*«* P/00/008 Section 29(1) Regulation 3,1(2)

### **AUSTRALIA** Patents Act 1990



s

### **NOTICE OF ENTITLEMENT**

We HUGHES AIRCRAFT COMPANY

of 7200 Hughes Terrace, Los Angeles, CALIFORNIA 90045-0066, U.S.A,

being the Applicant and Nominated Person in respect of Australian Patent Application No. 52916/93

state the following:

ון

5 j ' 1 '■{

! .

Ernest C. CHEN is the actual inventor of the invention the subject of the Application.

The inventor has assigned his rights in the invention to the nominated person. By virtue of the assignment the nominated person is entitled to rely on the basic application.

The applicant and nominated person is entitled to rely on the application listed in the declaration under Article 8 of the PCT.

Convention priority is claimed from the following basic application referred to in the declaration under Article 8 of the PCT:



The basic application referred to in the declaration under Article 8 of the PCT was the first application made in a Convention country in respect of the invention the subject of the Application.

DATED this 24th day of May 1994

HUGHES AIRCRAFT COMPANY By their Patent Attorney

RIFFITHEHACK & OO

OUR REF: P03782TW/CL

# **HARRY CONTRACTOR** AUQ3629tQ

# (12) PATENT ABRIDGMENT **(11) Document No,** AU-B-52916/93 (19) AUSTRALIAN PATENT OFFICE (1**0) Acceptance No,** 664129

**(54) Title DOPPLER TRACKING METHOD FOR OBJECT IMAGING FROM RADAR RETURNS**

- **International Patent Classliication(s) (51)<sup>s</sup> G01S 013/89 G01S 013/66**
- **(21) Application No.: 52916/93 (22) Application Date: 23.o9.93**

- **(87) PCT Publication Number: WO94/07156**
- **(30) Priority Data**

fj ί·

- **(31) Number (32) Date (33) Country 949920 24.09.92 US UNITED STATES OF AMERICA**
- **(43) Publication Date; 12.04.94**
- **(44) Publication Date of Accepted Application 02.11.95**
- **(71) Appllcanl(s) HUGHES AIRCRAFT COMPANY**
- **(72) Invonlor(s)** ERNEST C CHEN
- **(74) Attorney or Agent GRIFFITH HACK & CO, GPO Box 3125, BRISBANE OLD 4001**
- **(57) Claim**

1. A Doppler tracking method that provides for object imaging from radar return signals, said method comprising the steps of:

tracking an object by means of a coarse Doppler tracker that processes the radar return signals and removes translational motion of the object;

pulse pair processing output signals from the coarse Doppler tracker to produce an estimate of the Doppler centroid of the object;

filtering output signals from the pulse pair processing step with a predetermined low pass filter that is used to smooth out phase increments generated in the pulse pair processing step;

smoothing output signals from the filtering step with a predetermined smooth curve;

recursively filtering output signals from the smoothing step to produce a phase history;

outputting the difference in phase between the recursively filtered phase history and the updated phases that have been approximately delayed;

compensating difference in phase output signals; Fourier transforming the compensated difference in

# $(11)$  AU-B-52916/93  $-2$ -(10) 664129

R

phase signals to produce a Fourier transformed (FFT) image;

phase updating the output signals from the filtering step to integrate the output of the filtering step to update the phase history of the object based on phase increments derived from the filtering step;

delaying output signals from the phase updating step to match in timing the phases provided by the phase update step with those from the recursively filtering step; and

feeding back output signals from the phase updatingstep.

OPI DATE 12/04/94 APPLN. ID 52916/93<br>AOJP DATE 07/07/94 PCT NUMBER PCT/US93/09082



AU9352916





### (57) Abstract

A method of tracking an object in the Doppler dimension that provides for improved imaging. The method tracks the cen-A method of tracking an object in the Doppler dimension that provides for improved imaging. The method tracks the centroid of the object's Doppler and smooths out noisy estimates of its phase history. The tracking and smoo processing then produces a Fourier transformed image. The output from the filter is also processed to update the phase and the processing then produces a Fourier transformed image. The output from the friter is also processed to update the phase and the phase updated signals are fed back to the coarse Doppler tracker. The phase updating integrates

# SUBSTITUTE SHEET

 $-05 -$ -improved-imaging-The-present-method-tracks-the-centroid-of-the-object-s-Deppler-with--provides-for-a method-of-tracking an-object-in-the-Doppler-dimension-that-provides- $\epsilon$ In-order-to-provide-for-the-above-and-other-objectives-the-present-invention-

# NOILNEANI EHL JO ANYWHOS

object imaging from radar returns while eliminating all of the above-cited difficulties. It is therefore an objective of the present invention to provide for a method for

 $\vec{a}$ 

- $\overline{a}$ is obtained, a transition period will exist during which images may jump and defocus in another isolated strong scatterer must be acquired. Even if such a replacement scatterer to the dynamic motion of the object, such as acceleration or maneuvers, for example. using a long time constant for the tracking filter. However, the filter is less responsive the Doppler dimension. These undesimble effects may be alleviated to some degree by
	- blocked by other parts of the object as time goes on. If and when these events happen, The tracked scatterer may also fade away in terms of its radar eross section (RCS) or be moment. The tracked scatterer often sciniillates, which adversely affects image quality. Unfortunately, such a seatterer may not exist on any target and/or at any particular spot tracker relies on assumption that the object contains an isolated strong scatterer.
		- - synthetic array radar (ISAR) system is what is know as a "hot spot" tracker. The hot

 $\mathbf{c}$ 

- Currently, the most widely known method of object tracking using an inverse
- 

larly, to Doppler tracking methods that provide for object imaging from radar returns.

The present invention relates to Doppler tracking methods, and more particu-

**BACKGROUND** 

DOPPLER TRACKING METHOD FOR OBJECT INVOLUTE NEUVA REPRISING INVOLVED

- 
- 
- 

سو

**PCT/US93/09082** 

95120/16 O.M



According to the present invention there is provided a Doppler tracking method that provides for object imaging from radar return signals, said method comprising the steps of:

- 2 -

aasiisk<del>ijkin ka</del>

tracking an object by means of a coarse Doppler tracker that processes the radar return signals and removes translational motion of the object,\*

pulse pair processing output signals from the coarse Doppler tracker to produce an estimate of the Doppler centroid of the object;

filtering output signals from the pulse pair precessing step with a predetermined low pass filter that is used to smooth out phase Increments generated in the pulse pair processing step;

smoothing output signals from the filtering step with a predetermined smooth curve;

recursively filtering output signals from the smoothing step to produce a phase history;

**20** outputting the difference in phase between the recursively filtered phase hiscory with the updated phases that have been approximately delayed;

compensating difference in phase output signals?

Fourier transforming the compensated difference in phase signals to produce a Fourier transformed (FFT) image?

phase updating the output signals from the filtering step to integrate the output of the filtering step to update the phase history of the object based on phase increments derived from the filtering step;

delaying output signals from the phase updating step to match in timing the phases provided by the phase update step with those from the recursively filtering B step; and

35 feeding back output signals from the phase updating step.

### BRIEF DESCRIPTION OF THE DRAWINGS

A preferred embodiment of the present invention will now be described by way of example only with reference to

IS

**10**

5

**2S**

30

&037S2TW/703

the accompanying drawings in which:

 $\infty$   $-$ 



r I

i i

j,

i 1

f

Fig. 1 shows a functional block diagram illustrating a Doppler tracking method in accordance with the principles of the present invention that provides for object imaging from radar returns;

Fig. 2 illustrates pulse pair processing in accordance with the present invention  $5$  employed in the Doppler tracking method of Fig. 1;

Figs. 3a and 3b show images produced by a conventional hot spot tracker, and Figs. 3a and 3b show images produced by the tracking method in accordance with the present invention shown in Fig. 1.

### 10 DETAILED DESCRIPTION

Referring to the drawing figures, and with reference to Fig. 1, it a shows a functional block diagram illustrating a Doppler tracking method 10 in accordance with the principles of the present invention that provides for object imaging from radar return signals. The Doppler tracking method 10 processes Doppler signals generated 15 by a coarse Doppler tracker 11 that initially processes the radar return signals to remove translational motion of the object. The present Doppler tracking method 10 processes the Doppler output signals from the coarse Doppler tracker 11 by means of the following processing steps.

The Doppler tracking method 10 comprises a pulse pair processing step 12 that 20 processes the Doppler output signals from the coarse Doppler tracker 11. This produces pulse pair processed signals that are an estimate of the Doppler centroid of the object. For each pair of adjacent pulses, pulse pair processing is applied to individual range bins, and the outputs are combined to estimate the Doppler centroid of the object at that particular time. An alpha filtering step 13 is used to process the output signals 25 from the pulse pair processing step 12. The alpha filtering step 13 provides for a low pass filter that is used to smooth out phase increments obtained in the pulse pair processing step 12. A phase increment smoothing step 14 is performed after the alpha

filtering step 13 which filters the output signals of the alpha filtering step 13 with a second-degree polynomial, for example. A phase recursion step 15 is performed

30 subsequent to the phase incrementsmoothing step 14 to produce a phase history. An amount of phase equal to the difference between the output from the phase recursion step 14 and the delay step 18 is compensated in a fine phase compensation step 19. A fast Fourier transform (FFT) step 16 is then performed on the output of the fine phase compensation step 19 to produce a Fourier transformed (FFT) image.

35 The output from the alpha filtering step 13 is also processed by a phase update step 17 whose output is fed back for use in the coarse Doppler tracker 11. The phase update step  $17$  integrates the output of the alpha filtering step 13 to update the phase

4

history of the object based on phase increments derived from the alpha filtering step 13. In addition, the output of the phase update step  $17$  is processed by a delay step  $18$  to match the phases provided by the phase update step 17 with those from the phase recursion step 15, since the phase recursion step 15 only outputs a new group of 5 phases for every new image.

The advantages of the present method are that target tracking is more reliable and image quality is better. Since the Doppler centroid is tracked, each image is automatically centered in the Doppler dimension. This allows the image display area to be used more efficiently. Another consequence of tracking the Doppler centroid is that the

10 image sequence is stabilized in theDopplerdimension, whereas in conventional systems, images can be displaced vertically which normally distracts an operator and makes object classification more difficult. Stability of image sequence also implies that each image is in focus and therefore has high quality. Processing all range bins over the object range extent maximizes the signal strength while limiting sea clutter and noise

15 contributions. This improves the signal to clutterratio and signal to noise ratio for tracking. In addition, with regard to the phase incrementsmoothing step 14 described in detail below, phase refinement of the signals from the alpha filtering step 13 are provided and is applied before the Doppler FFT (step 16) to ensure that the effective phase compensation across the image integration time is smooth. This furtherreduces 20 noise in the image.

Since the present method tracks the Doppler centroid, it does not require an isolated strong scatterer as is required by the conventional hot shot tracker or tracking method. This ensures that tracking is continuousregardlessofa scatterers'distribution, scintillation, or blocking effects.

25 At the heart of the present invention is the pulse pair processing step 12. However, prior to performing the pulse pair processing 12, the residual object Doppler is reduced by the coarse Doppler tracker 11 to less than pi radians over a pulse repetition interval (PRI), or one effective PRI if presumming is used. The small error produced by this tracker 11 also ensures that range bins of adjacent pulses are sufficiently lined 30 up for Doppler processing. Methods of coarse Doppler tracking are generally wellknown in the art and will not be discussed in detail herein. A description of the pulse pair processing step 12 follows.

For each pair of adjacent pulses, pulse pair processing is applied to individual range bins, and the outputs are combined to estimate the Doppler centroid of the object 35 at that particular time. This is depicted in Fig. 2 which illustrates a plurality of range bins, one of which (m) is selected, and a plurality of pulses  $(k-1, k)$  that are combined

**WO 94/07156**

to estimate the Doppler centroid. The processing is performed in accordance with the following equations:

$$
D_k = \sum_{m} C_{k} m \tilde{C}_{k-1, m}
$$

$$
\varepsilon_{\Delta \theta_k} = \tan^{-1} \frac{\text{Im}(D_k)}{\text{Re}(D_k)}
$$

5

15

»

4

%

where  $C_{k,m}$  is the complex sample at the m-th range bin and the k-th pulse and  $\tilde{C}$  is the complex conjugate of C. Summation is over the target range extent and the complex sum, D<sub>k</sub>, is obtained. The summation implies that it is the Doppler centroid of the object that is tracked rather than any particular scatterer.

10 The alpha filtering step 13 provides for processing by means of a low pass filter that is used to smooth out phase increments obtained in the pulse pair processing step 12. The equation for the alpha filtering step 13 is

 $\Delta \phi_k = \Delta \phi_{k-1} + \alpha \epsilon_{\Delta \phi_k}$ .

The initial phase increment  $\Delta\phi$  is provided by the coarse Doppler tracker 11 and this increment should be unambiguous (no modulo  $2$  pi). An empirical value such as 0.05 may be used for*a.* The filtered phase increments generated by the alpha filtering step 13 are used in the phase update and phase increment smoothing steps 14, 17 of the present invention and are discussed below.

The phase update step 17 integrates the output of the alpha filtering step 13 to update the phase history of the object based on phase increments from the alpha filtering step

20 13. Outputs are generated at the PRF rate and are fed back to the coarse Doppler tracker 11 as is shown in Fig. 1. The equation is

 $\phi_k = \phi_{k-1} + \Delta \phi_k$ 

**with φο set at 0.**

The purpose of the Doppler tracker 11 is to remove translational motion of the object The object's motion, and therefore its phase history, is generally a smooth function of time. However, the phase increments obtained from the alpha filtering step 13 contain noise, including noise in the raw data and noise from the pulse pairprocessing step 12 with finite Doppler spread of the object. Smoothing is performed by the phase increment smoothing step 14 by filtering the outputs of the alpha filtering step 13 with a second-degree polynomial, although a higher-degree polynomial or other curves may be used for objects with high motion dynamics.

The phase increment smoothing step 14 is performed over each image integration time and at the image update rate. For example, if a one-second integration time is desired with a PRF of 256 Hz, then 256 phase increments are smoothed for each new image. If, in addition, the image update rate is 4 Hz, then 64 samples are skipped for each new smoothing function.

30

25

35

5

Smoothing may also be done over unwrapped phases rather than over phase increments, However, since values of the unwrapped phase history are expressed in radar wavelengths and thus have a huge dynamic range, this technique requires a longer computer word for data representation.

Once the phase increment smoothing step 14 is done, the phase history is efficiently obtained by a simple phase recursion step 15. If the smoothed phase increments are represented by a second-degree polynomial, for example, a third degree polynomial phase history is obtained. This means that phase errors up to the third orderare included for fine phase compensation on each image before processing by the Doppler

10 FFT step 16.

> For example, by using a second-degree polynomial, the smoothed phase increments are given by

 $\Delta \phi_n = a_0 + a_1 n + a_2 n^2$ .

The smoothed phase history obtained from the phase recursion step 15 is given by  $\frac{1}{2}$   $\frac{1}{2}$ 

$$
\begin{aligned}\n\phi_{\underline{n}} &= \left(\phi_{\underline{n+1}} + \Delta \overline{\phi}_{\underline{n+1}}\right)_{\text{mod } 2\pi} \\
\Delta \phi_{\underline{n}} &= \Delta \phi_{\underline{n+1}} + \Delta^2 \phi_{\underline{n+1}} \\
\Delta^2 \phi_{\underline{n}} &= \Delta^2 \phi_{\underline{n+1}} + 2a_2\n\end{aligned}
$$

with initial values given by

 $\phi_0 = 0$ ,  $\Delta \phi_0 = a_0$ , and  $\Delta^2 \phi_0 = a_1$ .

The smoothed phase history is the desired net compensation on the raw data. Since part of this phase has already been compensated in the coarse Doppler tracker 11 prior to the pulse pair processing step 12 as is shown in Fig. 1, the amount of fine phase compensation provided by the phase recursion step 15 is adjusted in the fine phase compensation step 19 according to the equation

**25**

**30**

35

15

20

 $\epsilon \phi_{\mathbf{k}} = \phi_{\mathbf{k}} - \phi_{\mathbf{k}}.$ 

The delay step 18 represents a memory buffer that stores the integrated and updated phases provided by the phase update step 17 that arrive at the PRF rate or the presumed PRF rate. The delay is necessary to match in timing the phases provided by the phase update step 17 with those from the phase recursion step 15, since the phase recursion step 15 outputs a new group of phases for every new image.

Thus there has been described new and improved Doppler tracking methods that provide for object imaging from radarreturns. It is to be understood that the abovedescribed embodiments are merely illustrative of some of the many specific embodiments that represent applications of the principles of the present invention. Clearly, numerous and other arrangements can be readily devised by those skilled in the art without departing from the scope of the invention.

## **THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:**

1. A Doppler tracking method that provides for object imaging from radar return signals, said method comprising the steps of:

 $-7 -$ 

5 tracking an object by means of a coarse Doppler tracker that processes the radar return signals and removes translational motion of the object;

pulse pair processing output signals from the coarse Doppler tracker to produce an estimate of the Doppler 10 centroid of the object;

filtering output signals from the pulse pair processing step with a predetermined low pass filter that is used to smooth out phase increments generated in the pulse pair processing step;

15 smoothing output signals from the filtering step with a predetermined smooth curve;

recursively filtering output signals from the smoothing step to produce a phase history;

outputting the difference in phase between the 20 recursively filtered phase history and the updated phases that have been approximately delayed;

compensating difference in phase output signals;

Fourier transforming the compensated difference in phase signals to produce a Fourier transformed (FFT) 25 image;

phase updating the output signals from the filtering step to integrate the output of the filtering step to update the phase history of the object based on phase increments derived from the filtering step;

30 delaying output signals from the phase updating step to match in timing the phases provided by the phase update step with those from the recursively filtering step; and

feeding back output signals from the phase updating 35 step.

2. The method of Claim 1 wherein the step of pulse pair processing the output signals from the coarse Doppler tracker comprises the step of:



for each pair of adjacent pulses, pulse pair processing individual range bins, and combining the outputs of each range bin to estimate the Doppler centroid of the object at a particular time



J

/ i

*i* it

I

1

\_s

 $\sum_{i=1}^N$ 

8

<span id="page-13-0"></span>3. The method of Claim 1 wherein the step of smoothing output signals from the filtering step comprises smoothing output signals from the filtering step with a predetermined order polynomial.

4. The method of Claim 2 wherein the step of pulse pair processing the output signals from the coarseDopplertrackerimplementsthe equations:

from the course Doppler in  
\n
$$
D_k = \sum_m C_{k,m} \tilde{C}_{k-1, m}
$$
 and  
\n $\varepsilon_{\Delta \theta_k} = \tan^{-1} \frac{\text{Im}(D_k)}{\text{Re}(D_k)}$ 

5

where  $C_{k,m}$  is a complex sample at the m-th range bin and the k-th pulse and  $\tilde{C}$  is a complex conjugate of C, and where the summation is over the target range extent.







 $\overline{c}$