the lower movable contact 611, the stationary core 642, the magnet switch cover 640 and the brush holding member 900. In short, the upper brush 910 and the lower brush 910 are short-circuited through the brush holding member 900. In this meanwhile, an electromotive force is generated in the armature coil 530 by the inertial rotation of the armature 540. Moreover, this electromotive force is short-circuited through the upper brush 910, the brush holding member 900 and the lower brush 910 so that the braking force is applied to the inertial rotation of the armature 540. As a result, the armature 540 is abruptly stalled.

[Effects of the Embodiment]

The stator coil 559 has its one end portion arranged in the space at the outer circumference of the planetary reduction gear mechanism 300, i.e., at the outer circumference of the center bracket 360 and its other end portion arranged in the space at the outer circumference of the brush 910. In short, the planetary reduction gear mechanism 300 has its external diameter d made smaller than the inner circumferential diameter D of the stator coil 559 so that the gap between the armature core 520 of the stator motor and the planetary reduction gear mechanism 300 can be decreased to reduce the axial structure.

As a result, the armature core 539 can have its external diameter D_2 made larger than the thickness L to set the torque of $D^2 EL$ to a larger value thereby to improve the

output of the starter. By enlarging the armature core 520 radially, moreover, the area of the upper-layer coil ends 534 to abut against the brush 910 can be enlarged together with the brush width in proportion to the increase in the armature diameter to lower the brush resistance thereby to improve the output effectively.

[Another Embodiment]

Incidentally, in the present invention, the stator coil 559 has its one end arranged at the outer circumference of the planetary reduction gear mechanism 300 and its other end arranged in the space at the outer circumference of the brush 910. However, only one end may be arranged at the outer circumference of the planetary reduction gear mechanism 300 or in the space at the outer circumference of the brush 910.

Moreover, the stationary magnetic pole 550 is composed of the stator core 558 and the stator coil 559 but may be replaced by a magnet.

INDUSTRIAL APPLICABILITY

As has been described hereinbefore, the starter according to the present invention can be used as a starter for a reduction gear mechanism, which can have its axial length suppressed and its mountability and impact-resistance.

CLAIMS

1. A starter with a planetary reduction gear mechanism, comprising:

5 a starter motor including an armature shaft for rotatably holding an armature core wound with an armature coil, a commutator connected with said armature coil and arranged generally in parallel with the end portion of said armature core, a brush slidably held by said commutator, and a field pole arranged on the outer circumference of said armature core;
10 and

a planetary reduction gear mechanism including a sun gear formed on the outer circumference of the armature shaft of said starter motor, a planetary gear borne on one end of a drive shaft arranged coaxially with said armature shaft and meshing with said sun gear, and an internal gear meshing with
15 said planetary gear,

wherein said field pole of said starter motor has its end portion overlapping at least one of said planetary reduction gear mechanism and said brush.

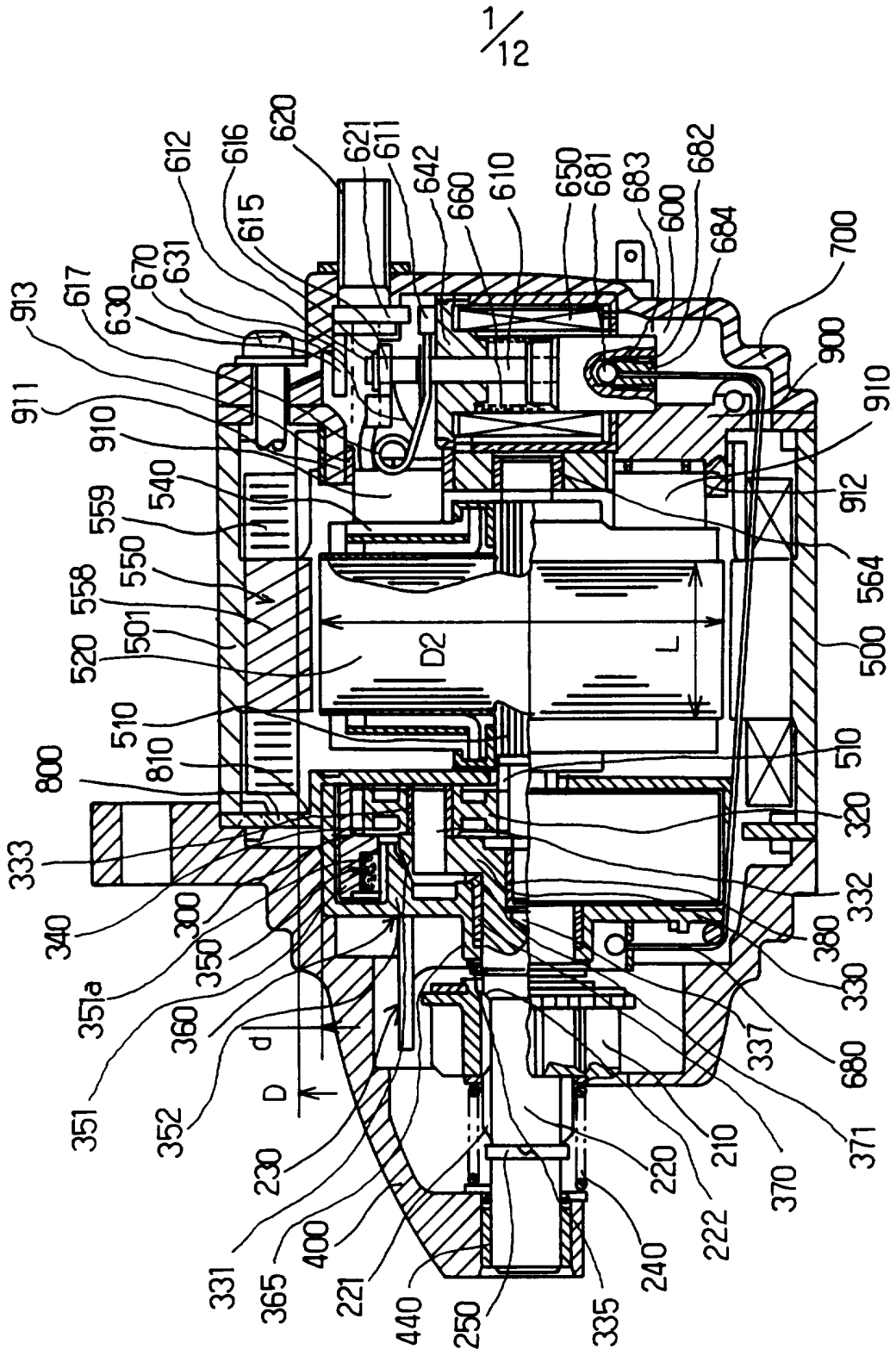
20 2. A starter with a planetary reduction gear mechanism, according to claim 1, wherein said armature coil has its end portion arranged generally in parallel with the end face of said armature core, and wherein said coil has its end portion formed as a commutator.

25 3. A starter with a planetary reduction gear mechanism, according to claim 1 or 2, further comprising:

a magnet switch for supplying an electric power to said

starter motor, said magnet switch being arranged at the brush side of said starter motor and generally perpendicularly to the axial direction of said armature shaft.

FIG. 1



2/12

FIG. 2A

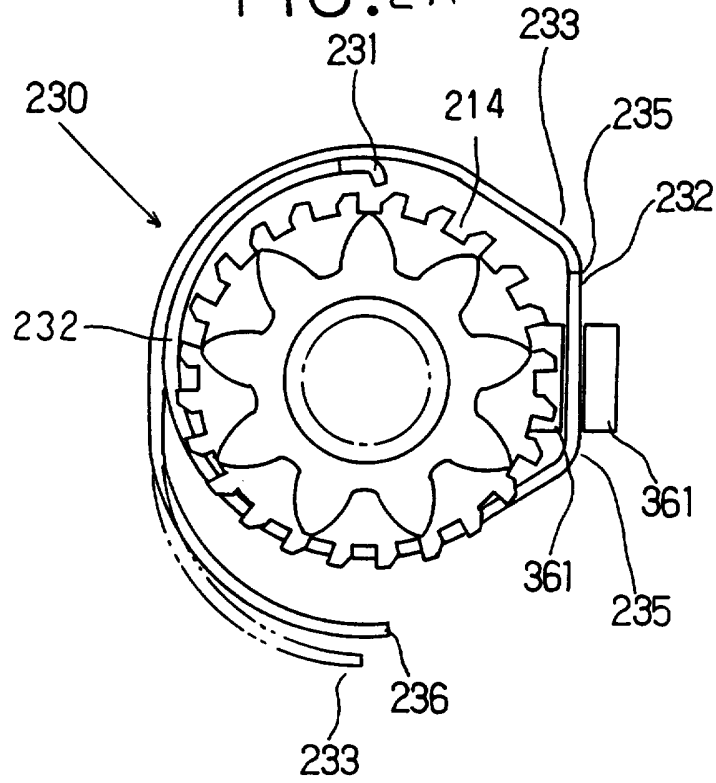
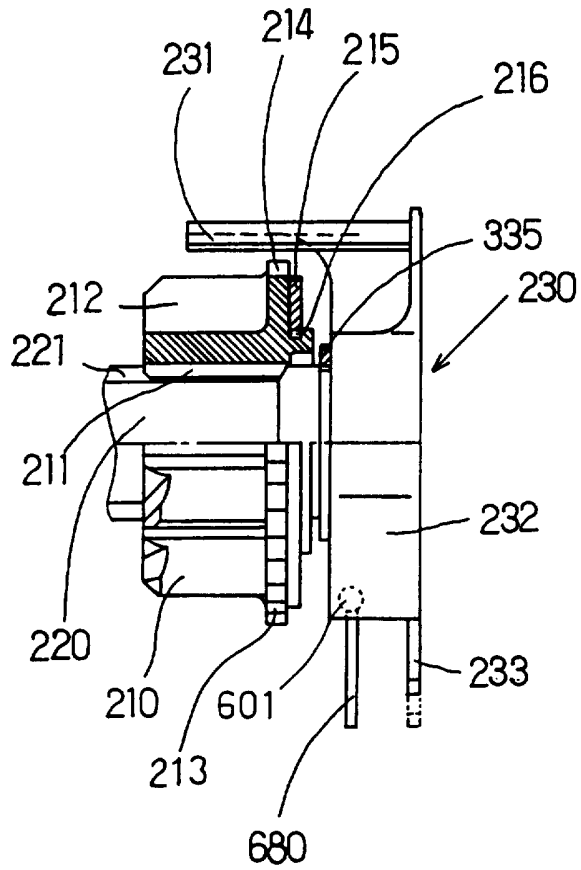
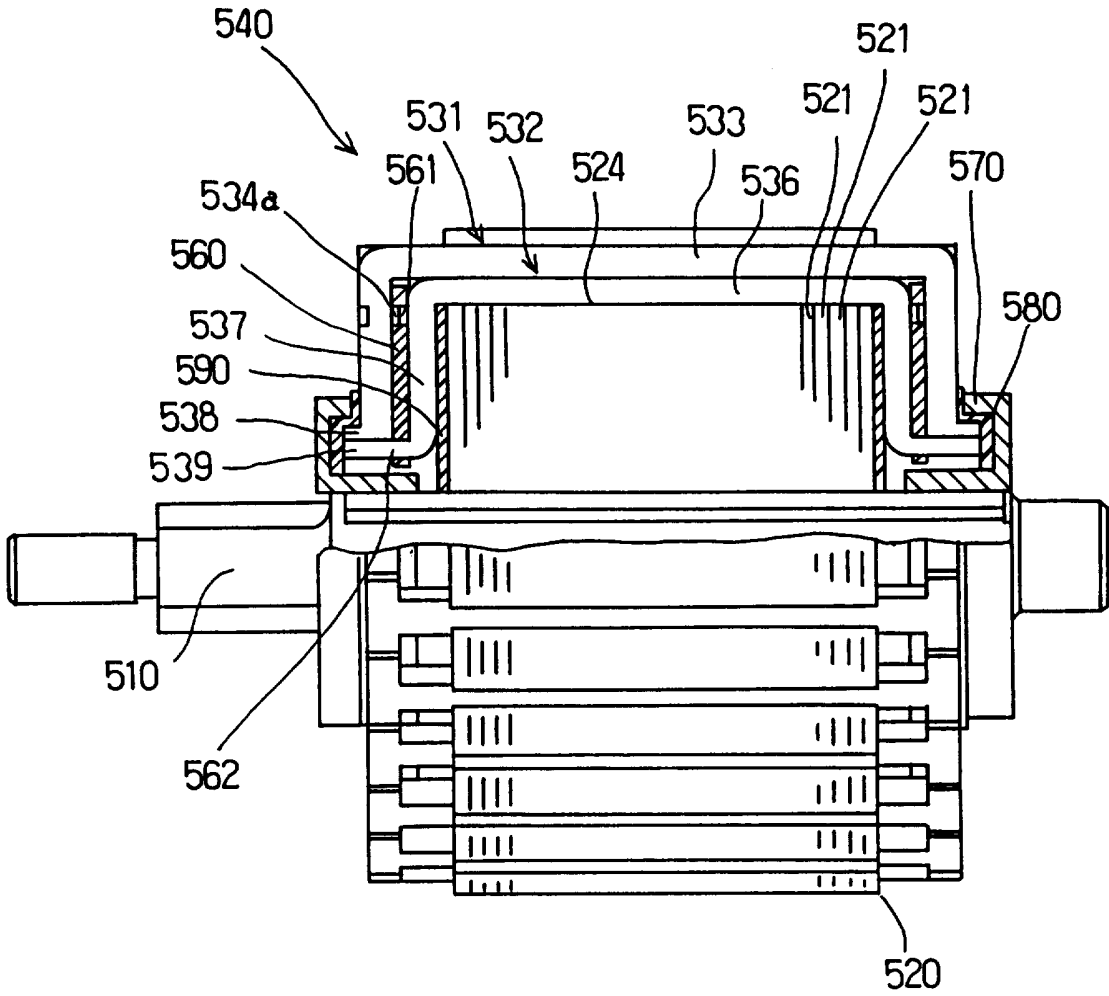


FIG. 2B



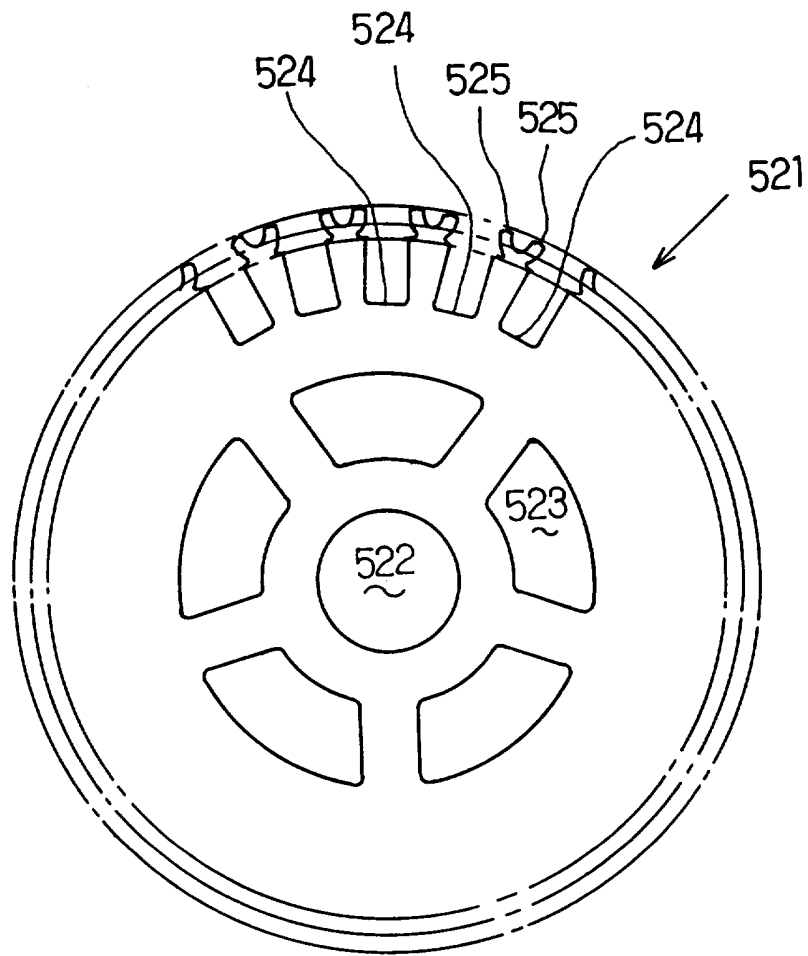
3/12

FIG. 3



4/12

FIG. 4



5/12

FIG. 5

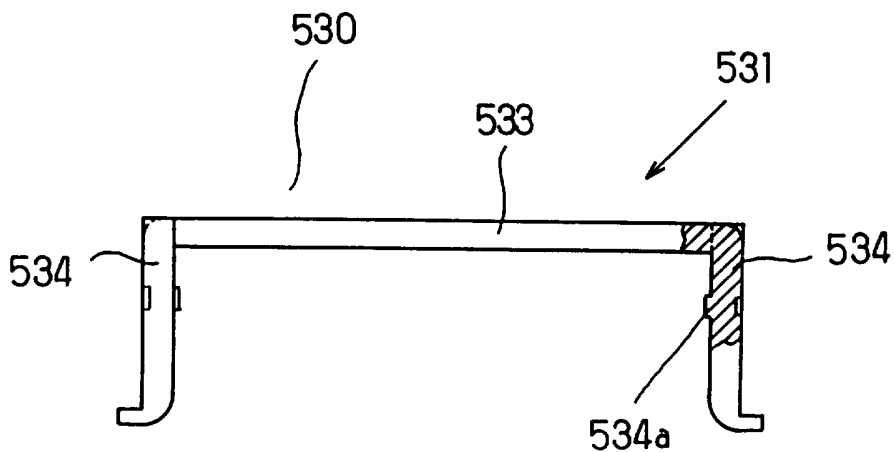
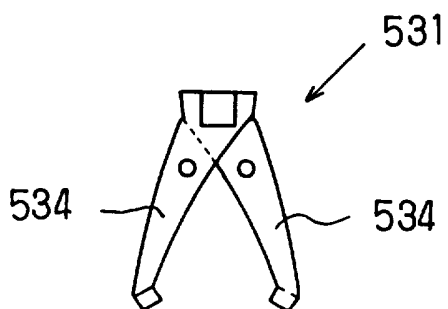
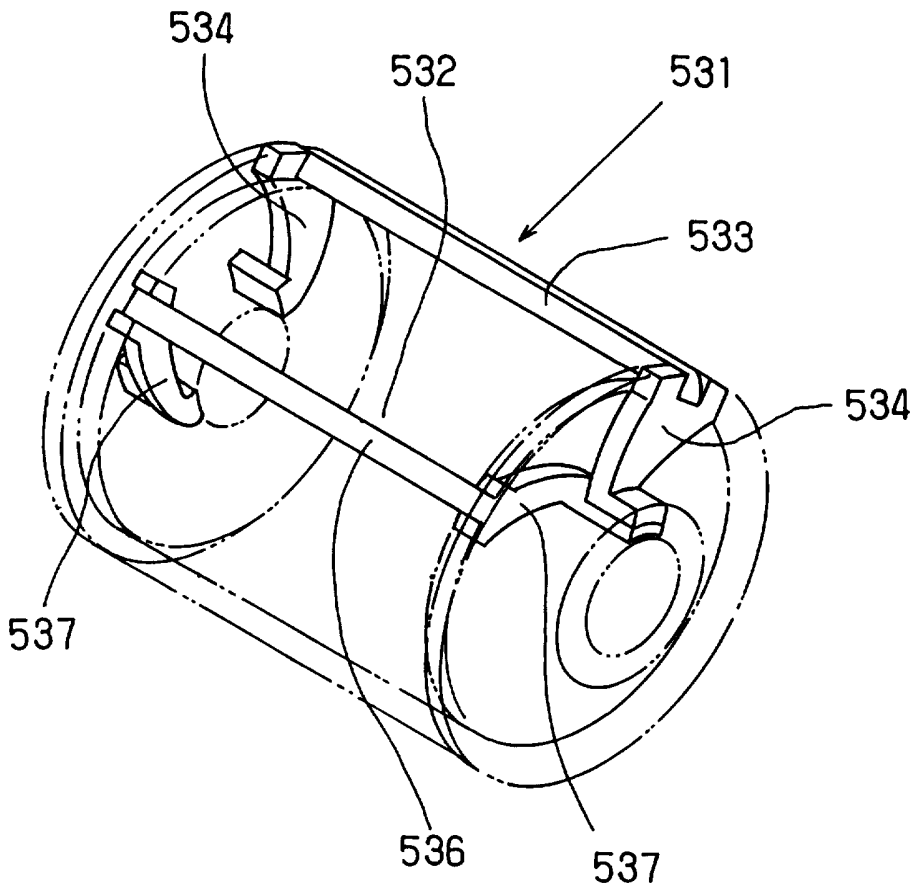


FIG. 6



6/12

FIG. 7



7/12

FIG. 8

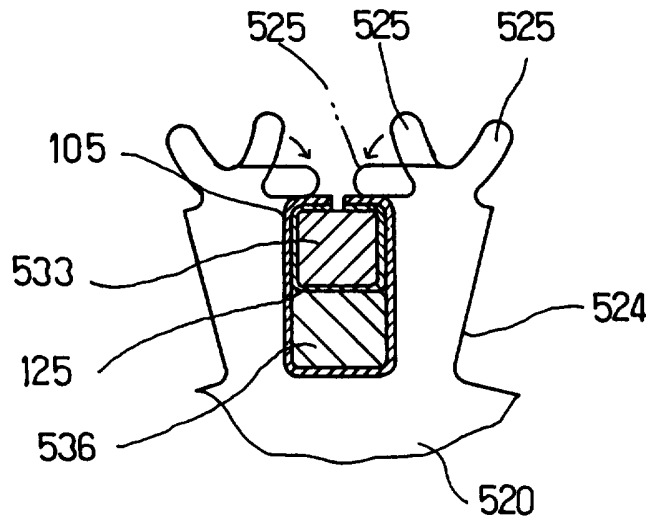
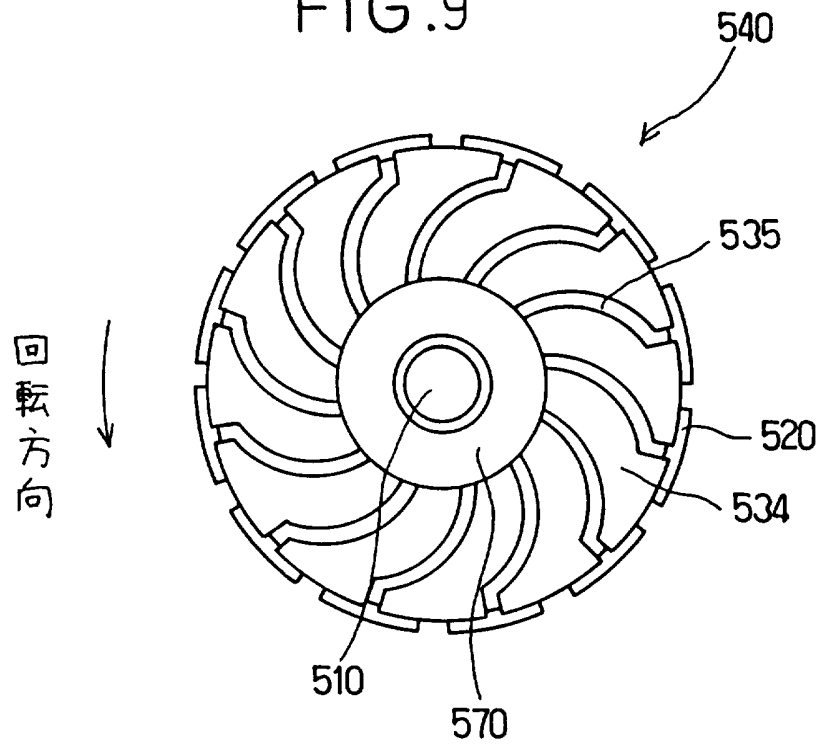
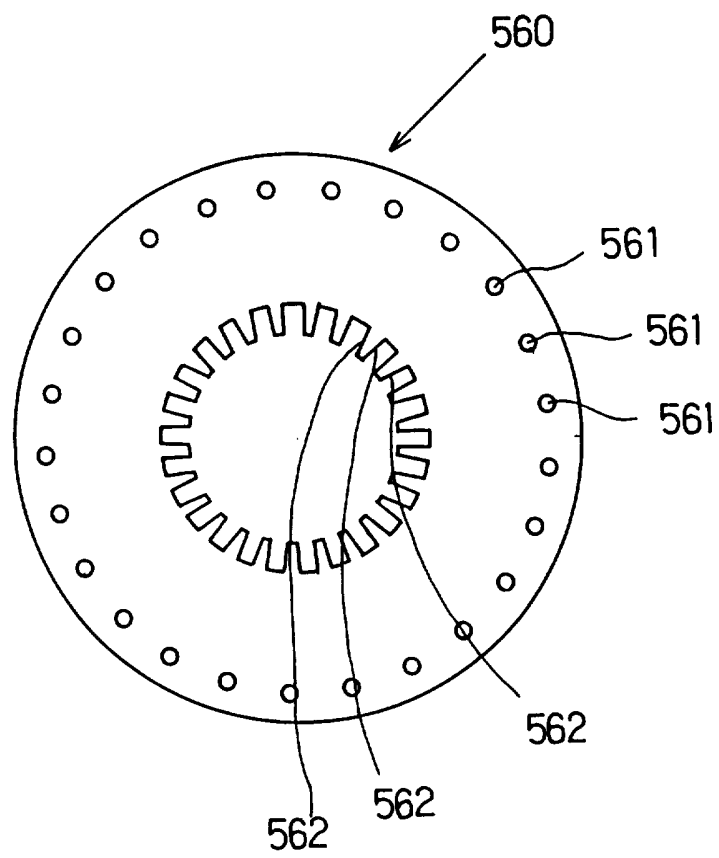


FIG. 9



$\frac{8}{12}$

FIG. 10



9/12

FIG.11

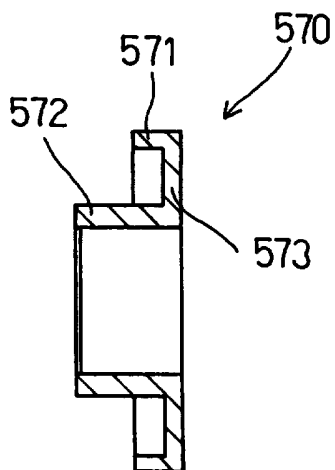
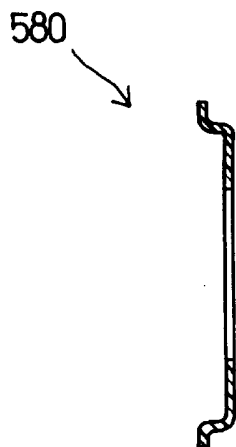


FIG.12



10
/ 12

FIG.13

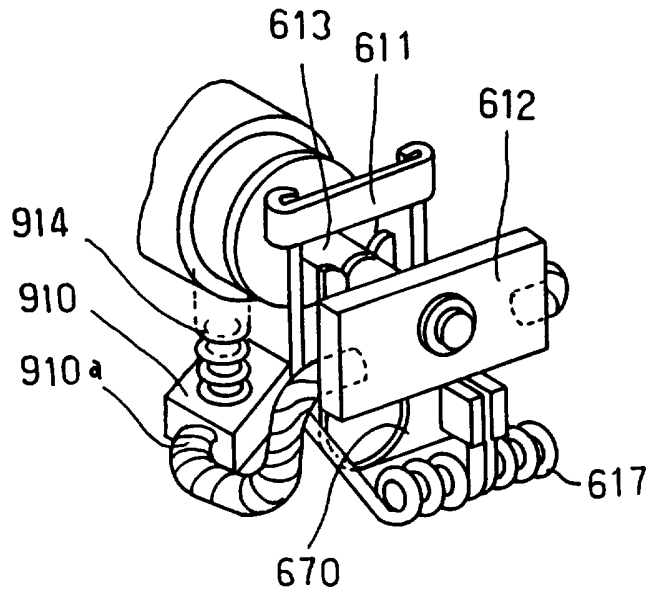
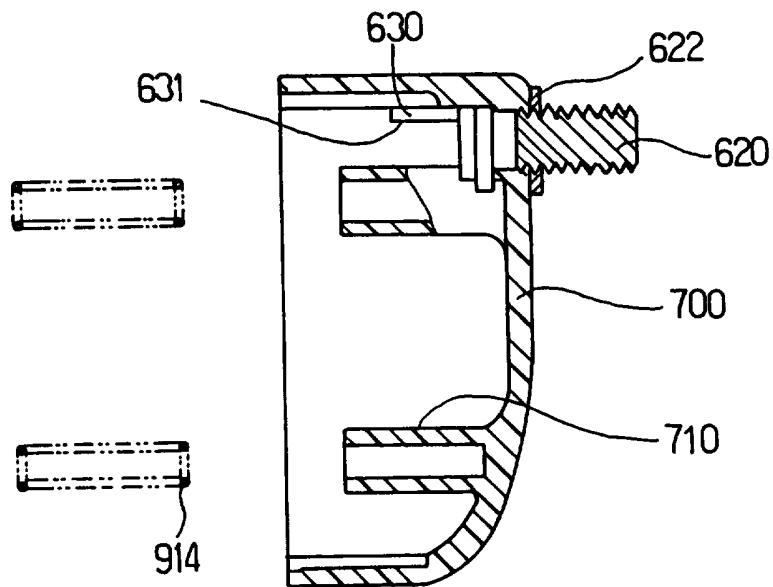


FIG.14



11/12

FIG. 15

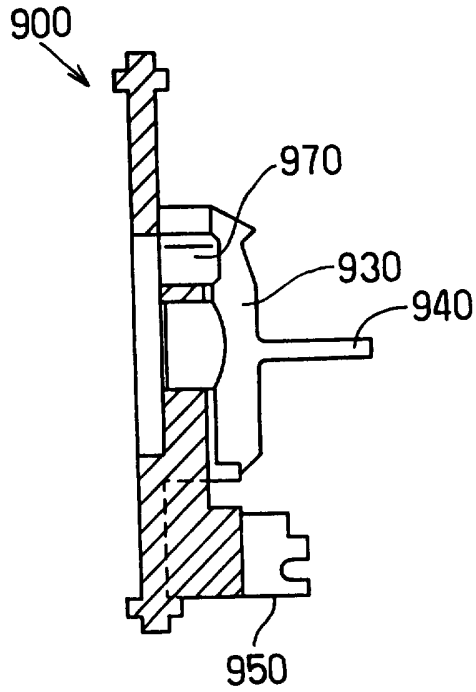
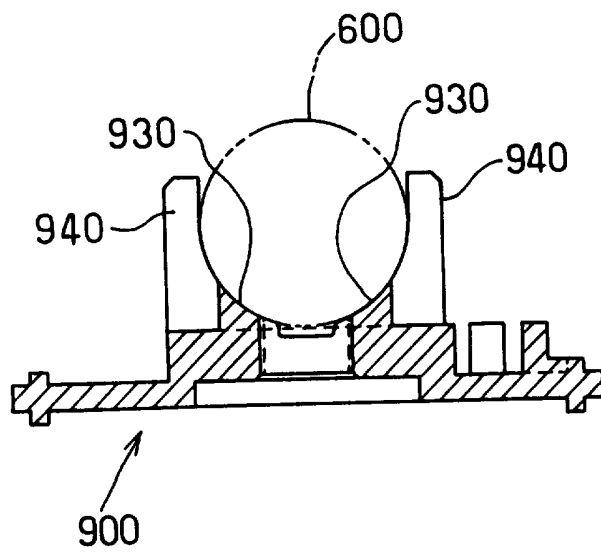


FIG. 16



12/12

FIG.17A

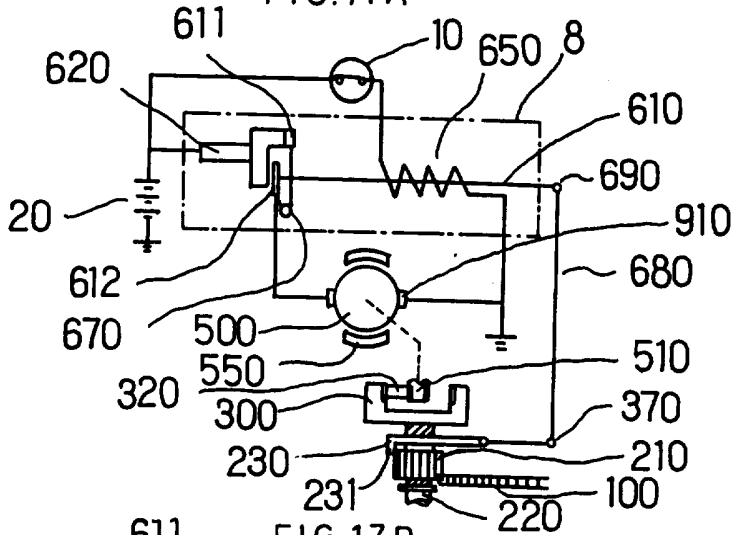


FIG.17B

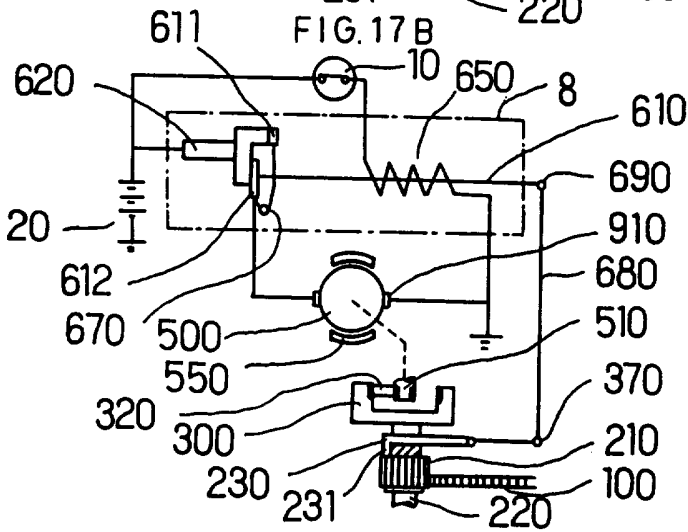
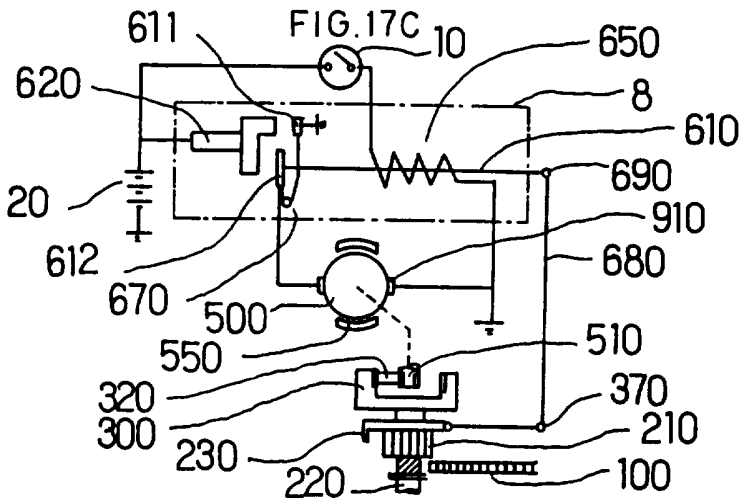


FIG.17C



INTERNATIONAL SEARCH REPORT

International Application No

PCT/JP 94/01987

A. CLASSIFICATION OF SUBJECT MATTER
 IPC 6 F02N15/04 F02N11/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 F02N

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US,A,5 258 651 (SHERMAN) 2 November 1993 see column 3, line 12 - line 56; figure 1 ---	1
A	US,A,3 497 706 (BURKETT) 24 February 1970 see column 3, line 40 - column 4, line 28; figure 1 ---	1,2
A A	US,A,4 816 712 (TANAKA) 28 March 1989 & JP,A,63 110 931 cited in the application -----	

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "I" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- "&" document member of the same patent family

Date of the actual completion of the international search

11 July 1995

Date of mailing of the international search report

14. 07. 95

Name and mailing address of the ISA
 European Patent Office, P.B. 5818 Patentlaan 2
 NL - 2280 HV Rijswijk
 Tel. (+ 31-70) 340-2040, Tx. 31 651 epo nl,
 Fax: (+ 31-70) 340-3016

Authorized officer

 Bijn, E

INTERNATIONAL SEARCH REPORT

International Application No

PCT/JP 94/01987

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A-5258651	02-11-93	NONE	
US-A-3497706	24-02-70	BE-A- 694619	31-07-67
		DE-A- 1588523	18-02-71
		DE-A- 1613852	30-07-70
		DE-A- 1613955	23-12-70
		FR-A- 1511813	18-04-68
		GB-A- 1149888	
		GB-A- 1149889	
		GB-A- 1149890	
		US-A- 3454860	08-07-69
		BE-A- 697003	18-09-67
		US-A- 3774303	27-11-73
US-A-4816712	28-03-89	JP-A- 63110931	16-05-88