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(72) Kumazawa, Kazuhiko, JP

(72) Kotani, Wataru, JP

(72) Kamiya, Masaomi, JP

(73) NGK INSULATORS, LTD., JP

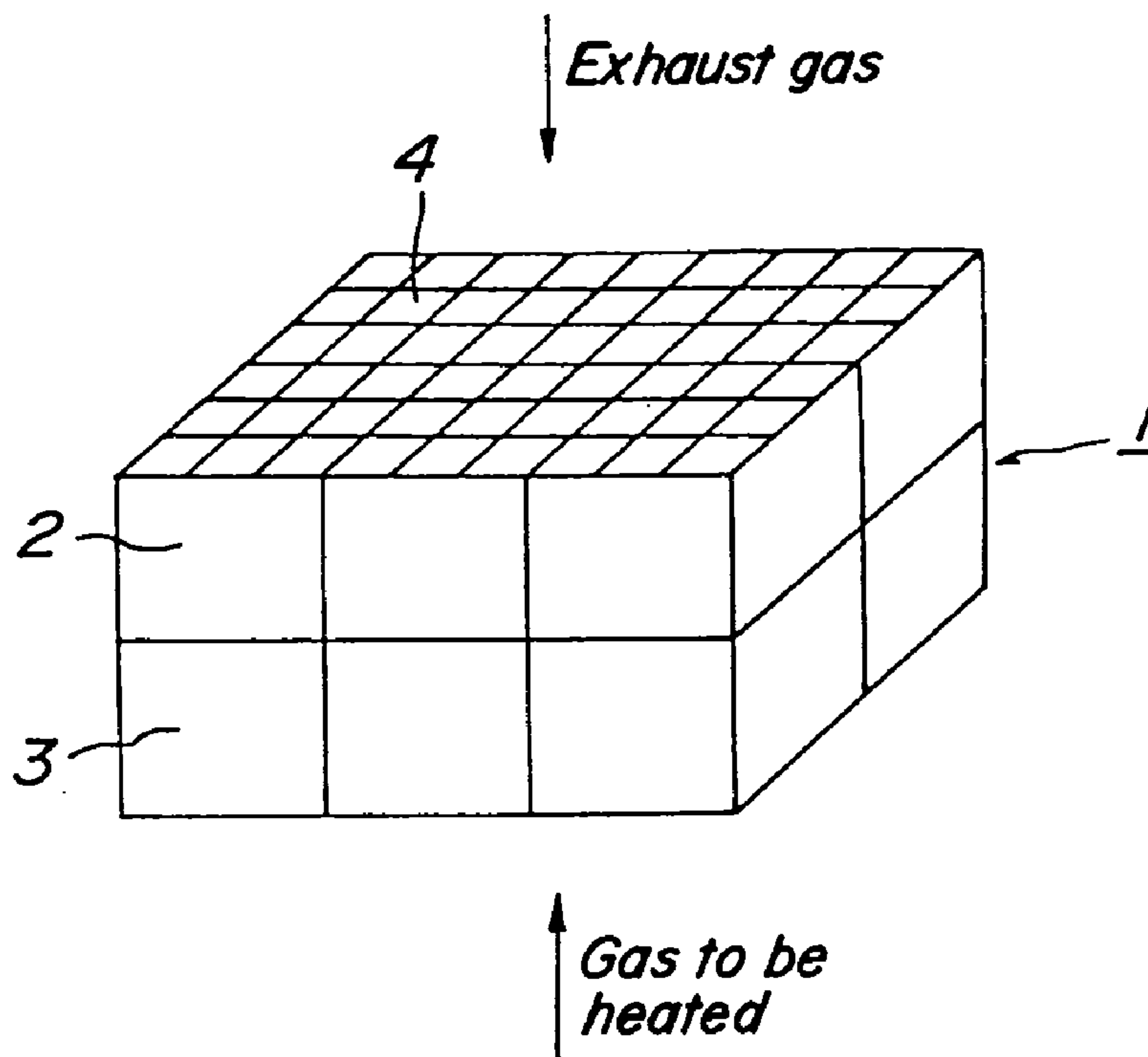
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(54) **RECUPERATEUR DE CHALEUR A STRUCTURE EN NID  
D'ABEILLES**

(54) **HONEYCOMB REGENERATOR**



(57) In a honeycomb regenerator for recovering a waste heat in an exhaust gas by passing the an exhaust gas and a gas to be heated alternately therethrough, which is constructed by stacking a plurality of honeycomb structural bodies, the honeycomb structural bodies arranged in a portion, to which the exhaust gas having a high temperature is contacted, are made of ceramics having anti-corrosive properties, and the honeycomb structural bodies arranged in a portion, to which the gas to be heated having a low temperature is contacted, are made of cordierite as a main crystal phase.



HONEYCOMB REGENERATORABSTRACT OF THE DISCLOSURE

In a honeycomb regenerator for recovering a waste heat in an exhaust gas by passing the an exhaust gas and a gas to be heated alternately therethrough, which is constructed by stacking a plurality of honeycomb structural bodies, the honeycomb structural bodies arranged in a portion, to which the exhaust gas having a high temperature is contacted, are made of ceramics having anti-corrosive properties, and the honeycomb structural bodies arranged in a portion, to which the gas to be heated having a low temperature is contacted, are made of cordierite as a main crystal phase.

6-135,745 comb.HONEYCOMB REGENERATORBACKGROUND OF THE INVENTIONField of the Invention

The present invention relates to a honeycomb regenerator for recovering a waste heat in an exhaust gas by passing the exhaust gas and a gas to be heated alternately therethrough, which is constructed by stacking a plurality of honeycomb structural bodies each having a rectangular shape in such a manner that flow passages constructed by through-holes are aligned in one direction, and especially relates to the honeycomb regenerator used in a corrosive atmosphere.

Related Art Statement

In a combustion heating furnace used for an industries such as a blast furnace, an aluminum melting furnace, a glass melting furnace or the like, a regenerator used for improving a heat efficiency, in which a firing air is pre-heated by utilizing a waste heat of an exhaust gas, has been known. As such regenerators, Japanese Patent Laid-Open Publication No. 58-26036 (JP-A-58-26036) discloses a regenerator utilizing ceramic balls, and also Japanese Patent Laid-Open Publication No. 4-251190 (JP-A-4-251190) discloses

a regenerator utilizing honeycomb structural bodies.

In the known regenerator mentioned above, at first an exhaust gas having a high temperature is brought into contact with the ceramic balls or the honeycomb structural bodies to store a waste heat of the exhaust gas in the regenerator, and then a gas to be heated having a low temperature is brought into contact with the thus pre-heated regenerator to heat the gas to be heated, thereby utilizing the waste heat in the exhaust gas effectively.

Among the known regenerators mentioned above, in the case of using the ceramic balls, since a contact area between the ceramic balls and the exhaust gas is small due to a large gas-flowing resistivity of the ceramic balls, it is not possible to perform a heat exchanging operation effectively. Therefore, there occurs a drawback such that it is necessary to make a dimension of the regenerator large.

Contrary to this, in the case of using the honeycomb structural bodies, since a geometrically specific surface thereof is large as compared with a volume thereof, it is possible to perform the heat exchanging operation effectively even by a compact body. However, in an actual industrial furnace, since use is made of a natural gas, a light oil, a heavy oil or the like as a fuel, a corrosive gas such as SO<sub>x</sub>, NO<sub>x</sub> or the

like is generated. Moreover, in the aluminum melting furnace, the exhaust gas includes an alkali metal component or the like. Therefore, a catalyst carrier made of cordierite used for purifying the exhaust gas of an automobile as disclosed in JP-A-4-251190 has a drawback on anti-corrosive properties.

Further, in order to improve the anti-corrosive properties, Japanese Utility Model Publication No. 2-23950 discloses a regenerator utilizing an alumina. In this case, since all the honeycomb body is made of an alumina and an alumina has a high thermal expansion coefficient, there occurs a problem such that the regenerator is fractured due to a thermal shock if a heat cycle having a large temperature difference is applied thereto.

#### SUMMARY OF THE INVENTION

An object of the present invention is to eliminate the drawbacks mentioned above and to provide a honeycomb regenerator which can perform a heat exchanging operation effectively even in a corrosive atmosphere.

According to the invention, a honeycomb regenerator for recovering a waste heat in an exhaust gas by passing said exhaust gas and a gas to be heated alternately therethrough, which is constructed by stacking a plurality of honeycomb structural bodies, is

characterized in that said honeycomb structural bodies arranged in a portion, to which said exhaust gas having a high temperature is contacted, are made of ceramics having anti-corrosive properties, and said honeycomb structural bodies arranged in a portion, to which said gas to be heated having a low temperature is contacted, are made of cordierite as a main crystal phase.

In the construction mentioned above, the portion of the honeycomb regenerator, to which the exhaust gas having a high temperature is contacted, is formed by the honeycomb structural bodies made of ceramics having the anti-corrosive properties, and the portion of the honeycomb regenerator, to which the gas to be heated having a low temperature is contacted, is formed by the honeycomb structural bodies made of cordierite. Therefore, since the problems in the case of using the ceramics having the anti-corrosive properties or the cordierite only as the honeycomb structural bodies can be eliminated, it is possible to perform the heat exchanging operation of the honeycomb regenerator effectively even in the corrosive gas having a high temperature.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic view showing one embodiment of a honeycomb regenerator according to the invention;

Fig. 2 is a schematic view illustrating one embodiment such that a heat exchanging apparatus utilizing the honeycomb regenerator according to the invention is applied to a combustion room of a combustion heating furnace;

Fig. 3 is a schematic view for explaining one embodiment of flow passages of the honeycomb regenerator according to the invention; and

Fig. 4 is a schematic view for explaining another embodiment of flow passages of the honeycomb regenerator according to the invention.

#### DESCRIPTION OF THE PREFERRED EMBODIMENT

Fig. 1 is a schematic view showing one embodiment of a honeycomb regenerator according to the invention. In the embodiment shown in Fig. 1, a honeycomb regenerator 1 is formed by stacking a plurality of honeycomb structural bodies 2 having anti-corrosive properties and a plurality of cordierite honeycomb structural bodies 3 in such a manner that flow passages thereof constructed by through-holes 4 are aligned in one direction. The honeycomb structural bodies 2 having anti-corrosive properties are made of a material selected from a group consisting of alumina, zirconia, mullite, SiC, Si<sub>3</sub>N<sub>4</sub> as a main crystal phase. The cordierite honeycomb structural bodies 3 are made of cordierite as a main crystal phase. Moreover, both of

the honeycomb structural bodies 2 and 3 have a rectangular shape.

In this embodiment, a portion of the honeycomb regenerator 1 to which an exhaust gas having a high temperature is contacted, i.e., six honeycomb structural bodies forming an upper plane of the honeycomb regenerator 1 in Fig. 1 are constructed by the honeycomb structural bodies 2 having anti-corrosive properties. Moreover, a portion of the honeycomb regenerator 1 to which a gas to be heated having a low temperature is contacted, i.e., six honeycomb structural bodies forming a lower plane of the honeycomb regenerator 1 in Fig. 1 are constructed by the cordierite honeycomb structural bodies 3. In this case, six honeycomb structural bodies 2 having anti-corrosive properties may be formed by the same material or may be formed by different materials within the group mentioned above.

Further, from the view point of the anti-corrosive properties, it is preferred to set a length in the flow passage direction of a layer in which six honeycomb structural bodies 2 having anti-corrosive properties exist to more than 2 cm from a surface of an exhaust gas inlet, and it is more preferred to set the length mentioned above to more than 5 cm. Moreover, it is preferred to set the length mentioned above to less than 9/10 of a whole length of the honeycomb regenerator



1, and it is more preferred to set the length mentioned above to less than  $2/3$  of the whole length mentioned above. Furthermore, from the view point of improving heat storing properties and a strength, it is preferred to set a porosity of the cordierite honeycomb structure bodies 3 to 20~50%. Moreover, from the view point of removing a corrosive exhaust gas component, it is effective to set a porosity of the honeycomb structural body 2 having anti-corrosive properties larger than that of the cordierite honeycomb structural body 3.

In the present invention, the reason for limiting the length of arranging the anti-corrosive honeycomb structural body 2 to preferably more than 2 cm, more preferably more than 5 cm is as follows. That is to say, since a corrosion of the portion, to which the exhaust gas having a high temperature is directly contacted, becomes extraordinary, it is necessary to use the anti-corrosive honeycomb structural body 2 having at least such a thickness mentioned above. Moreover, the reason for limiting the length of arranging the anti-corrosive honeycomb structural body 2 to preferably less than  $9/10$ , more preferably less than  $2/3$  of the whole length of the honeycomb regenerator 1 is as follows. That is to say, since a large thermal shock is applied to the portions, to which an air having a room temperature is generally contacted, it is

necessary to use the cordierite honeycomb structural body 3 with a good thermal shock property having preferably not less than 1/10, more preferably not less than 1/3 of the whole length mentioned above.

05 Further, the reason for limiting a porosity of the cordierite honeycomb structural body 3 to preferably 20~50% is as follows. That is to say, a heat storing property is increased if the honeycomb structural body 3 becomes porous more and more, it is preferred to have a  
10 porosity at least more than 20%. Moreover, since a strength is decreased if a porosity of the honeycomb structural body 3 is increased, an upper limit of the porosity is preferably less than 50%. Moreover, the  
15 reason for preferably limiting a porosity of the anti-corrosive honeycomb structural body 2 larger than that of the cordierite honeycomb structural body 3 in a corrosive atmosphere is as follows. That is to say, in this case, a corrosive exhaust gas component can be temporarily trapped by a high temperature portion i.e.  
20 the anti-corrosive honeycomb structural bodies 2, and an amount of the corrosive exhaust gas component passing through a low temperature portion i.e. the cordierite honeycomb structural bodies 3 can be reduced.

25 In the embodiment shown in Fig. 1, one layer is constructed by six anti-corrosive honeycomb structural bodies 2 and the other layer is constructed by six

cordierite honeycomb structural bodies 3. However, it should be noted that the number of the honeycomb structural bodies consisting one layer and the number of the stacking layers are not limited. The important  
05 point of the present invention is that, if the honeycomb structural body is constructed by the honeycomb structural bodies in any way, the anti-corrosive honeycomb structural bodies 2 are arranged at least to the portion to which the high temperature exhaust gas is  
10 contacted, and also the cordierite honeycomb structural bodies 3 are arranged at least to the portion to which the low temperature gas to be heated is contacted.

In the case of using multiple i.e. more than two layers of the honeycomb structural bodies, use is made of both  
15 of the anti-corrosive honeycomb structural body 2 and the cordierite honeycomb structural body 3 as an intermediate layer, but it is preferred to satisfy the preferable conditions mentioned above.

In the honeycomb regenerator 1 shown in Fig. 1,  
20 at first the high temperature exhaust gas is flowed downwardly through the honeycomb regenerator 1 for a predetermined time period to store a heat in the honeycomb regenerator 1, and then after changing the flow direction the low temperature gas to be heated is  
25 flowed upwardly through the honeycomb regenerator 1 for a predetermined time period to heat the gas to be heat.

Therefore, it is possible to perform the heat exchanging operation effectively by repeating the operation mentioned above.

As for a material of the anti-corrosive  
05 honeycomb structural bodies 2, it is possible to use one  
or more materials selected from a group of alumina,  
zirconia, mullite, SiC, Si<sub>3</sub>N<sub>4</sub> as a main crystal phase as  
mentioned above, but, in the case, it is preferred to  
select the materials with taking into account of the  
10 properties mentioned below. Alumina and zirconia have a  
resistivity to a corrosion, but have a large thermal  
expansion coefficient (CTE), so that they have a worse  
thermal shock resistivity. Mullite has a superior  
corrosion resistivity as compared with that of  
15 cordierite, but it is inferior as compared with that of  
alumina. Further, mullite has an excellent thermal  
shock resistance as compared with that of alumina. SiC  
and Si<sub>3</sub>N<sub>4</sub> have an excellent corrosion resistivity and  
have an intermediate thermal expansion coefficient.  
20 Therefore, they have an excellent thermal shock  
resistivity, but there occurs a problem of a  
deterioration due to an oxidization in an oxidizing  
atmosphere. The properties mentioned above are  
summarized in the following Table 1.

Table 1

	cordierite	almina	zirconia	mullite	SiC	Si <sub>3</sub> N <sub>4</sub>
CTE ( $\times 10^{-6}/^{\circ}\text{C}$ )	0.6	7.8	7.8	4.5	3.5	3.5
Corrosion resistivity	×	○	○	△	○	○
oxidization resistivity	○	○	○	○	×	×
Specific gravity	2.52	3.98	6.27	3.16	3.22	3.17

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As a method of using the anti-corrosive ceramics, since alumina and zirconia have a worse thermal shock resistivity, it is effective to make it into blocks as small as possible in an actual use. Moreover, since they have an excellent corrosion resistivity, it is possible to make a porosity thereof high. If the porosity thereof is increased, it is effective to store a heat therein, and it is possible to reduce an amount of the corrosive gas passing through the cordierite portion by trapping the corrosive gas temporarily therein.

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Mullite has a superior thermal shock resistivity as compared with alumina, but a corrosion resistivity thereof is not sufficient. If a porosity of mullite is decreased to less than 10%, mullite has a sufficient corrosion resistivity in an actual use. SiC and Si<sub>3</sub>N<sub>4</sub> have an intermediate thermal expansion coefficient and have a good thermal shock resistivity as is not the same as that of cordierite. Moreover, since they have an

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excellent corrosion resistivity, they can be used in a reduction atmosphere. However, if SiC and Si<sub>3</sub>N<sub>4</sub> are used in a high temperature oxidizing atmosphere above 1000°C, SiO<sub>2</sub> glass is generated on a surface thereof due to the oxidization, and a thermal expansion coefficient thereof becomes high. Moreover, they are liable to be deteriorated by the corrosive gas such as SO<sub>x</sub>, NO<sub>x</sub> or the like. In this case, in order to increase the oxidization resistivity, it is preferred to form a dense body having a porosity of less than 10%. As a method of making a porosity of SiC to less than 10%, it is effective to include a Si in SiC. SiC honeycomb including Si having a porosity of less than 10% shows an excellent oxidization resistivity, a high thermal expansion coefficient and an excellent thermal shock resistance, and thus it can be preferably used for the anti-corrosive ceramics.

As for a heat storing property, it is effective to be a porous body from the view point of a heat conductivity and also it is effective to use a body having a high bulk specific gravity i.e. a heavy body from the view point of a specific heat. Cordierite has a relatively low specific gravity, but a cordierite porous body having a porosity of more than 20% shows a sufficient heat storing property. Alumina and zirconia have a high specific gravity, and thus an alumina body

or a zirconia body having a high porosity is effective for a heat storing body. SiC and Si<sub>3</sub>N<sub>4</sub> are preferably used as a densified body having a porosity of less than 10% so as to improve the oxidization resistivity. They  
05 have a worse heat storing property, but, since a specific gravity thereof is high, they have expectedly the same heat storing property as that of cordierite.

Fig. 2 is a schematic view showing one embodiment such that a heat exchanging apparatus  
10 utilizing the honeycomb regenerator according to the invention is applied to a combustion room of a combustion heating furnace. In the embodiment shown in Fig. 2, a numeral 11 is a combustion room, numerals 12-1 and 12-2 are a honeycomb regenerator having a  
15 construction shown in Fig. 1, numerals 13-1 and 13-2 are a heat exchanging apparatus constructed by the honeycomb regenerator 12-1 or 12-2, and numeral 14-1 and 14-2 are a fuel supply inlet of the heat exchanging apparatus  
20 13-1 or 13-2. In the embodiment shown in Fig. 2, two heat exchanging apparatuses 13-1 and 13-2 are arranged for performing the heat storing operation and the heating operation at the same time. That is to say, when one of them performs the heat storing operation, the other can perform the heating operation at the same  
25 time, thereby performing the heat exchanging operation effectively.

As shown by an arrow in Fig. 2, an air to be heated is supplied upwardly in the heat exchanging apparatus 13-1 in which the honeycomb regenerator 12-1 is pre-heated by storing a heat, and, at the same time, an exhaust gas having a high temperature is supplied from the combustion room 11 to the heat exchanging apparatus 13-2. Moreover, a fuel is supplied in the heat exchanging apparatus 13-1 via the fuel supply inlet 14-1 at the same time. Therefore, the pre-heated air is supplied in the combustion room 11 with a fuel, and the honeycomb regenerator 12-2 of the heat exchanging apparatus 13-2 is pre-heated.

Then, the gas flows are changed in a reverse direction with respect to the arrows in Fig. 2. After that, an air to be heated is supplied upwardly in the heat exchanging apparatus 13-2, and, at the same time, an exhaust gas having a high temperature is supplied from the combustion room 11 to the heat exchanging apparatus 13-1. In the embodiment mentioned above, the heat exchanging operation can be performed by repeating continuously the steps mentioned above.

The present invention is not limited to the embodiments mentioned above, and various variations are possible. For example, as a combination method of the anti-corrosive honeycomb structural bodies, it is possible to use one layer or two or three layers of the



honeycomb structural bodies made of SiC as a main  
crystal phase having an excellent thermal shock  
resistivity at the high temperature portion and to use a  
few layers of the honeycomb structural bodies made of  
05 alumina as a main crystal phase having an excellent  
corrosion resistivity, which is arranged inside of the  
SiC honeycomb structural bodies.

Moreover, it is preferred to align the flow  
passages of the honeycomb structural bodies, which are  
10 constructed by the through-holes 4, in one direction.  
However, it is possible to use the honeycomb structural  
bodies having different flow passage density defined by  
the number of flow passages with respect to a unit area.  
For example, as shown in Fig. 3, it is possible to use  
15 the construction such that the flow passage density of  
one of the honeycomb structural bodies consisting of an  
upper or a lower layer is two times or more than three  
times as large as that of the other honeycomb structural  
bodies consisting of the lower or the upper layer.  
20 Moreover, it is possible to use the construction such  
that positions of flow passage walls of the honeycomb  
structural bodies are not made identical with each  
other. That is to say, as shown in Fig. 4, it is  
possible to use the construction such that the upper  
25 honeycomb structural bodies and the lower honeycomb  
structural bodies are stacked in such a manner that they

are slid with each other by a half or one third of a length between the flow passage walls.

As clearly understood from the above explanation, according to the invention, since the  
05 portion, to which the high temperature exhaust gas is contacted, is constructed by the anti-corrosive honeycomb structural bodies and the portion to which the low temperature gas to be heated is contacted, is constructed by the cordierite honeycomb structural  
10 bodies, it is possible to perform the heat exchanging operation effectively without being fractured even in the high temperature corrosive gas.

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What is claimed is:

1. A honeycomb regenerator for recovering a waste heat in an exhaust gas by passing an exhaust gas and a gas to be heated alternately therethrough, which is constructed by stacking a plurality of honeycomb structural bodies, characterized in that said honeycomb structural bodies arranged in a portion, to which said exhaust gas having a high temperature is contacted, are made of ceramics having anti-corrosive properties, and said honeycomb structural bodies arranged in a portion, to which said gas to be heated having a low temperature is contacted, are made of cordierite as a main crystal phase.

2. The honeycomb regenerator according to claim 1, wherein said honeycomb structural bodies are formed by at least one body having one main crystal phase selected from a group of alumina, zirconia, mullite, SiC, and  $\text{Si}_3\text{N}_4$ .

3. The honeycomb regenerator according to claim 1, wherein a length in a flow passage direction of a portion constructed by said anti-corrosive honeycomb structural bodies is more than 2 cm from a surface of an exhaust gas inlet and is less than  $9/10$  of a whole length of said honeycomb regenerator.

4. The honeycomb regenerator according to claim 3, wherein said length in the flow passage direction of the

portion constructed by said anti-corrosive honeycomb structural bodies is more than 5 cm from the surface of the exhaust inlet and is less than  $2/3$  of the whole length of said honeycomb regenerator.

5. The honeycomb regenerator according to claim 1, wherein a porosity of said cordierite honeycomb structural body is in a range of 20~50%.

6. The honeycomb regenerator according to claim 5, wherein a porosity of said anti-corrosive honeycomb structural body is larger than that of said cordierite honeycomb structural body.

7. The honeycomb regenerator according to claim 6, wherein said anti-corrosive honeycomb structural body is formed by a honeycomb structural body made of alumina as a main crystal phase.

8. The honeycomb regenerator according to claim 6, wherein said anti-corrosive honeycomb structural body is formed by a honeycomb structural body made of zirconia as a main crystal phase.

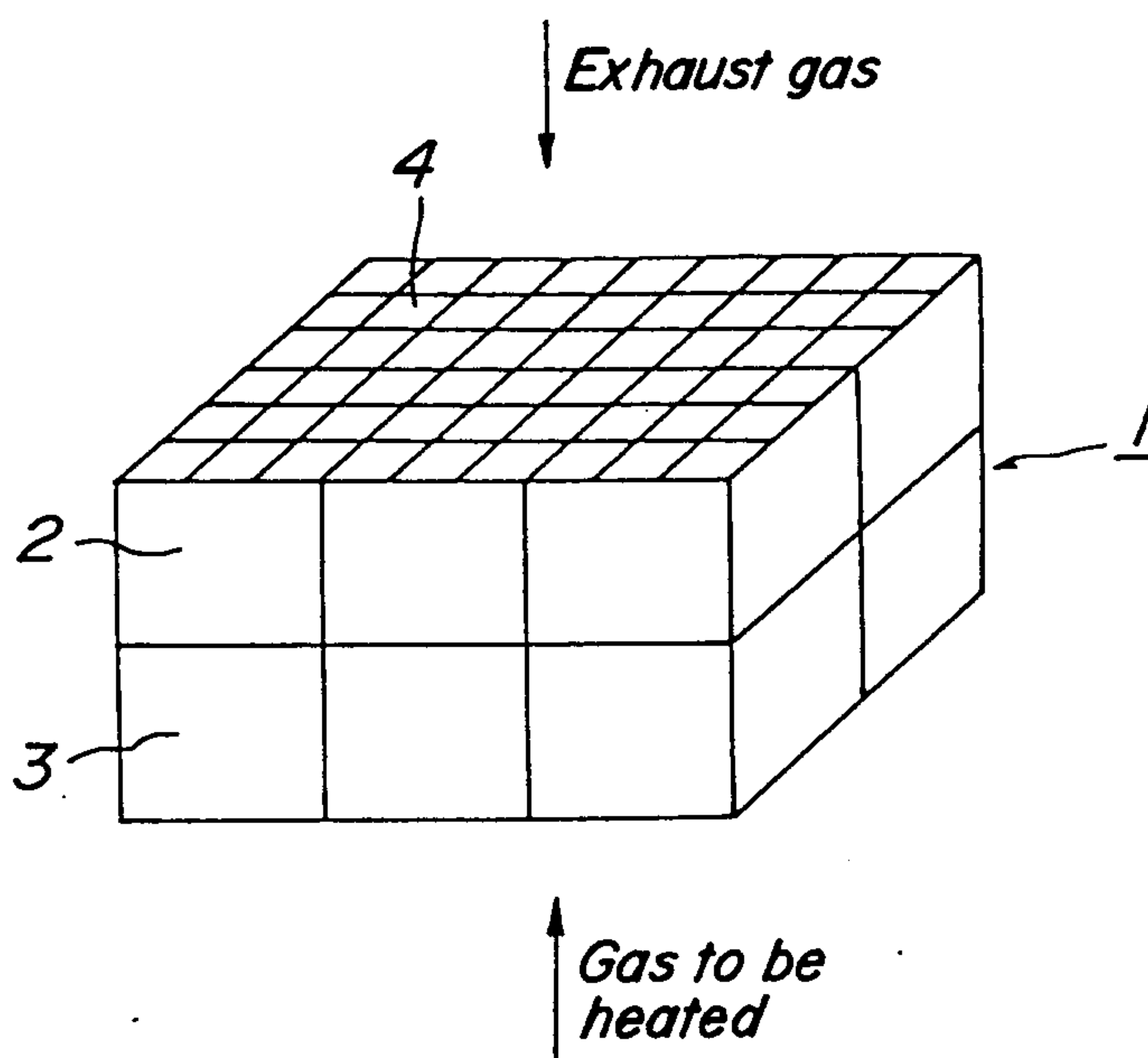
9. The honeycomb regenerator according to claim 2, wherein said anti-corrosive honeycomb structural body is formed by a honeycomb structural body made of SiC or  $\text{Si}_3\text{N}_4$  as a main crystal phase, and a porosity of said anti-corrosive honeycomb structural body is less than 10%.

10. The honeycomb regenerator according to claim 9, wherein said SiC honeycomb structural body having a porosity less than 10% is made of SiC including Si.

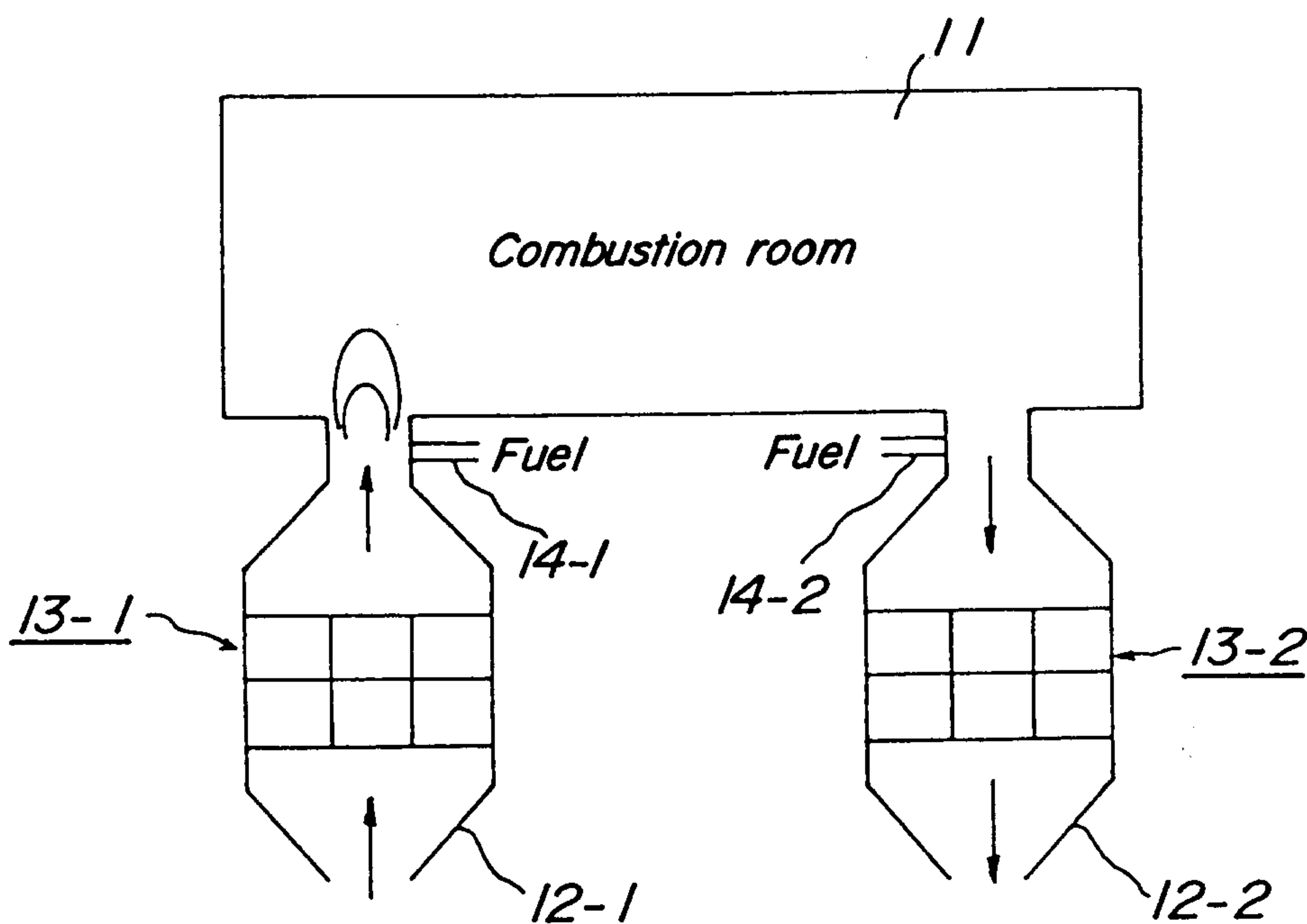
11. The honeycomb regenerator according to claim 2, wherein said anti-corrosive honeycomb structural body is formed by a honeycomb structural body made of mullite as a main crystal phase, and a porosity of said anti-corrosive honeycomb structural body is less than 10%.

**Smart & Biggar  
Ottawa, Canada  
Patent Agents**

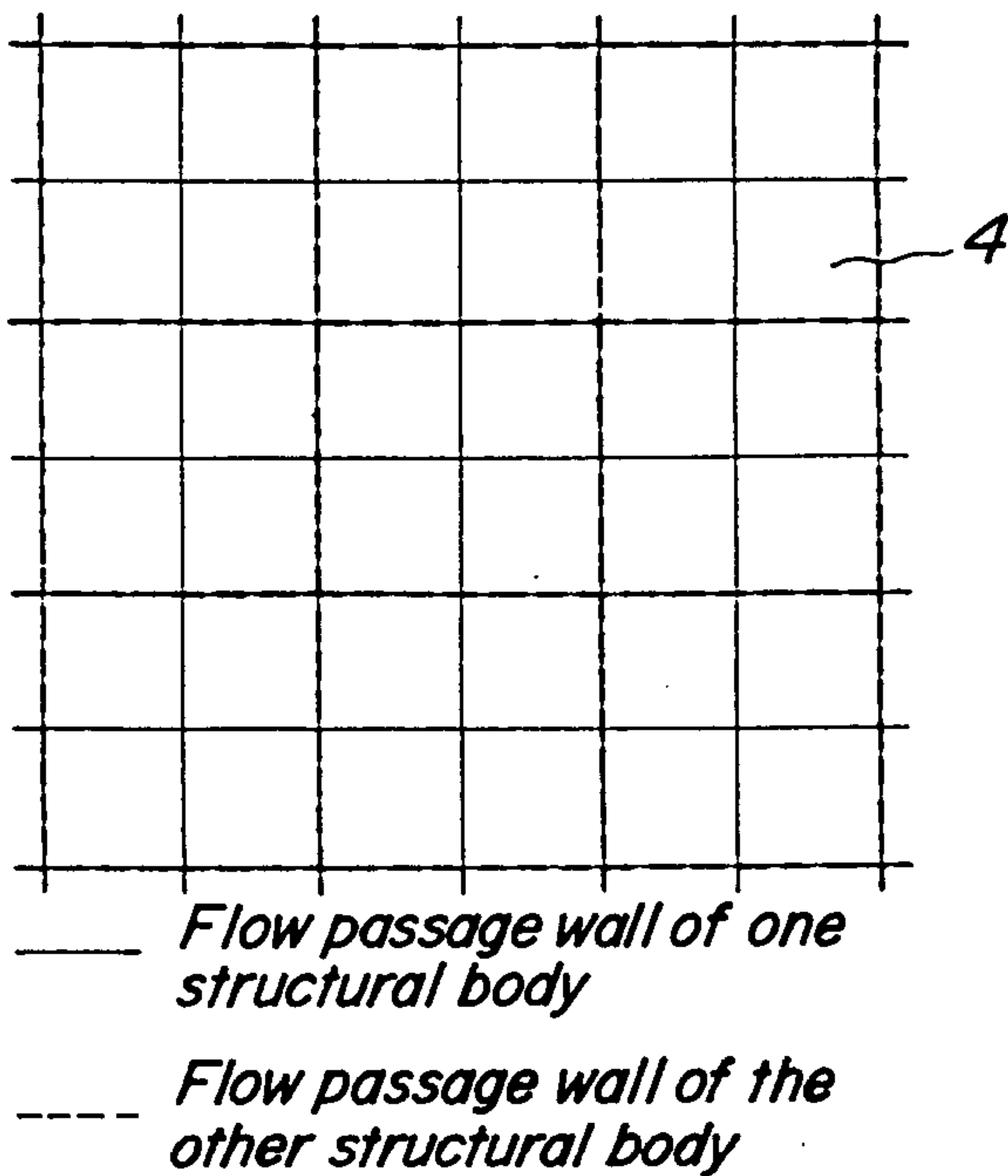
**FIG. 1**



**FIG. 2**



**FIG. 3**



**FIG. 4**

