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(56) Documents Cited:
GB 2535163 A **EP 2557316 A2**
WO 2002/018794 A1 **DE 004140379 C1**
US 3751693 A **US 20150030475 A1**
JPS5778332

(58) Field of Search:
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Other: **EPODOC, WPI, TXTA**

(54) Title of the Invention: **Vacuum pump assembly**
Abstract Title: **A Motor for a Vacuum Pump**

(57) A motor for a vacuum pump configured to mitigate stray electromagnetic flux in applications such as Scanning Electron Microscopes (SEM). The motor comprises a permanent magnet rotor 24 and stator 26, the motor rotor magnet has an axial length of two thirds or less than that of the stator. Preferably the rotor may be up to 50% shorter than the stator and has a greater diameter than an equivalent rotor of the same axial length as the stator, allowing the magnetic field of the rotor to be substantially contained within the stator. The rotor may comprise a solid cylindrical magnet recessed in the vacuum pump shaft or a tubular magnet mounted on the exterior of the shaft. The vacuum pump may be a turbomolecular pump.

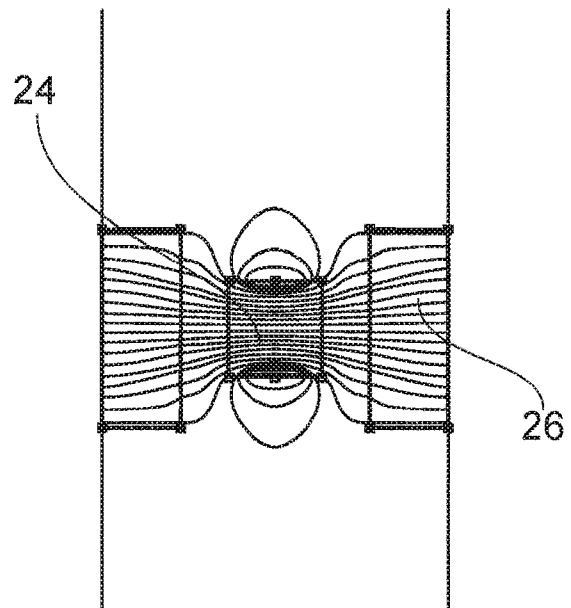


FIG. 2b

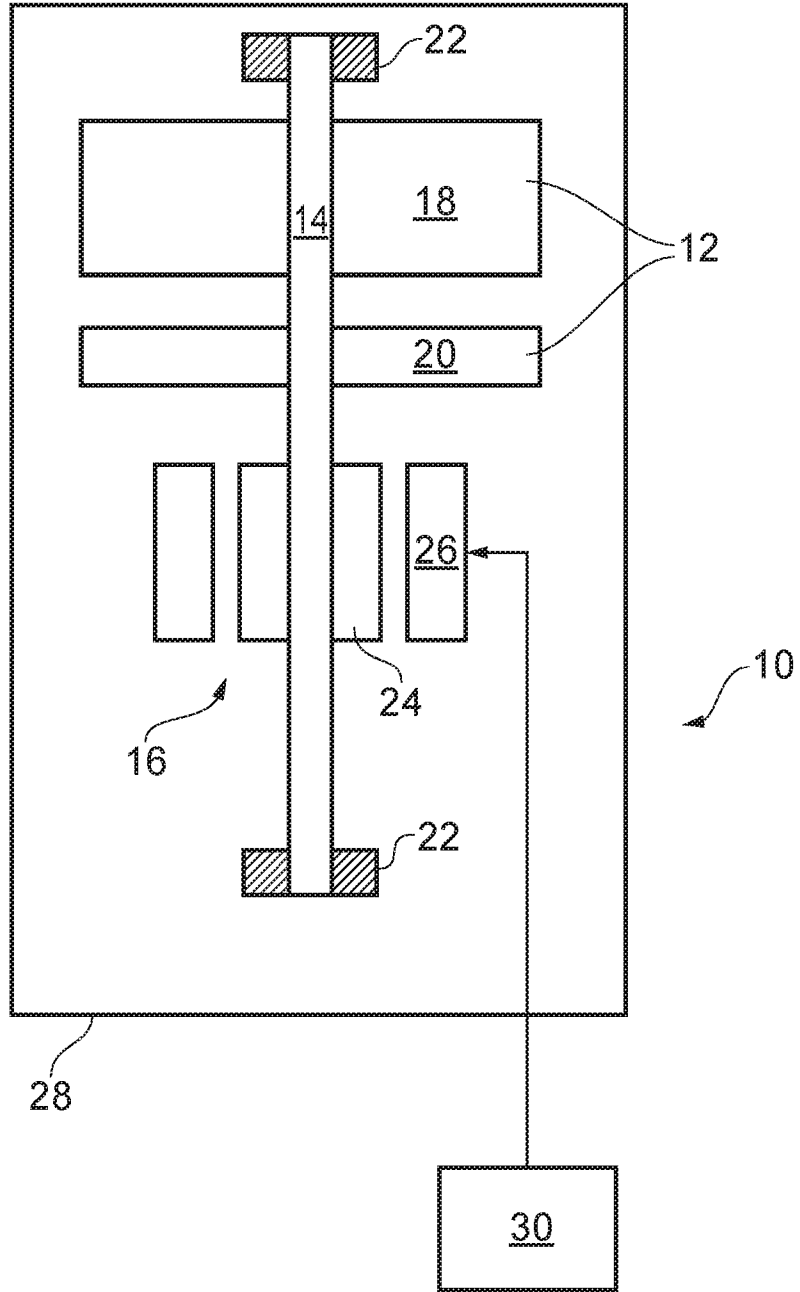


FIG. 1

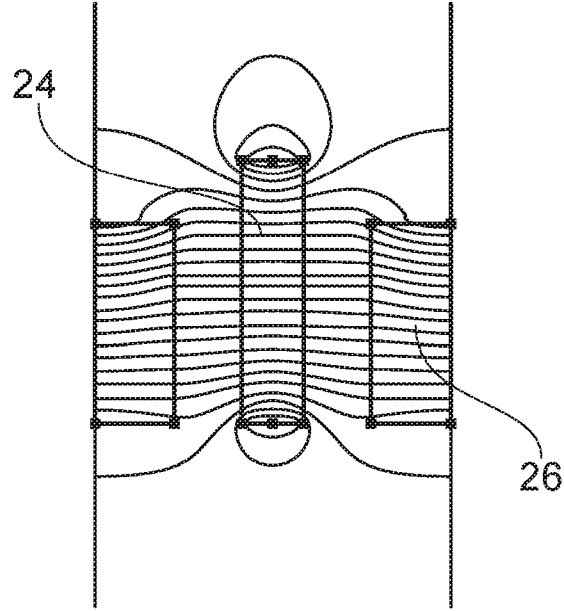


FIG. 2a

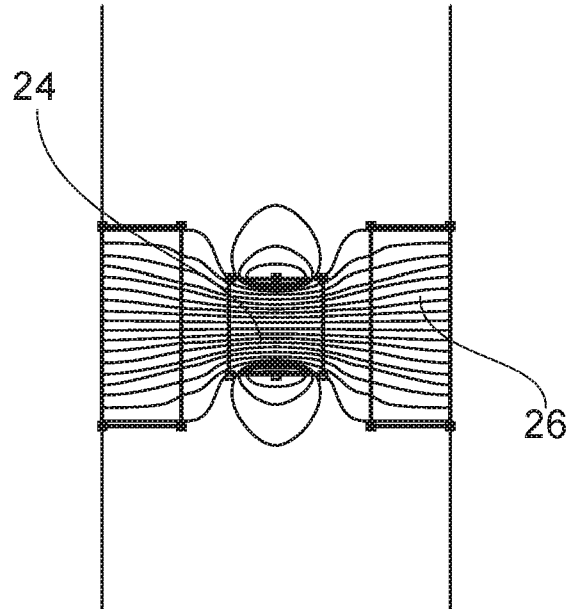


FIG. 2b

VACUUM PUMP ASSEMBLY

FIELD OF THE INVENTION

The invention relates to a vacuum pump assembly and in particular to the
5 arrangement of a motor in such a vacuum pump assembly

BACKGROUND

Turbomolecular pumps are often employed as a component of a vacuum
system used to evacuate devices such as scanning electron microscopes
10 (SEMs) and lithography devices.

The performance of scanning electron microscopes is highly susceptible to
mechanical vibrations and stray magnetic fields emitted from turbomolecular
pumps. In particular, stray fields which vary with time as a result of rotation of
15 the pump may cause issues in operation of apparatus around a vacuum
pump. For example, stray fields are known to directly interfere with the
electron beam or with the instruments' electrical circuits.

It would be desirable to provide a means to mitigate stray magnetic fields
20 emitted from turbomolecular pumps.

SUMMARY

A first aspect provides a vacuum pump assembly comprising a motor;
the motor comprising: a motor rotor magnet and a stator; the rotor motor
25 magnet being configured to be rotatable relative to the stator about an axis to
drive a vacuum pump mechanism; the motor rotor magnet having an axial
length of two thirds or less than that of the stator.

The first aspect recognises that a motor rotor magnet in a permanent magnet
30 motor for vacuum pumps, including, for example, turbomolecular vacuum
pumps, may be dimensioned such that it is shorter than the length of the
motor stator stack. Such a configuration may help to mitigate the

electromagnetic stray field emitted by the motor and, in turn, the vacuum pump.

The first aspect recognises that mitigating stray rotating fields emitted by vacuum pumps, such as turbo molecular vacuum pumps, allows for use of such products in, for example, scientific instrument applications sensitive to magnetic fields. Such instruments and applications include, for example, Scanning Electron Microscopes (SEM) and similar.

10 In a typical stator and rotor motor arrangement in a vacuum pump, the stator stack and motor magnet are of comparable axial lengths. Such an arrangement allows for efficient use of magnetic material. The size of the variable stray magnetic field generated by permanent magnet electrical motors typically used in vacuum pumps can cause problems in some vacuum pump applications, particularly if the design of the motor rotor is not optimised to achieve low variable stray field. That is to say, the ends of the permanent magnet forming part of the rotor emit an electromagnetic field which includes time varying components and could be considered “stray” since that field is not typically well shielded. Indeed, in some typical arrangements, a rotor motor magnet may extend beyond the length of the stator, such that any time varying field can be used to sense properties of motor operation, for example, rotation of the motor may be detected by a Hall sensor. Since a time varying field may stray, or be designed to exist, outside the motor, a time varying electromagnetic field may also stray outside the vacuum pump and be detrimental in some vacuum pump applications.

The first aspect recognises that by decreasing the length of the permanent motor rotor magnet may ensure that the field induced at the end of the rotor magnets substantially remain within the extent of the longer surrounding stator arrangement. In other words, the fields emitted at the end of the rotor magnets may be configured such that, for example, the stator may act to collect a greater portion of the magnetic field generated by the rotor motor

magnet, thus reducing stray field. The first aspect recognises that such an arrangement can reduce the stray magnetic field from the magnets which could escape the motor and be measurable outside a vacuum pump assembly.

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The first aspect recognises that by providing a rotor motor magnet which is less than two thirds the axial length of the stator, stray field experienced outside the stator and thus the motor and pump in general may be mitigated.

10 The vacuum pump assembly may comprise a turbo molecular vacuum pump. The vacuum pump assembly may comprise a motor. The motor may comprise a permanent magnet rotor motor. The motor may comprise a two pole motor magnet design, a four pole motor magnet design or a multi-pole permanent magnet motor magnet design. The motor may comprise: a motor
15 rotor magnet and a stator. The stator may comprise a lamination stack, a sintered stator, a powdered iron stator or similar. The stator may further comprise windings. The stator may comprise a lamination stack. The stator may be substantially cylindrical in arrangement and concentric with said rotor motor magnet. The rotor motor magnet may be positioned within a volume
20 enclosed by said stator. A gap, for example, an air gap, may typically be provided between the rotor motor magnet and the stator, to allow for relative motion between the two. The rotor motor magnet may be configured to be rotatable relative to the stator about an axis to drive a vacuum pump mechanism. The rotor motor magnet may be mounted on or in a drive shaft.
25 The drive shaft may drive the vacuum pump mechanism. The motor rotor magnet may have an axial length which is shorter than the axial length of the stator. The rotor motor magnet may have an axial length of two thirds or less than that of the stator. The rotor motor magnet may have an axial length of two thirds or less than that of the lamination stack. The rotor motor magnet
30 may have an axial length of two thirds or less than that of a powdered iron, sintered material or other similar component.

In some embodiments, the axial length of the motor rotor magnet is selected such that the magnetic field associated with the motor rotor magnet and stator is substantially contained or collected within a volume enclosed by the stator. Accordingly, the length of the motor rotor magnet may be selected such that
5 the stator can “collect” a greater proportion of the associated field. In other words, the stator may effectively shield the area outside the volume enclosed within the stator.

In some embodiments, the motor rotor magnet has a diameter selected, for a
10 stator having a given number of winding turns, such that the magnetic flux generated by the motor rotor magnet and the stator is substantially identical to an arrangement in which the motor rotor magnet has an axial length comparable to that of the stator. According to some embodiments, the product of the number of stator winding turns and the flux generated by a
15 shorter motor rotor magnet remains substantially constant compared to an arrangement in which the rotor motor magnet and stator are of comparable lengths. It will be appreciated that overall dimensions of a motor within a vacuum pump assembly may be of significance and may not be easily altered. It will also be appreciated that overall performance of a motor within a vacuum
20 pump assembly may be of significance. Accordingly, it may be possible, in some arrangements, to dimension a motor rotor magnet such that overall dimensions of the motor remain constant. In other words, if desirable for a particular vacuum pump assembly, the same stator with the same windings may be used with a shorter motor rotor magnet and achieve the same
25 performance, provided the operational characteristics of the motor magnet are appropriately chosen. That is to say, a magnetic material having a different magnetic strength may be chosen; the diameter of the rotor motor magnet may be chosen; the airgap between the rotor motor magnet and stator may be chosen; and similar. Furthermore, if the operational characteristics, such as
30 the dimensions and/or material and/or shape of the shorter motor rotor magnet are chosen appropriately, overall motor performance may not be significantly altered. Such a configuration may, for example, be achieved by

making a motor rotor magnet shorter, but also wider. It will be appreciated that the extent to which the rotor motor magnet may be made wider may be limited by the inner diameter of the stator, the shaft mechanical strength and/or flexibility and similar. A gap must be maintained between the stator
5 and the rotor motor magnet to allow for smooth relative movement between the two.

Provided the same magnetic material is used, the overall volume of the rotor motor magnet may, in some embodiments, remain a constant, compared to a
10 rotor motor magnet having a comparable length to that of the stator. It will be appreciated that the extent to which a motor rotor magnet may be made shorter whilst maintaining performance can be limited by the dimensions of a stator, especially if it is desirable to maintain a stator having particular physical dimensions, and using a particular number of winding turns. It will
15 also be appreciated that operational characteristics of a stator may be adjusted to try to maintain operation of a vacuum pump motor. In particular, the stator material may be changed or the number of winding turns may be changed, in order to achieve a desired performance or a desired physical dimension.

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In some embodiments, the motor rotor magnet has an axial length between one third and two thirds of that of the stator. In some embodiments, the motor rotor magnet has an axial length between two fifths and three fifths of that of the stator. In some embodiments, the motor rotor magnet has an axial length
25 in the region of a half of the axial length of the stator. It has been determined experimentally that a benefit may be measured if the rotor motor magnet is approximately 30% shorter than the stator and that benefit may be significant if the rotor motor magnet is approximately 50% shorter than the stator.

30 In some embodiments, the motor rotor magnet is substantially longitudinally symmetrically located within the stator. Centrally locating the rotor motor magnet may help to mitigate stray field within the vacuum pump assembly.

Locating the rotor motor magnet towards one or other end of the stator may aid mitigation of stray field in the region of the other end of the stator.

It will be appreciated that the physical configuration of the stator and rotor magnets may take various forms. In some embodiments, for example, the motor rotor magnet may comprise a solid substantially cylindrical magnet. That cylindrical magnet may have a substantially circular cross section. In some embodiments, such a motor rotor magnet may be mounted in an appropriate axial position on the motor shaft. The shaft may, for example, comprise an appropriate recess or hole configured to received such a motor rotor magnet. In some embodiments, the rotor motor magnet may be glued or otherwise affixed within an appropriate recess or hole.

In some embodiments, for example, the motor rotor magnet may comprise a solid substantially cylindrical magnet. That cylindrical magnet may have a substantially circular cross section. That cylindrical magnet may comprise a hollow portion or may comprise a generally tubular magnet. In some embodiments, such a motor rotor magnet may be mounted in an appropriate position on the motor shaft. The magnet may, for example, may be mounted, affixed, glued or shrunk in position on the shaft of the rotor.

In some embodiments, the motor rotor magnet comprises a solid cylindrical magnet. In some embodiments, the solid cylindrical magnet is mounted within a recess provided on a vacuum pump shaft. In some embodiments, the motor rotor magnet comprises a substantially tubular cylindrical portion. In some embodiments, the substantially tubular cylindrical portion is mounted on the exterior of a vacuum pump shaft. Such an arrangement may further comprise a retaining sleeve, for example, a carbon fibre sleeve, configured to surround the outer diameter of the rotor motor magnet. Such a sleeve may help to mitigate break-up of the magnet on rotation and thus exposure to centrifugal stresses and strains.

Further particular and preferred aspects are set out in the accompanying independent and dependent claims. Features of the dependent claims may be combined with features of the independent claims as appropriate, and in combinations other than those explicitly set out in the claims.

5

Where an apparatus feature is described as being operable to provide a function, it will be appreciated that this includes an apparatus feature which provides that function or which is adapted or configured to provide that function.

10

BRIEF DESCRIPTION OF THE DRAWINGS

Embodiments of the present invention will now be described further, with reference to the accompanying drawings, in which:

Figure 1 is a schematic diagram of one example arrangement of some of the main components of a typical vacuum pump;

15

Figure 2a illustrates schematically one possible rotor motor magnet and stator arrangement; and

Figure 2b illustrates schematically one possible rotor motor magnet and stator arrangement according to aspects and embodiments of the present invention.

20

DESCRIPTION OF THE EMBODIMENTS

Before discussing the embodiments in any more detail, first an overview will be provided.

25 Referring to Figure 1, an example of a vacuum pump 10 is shown. The vacuum pump comprises a vacuum pumping mechanism 12 mounted for rotation by a shaft 14 and a brushless motor 16 for rotating the shaft. The vacuum pumping mechanism 12 comprises a turbo pumping mechanism 18. The turbo pumping mechanism comprises a plurality of pumping stages. The vacuum pumping mechanism further comprises a molecular drag pumping
30 mechanism 20 which includes at least one pumping stage. Shaft 14 is supported for rotation on appropriate bearings 22.

The vacuum pumping mechanism 12 may comprise any one or more types of appropriate turbomolecular pumping mechanism, for example, turbo, Gaede, Siegbahn or Holweck type mechanisms. Figure 1 illustrates an example in which turbo and Siegbahn mechanisms are used.

Vacuum pumping mechanisms require rotation at high speed, typically at speeds of at least 20,000 rpm and generally at speeds of between about 36,000 and 90,000 rpm. Such high speeds are necessary to achieve compression from pressures of about 1×10^{-10} Torr at an inlet of the pump and 1 Torr at an outlet of the pump. Vacuum pumps are thus considered to be very high speed pumps.

In the example shown in Figure 1, the motor 16 comprises a permanent magnet rotor 24 fixed relative to the shaft 14. The motor further comprises a stator 26 fixed relative to a pump housing 28.

A motor control means 30 is provided and operates to control the rotor and stator coils dependent on a relative position of the rotor 24 and the stator 26 so that the rotor can be rotated relative to the stator to drive the pumping mechanism 12.

It will be appreciated that various vacuum pump motor assembly arrangements are possible. In particular, it will be appreciated that within the specification of a given vacuum pump arrangement, components may take various forms. For example, a rotor motor magnet may comprise a substantially tubular arrangement, such as that shown in Figure 1, or may comprise a solid permanent magnet housed in an appropriate recess provided in shaft 14.

Figure 2a illustrates schematically one possible rotor motor magnet 24 and stator 26 arrangement in a typical vacuum pump assembly such as that

illustrated in Figure 1. As shown in Figure 2a, a portion of a vacuum pump assembly is illustrated. In this arrangement, the pump motor comprises a solid rotor motor magnet 24, arranged within a hollow cylindrical stator stack 26. The motor magnet 24 is longer than the lamination stack so that it can trigger hall sensors, provided to feed information about the rotation of the motor to a motor controller. An indication of magnetic flux between the motor magnet and the stator stack are shown schematically in Figure 2a. It can be seen that the top (as shown in Figure 2a) of the motor rotor magnet extends beyond the top of the surrounding stator lamination stack 26. The magnetic field also extends significantly outside the volume enclosed by the stator lamination stack 26. It can also be seen that in the arrangement shown that although the bottom of the motor rotor magnet does not extend significantly outside the volume enclosed by the stator lamination stack, the magnetic field does. As a consequence, stray magnetic fields may be encountered outside the motor and the vacuum pump assembly may be unsuitable for use with scientific or manufacturing equipment which is sensitive to magnetic interference.

Figure 2b illustrates schematically one possible rotor motor magnet 24 and stator 26 arrangement in accordance with some aspects and embodiments of the present invention for use in a typical vacuum pump assembly such as that illustrated in Figure 1. It can be seen that, in order to be used in a vacuum pump assembly similar to that shown in Figure 1 and Figure 2a, the dimensions of the stator lamination stack 26 may be substantially fixed. Nonetheless, Figure 2b illustrates schematically a rotor motor magnet configuration in which stray magnetic field (field outside the volume enclosed by the stator lamination stack 26) may be mitigated.

In the arrangement shown in Figure 2b, the motor rotor magnet is shorter than the stator lamination stack. It can be seen, from the schematic magnetic flux lines, that such an arrangement may help to mitigate stray field. In the arrangement of Figure 2b, it will be appreciated that the dimensions of the

motor rotor magnet may be selected such that operation of the motor is maintained, compared to a longer motor rotor magnet. In particular, although the motor rotor magnet 24 is shorter, it is also wider and has a smaller air gap, so that the product of the magnetic flux generated by the motor rotor magnet and the lamination stack winding turns is maintained compared to the arrangement shown in Figure 2a.

TEST RESULTS

Tests performed at high speed (1500Hz) with a fixed length lamination stack and variable length solid cylindrical rotor motor magnet illustrate that reducing the rotor motor magnet length can achieve a significant reduction in a maximum measured stray field 200mm from a pump assembly, measured in the proximity of the electric motor plane as set out in the following table:

ROTOR MAGNET DESIGN	Magnet length comparable to stator (average)	Reduced length magnet - 71% of stator length	Reduced length magnet - 48% of stator length
Relative stray field at 200 mm from pump [as ratio] (high speed)	1	0.70	0.22

Although illustrative embodiments of the invention have been disclosed in detail herein, with reference to the accompanying drawings, it is understood that the invention is not limited to the precise embodiment and that various changes and modifications can be effected therein by one skilled in the art without departing from the scope of the invention as defined by the appended claims and their equivalents.

REFERENCE SIGNS

- 10 Turbomolecular vacuum pump
- 12 Vacuum pumping mechanism
- 14 Shaft
- 5 16 Brushless motor
- 18 Turbo pumping mechanism
- 20 Molecular drag pumping mechanism
- 22 Bearings
- 24 Permanent magnet rotor (of motor)
- 10 26 Stator (of motor)
- 28 Pump housing
- 30 Motor controller

CLAIMS

1. A vacuum pump assembly comprising a motor;
said motor comprising:
5 a motor rotor magnet and a stator; said rotor motor magnet being
configured to be rotatable relative to said stator about an axis to drive a
vacuum pump mechanism;
said motor rotor magnet having an axial length of two thirds or less
than that of said stator.
10
2. A vacuum pump assembly according to claim 1, wherein said axial
length of said motor rotor magnet is selected such that variable
magnetic field associated with rotation of said motor rotor magnet and
stator is substantially contained within a volume enclosed by said
15 stator.
3. A vacuum pump assembly according to claim 1 or claim 2, wherein, for
a given stator, said motor rotor magnet has a diameter selected such
that a product of magnetic flux between said motor rotor magnet and
20 winding turns of said stator is substantially identical to an arrangement
in which said motor rotor magnet has an axial length comparable to
that of said stator.
4. A vacuum pump assembly according to any preceding claim, wherein
25 said motor rotor magnet has an axial length between one third and two
thirds of that of said stator.
5. A vacuum pump assembly according to any preceding claim, wherein
said motor rotor magnet has an axial length between two fifths and
30 three fifths of that of said stator.

6. A vacuum pump assembly according to any preceding claim, wherein said motor rotor magnet has an axial length in the region of a half of the axial length of said stator.
- 5 7. A vacuum pump assembly according to any preceding claim, wherein said motor rotor magnet is substantially longitudinally symmetrically located within said stator.
8. A vacuum pump assembly according to any preceding claim, wherein
10 said motor rotor magnet comprises a solid cylindrical magnet.
9. A vacuum pump assembly according to claim 8, wherein said solid cylindrical magnet is mounted within a recess provided on a vacuum pump shaft.
15
10. A vacuum pump assembly according to any one of claims 1 to 7, wherein said motor rotor magnet comprises a substantially tubular cylindrical portion.
- 20 11. A vacuum pump assembly according to claim 10, wherein said substantially tubular cylindrical portion is mounted on the exterior of a vacuum pump shaft.
12. A vacuum pump assembly substantially as herein described with
25 reference to the accompanying drawings.



Application No: GB1615048.4

Examiner: Mr Matthew Harle

Claims searched: 1-11

Date of search: 6 December 2016

Patents Act 1977: Search Report under Section 17

Documents considered to be relevant:

Category	Relevant to claims	Identity of document and passage or figure of particular relevance
X	1-11	US2015/030475 A1 (PFEIFFER VACUUM) See Figures 1 and 2, showing motor rotor magnets.
X	1, 10, 11	EP2557316 A2 (PFEIFFER VACUUM) See Figure 2, showing motor rotor magnets at stator.
X	1, 10, 11	WO02/18794 A1 (LEYBOLD VAKUUM) See Figures, showing motor rotor magnets and stator coils in pump assembly.
A	None	JPS5778332 A (HITACHI LTD) A shortened armature to reduce stray flux, see abstract.
A	None	US3751693 A (DIABLO SYSTEMS INC) shows a motor including shielding prevent stray magnetic flux, see whole document.
A	None	DE4140379 C1 (PAPST MOTOREN GMBH & CO) A further example of shielding to prevent leakage flux.
A	None	GB2535163 A (EDWARDS LTD) An example of a turbo-molecular pump similar to that described in the present application, Figure 1 is particularly useful.

Categories:

X	Document indicating lack of novelty or inventive step	A	Document indicating technological background and/or state of the art.
Y	Document indicating lack of inventive step if combined with one or more other documents of same category.	P	Document published on or after the declared priority date but before the filing date of this invention.
&	Member of the same patent family	E	Patent document published on or after, but with priority date earlier than, the filing date of this application.

Field of Search:

Search of GB, EP, WO & US patent documents classified in the following areas of the UKC^X :

Worldwide search of patent documents classified in the following areas of the IPC

F04B; F04C; F04D; H02K

The following online and other databases have been used in the preparation of this search report



EPODOC, WPI, TXTA

International Classification:

Subclass	Subgroup	Valid From
F04D	0025/06	01/01/2006
F04D	0019/04	01/01/2006