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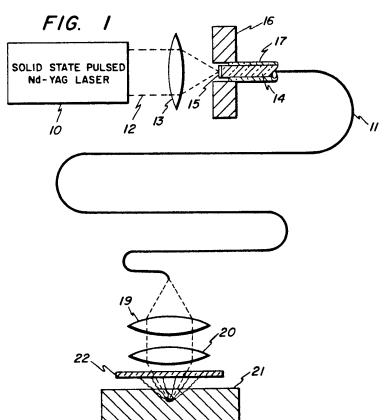
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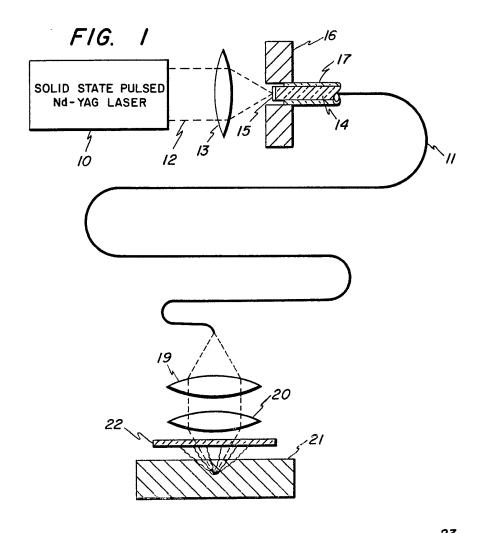
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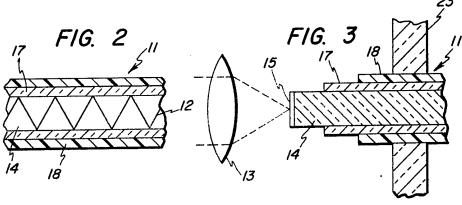
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(54) Laser material processing through a fiber optic

(57) Pulse laser energy in the near infrared and visible spectrum is passed through a single fiber optic at power levels required for material and metal processing. For example, a neodymium-YAG used in pulsed mode is coupled to the end of a quartz fiber optic which transmits peak powers in the kilowatt range. The beam at the output of the fiber optic is focused to achieve power densities capable of cutting, drilling, etc.







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SPECIFICATION

Laser material processing through a fiber optic

Background of the Invention

This invention relates to a laser beam deliver method and system and more particularly to transmission of laser energy through a fiber 10 optic at power levels high enough for manufacturing purposes.

Typically, laser beam delivery for material processing is accomplished through the use of an ensemble of mirrors and prisms for beam 15 steering. An increase in beam steering flexibility is possible when a laser beam is passed through a fiber optic. This flexibility enhances the access to difficult locations on a workpiece during manufacture. Such material processing 20 as drilling, cutting, welding, and selective heat treating and laser surfacing is possible with the laser remote from the workstation.

Laser energy has been transferred along a fiber optic for the purpose of laser communications and laser surgery in the medical field. In both cases, the laser beam is a continuous wave (CW) and average power levels of 100 watts have not been exceeded. As much as 20 watts of CW power from a CO₂ laser,
which has a 10.6 micrometer wavelength in the far infrared, have been transmitted through a fiber optic. The 100 watt CW power level was achieved from a laser that has a 1.06 micrometer wavelength in the near infrared. Only the CO₂ laser has been used

with a fiber optic for material processing with applications such as engraving and cloth cutting. The average or peak powers are not sufficient for welding, cutting, drilling, and 40 heat treating metals at cost effective rates.

The CO₂ laser fiber optic which is composed

The CO₂ laser fiber optic which is composed of thallous bromide and thallous iodide is capable of 55 percent transmittance at 10.6 micrometers, and because of this level of

45 transmissivity requires cooling. The neodymium-yttrium aluminum garnet laser, a source of 1.06 micrometer wavelength energy, has provided the 100 watt CW average power for surgical applications. Such power levels are

50 adequate for limited metal processing but have not been applied. Peak powers in excess of 1000 watts would be more desirable for metal processing.

55 Summary of the Invention

Laser energy is coupled into a single fiber optic which is used as a lightguide to deliver sufficient pulse energy to a workpiece for material processing. A laser beam generated 60 by a solid state neodymium-YAG laser or other laser which is operated in pulsed mode and has a wavelength in the near infrared and visible spectrum, is focused onto one end of the fiber optic core, preferably made of 65 quartz. Energy with a peak power in the

kilowatt range is passed through the fiber to the output end. The emerging laser beam is focused onto the workpiece at a power density high enough for manufacturing processes 30 such as drilling, cutting, welding, heat treat-

ing, and laser surfacing.

The system has a lens that focuses the laser's beam to a small spot whose diameter is less than the fiber core diameter; the

75 numerical aperture is such that the included angle of the focused beam is less than about 24°. In a specific embodiment, coupling takes place through a holding fixture made of copper or gold which reflects laser energy and prevents stray energy from entering the fiber optic cladding and melting it. The cladding at the fiber end is removed and the fiber is received in a hole in the fixture. A second embodiment for average power levels up to 250 watts has another input coupler. The fiber end is stripped of cladding and shielding

fiber end is stripped of cladding and shielding and only the shielding is removed in the next section, and the prepared fiber end is mounted in a glass holder. At the output is a 90 lens system to recollimate and refocus the

laser beam onto the workpiece.

This is a flexible laser beam delivery system with minimum optical losses, and increases the degrees of freedom of laser beam manipulation. It is especially attractive for metal processing with robotic control.

Brief Description of the Drawing

Figure 1 is a diagram of the laser coupled 100 fiber optic system used to apply laser energy to a metal workpiece.

Figure 2 is a longitudinal cross section through the fiber optic and shows passage of the laser beam along the core.

105 Figure 3 shows an improved input mechanism to transmit higher amounts of average power into the fiber optic.

Detailed Description of the Invention

110 Metal processing and the processing of other materials is accomplished by the laser energy delivery system in the figures. Average power levels on the order of 250 watts and peak powers of several kilowatts have been

115 transmitted through an individual fiber optic.
A neodymium-yttrium aluminum garnet laser, which has a wavelength in the near-infrared, is operated in pulsed mode. Other suitable solid state lasers are the ruby laser with a

120 wavelength of 680 nanometers, and the alexandrite laser with a wavelength of 630–730 nanometers, both in the visible spectrum. All the near infrared and visible wavelengths are transmitted in a quartz fiber optic without

125 melting the quartz. This kind of fiber optic is preferred because the fiber is flexible and quartz can be drawn into long fibers and is a pure material; impurities tend to absorb energy. The system includes provision for cou-

130 pling the laser energy into the fiber and

focusing the beam leaving the fiber to a power density sufficient for material processing.

In Fig. 1, a Nd-YAG laser 10 being used in 5 a pulsed mode is coupled to a 1000 micrometer diameter fused quartz fiber optic 11 by focusing the laser beam 12 down on the end of the fiber with a lens 13. In order for the laser energy to enter the fiber, two conditions 10 are needed. First, the small spot at the focal plane has a diameter less than the diameter of quartz core 14. Second, the numerical aperture of the fiber optic is such that the included angle of the focused beam (like a cone angle) 15 is smaller than 22°-24°. For best results the end of core 14 is ground optically flat and has an antireflection coating 15. Coupling takes place through a holding fixture 16 made of copper which has a hole to receive the fiber

20 11. About one-quarter inch of the transparent silicon cladding 17 is removed from the end of the fiber. The copper fixture 16 helps to protect the fiber cladding from any stray laser energy that does not enter the end of the

25 fiber, and prevents melting of the cladding. Copper tends to reflect 1.06 micrometer laser energy at moderate power levels. A better material would be gold, a higher reflective material.

30 Referring to the cross section of fiber optic 11 in Fig. 2, the laser beam travels along quartz core 14 in a zig-zag path and is reflected at the interface with silicon cladding 17. The optical fiber has a nylon shielding or 35 jacket 18. If a fused quartz fiber optic with a glass cladding is used, the flexibility of the fiber would be decreased but the power carrying capability may increase, since the 1.06

micrometer wave length is transparent to 40 glass, thus leading to lower risk in potential cladding damage. The fiber has a diameter less than 1 millimeter; fibers larger than this are less flexible.

Having transmitted laser energy through the 45 fiber optic 11 a lens assembly 19, 20 is used to collimate and focus the laser beam. The emerging beam at the output end of the fiber optic tends to spread out. The beam is recollimated by lens 19 and refocused by lens 20

50 onto the metal workpiece 21. The power density of the focused beam at the focal plane is sufficient for various metal processes. The laser beam may be passed through a glass plate 22 to protect the lenses from any metal

55 vapor. An antireflection coating on the three lens elements increases the transmissivity.

Average power levels up to 155 watts were transmitted into the fiber. With a pulse width (pulse length) of 0.6 milliseconds and a pulse 60 rate of 30 pulses per second, a peak power range of 4000–6000 watts was achieved. After focusing this beam at the output of the fiber optic, power densities of 10⁶–10⁷ watts/cm², capable of drilling and cutting, 65 were achieved. The 155 watts of laser pulse

energy were transmitted through a 1 millimeter fiber optic without any detectable attenuation with bend radii greater than 8 inches (200 millimeters). With fiber bend radii of 1.5 inches (37.5 millimeters), transmittance at 1.06 micrometers is 87 percent. The laser beam output from the fiber optic was focused on a 0.30 inch (0.75 millimeters) thick Inconel 718 workpiece resulting in both drilling and cutting the material.

The diameter of output lens 19, 20 may be much smaller than illustrated, resulting in an output end that is much easier to move around. The end of the fiber may be ground to be a lens element or part of a lens, or a separate element may be attached to the fiber.

The input mechanism in Fig. 1 allows only up to 155 watts of average laser energy, not enough for all processing tasks; higher powers are prohibited due to thermal limitations at the input coupling. Up to 250 watts of average power were transmitted into the fiber optic with the improved coupler in Fig. 3. The 90 fiber tip is stripped of silicon cladding 17 and shielding 18 for 0.75 inches. In the next section just the shielding is removed for an equal distance. This prepared end is then placed in a Pyrex (RTM) holder 23 and set at 95 the proper focal plane of the laser. The prepared end allows beam coupling through two zones, core-air and core-cladding. The first region permits the highly divergent incident beam to enter the fiber 11 through a greater 100 acceptance angle provided by the core-air interface. The second zone will provide additional reflections to insure transmission of the collected light energy. The third zone of core, cladding and shielding provide a rugged hous-105 ing for fiber handling.

Average power levels up to 250 watts were transmitted into a fiber of approximately five meters in length. With a pulse width of 0.2 millisecond and a pulse rate of 200 pulses per second, a peak range of 5000–9000 watts was achieved. After focusing the beam at the output of the fiber optic, power densities (10⁶–10⁷ watts/cm²) capable of drilling and cutting were achieved.

115 Up to 250 watts of Nd-YAG laser pulse energy can be transmitted through a 1 millimeter fiber optic without detectable attenuation with fiber bend radii greater than 4 inches (100 millimeters). At the 4 inch radii,

120 transmittance at 1.06 micrometers is 90 percent. A 0.060 inch (154 millimeter) thick titanium 6A1-4V workpiece was both drilled and cut. With the ability to transmit the higher amounts of average power the system

125 is much more versatile to the materials processing industry.

The main advantage of the fiber optic laser delivery system is an increase in beam steering flexibility. The degrees of freedom of laser beam manipulation are increased. With the

fiber optic basically light in weight, the laser beam is moved in almost any direction at a rapid speed. Being able to locate the laser remotely from the workstation is an additional advantage of transmitting a laser beam through a lightguide such as a fiber optic. The flexiblity inherent in a fiber optic laser beam delivery system also makes it very attractive for laser material processing with robotic con-

While the invention has been particularly shown and described with reference to preferred embodiments thereof, it will be understood by those skilled in the art that changes in form and details may be made therein without departing from the spirit and scope of the invention.

CLAIMS

 The method of delivering laser energy to perform manufacturing processes comprising:

generating a near infrared or visible wavelength pulsed laser beam;

25 focusing said laser beam to a small spot onto the end of the core of a single fiber optic;

transmitting energy with a peak power in the kilowatt range through said fiber optic; 30 and

refocusing the emerging beam onto a workpiece at a power density sufficient for material processing.

- The method of claim 1 wherein said
 laser beam is focused to a small spot whose diameter is less than the core diameter and the numerical aperture is such that the focused beam has an included angle smaller than about 24°.
- 40 3. The method of claim 1 wherein the end of said fiber optic core is optically flat and has an anti-reflection coating to enhance coupling of energy.
- 4. The method of claim 1 wherein average 45 power levels up to about 250 watts are transmitted into said fiber optic.
 - 5. An industrial laser energy delivery system comprising:
- a laser operating in pulsed mode that pro-50 duces a near infrared or visible wavelength laser beam;
 - a fiber optic having a quartz core and a cladding;
- means for focusing said laser beam to a 55 small spot onto the end of said quartz core, said fiber optic transmitting peak powers in excess of one kilowatt to the output end; and

means for collimating and focusing the emerging laser beam onto a workpiece to 60 perform material processing.

6. The system of claim 5 wherein said laser is selected from the group comprising a neodymium-YAG laser, a ruby laser, and an alexandrite laser.

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7. The system of claim 5 wherein a hold-

ing fixture for the end of said fiber optic reflects said laser beam and prevents stray beam from entering said cladding.

- 8. The system of claim 5 wherein the 70 cladding at one end of said fiber optic is removed and said fiber optic is received in a hole in a holding fixture made of a metal such as copper and gold that reflects said laser beam and prevents melting of said cladding.
- 75 9. The system of claim 5 wherein the cladding and a shielding thereon are removed from one end of said fiber optic for a short distance and only said shielding is removed in the next section, and the fiber end so pre-80 pared is mounted on a glass holder.
 - An industrial laser energy delivery system comprising:
- a neodymium-YAG laser operated in pulsed mode that produces a 1.06 micrometer wave-85 length laser beam;

a single fiber optic having fused quartz core, a cladding and shielding;

a lens which focuses said light beam onto one end of said fiber optic core to a small 90 spot whose diameter is less than the core diameter, the numerical aperture being such that the included angle of said focused beam is smaller than 24°;

said fiber optic serving as a lightguide that 95 transmits peak powers in the kilowatt range to the output end; and

a lens system that collimates and focuses the emerging laser beam onto a workpiece to perform metal processing.

- 100 11. The system of claim 10 wherein the cladding and shielding on one end of said fiber optic is received in a hole in a copper holding fixture that reflects said laser beam and prevents
 105 stray light from melting said cladding.
- 12. The system of claim 10 wherein the cladding and shielding are removed from one end of said fiber optic for a short distance and only said shielding is removed for an approximately equal distance in the next section, and the fiber end so prepared is placed in a glass holder.
 - 13. The system of claim 10 wherein said fiber optic cladding is transparent silicon.
- 115 14. The system of claim 10 wherein the one end of said fiber optic to which said laser beam is coupled is optically flat and has an antireflection coating.

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